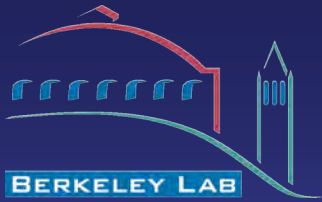


Hydrologic, Geomechanical, and Geophysical Measurements on Laboratory-Formed Hydrate- Bearing Samples

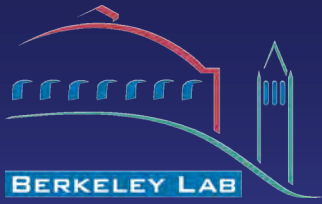
Tim Kneafsey

Earth Sciences Division
Lawrence Berkeley National Laboratory



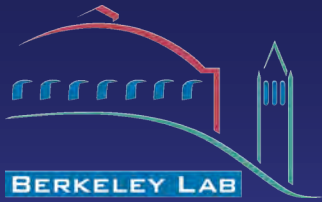
Contributors

- Timothy J. Kneafsey, P.E., Ph.D. (hydrologic tests, imaging, process, test development)
- Seiji Nakagawa, Ph. D. (geomechanical and geophysical measurements and interpretation)
- Teamrat Ghezzehei, Ph.D. (hydrologic measurements, modeling/inverse modeling)
- Yongkoo Seol, Ph.D. (now at NETL - hydrologic tests, modeling/inverse modeling, test development)
- Liviu Tomutsa, Ph.D. (imaging, micro CT, test development)
- George Moridis, Ph.D. (modeling)
- Arvind Gupta, Ph.D. (Colorado School of Mines - now at Shell - hydrologic measurements)
- Matt Walsh (Colorado School of Mines - hydrologic measurements)



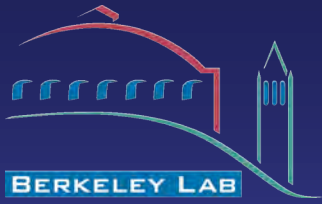
Hydrate Research Areas

- Hydrologic Properties (necessary for accurate hydrologic modeling)
 - Relative Permeability
 - Capillary Pressure
- Geomechanical and Geophysical Properties (necessary for understanding well/seafloor/slope stability)
- Other
 - Mt. Elbert, NGHP core scanning
 - Gas Production from Natural Samples
 - Effects of Brief Depressurization
 - Properties of HBS
 - Water Flow Through Heterogeneous Hydrate
 - ...



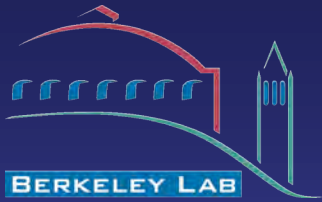
Expenditures

- FY 2006 ~\$254K
- FY 2007 ~\$375K
- FY 2008 (June) \$331K



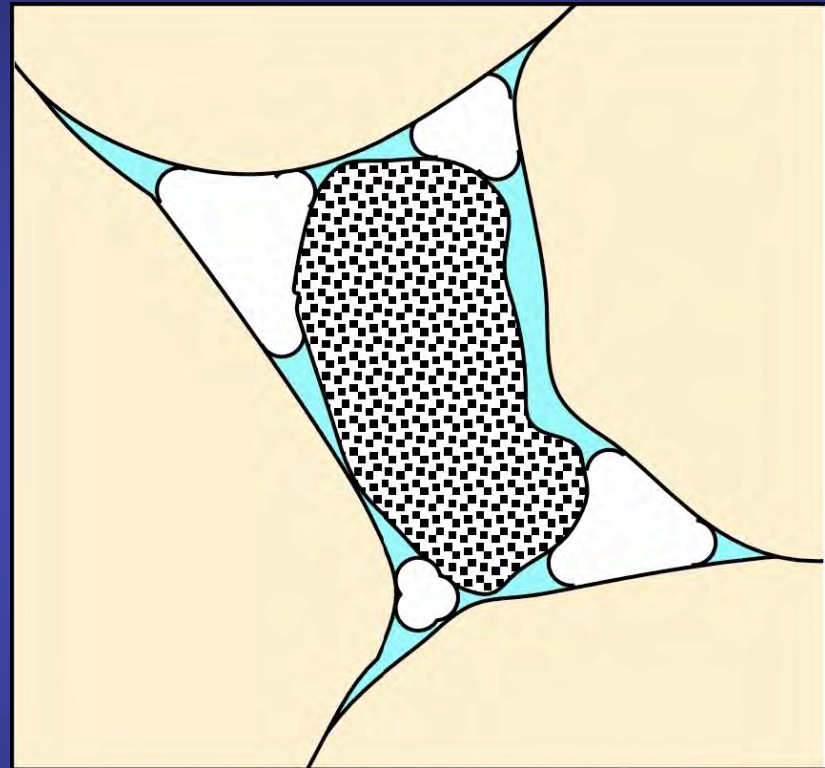
Hydrologic Properties

Relative Permeability



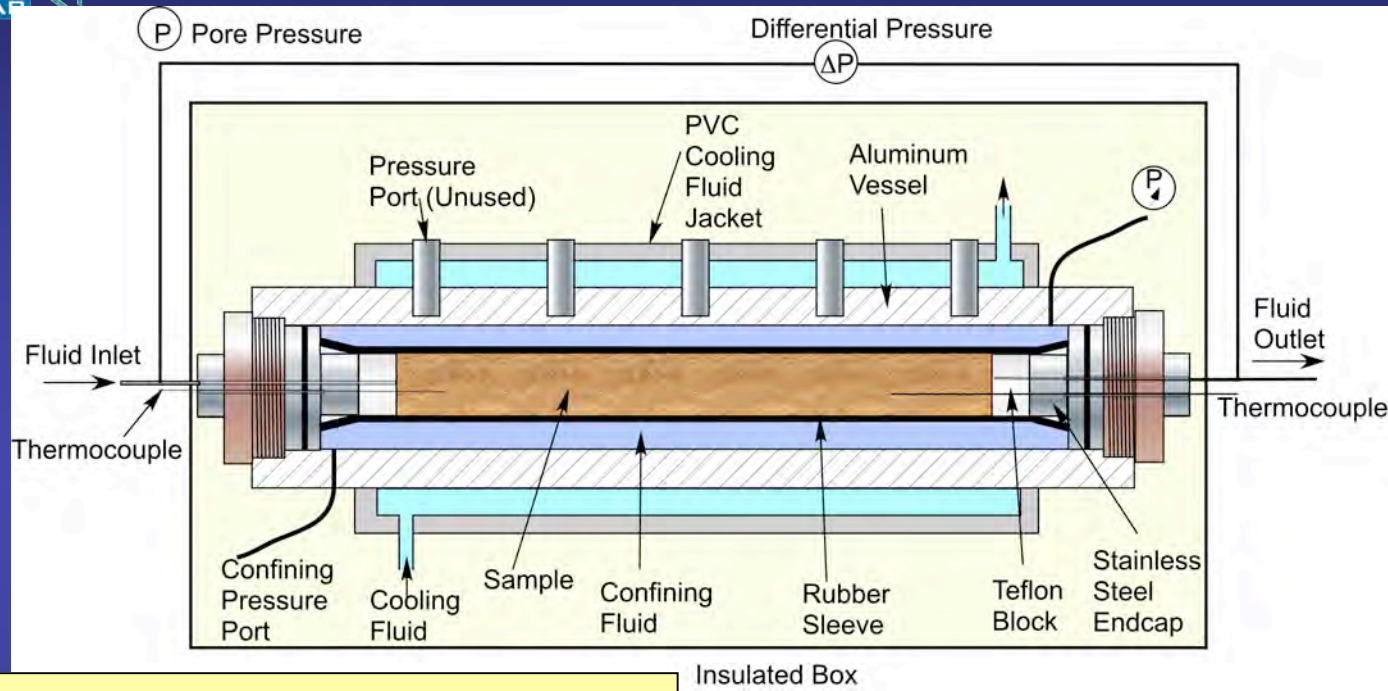
Relative Permeability

- Permeability (k) - measure of the ability for a fluid to move through a medium.
- Relative permeability (k_r) - measure of how the presence of interfering phases (hydrate, water, gas) affect the fluid movement.
- Gas hydrate in the porespace will strongly affect flow behavior
- k_r is also affected by hydrate location (e.g. grain contacts, pore bodies) and saturation in the porespace.





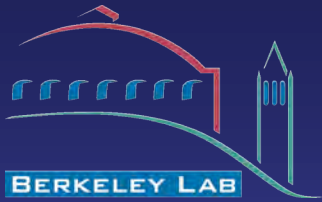
Relative Permeability [$k_r(S_h, S_w)$] Measurements



Challenges:

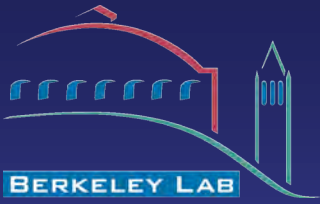
- Maintaining stable conditions while introducing water and/or methane and applying a pressure gradient
- Simultaneously knowing phase saturations

Approach: Sample characterization including x-ray CT, and waterflood technique with inverse modeling (iTOUGH2) to reduce measurement duration and number of fluids introduced.

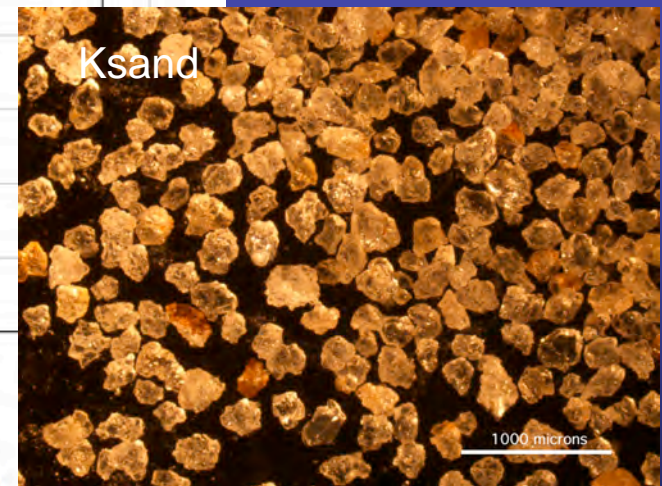
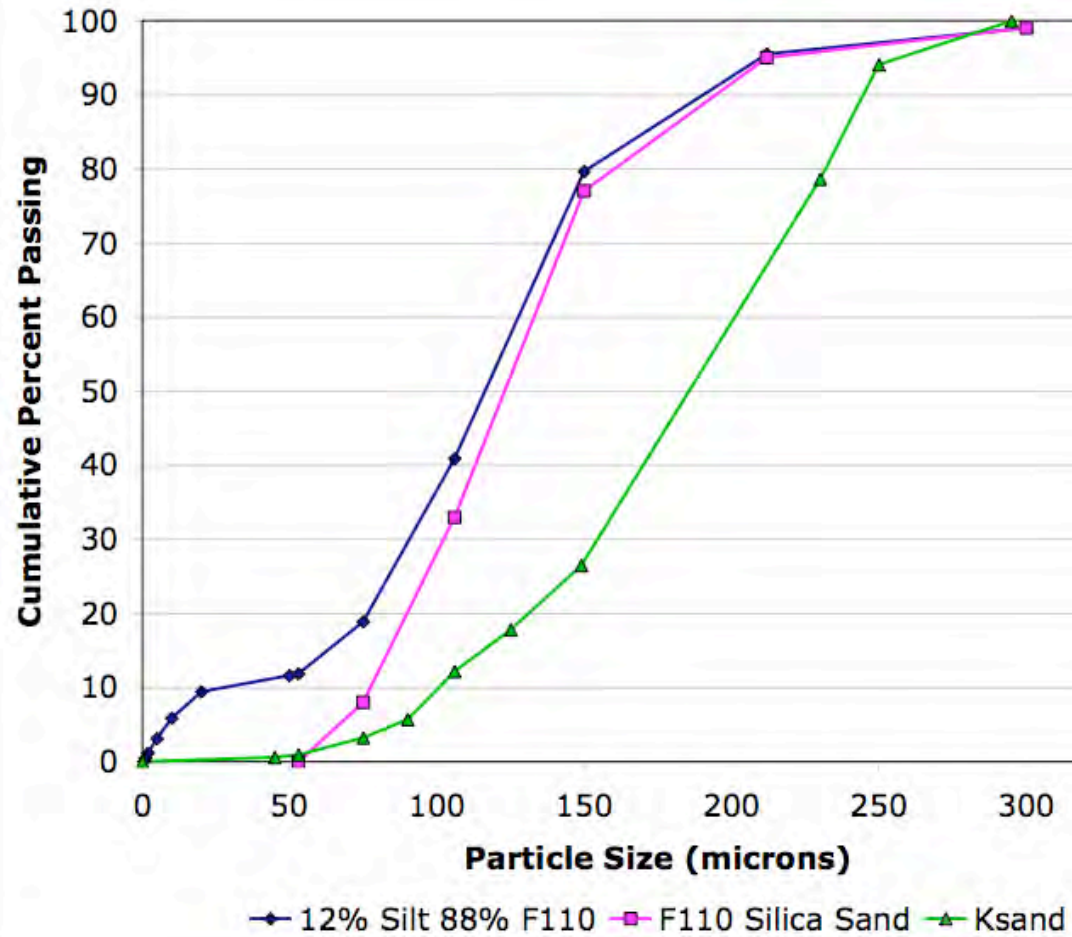


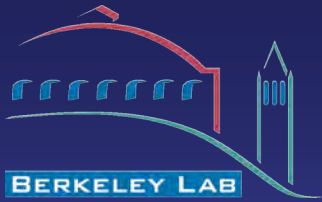
Method

- Moisten sand and pack column
- Apply a series of conditions - moist, frozen, hydrate-bearing, (*), water saturated, dry
- Measure permeability and CT scan each condition
- * Perform waterflood on the hydrate-bearing sand
- Compute/extend k_{rg} and k_{rw} by inverse modeling of waterflood data using ITOUGH2



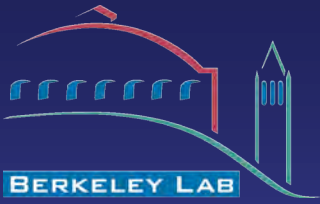
Media Investigated





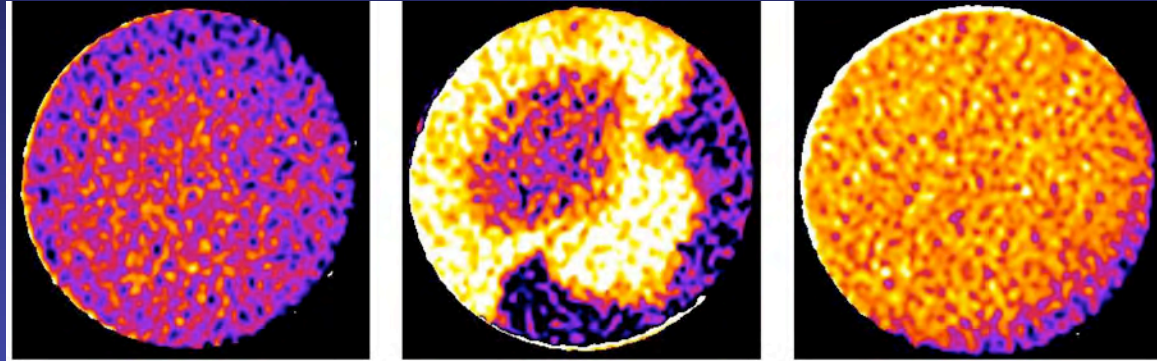
Conditions Investigated

| Sample | Porosity (from CT) | Initial Water Sat | Hydrate Sat | Gas Sat with Hydrate Present | Conversion of Water to Hydrate | Sample Diam. (cm) | Sample Volume (cm ³) | Sample Length (cm) |
|--------------|--------------------|-------------------|-------------|------------------------------|--------------------------------|-------------------|----------------------------------|--------------------|
| Fsand28 | 0.31 | 0.28 | 0.24 | 0.65 | 1.00 | 5.25 | 789 | 36.5 |
| Fsand40 | 0.31 | 0.40 | 0.42 | 0.50 | 0.93 | 5.44 | 894 | 38.5 |
| Fsand60 | 0.31 | 0.60 | 0.58 | 0.28 | 0.76 | 5.48 | 908 | 38.5 |
| Ksand20 | 0.38 | 0.20 | 0.21 | 0.75 | 0.82 | 5.89 | 969 | 35.6 |
| Ksand28 | 0.38 | 0.28 | 0.31 | 0.63 | 0.82 | 5.78 | 945 | 36.0 |
| Ksand42 | 0.38 | 0.42 | 0.36 | 0.50 | 0.67 | 5.71 | 917 | 35.9 |
| FsandSilt 21 | 0.31 | 0.22 | 0.26 | 0.71 | 0.89 | 5.28 | 291 | 13.3 |
| FsandSilt 39 | 0.30 | 0.39 | 0.43 | 0.50 | 0.81 | 5.41 | 312 | 13.6 |
| FsandSilt 56 | 0.30 | 0.56 | 0.49 | 0.42 | 0.72 | 5.41 | 313 | 13.6 |

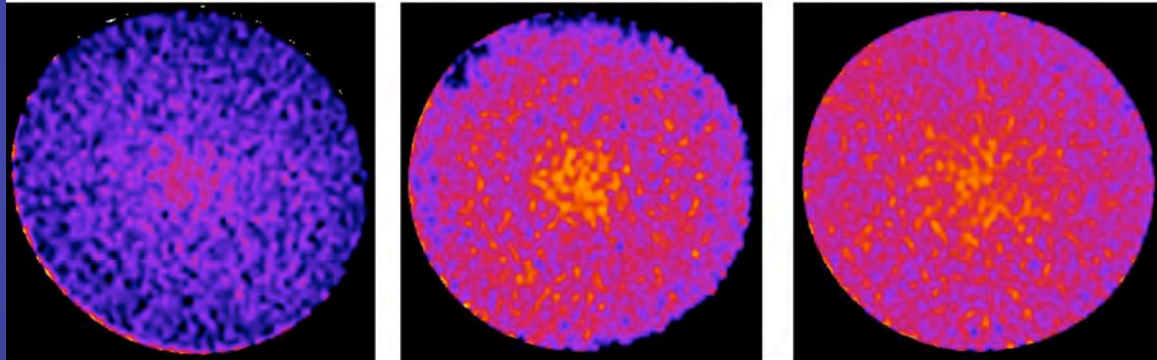


Hydrate Saturation Distributions

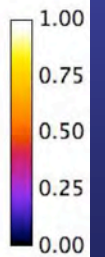
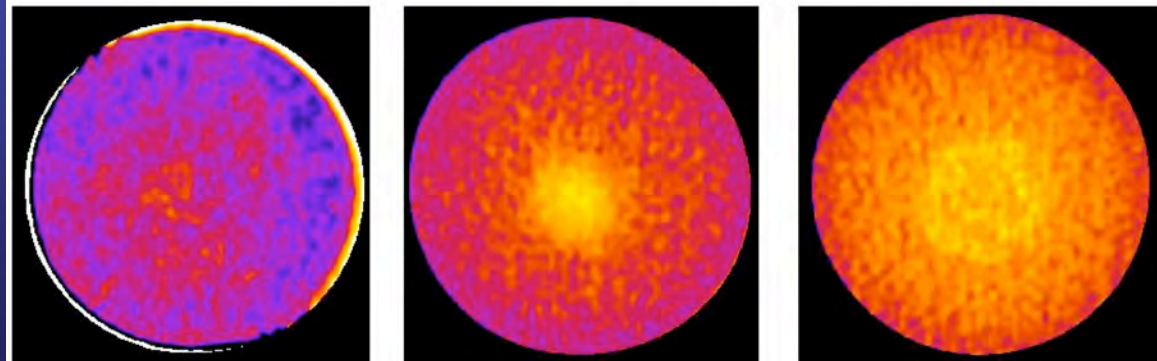
F110 Sand

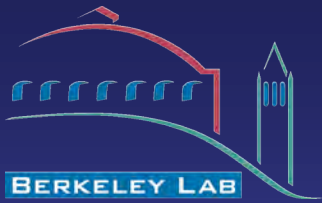


Ksand

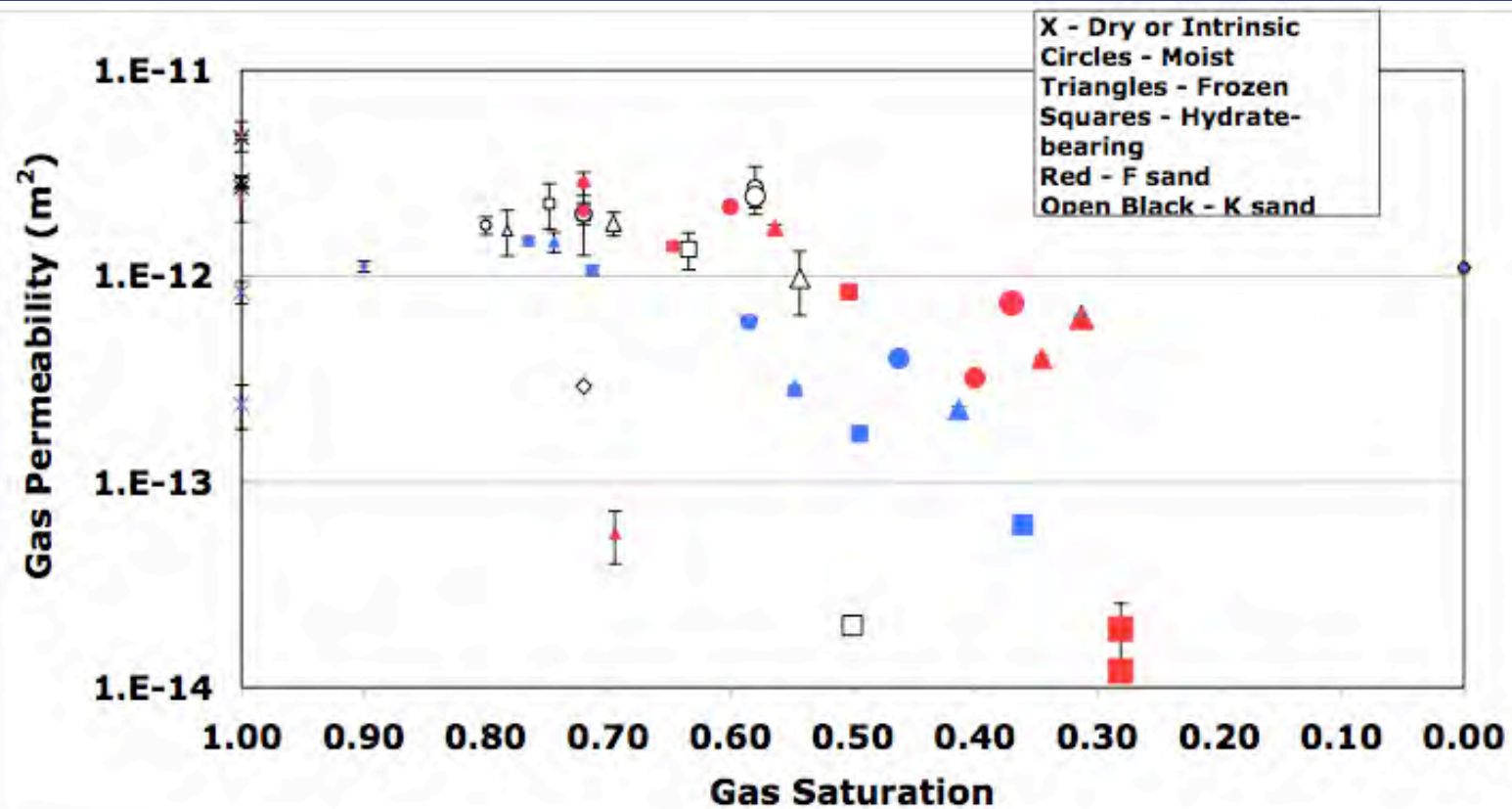


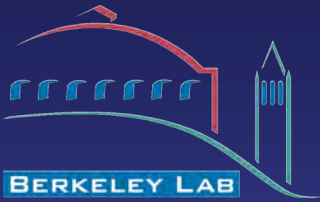
F110 Sand/Silt



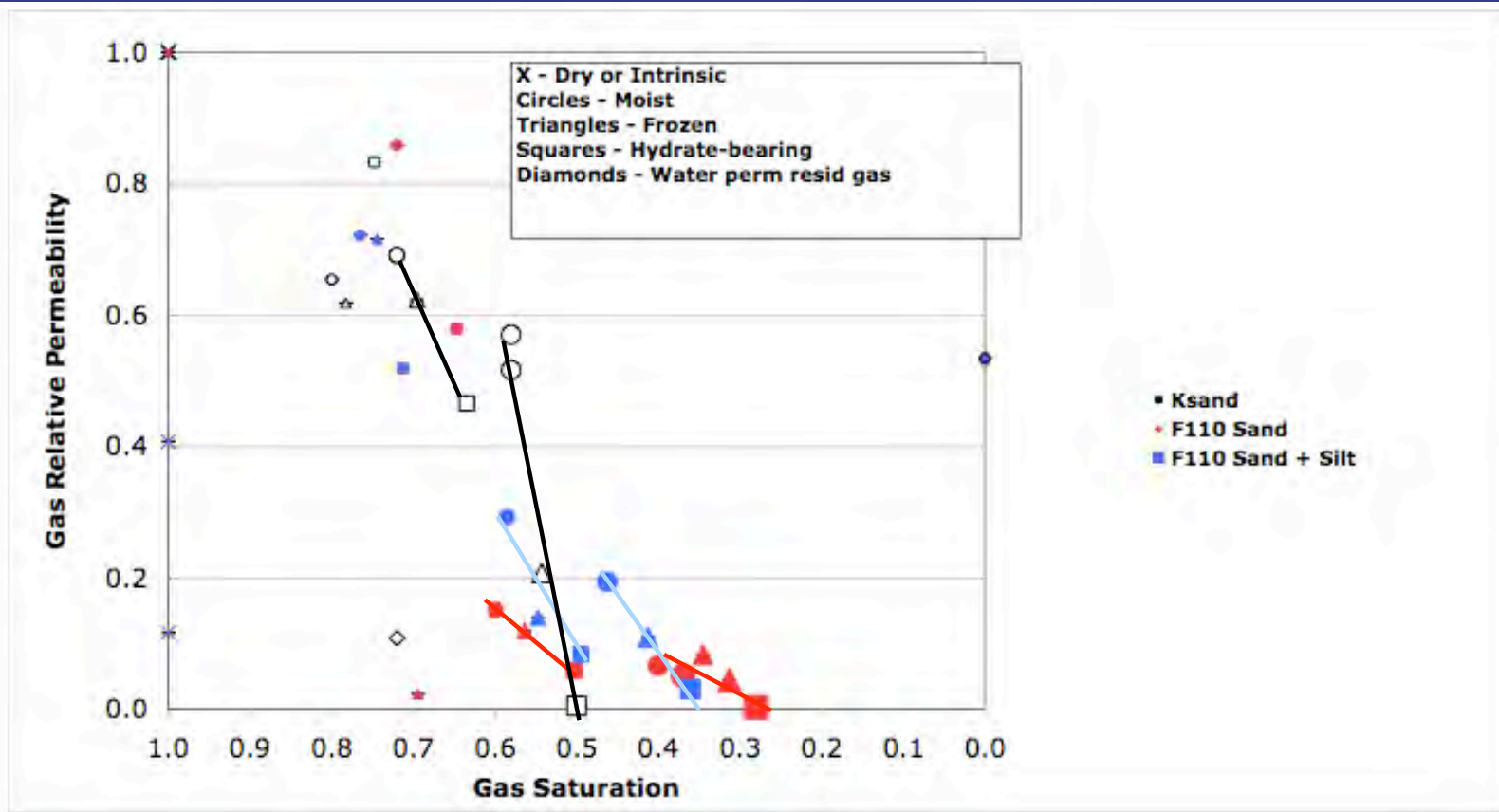


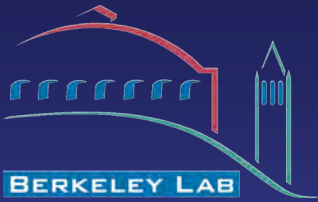
Gas Permeabilities



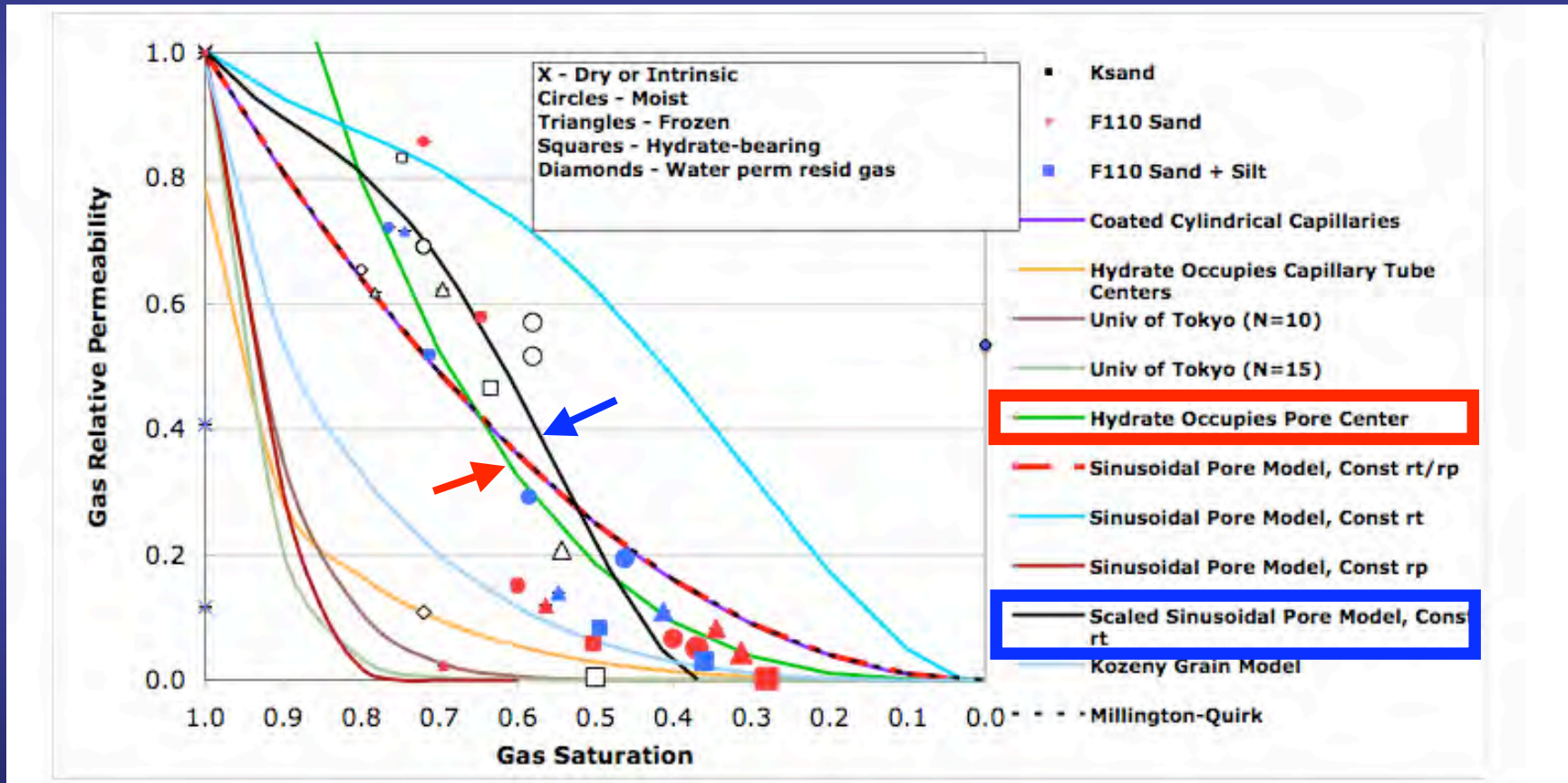


Gas Relative Permeabilities

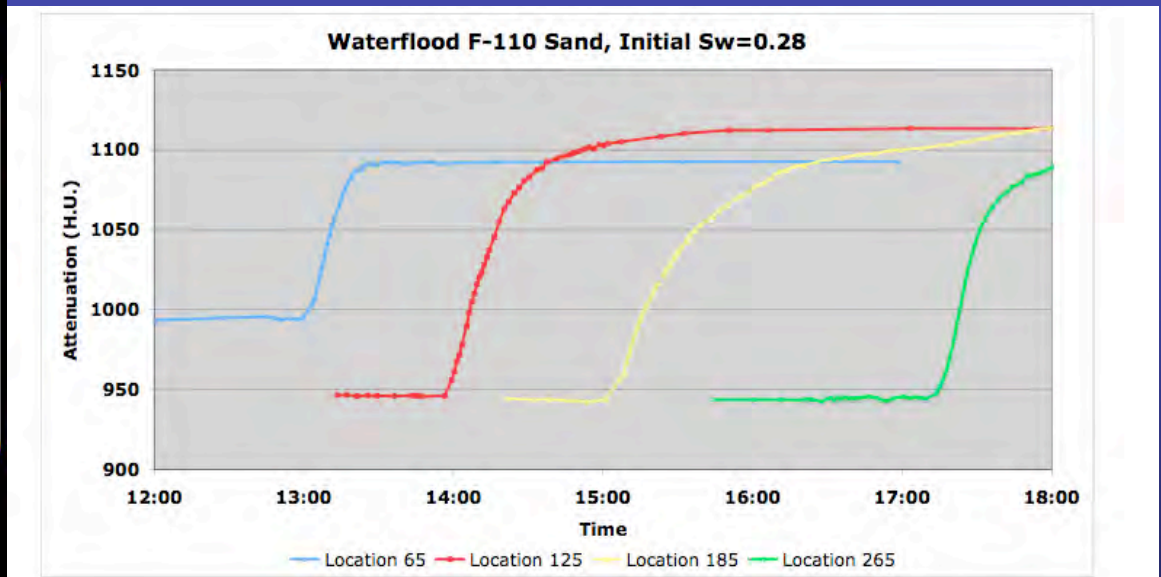
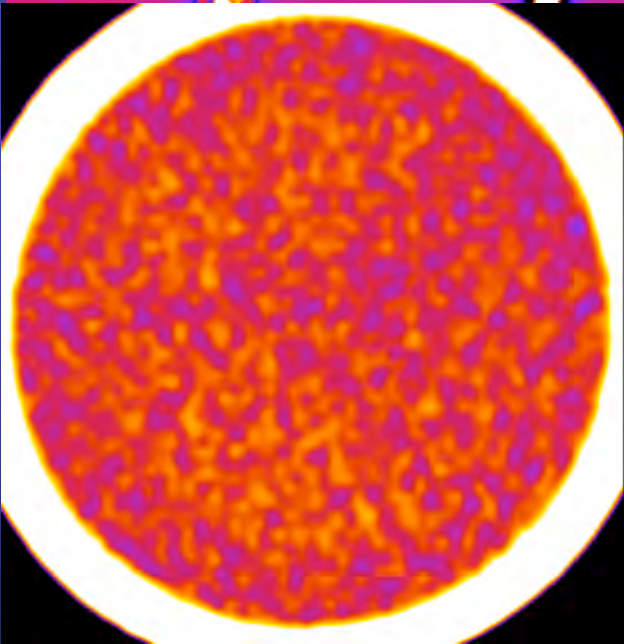
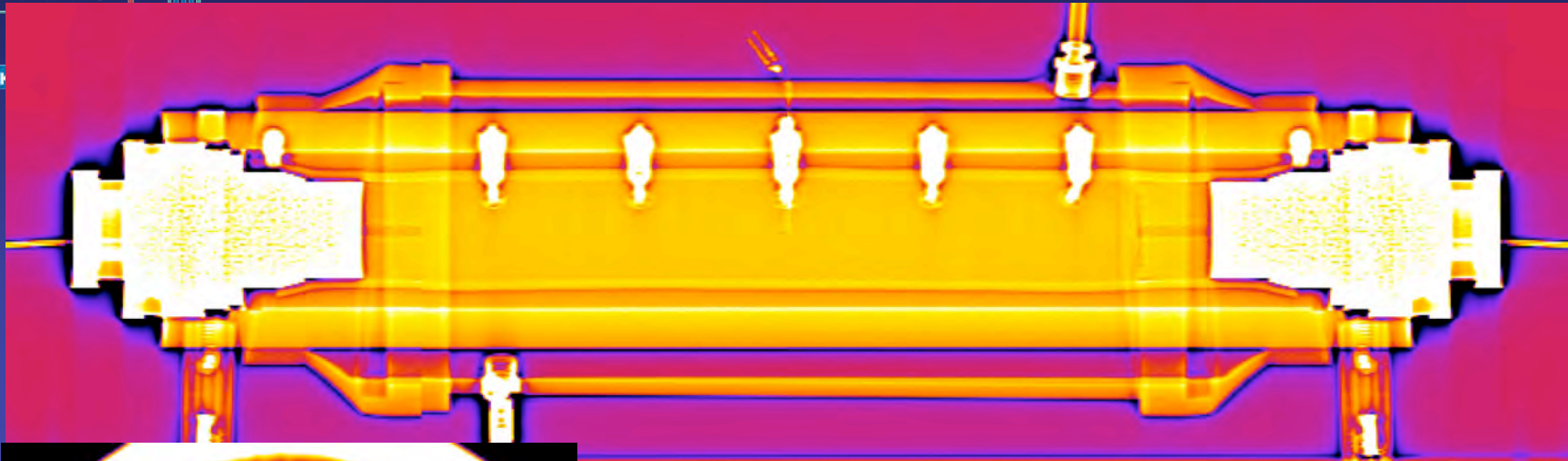




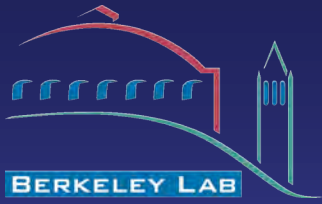
Comparison with Models



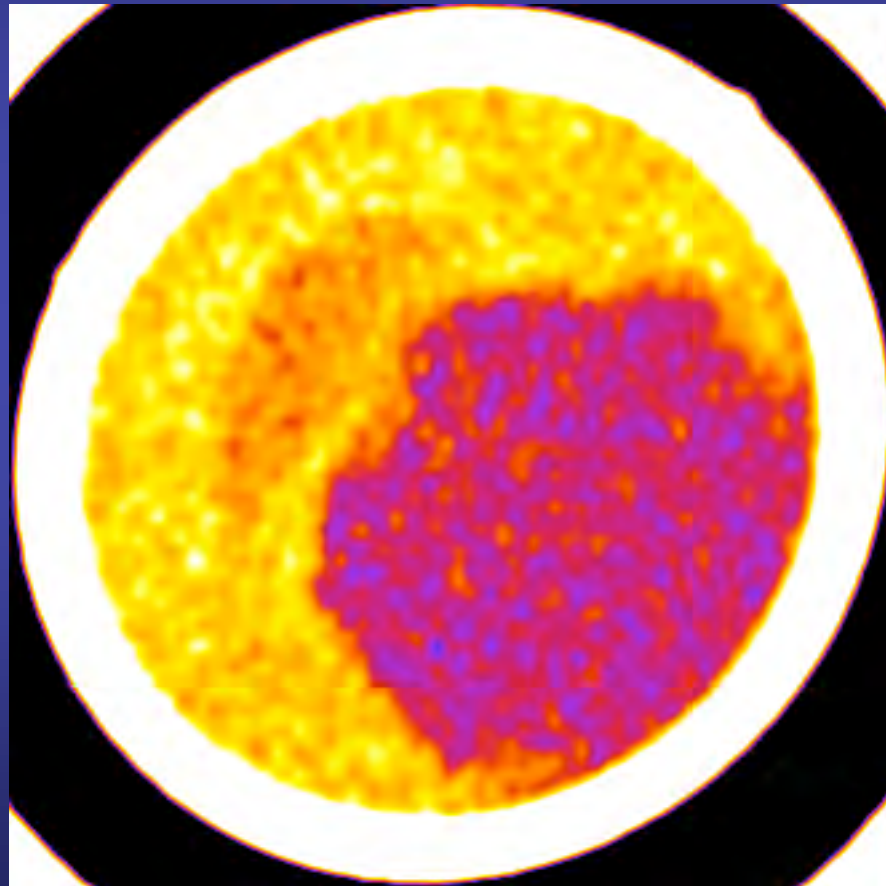
Waterflood

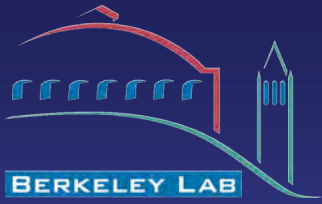


Water saturation during waterflood through “uniform” sandpack having “uniform” hydrate saturation



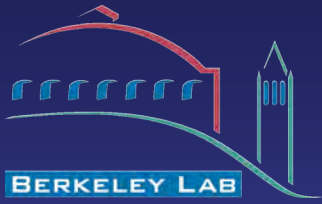
Flow - Heterogeneous S_h





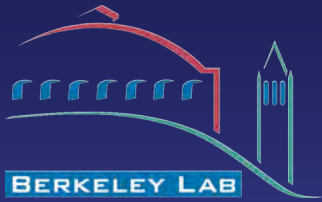
Numerical Inversion

- Numerical inversion of waterflood data using iTOUGH2 is ongoing.
- Initial analyses indicate that relative permeability estimations will be nonunique without measured capillary pressure-saturation data.
- Measurements of capillary pressure-saturation are ongoing.
- We are developing a technique to obtain both relative permeability and capillary pressure from a single test.



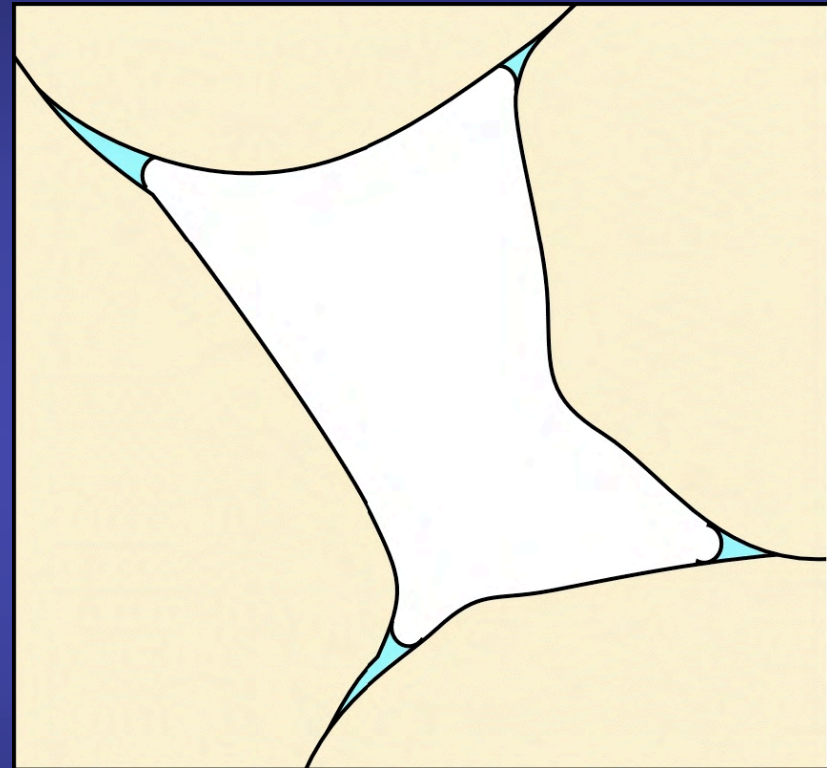
Hydrologic Properties

Capillary Pressure and Relative Permeability Functions

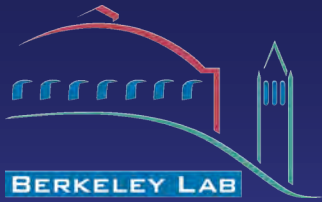


Capillary Pressure

- Pressure difference between two phases (e.g. water and gas)
- Caused by interfacial tension, surface wettability, and pore geometry
- $P_c \propto \sigma/r_K$
- Function of saturations of all phases

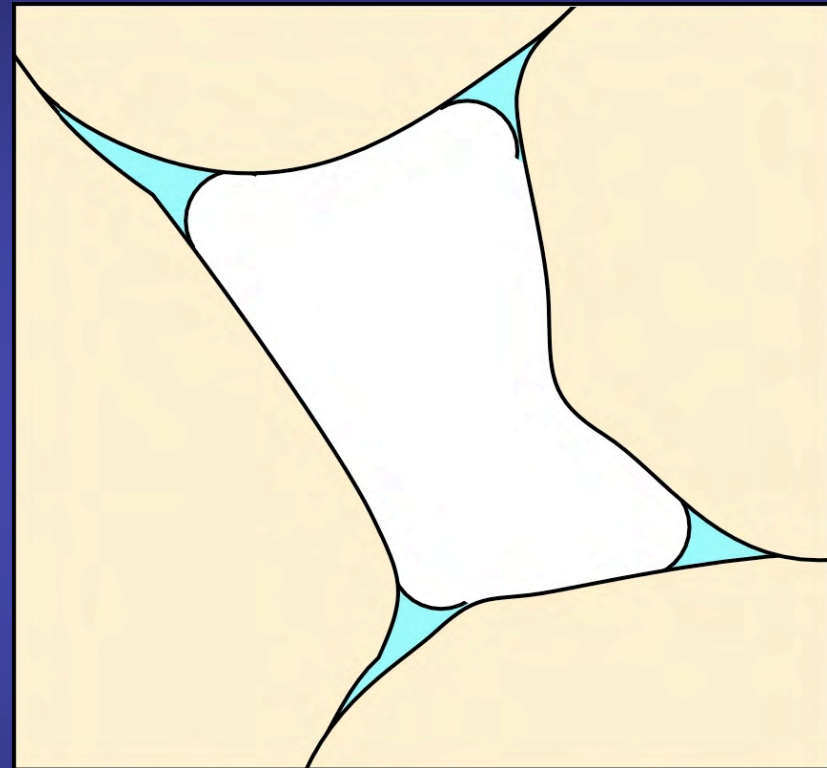


| r_K | P_c | Sat_w |
|-------|-------|---------|
| small | large | low |

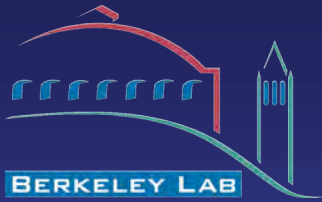


Capillary Pressure

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- Caused by interfacial tension, surface wettability, and pore geometry
- $P_c \propto \sigma / r_K$
- Function of saturations of all phases

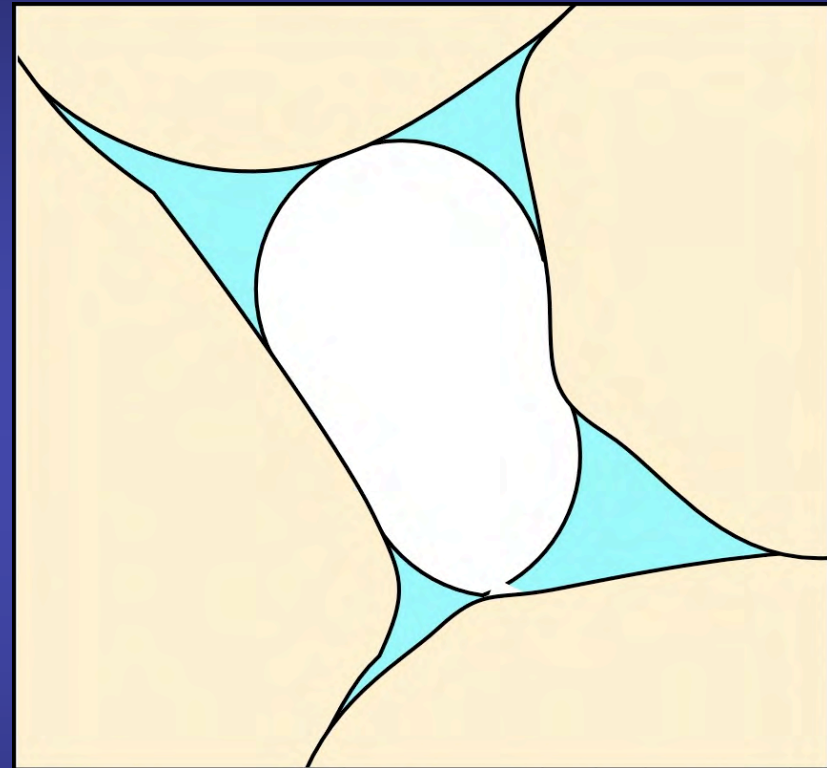


| r_K | P_c | Sat _w |
|-------|-------|------------------|
| med | med | med |

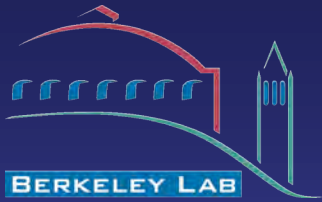


Capillary Pressure

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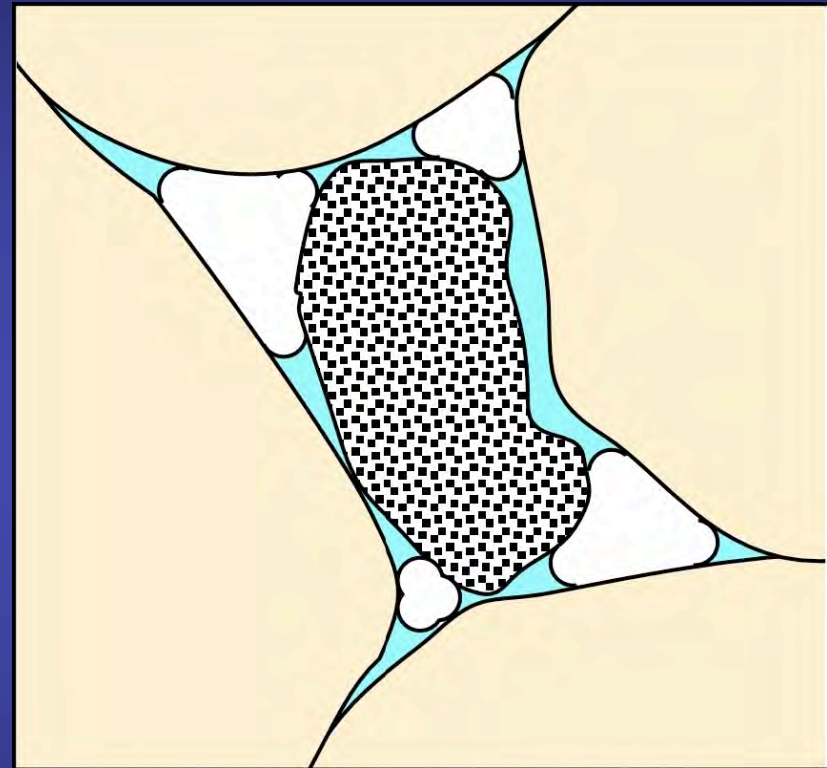


| r_K | P_c | Sat_w |
|-------|-------|---------|
| large | small | high |

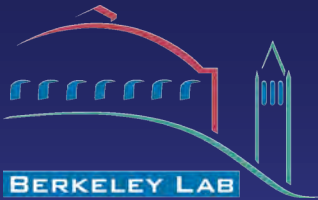


Capillary Pressure

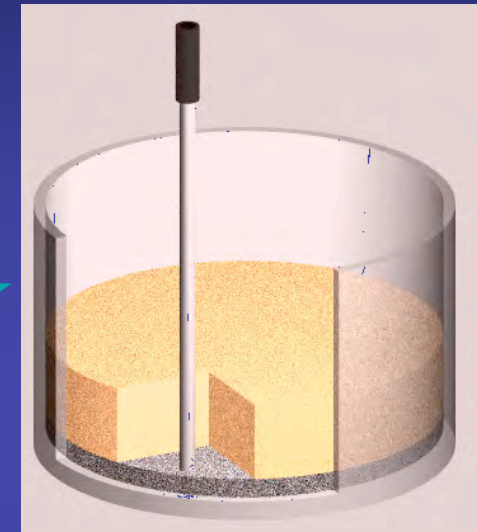
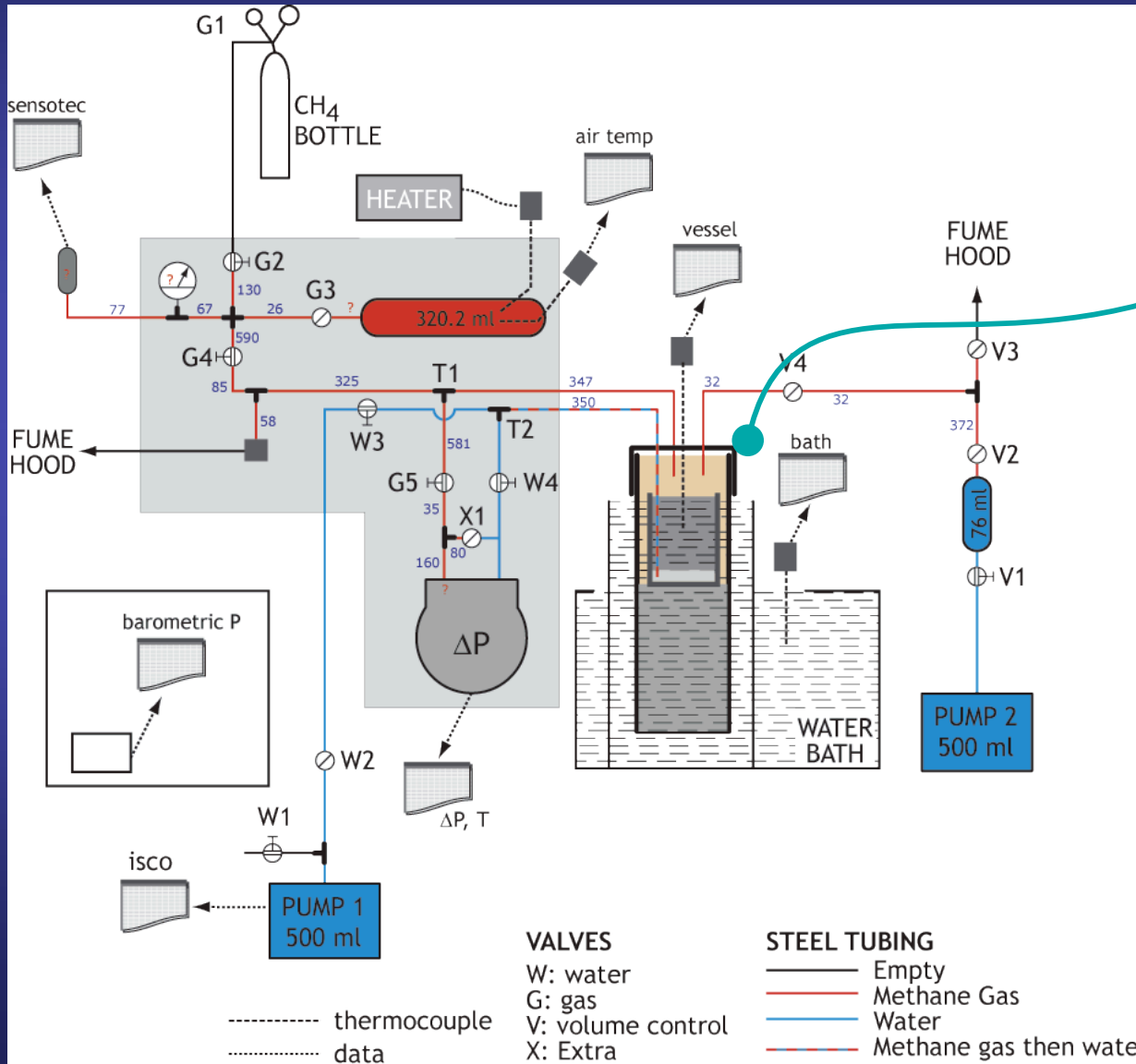
- Pressure difference between two phases (e.g. water and gas)
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- $P_c \propto \sigma/r_K$
- Function of saturations of all phases

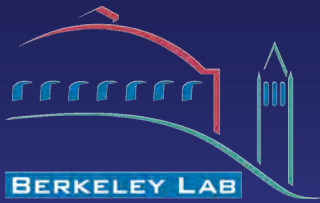


| | | |
|-------|-------|---------|
| r_K | P_c | Sat_w |
| small | large | med |



Experimental Setup



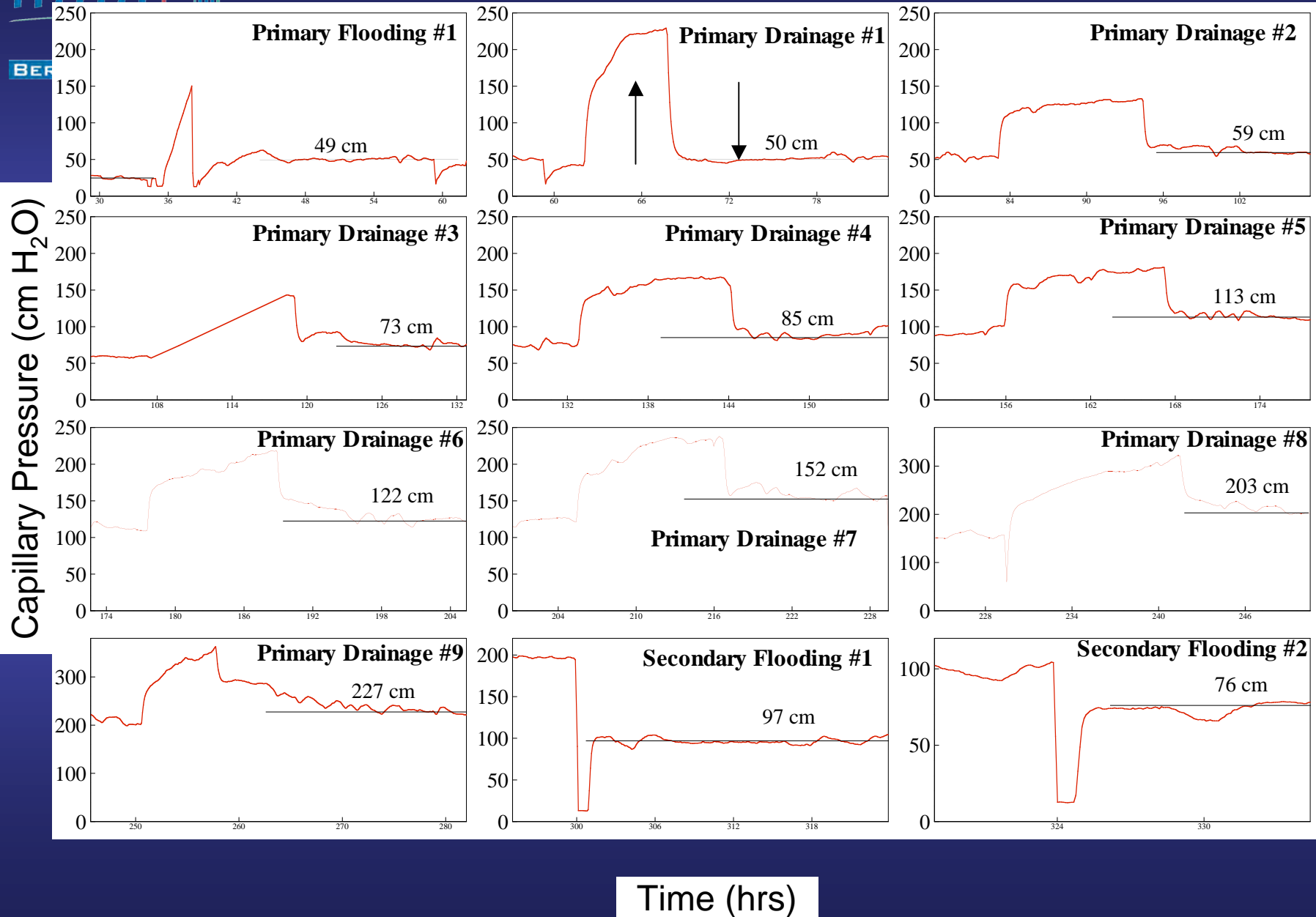


Summary of Tests Conducted

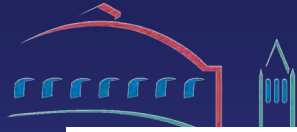
| Test # | Material | Hydrate Sat | Start | End |
|--------|----------|-------------|------------|------------|
| 1 | KSand | 35% | 10-05-2007 | 10-29-2007 |
| 2 | KSand | 35% | 10-30-2007 | 11-21-2007 |
| 3 | KSand | 20% | 11-24-2007 | 12-15-2007 |
| 4 | KSand | 20% | 01-07-2008 | 01-14-2008 |
| 5 | KSand | 20% | 01-14-2008 | 02-04-2008 |
| 6 | KSand | 0% | 12-28-2007 | 02-08-2008 |
| 7 | KSand | 45% | 02-11-2008 | 03-05-2008 |
| | | | | |
| 8 | F110 | 20% | 03-11-2008 | 04-13-2008 |
| 9 | F110 | 35% | 04-15-2008 | 04-27-2008 |
| 10 | F110 | 35% | 04-29-2008 | 05-03-2008 |
| 11 | F110 | 35% | 05-03-2008 | 06-19-2008 |
| 12 | F110 | 45% | 06-20-2008 | 07-30-2008 |

Successful test

K-Sand, 45% Saturation, Part 1

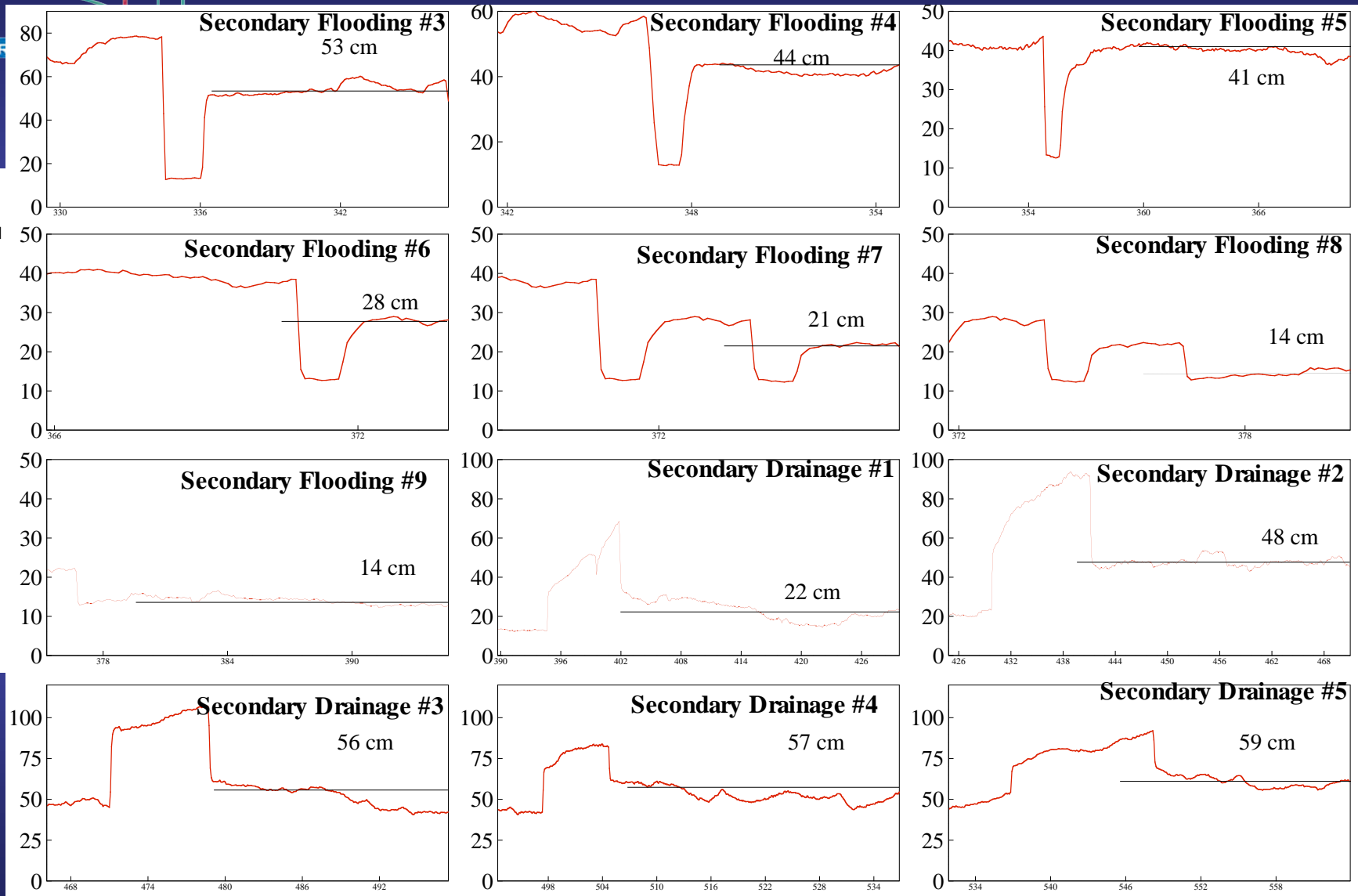


K-Sand, 45% Saturation, Part 2

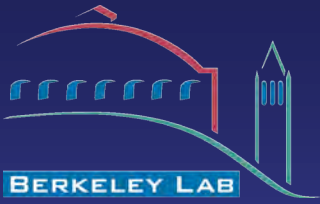


BER

Capillary Pressure (cm H₂O)



Time (hrs)



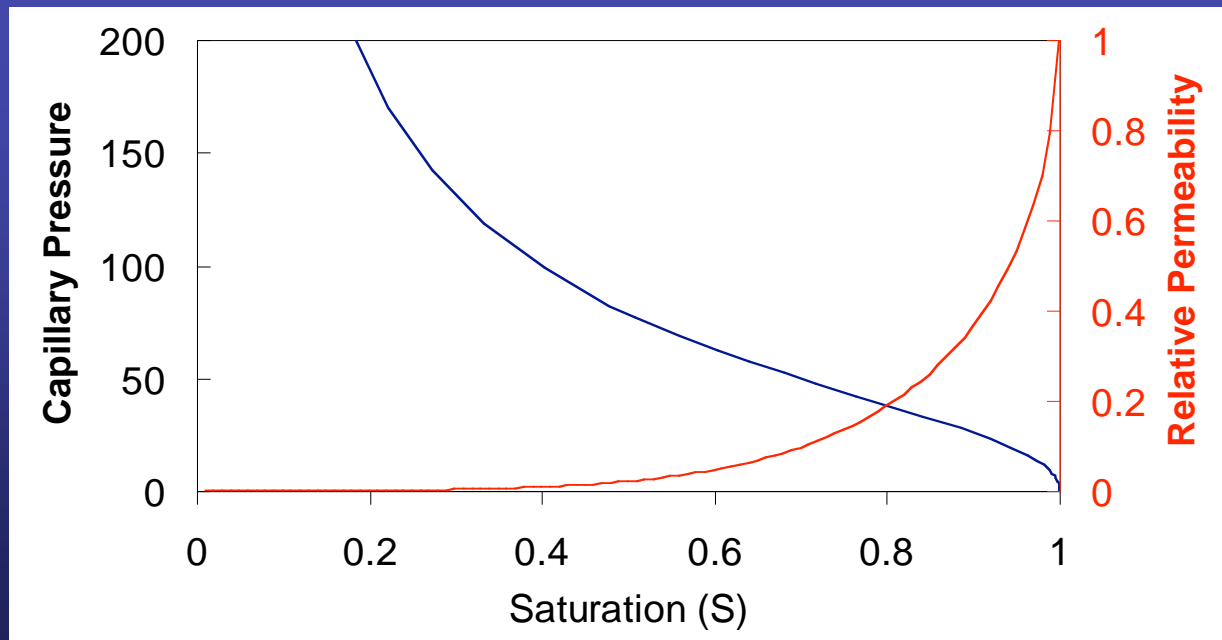
P_c , k_r Models

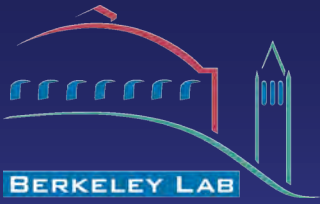
van Genuchten (**vG**) model of capillary pressure (where $m=1-1/n$), with P_o and n as fitting parameters:

vG model allows to estimate relative permeability function from capillary pressure function (k_S = absolute permeability)

$$S(P_c) = \left(1 + \left(\frac{P_c}{P_o} \right)^n \right)^{-m}$$

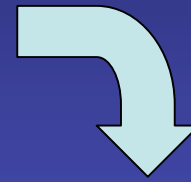
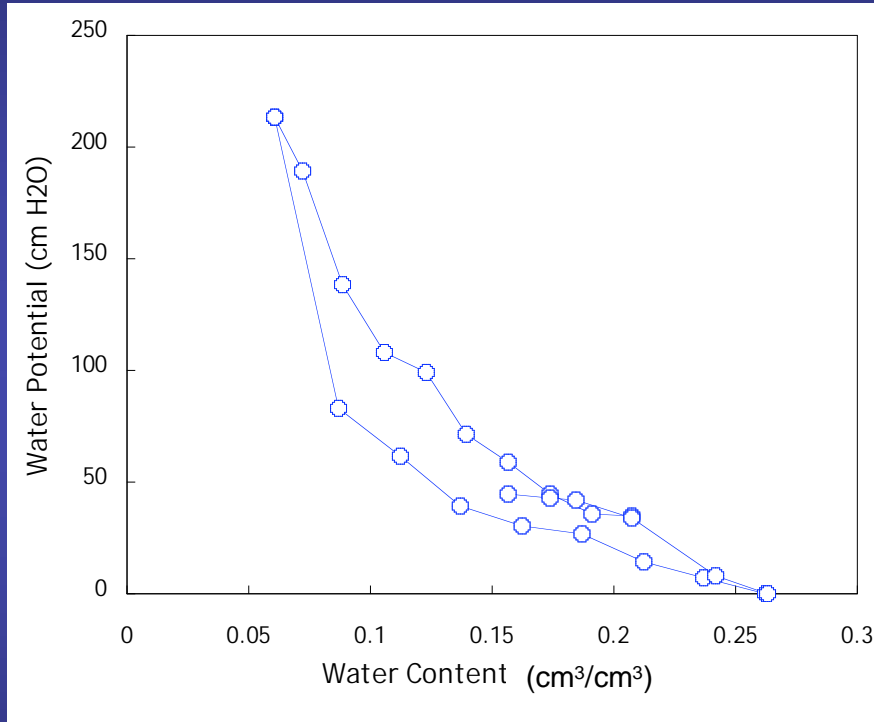
$$k(S) = k_S \sqrt{S} \left(1 - \left(1 - S^{1/m} \right)^m \right)^2$$



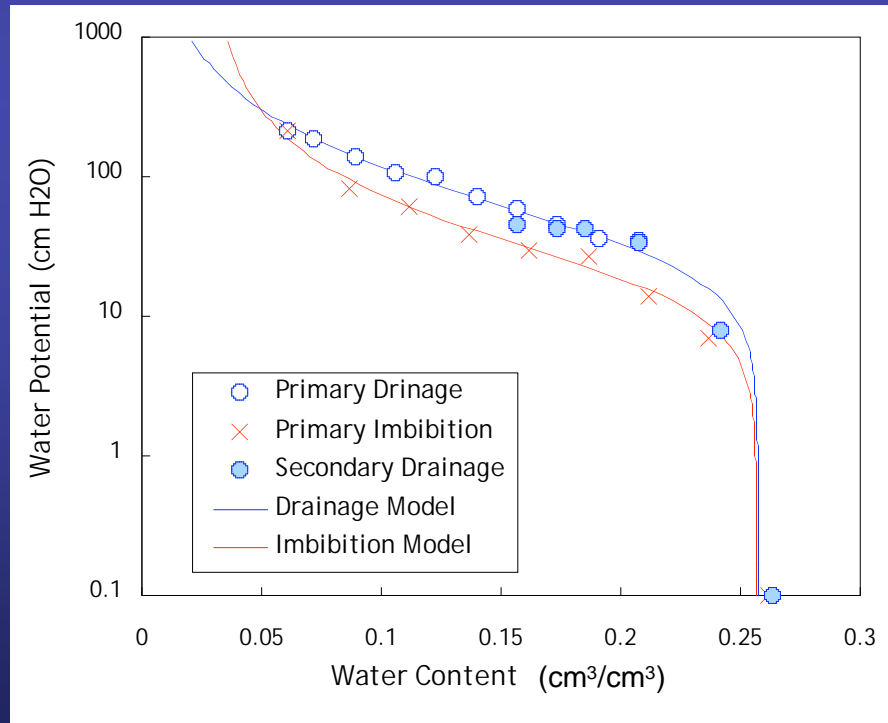


K-Sand, 45% Saturation

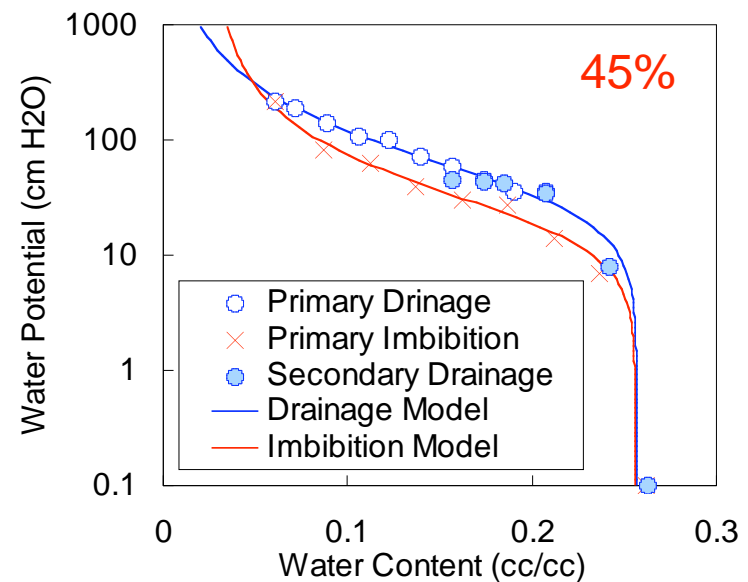
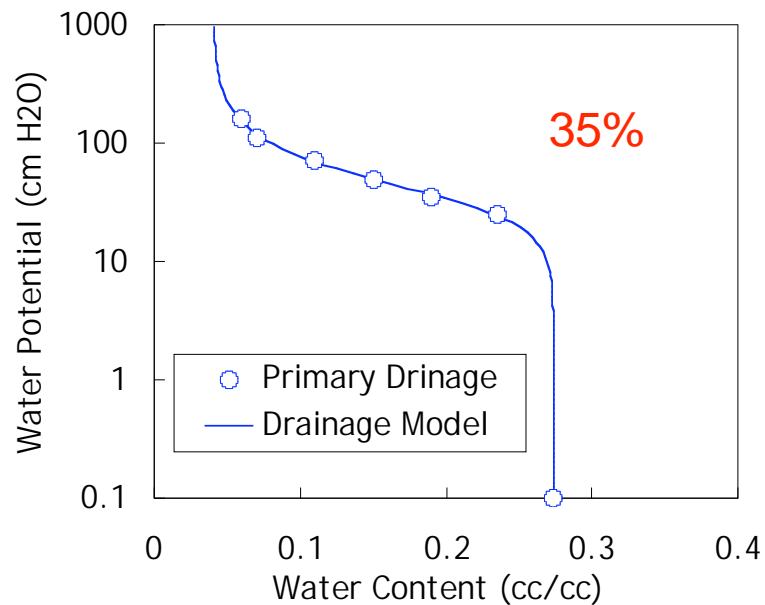
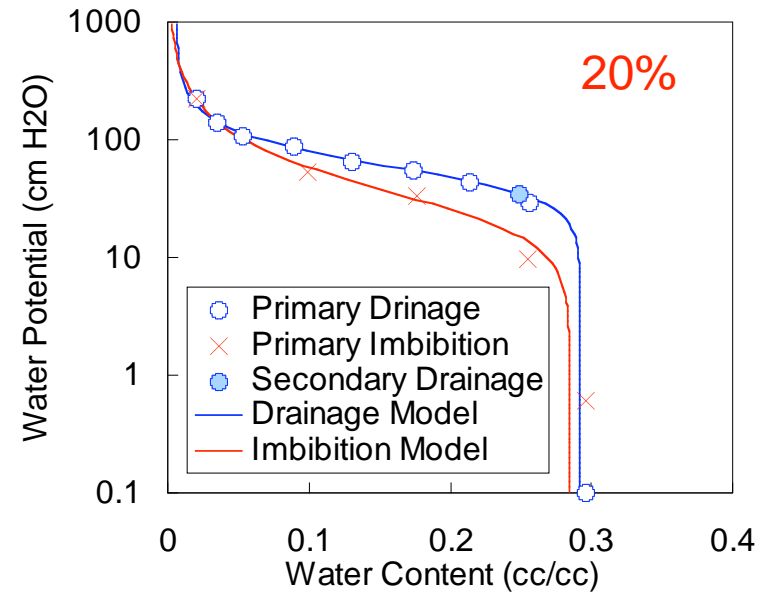
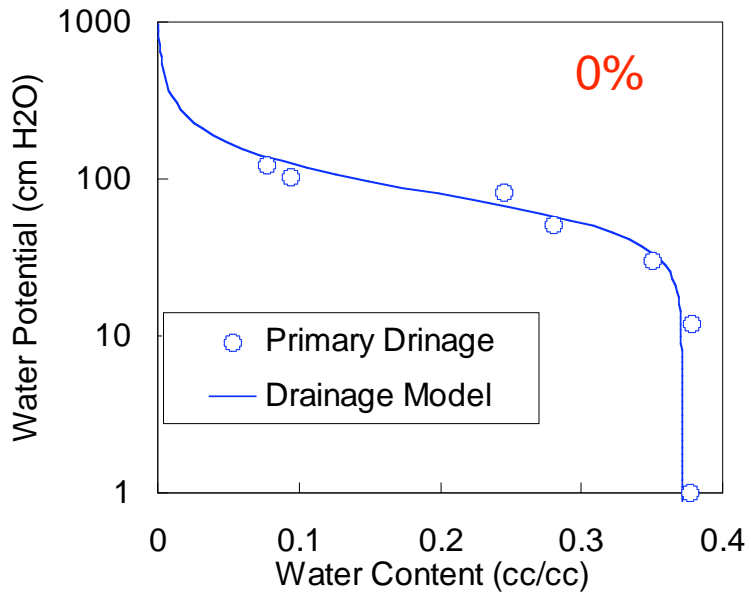
Hysteretic Capillary Pressure Data



van Genuchten Model Fits



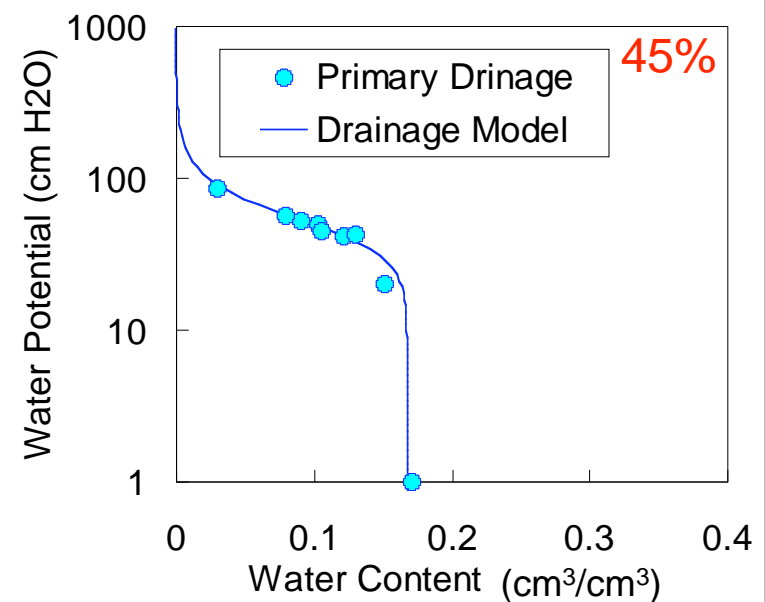
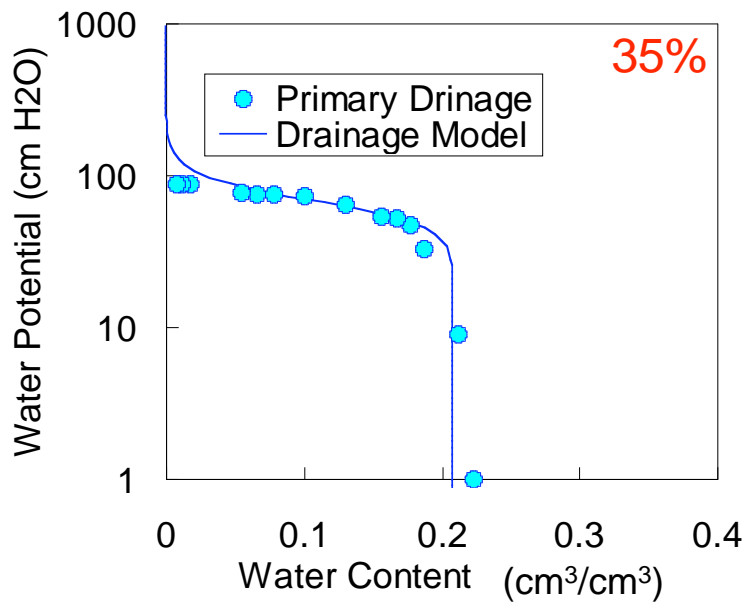
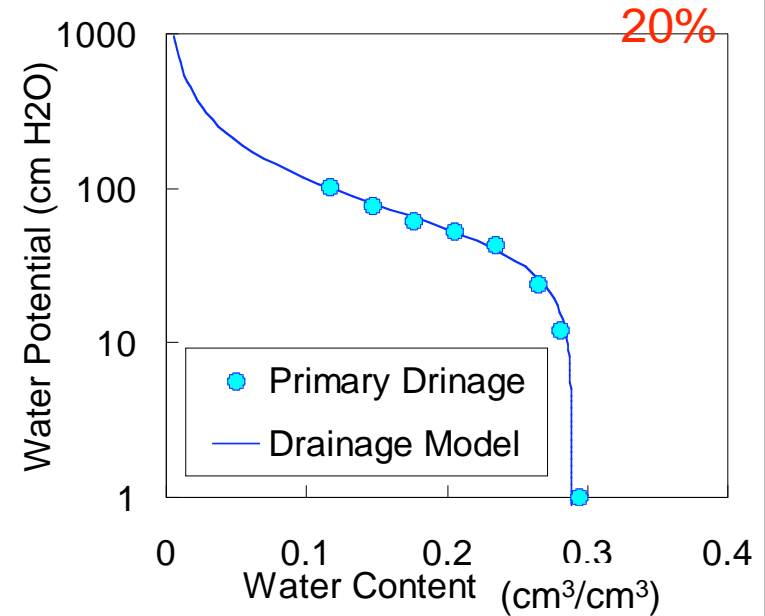
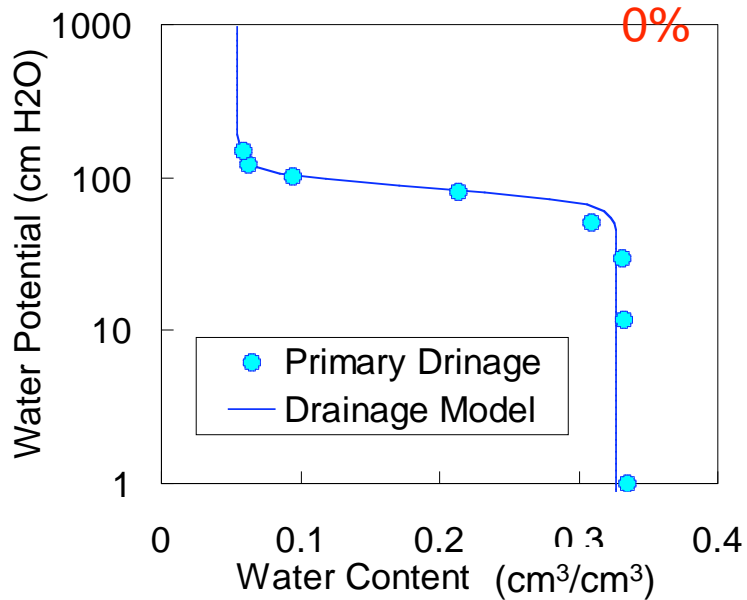
K-Sand: All Saturations

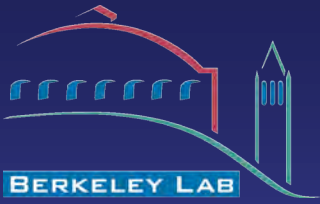




F110 Sand: All Saturations

BER

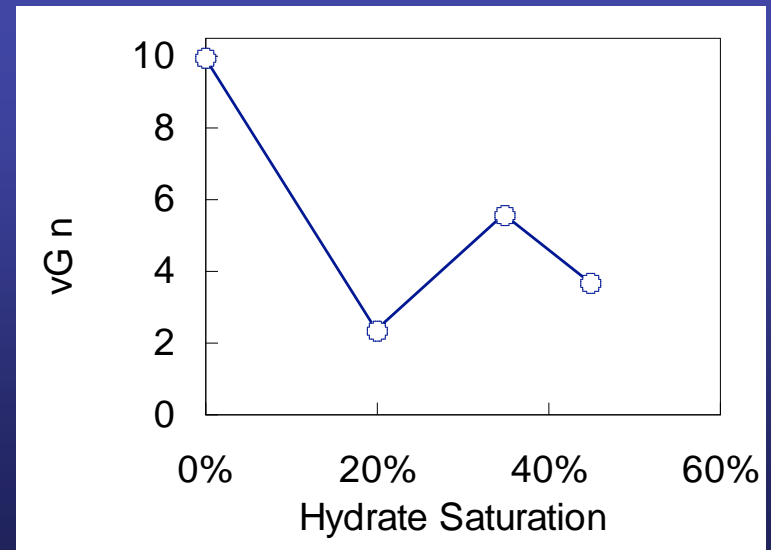
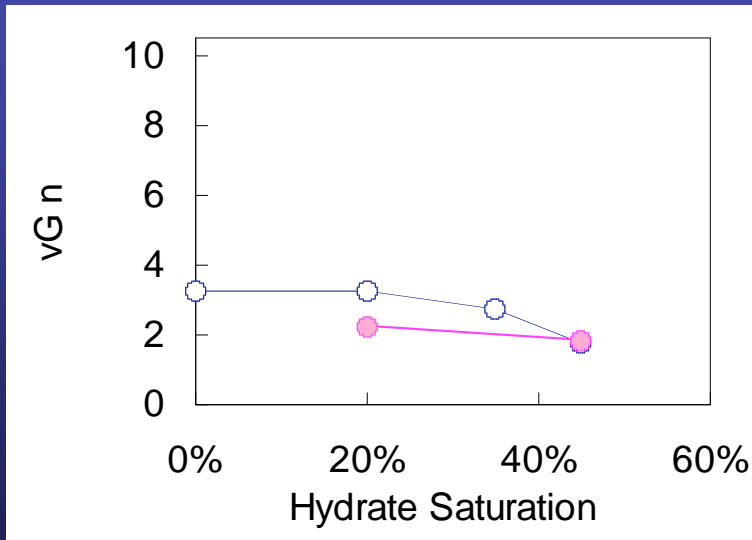
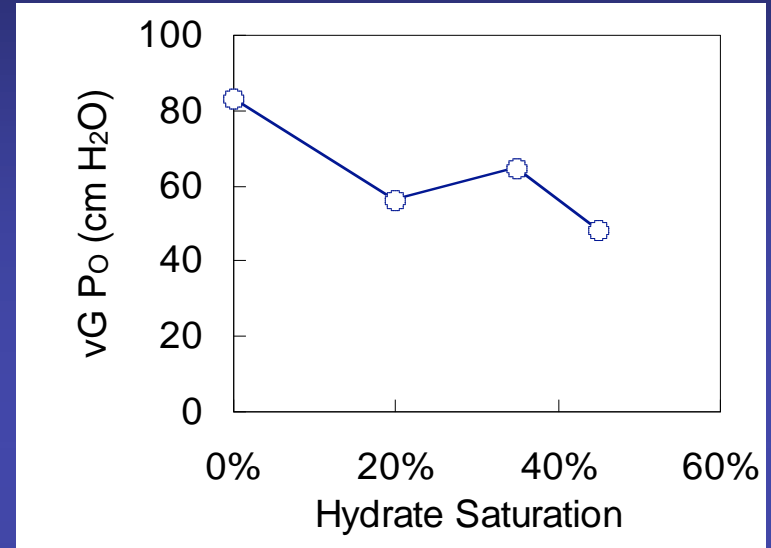
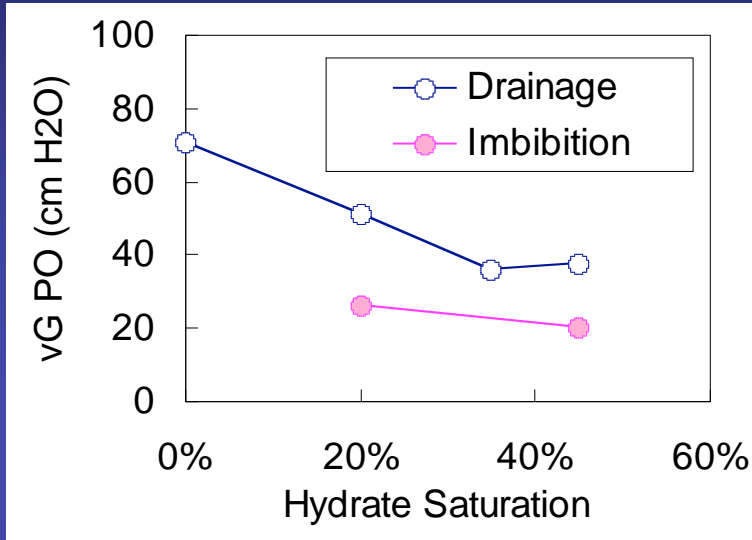


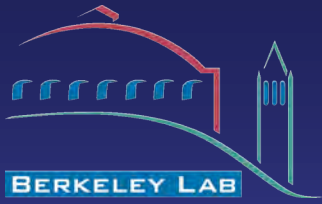


Capillary Pressure Parameters

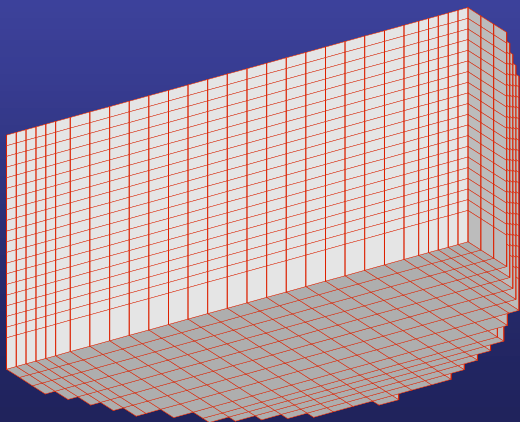
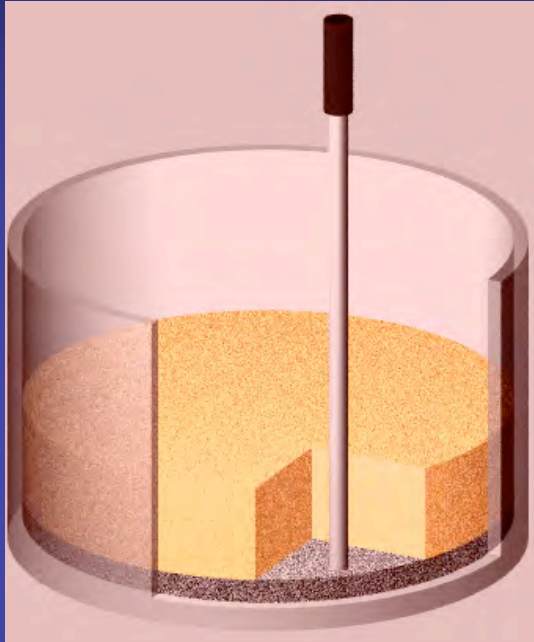
K-Sand

F110

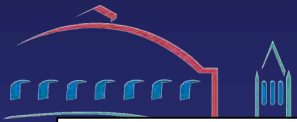




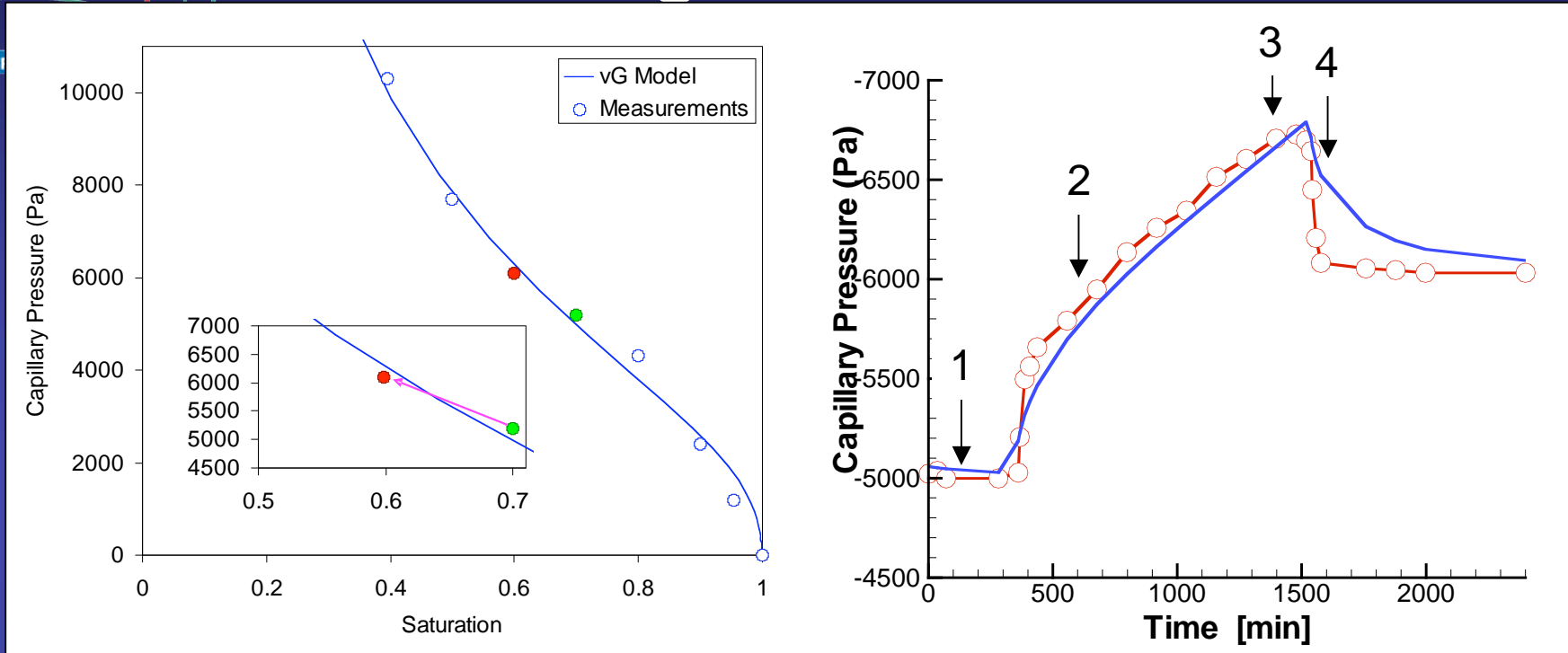
Inverse Modeling of Transient



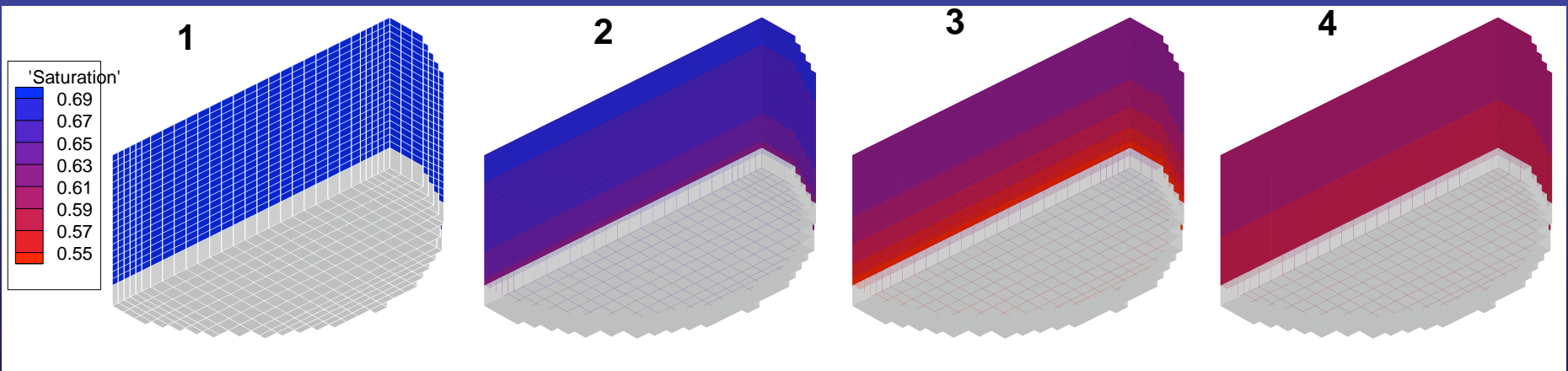
- **Objective:** To infer relative permeability from transient pressure data.
- Assume decoupled capillary pressure and relative permeability curves.
- Optimize m & k_s in vG model
- Consider only half volume: 6,680 grid blocks, 18,700 connections.
- Isothermal flow, with passive gas and hydrate phases.



Modeling Result: F110, 20%

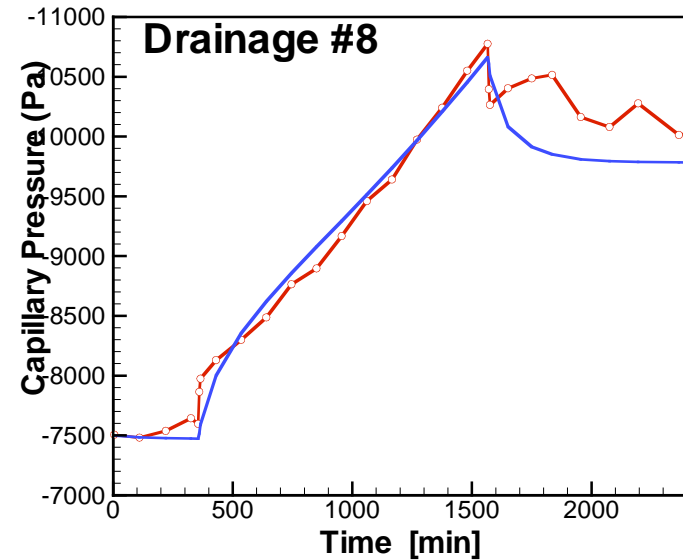
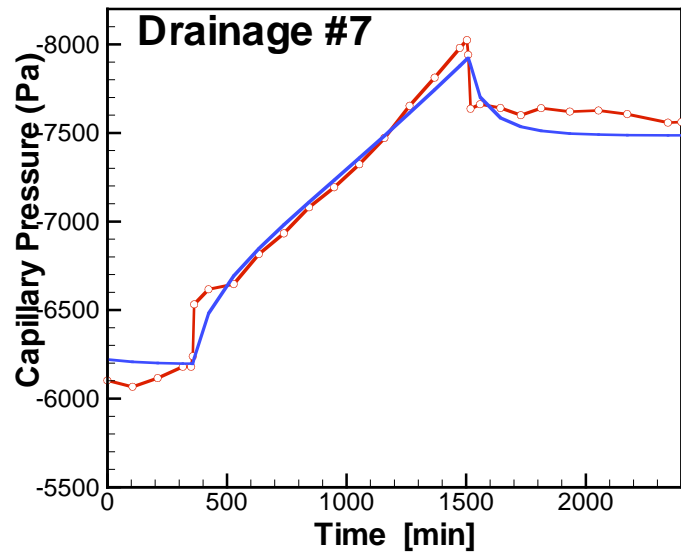
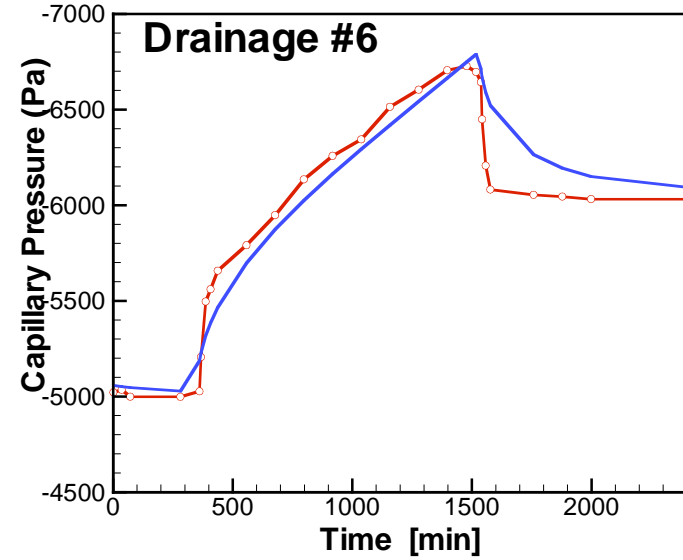
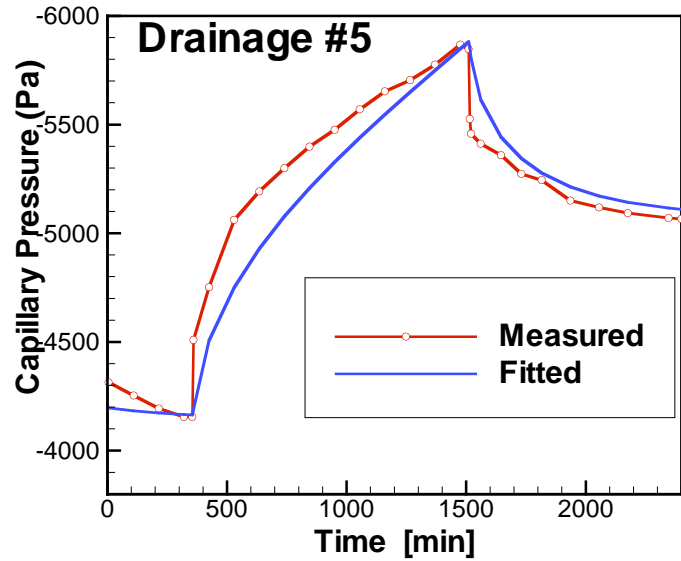


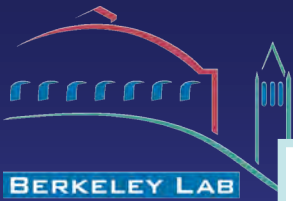
Moisture distributions during drainage



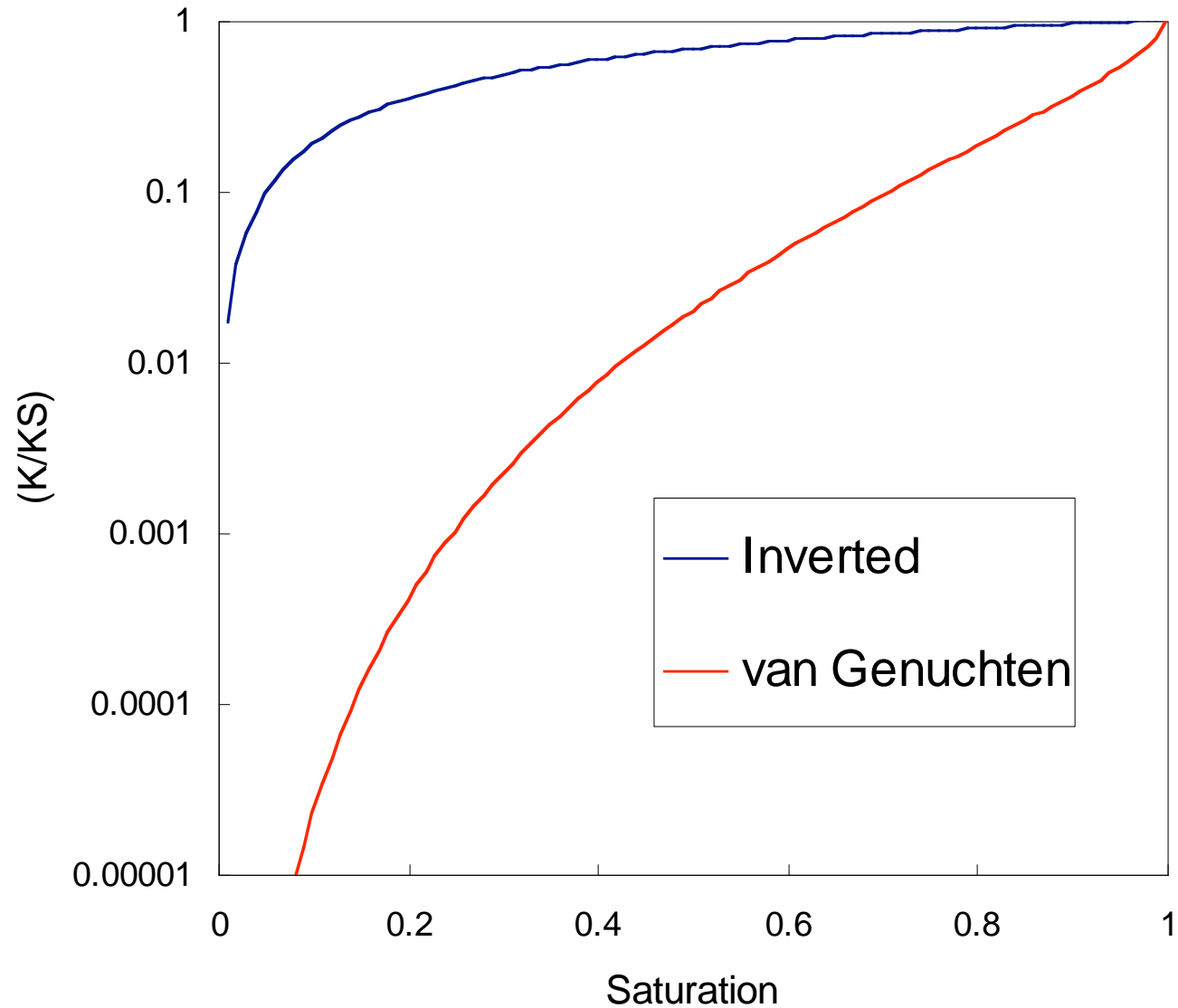


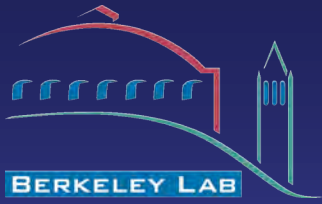
Fits at Multiple Drainage Stages: F110, 20%





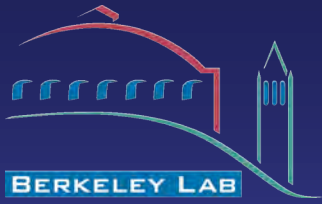
Fitted Relative Permeability Function: F110, 20%





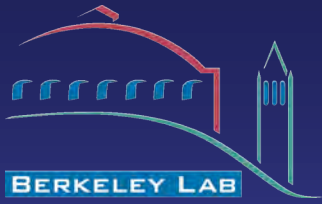
Challenges

- Minor temperature differences cause large apparent capillary pressures
- Uncertainty in packing density within a sample and between samples
- At low saturation and/or permeability, imposed flow rate can be higher than permeability. This may lead to strong capillary-pressure gradients and/or hydraulic discontinuity



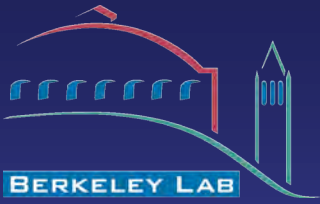
Hydrologic Properties Path Forward

- Complete k_r repeat measurements
- Complete capillary pressure measurements
- Complete waterflood k_r modeling (with NETL)
- Complete capillary pressure/ k_r inversions to estimate k_r and $P_c(S)$ functions
- Compare and understand k_r values estimated by each method
- Understand hydrate formation distribution in samples (would like to work with a graduate student on this)
- Continue investigating hydrate porespace occupation importance relevance [with USGS, and others (Ebinuba?)]



Geomechanical and Geophysical Properties

**Mechanical strength and seismic property
measurements of hydrate-bearing sediments
(HBS) during hydrate formation and loading tests**



Delays in CH4-HBS Test Approval

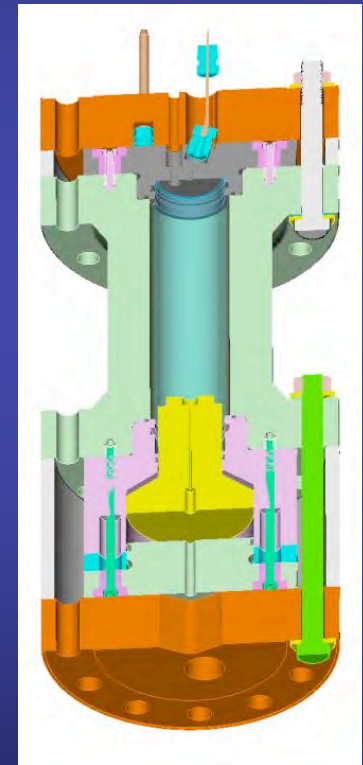
DOE mandates strict Environment, Health, and Safety practices at national labs

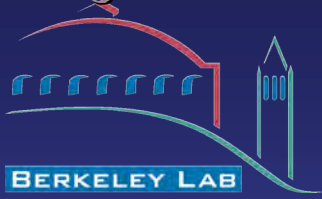
New mechanical safety approver

- Enforcing *very* strict safety requirement for “high-hazard” pressure vessels
- Full-scale 3-D finite element stress analysis
- Formerly acceptable Mech.Eng.Handbook/ASME code-based analysis and actual pressure testing (completed in Jan.'08) not sufficient

Vessel modifications to satisfy safety requirements

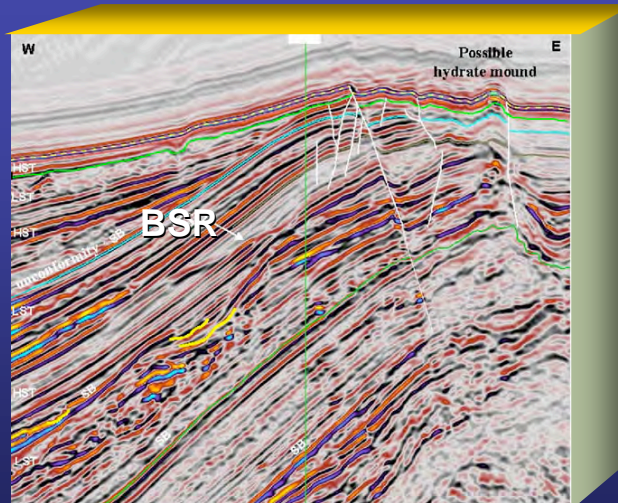
- Many modifications have been made through interactions among scientists (user), engineers (FEM modelers, machinists), and the safety approver
- LBNL/Eng. Spent \$>75K from the lab’s internal safety budget
- Modified test vessel currently in production





Introduction

- Gas hydrate → Understanding the geomechanical and geophysical properties is important for
 - (1) Assessing stability of oil and gas wells and seafloor, and
 - (2) Resource development (methane gas) and production monitoring
- Laboratory data for geomechanical and geophysical properties of hydrate-bearing sediments (esp. for methane hydrate) is still scarce

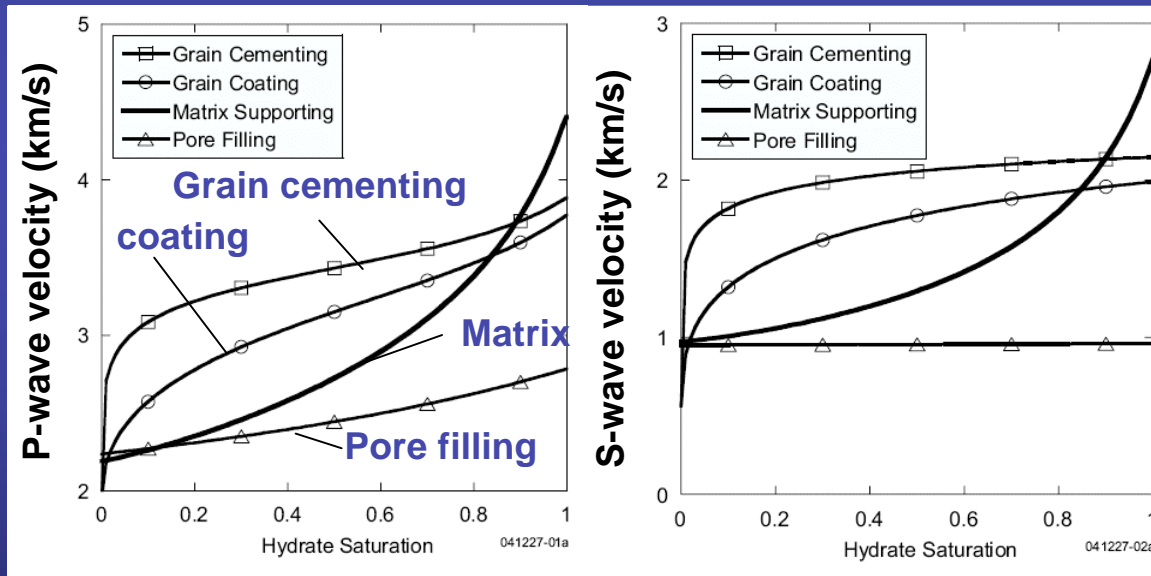


(from Snyder et al., AAPG, 2004)



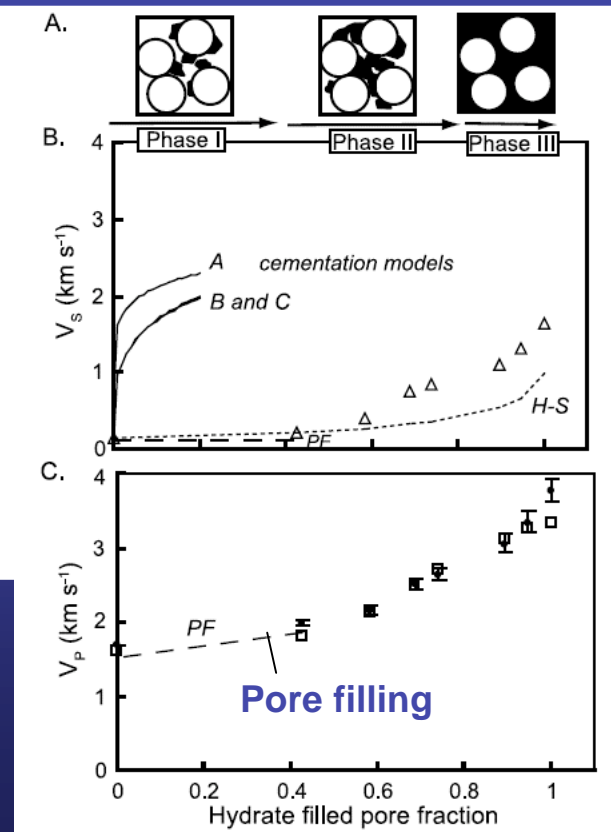
Introduction

- Gas hydrate within sediments can exist in a variety of forms
- Both geomechanical properties (e.g., strength) and geophysical properties (e.g., seismic velocities) are a strong function of hydrate distribution within sediment pore space



Kleinberg and Dai, OTC17205 (2005)

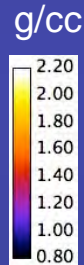
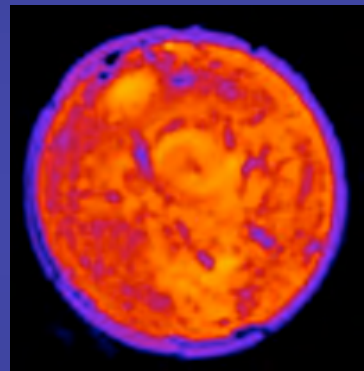
Yun et al., GRL (2005)



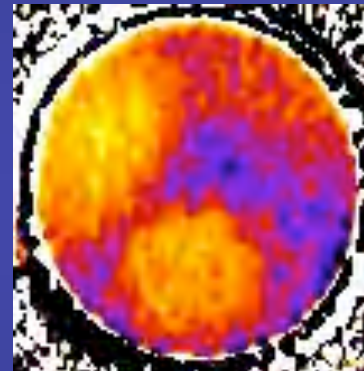


Introduction

- Both laboratory and field samples are often heterogeneous, which could lead us to wrong conclusions on their properties→Needs for visualization



Natural HBS core from oceanic floor

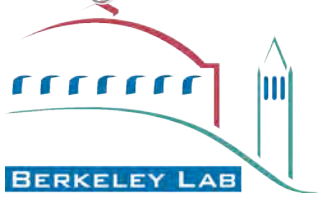


% hydrate saturation



Laboratory -synthesized HBS core
(difference image by subtraction)

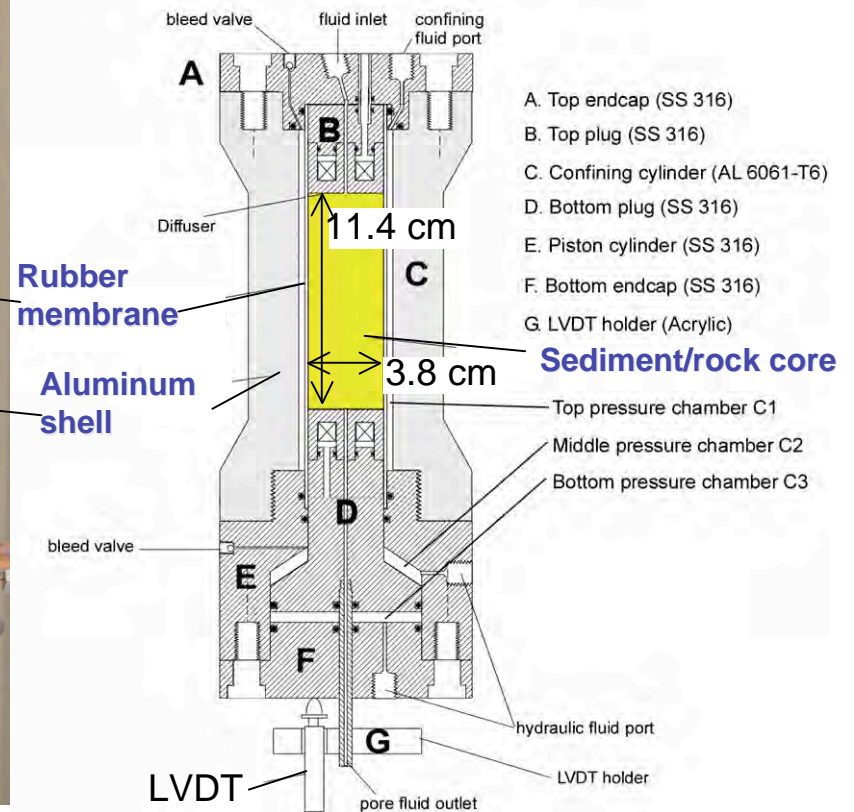
We conduct concurrent measurements of hydrate's mechanical and geophysical (seismic) properties, with real-time x-ray CT imaging



Experimental Setup

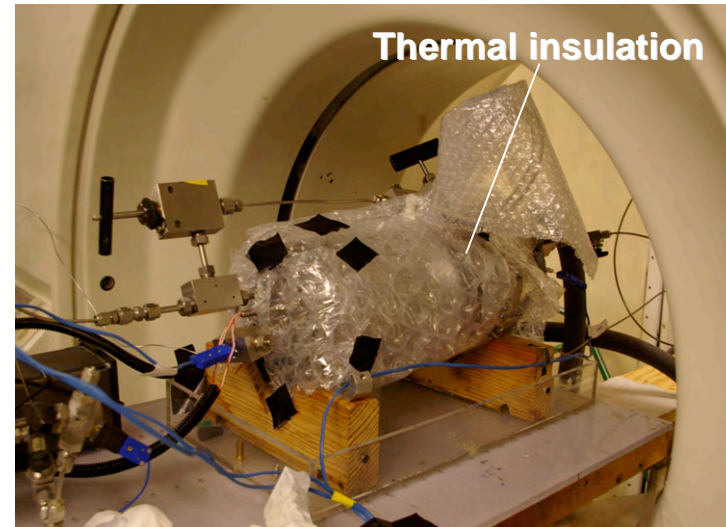
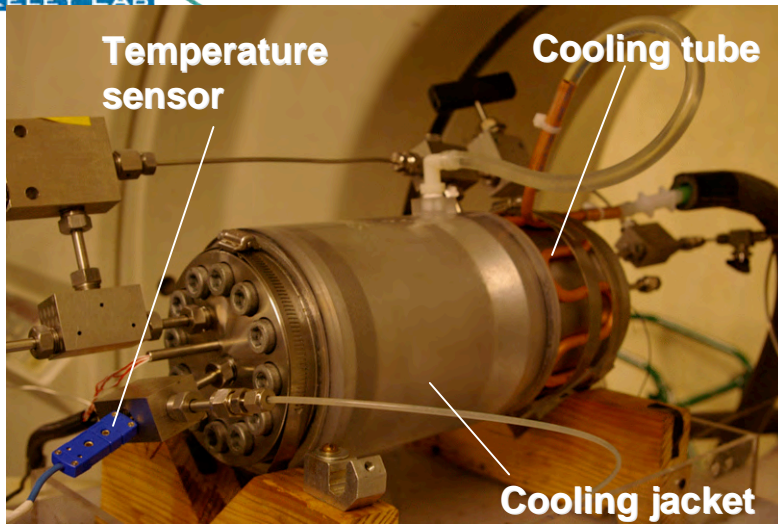


Xray-transparent triaxial testing cell





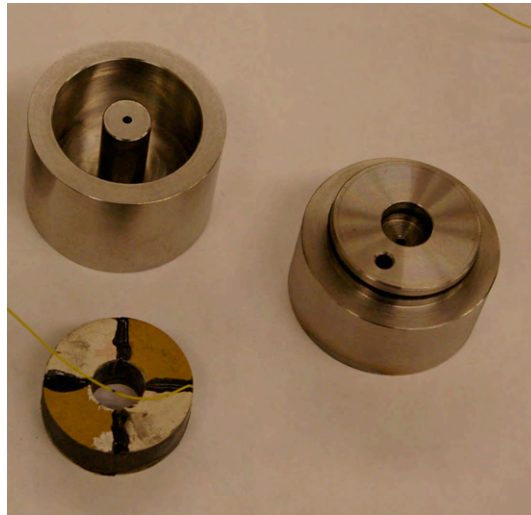
Experimental Setup





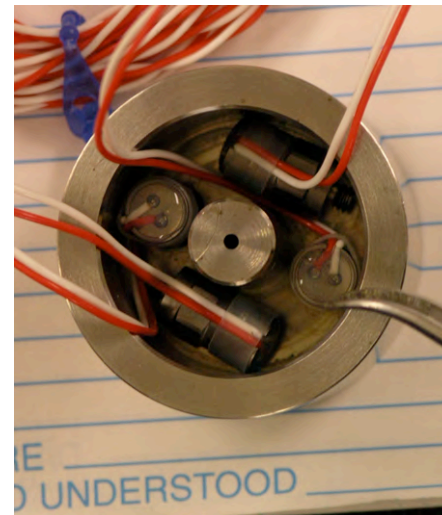
Experimental Setup

Seismic Source

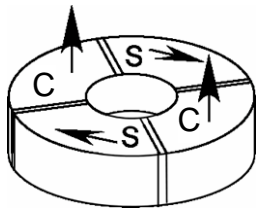


Hybrid compression/torsion piezoceramic (PZT) source

Seismic Sensor



Miniature piezoelectric accelerometers (PCB Piezoetronics)





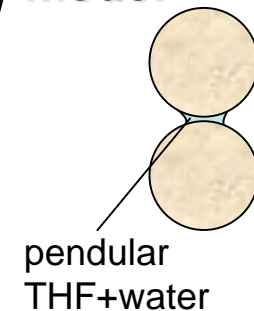
Samples

- Silica sand pack (US Silica, F-110, nominal grain size~100 μm)
- Tetrahydrofuran (THF)+H₂O mix \rightarrow THF hydrate forms under ambient pressure
- Three samples:

| | Sample#1 | Sample#2 | Sample#3 |
|--|--------------|---------------|--------------|
| Porosity | 36% | 34% | 38% |
| Sample Volume (from CT) | 120.01 cc | 122.15 cc | 134.98 cc |
| THF hydrate Saturation | 100% | 50% | 40% |
| THF (liquid) Saturation | 0% | 50% | ~0% |
| Cooling temp. (hydrate formation temp.) | +1°C (4.4°C) | -12°C (-10°C) | +1°C (4.4°C) |

Pore-filling model

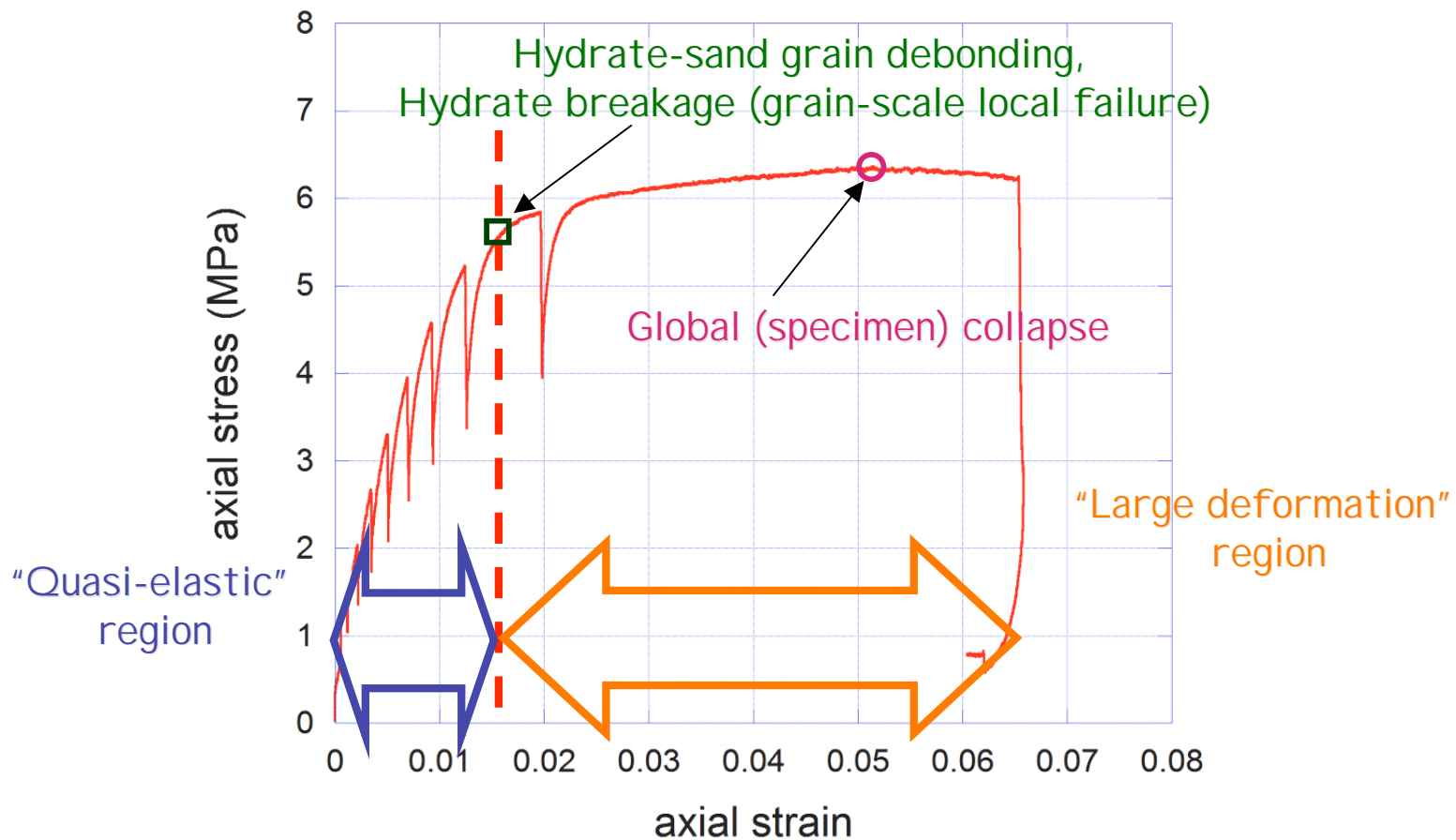
Cementation model





Triaxial Loading Test

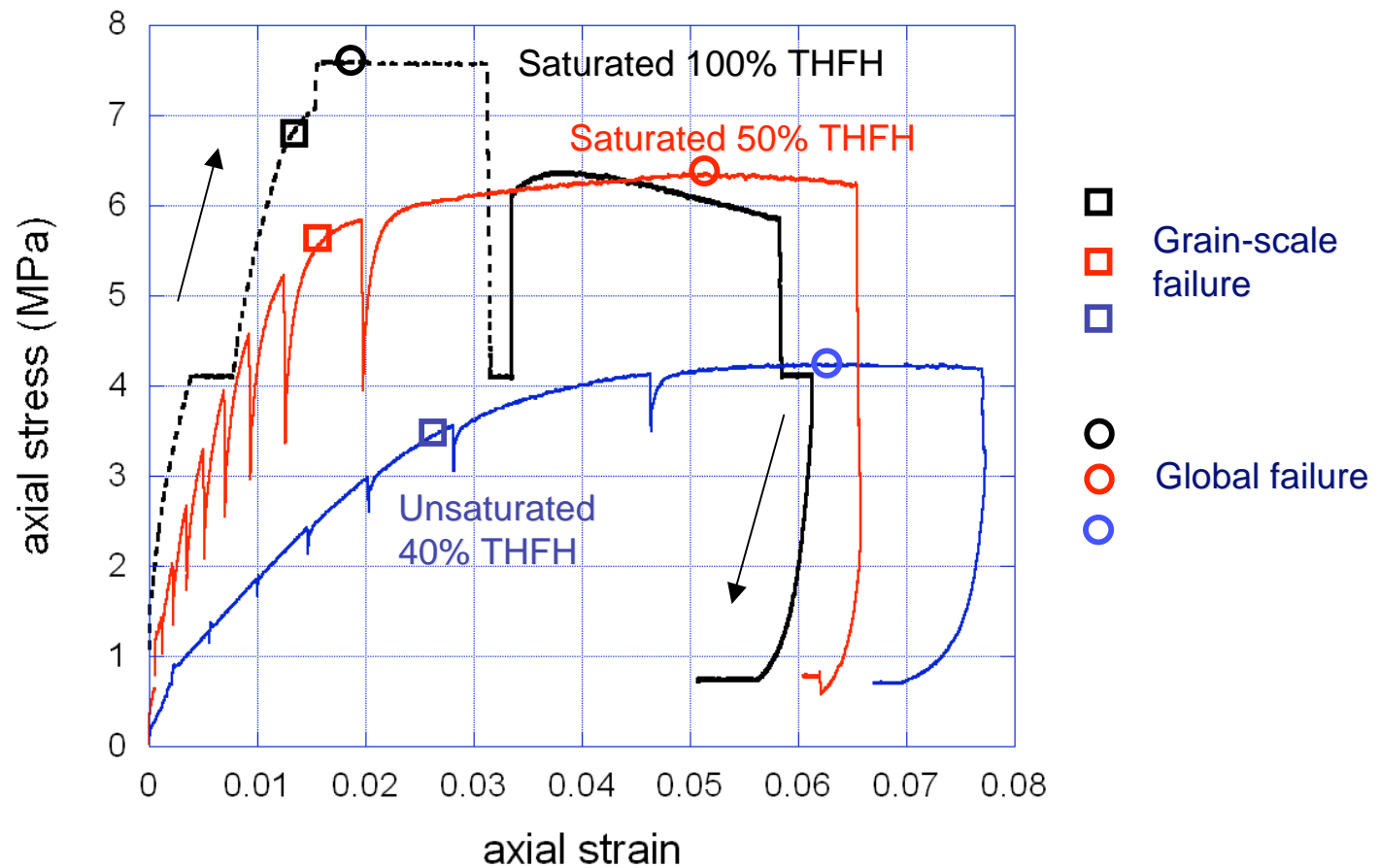
- Confining stress=0.69 MPa (100 psi)
- Loading rate=
 - Disp.controlled (solid lines): 0.077 %/min (1.28×10^{-5} /s)

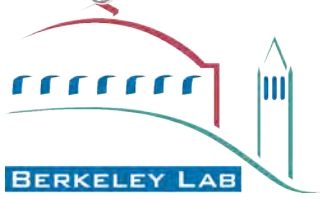




Triaxial Loading Test

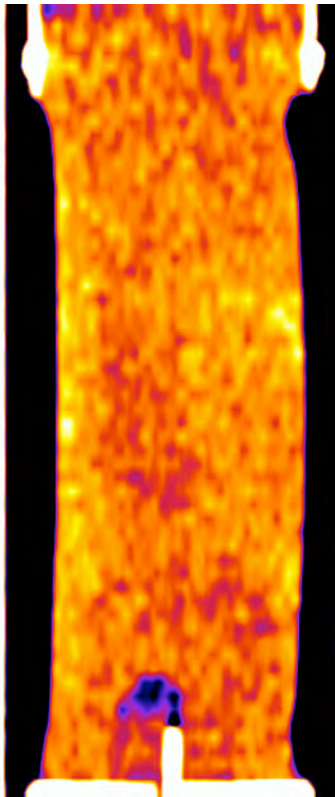
- Confining stress=0.69 MPa (100 psi)
- Loading rate=
 - Stress controlled (broken lines): 0.33 MPa/min
 - Disp.controlled (solid lines): 0.077 %/min (1.28×10^{-5} /s)



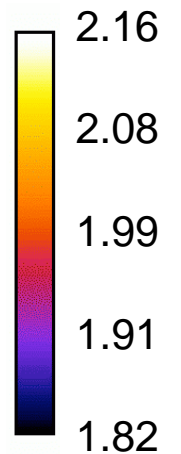


Fully THF hydrate-saturated sand

Before hydrate formation



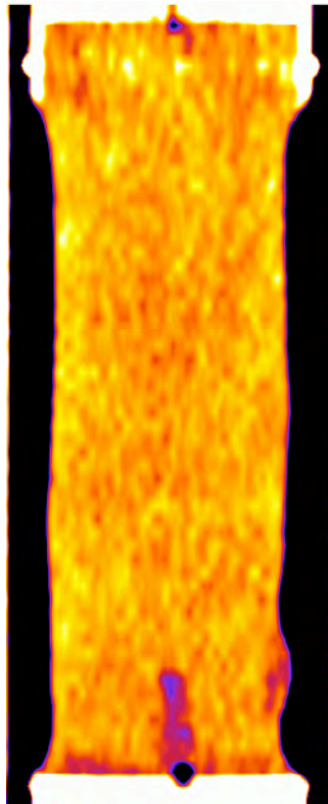
CT density
(g/cc)



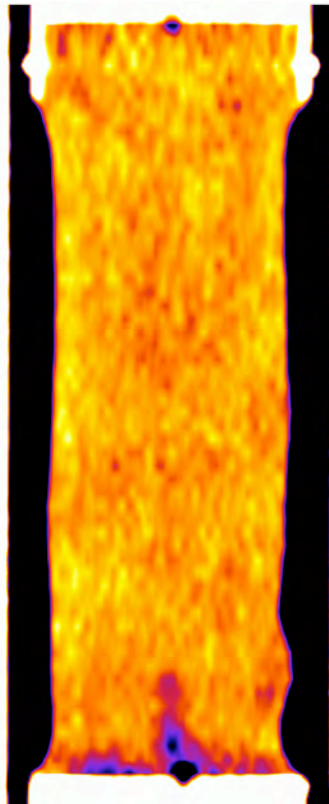


50% THF+50% THF-Hydrate

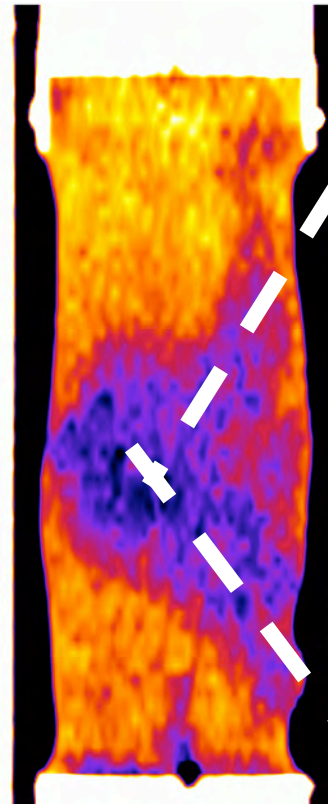
Before hydrate formation



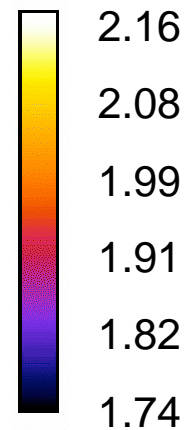
After hydrate formation



After failure



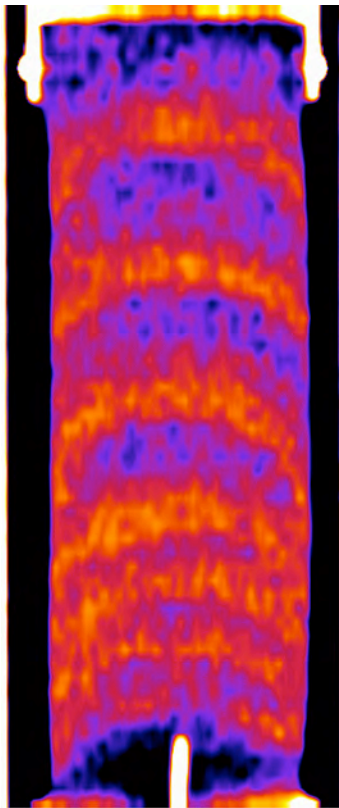
CT density
(g/cc)



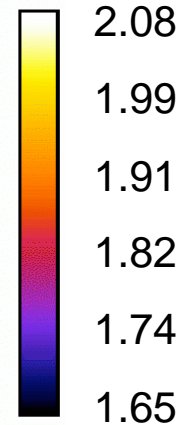


40% THF-Hydrate (partially saturated sand)

Before hydrate
formation



CT density
(g/cc)

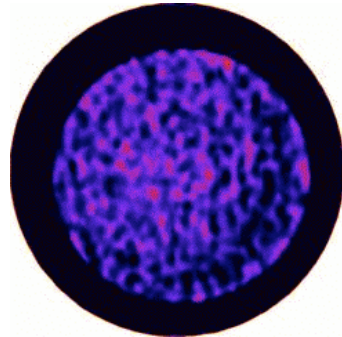


Shear localization?

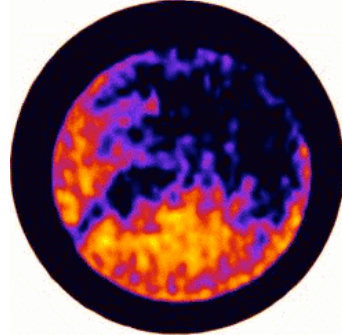


40% THF-Hydrate Saturated

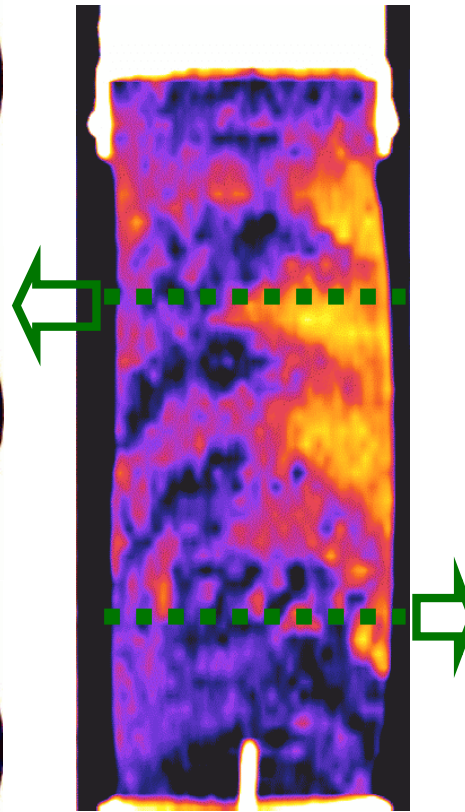
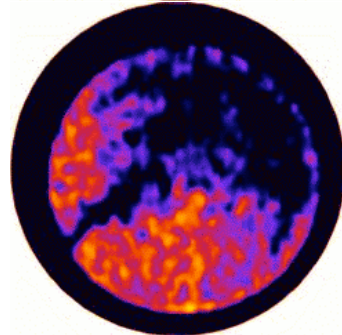
Before hydrate formation



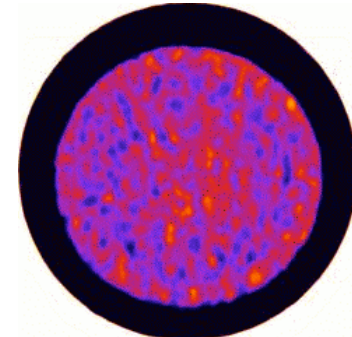
After hydrate formation



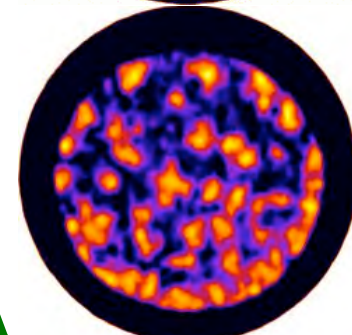
After failure



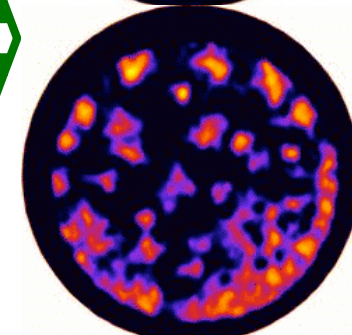
Before hydrate formation

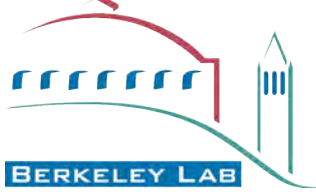


After hydrate formation



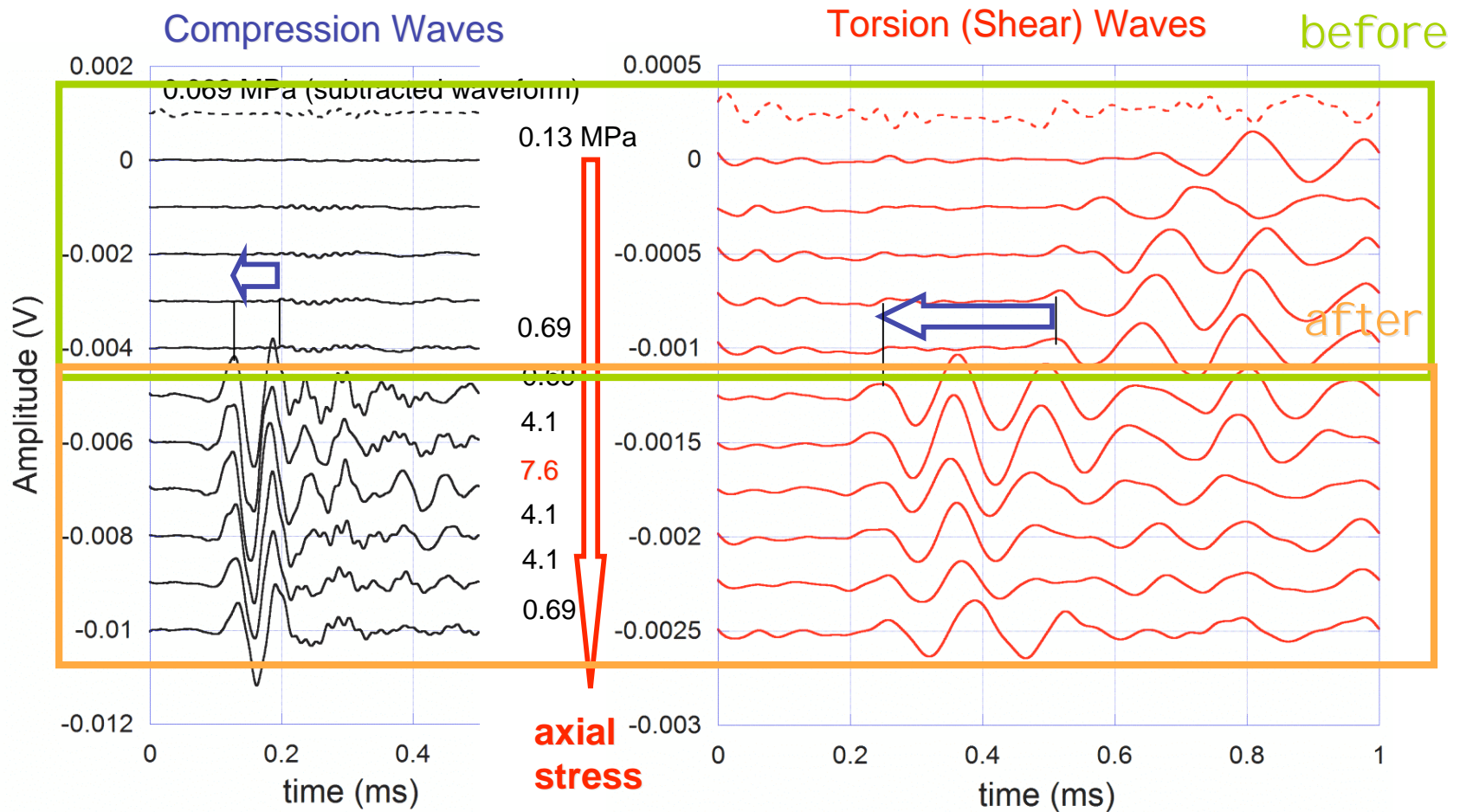
After failure





Seismic Measurement (Sample#1)

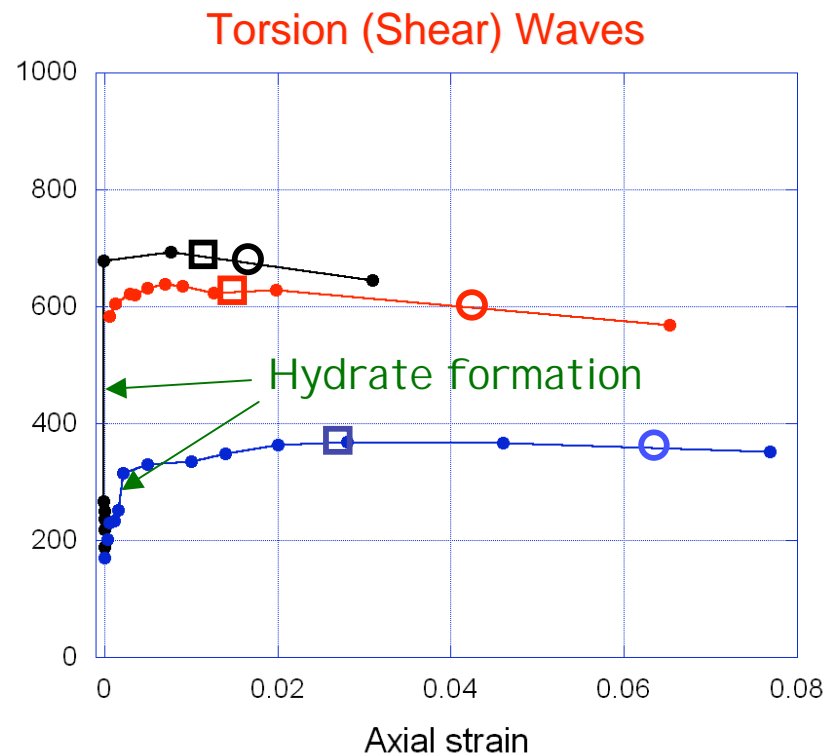
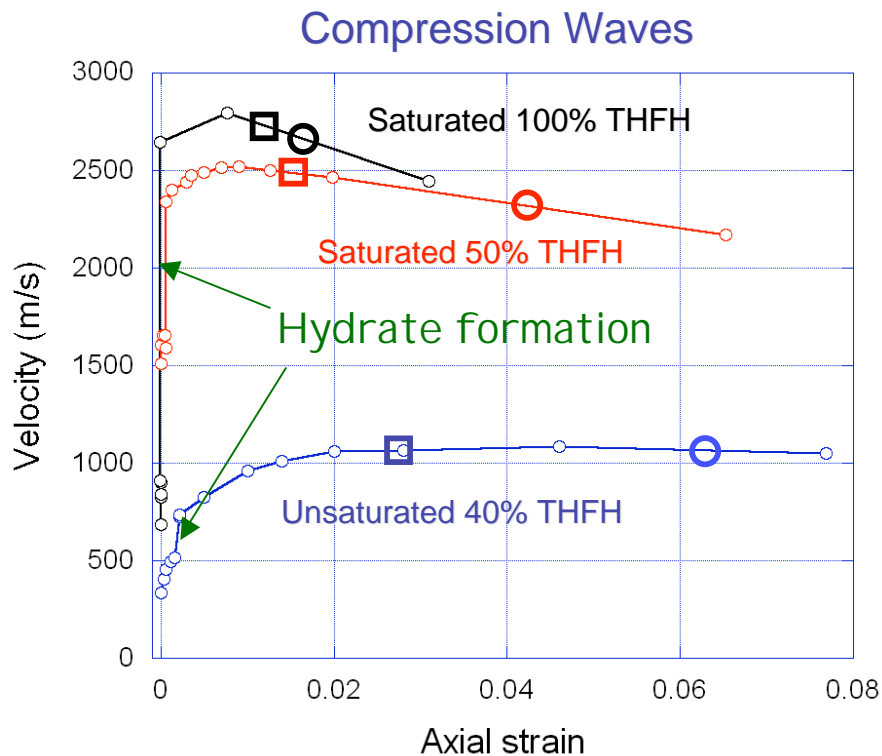
- Small wave amplitudes → Intense noise reduction is required

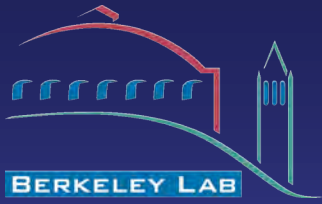




Velocities vs. Strain

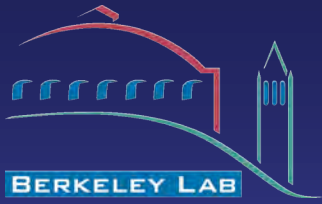
- Brittle sample (100%THFH) fails immediately after the peak velocities
- More ductile samples (50% and 40% THFH) appear to show velocity peaks before the sample failure strain





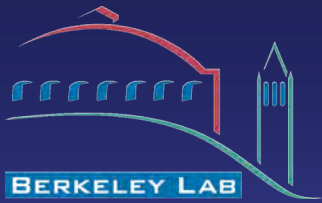
Geomechanical and Geophysical Properties Path Forward

- Complete vessel rebuild
- Perform triaxial and geophysical measurements on methane hydrate-bearing samples
- Compare results with existing measurements on THF hydrate-bearing samples from others
- If applicable, perform needed tests with THF hydrate to bridge to the existing THF hydrate data set



Other Tests

- NGHP and Mt. Elbert Core Scanning and Evaluation
- Natural Gas Production from Natural Samples
- Five Minute Sample Depressurization
- Hydrate Crystal Observation
- Properties of HBS
- ...

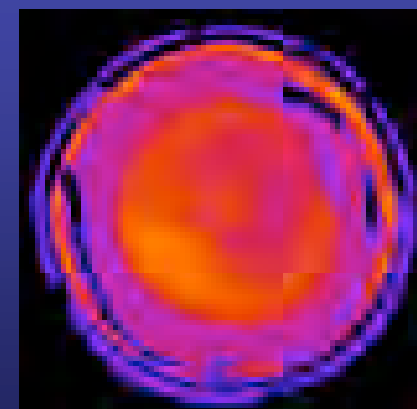
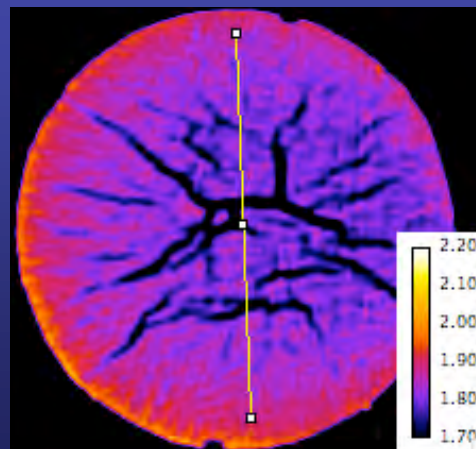
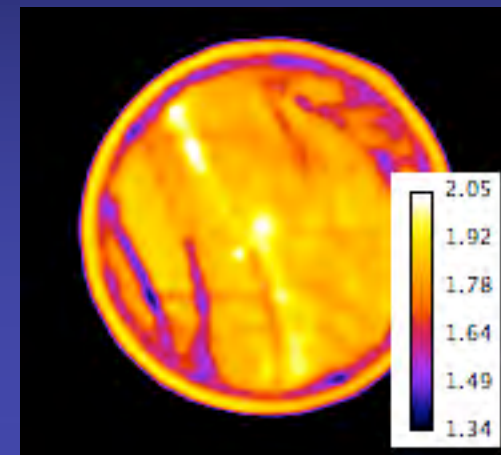
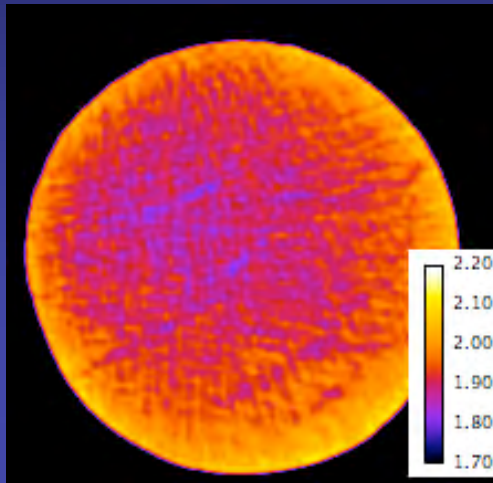


Core Scanning

Mt Elbert

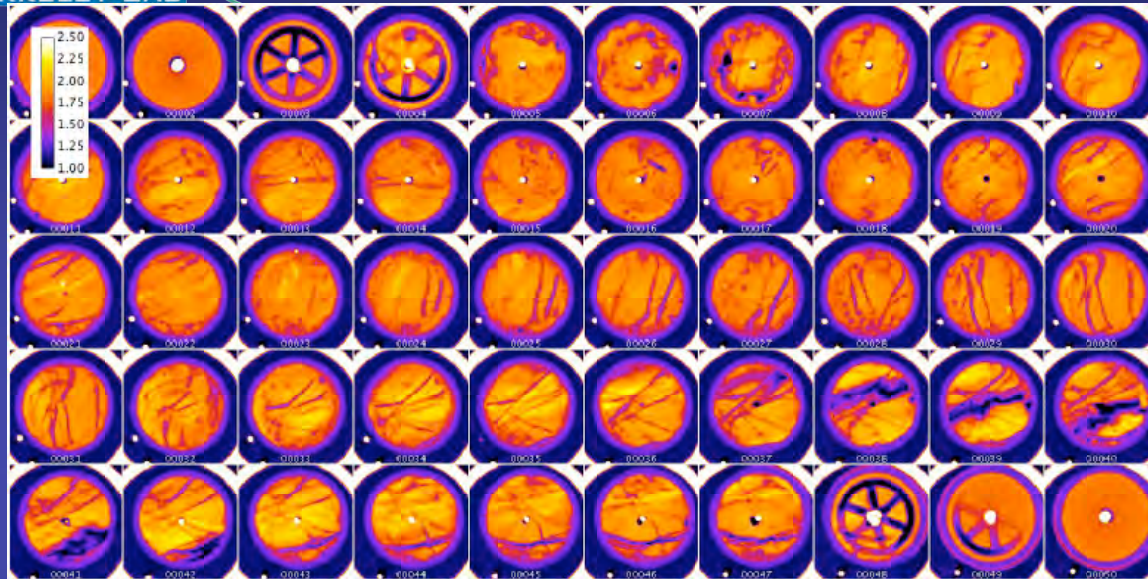
NGHP

- CT scanned many cores to aid in deciding tests to be performed.
- Performed initial analyses on CT data prior to sending samples to recipients

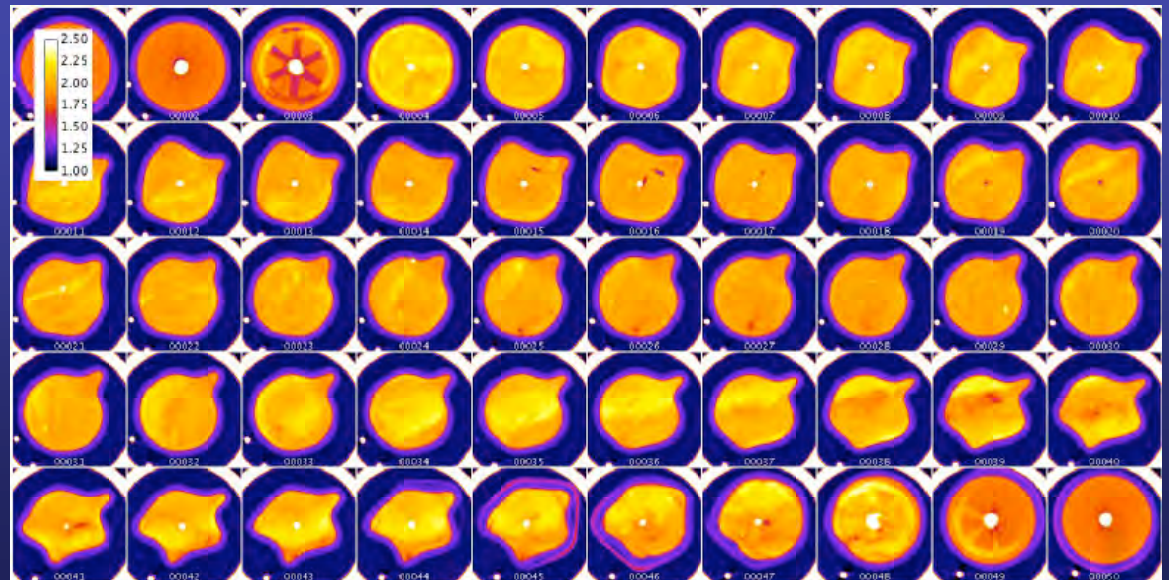


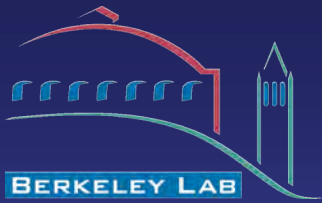


Gas Production Test

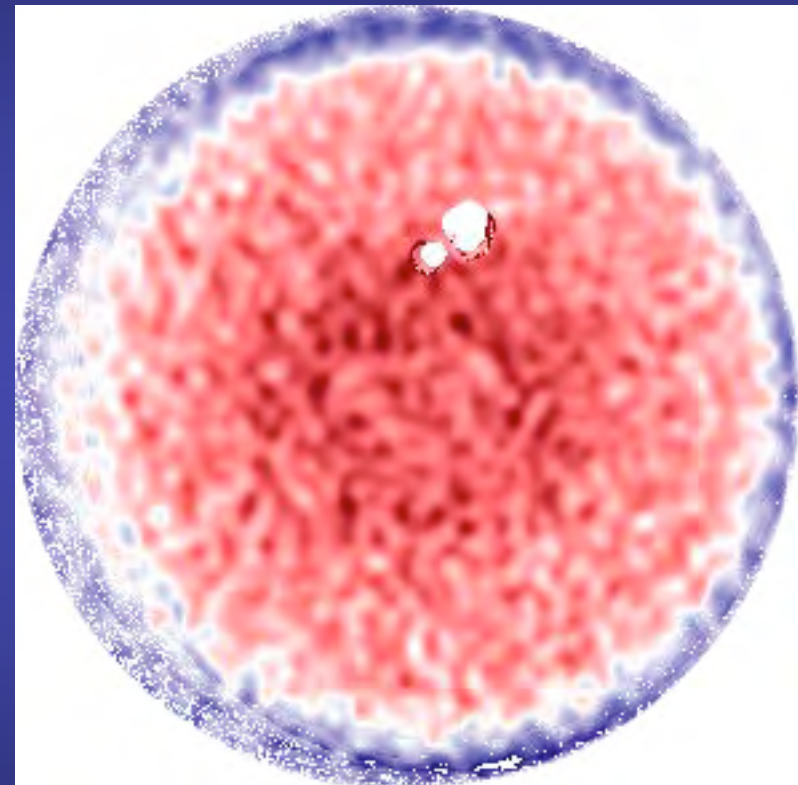
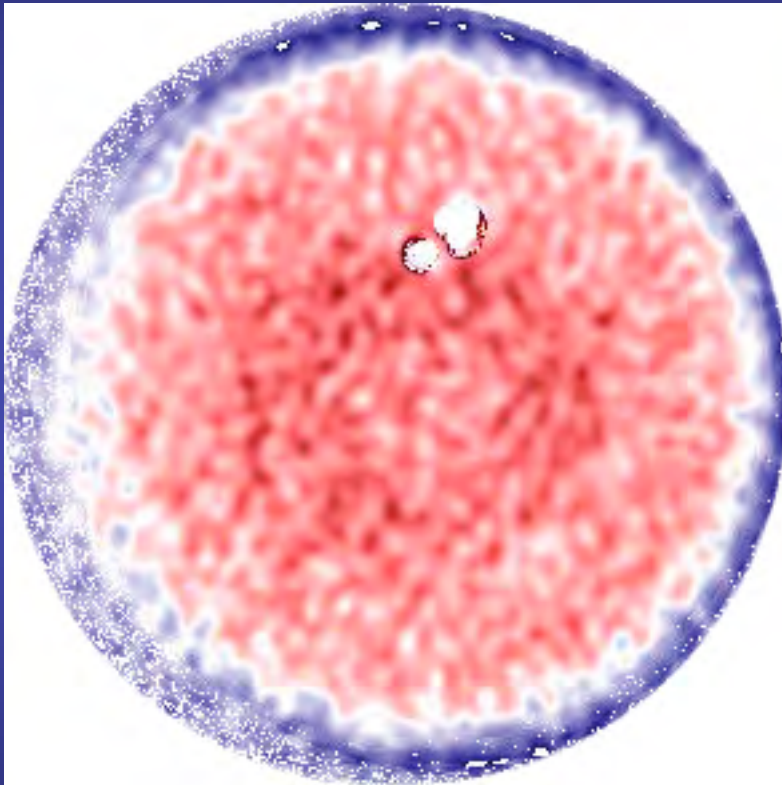


- Weak clayey material
- Produced mud
- No gas in spite of dissociation

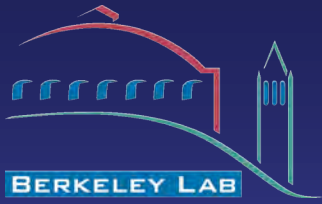




Effect of Sample Handling - Five Minute Depressurization



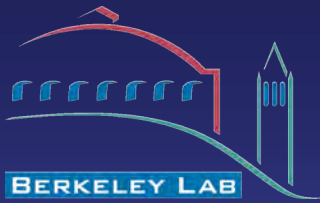
-0.10 -0.05 0 0.05 0.10
Density Change (g/cm³)



Other Tests

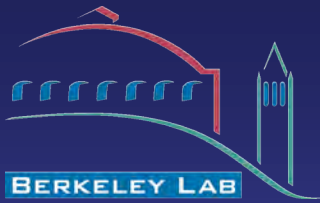
Paths Forward

- Continue to provide CT scanning of samples for others when requested
- Perform production test on Mt. Elbert sample by depressurization
- Look into hydrate crystal formation and morphology changes near equilibrium surrounded by 1) gas and 2) water.
- Measure p- and s-wave velocities and CT scan unsaturated and water saturated samples held near equilibrium over time.



Presentations

- Seol, Y., and T.J. Kneafsey, Fluid flow through heterogeneous methane hydrate bearing sand: Observations using x-ray CT scanning, Proceedings of the 6th International Conference on Gas Hydrates (ICGH 2008), Vancouver, British Columbia, Canada, July 6-10, 2008.
- Nakagawa, S., T.J. Kneafsey, and G.J. Moridis, Mechanical strength and seismic property measurements of hydrate-bearing sediments (HBS) during hydrate formation and loading tests, 2008 Offshore Technology Conference held in Houston, Texas, U.S.A., 5-8 May 2008, OTC 19559
- Kneafsey, T.J., Y. Seol, A. Gupta, and L. Tomutsa, Permeability of Laboratory-Formed Methane-Hydrate-Bearing Sand, 2008 Offshore Technology Conference held in Houston, Texas, U.S.A., 5-8 May 2008, OTC 19536-PP
- Kneafsey, T.J., and L. Tomutsa, X-Ray CT Scan of cores from NGHP Expedition 01, 2006, Presented at NGHP GAS HYDRATE CONFERENCE 2008 (Under the Aegis of Indian National Gas Hydrate Program) NEW DELHI, INDIA JANUARY 29TH TO 31ST 2008, Organized by Directorate General of Hydrocarbons, Ministry of Petroleum & Natural Gas, Government of India
- Kneafsey, T.J., and L. Tomutsa, CT Scanning, Analysis, and Production Test - Mt Elbert Core Samples, presented at BP-DOE Mount Elbert-01 Gas Hydrate Stratigraphic Test Data Analyses/ Interpretation & Production Test Design Workshop, March 2008
- Kneafsey, T.J., Y. Seol, A. Gupta, L. Tomutsa, G.J. Moridis; (2007), Relative Permeability of Gas Hydrate Bearing Sediments, Eos Trans. AGU, 88(23), Jt. Assem. Suppl., Abstract NS51B-02
- Seol, Y, T.J. Kneafsey, and G.J. Moridis (2007), Numerical simulation of hydrate formation morphology in cylindrical experimental sand columns, Eos Trans. AGU, 88(52), Fall Meet. Suppl., Abstract OS23A-1037
- Seol, Y., T.J. Kneafsey, L. Tomutsa, and G.J. Moridis. "Preliminary relative permeability estimates of methane hydrate-bearing sand". In TOUGH Symposium 2006; Berkeley, CA; 15-17 May 2006. 2006. LBNL-60368
- Kneafsey, T.J., L. Tomutsa, Y. Seol, G.J. Moridis. Relative Permeability Measurements of Hydrate-Bearing Sediments, Science and Technology Issues in Methane Hydrate R&D, Engineering Conferences International, Kauai, March 5-9, 2006
- W.F. Waite, **T.J. Kneafsey**, J.C. Santamarina, W.J. Winters, T-S Yun, D.H. Mason, C. Ruppel, Physical Property Changes in Hydrate-Bearing Sediment Samples due to Depressurization/ Repressurization, American Geophysical Union, San Francisco CA, Dec. 11-15, 2006



Publications

Kneafsey, T.J., Y. Seol, A. Gupta, and L. Tomutsa, Permeability of Laboratory-Formed Methane-Hydrate-Bearing Sand, Submitted to the Journal of Petroleum Technology, 2008

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