#### A New Process for Carbon Dioxide Conversion to Fuel (DE-FE0029866)



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2018 NETL CO<sub>2</sub> Capture Technology Project Review Meeting

**DE-FE0029866** 

August 17, 2018

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# **Project Objectives**

- The objective is to develop a new sorbent and the process around it for CO<sub>2</sub> utilization
- The sorbent converts CO<sub>2</sub> into CO in a redox process using H<sub>2</sub> generated by water electrolysis
  - CO and H<sub>2</sub> mixture (referred to as synthesis gas) is then used to synthesize a wide range of synthetic fuels and chemicals, via Fischer-Tropsch and oxo-synthesis processes
- Specific objectives
  - Sorbent synthesis and development
  - Bench-scale tests to assess technical feasibility
  - Long-term cycling
  - Reactor design (supported by modeling and CFD analysis)
  - Prototype fabrication to carry out proof-of-concept tests
  - Process design and development
    - Gasoline synthesis via methanol-to-gasoline process
    - Diesel fuel synthesis via Fischer-Tropsch



## **Project Partners**



#### **Project Duration**

- Start Date = June 15, 2017
- End Date = July 14, 2019

#### <u>Budget</u>

- Project Cost = \$1,000,000
- DOE Share = \$800,000
- TDA and its partners = \$200,000



### **Process Schematic**





# **Preliminary Cost Estimate**

- In a process (which utilizes over 99% of the CO<sub>2</sub> processed in the system) may deliver gasoline fuel at \$3.25/gallon
  - Based on energy costs only
  - Capital cost burden is not included
- A potential more near-term commercial application may use natural gas in place of H<sub>2</sub> to carry out the sorbent reduction
  - While there will be a net reduction in the overall CO<sub>2</sub> emissions, the final product will not contain only captured CO<sub>2</sub>

# Estimated energy consumption for CO<sub>2</sub> to gasoline conversion

Power	Purpose
331.64	MW <sub>e</sub> for Electrolysis
23.57	MW <sub>e</sub> for CO2 Reduction
-11.41	MW <sub>e</sub> from Methanol Synthesis
-12.85	MW <sub>e</sub> from Combustor
-6.20	MW <sub>e</sub> from MTG process
324.75	MW <sub>e</sub> net power needed (Total)
64.95	kWh per gallon gasoline
3.25	\$/ga gasoline

- energy cost assumed to be \$0.05 per kWh
- 80% eff. used for electrolysis
- 45% thermal to electric conversion eff. used for high temperature processes ~ 800°C
- 33% thermal to electric conversion eff. used for low temperature processes ~ 200-300°C



## **Process Schematic – NG Reduction**



Dry reforming can be achieved with very high level of conversion



# **TDA's Sorbent**

- Our process uses a unique mixed metal oxide phase to reduce CO<sub>2</sub>
- A low oxidation state metal oxide phase directly reacts with CO<sub>2</sub>, stripping off the oxygen to form CO and a higher oxidation state metal oxide forms
- In a subsequent step the sorbent material is contacted with H<sub>2</sub> to reduce it to complete the redox cycle





## **TDA's Sorbent**



- The sorbent will be prepared using a structure referred to as a "geode", based on a TDA proprietary synthesis technique
  - A large amount of active ingredients (to ensure a high oxygen uptake)
  - A high mechanical integrity during the large expansions and contractions associated with changes in molar volume of the active material in oxygen absorption and desorption
  - A high chemical stability
  - A high surface area maintained through repeated cycles



# **Moving Bed Contactors**

- Early designs were based on circulating beds due to the high temperature needed for CO<sub>2</sub> activation
  - To eliminate the need for high temperatures flow selection valves
- Advances in increasing material activity enables the use of fixed bed reactors



# **TGA Screening Results**



- New materials based on the use of different promoter phases were evaluated to improve:
  - Solid diffusion rates
  - Increase in the oxygen uptake and the rate of reduction
  - Decrease the onset temperatures for these process
- The new materials allowed operation at lower temperatures down with high oxygen uptake at 600°C



#### **Sorbent Evaluation**

- Sorbent samples that meet our physical properties and chemical activity requirements was then evaluated in a microreactor
- We compared the activity of these formulations under representative conditions
- Parametric tests to identify optimum operating conditions
  - Temperature
  - Pressure
  - Gas-solid contact time



2 in Schedule 40 Stainless Steel Reactor 2.07 in Internal Diameter 24 in Heated Bed Length 1324 cm<sup>3</sup> Sorbent Bed

Scieutie 40 Z	Ріре кеа	
Internal Diameter	2.07	in
Cross Sectional Area	3.37	in <sup>2</sup>
Heated Length	24.00	in
Red Volume	80.77	in <sup>3</sup>
Ded Volume	1323.56	cm <sup>3</sup>





# Reactor Results – CO<sub>2</sub>/H<sub>2</sub> Cycling



- Stable sorbent capacity was achieved at a range of temperatures
  - At high temperatures after an initial drop performance stabilized
- CO production rate increased an order of magnitude increasing the temperature from 500 to 700°C



## **Reactor Results – CO<sub>2</sub>/CH<sub>4</sub> Cycling**



High CH<sub>4</sub> conversion was achieved at 600-700°C



#### Working Capacity >2% wt. per cycle





# **CFD Analysis**

- GTI is supporting a CFD analysis to identify the best configuration for the gas-solid contactor
  - To provide information on the flow, concentration and temperature distributions in the reactors



### **Sorbent Life Testing**



**High-Temperature Mellen Furnace Incoloy 800H** Reactor

- The most promising sorbent will be tested for a minimum of 10,000 cycles (1-10 kg/day)
- **6" diameter 36" height vessels to house 12L (0.4 CF) sorbent** 
  - Incoloy HT is chosen for the material with a design temperature of 805°C and pressure of 295 psig



# **Process Design and Simulations**

- In collaboration with UCI, we are working to configure and optimize the entire CO<sub>2</sub> utilization plant starting at a subsystem level
- We established the basis for process design and develop the Aspen Plus<sup>™</sup> models that use TDA's CO<sub>2</sub> utilization system integrated with two chemical conversion processes
  - To diesel fuel via Fisher-Tropsch synthesis
  - To gasoline via MTG process
- Net process efficiency and the cost of fuel produced will be estimated
  - Material and Energy Balances
  - Cost Estimates
    - Capacity Factored Estimates
    - Equipment Modeled Estimates
    - Vendor Supplied Estimates
- Capital requirements, operating and maintenance costs will be developed in accordance with the DOE NETL's Cost and Performance Metrics Used to Assess Carbon Utilization and Storage Technologies document



## **Case 2: H<sub>2</sub>-Fischer Tropsch**



# **Preliminary Simulation Results**

		CASE	
	Case 1	Case 2	Case 2
	H2-MeOH	H2-FT	NG-FT
CO2 Entering Plant, tonne/h	56	56	32
Steam Turbine Power, kWe	10,395	11,793	10,625
Net Electricity Imported, kWe	427,905	375,798	133,505
Product(s), tonne/h	37.54	13.97	13.97
Cost of Product(s), \$/tonne	567	1,362	784
Cost of Product(s), \$/gal	1.71	3.81	2.19

- Methanol can be produced at \$1.71/gal using H<sub>2</sub> reductant
- FT Liquids are produced at \$3.81/gal or \$2.19/gal based on the reductant source (H<sub>2</sub> or CH<sub>4</sub>, respectively)



## Life Cycle Analysis (LCA)

- We will complete a detailed product life cycle analysis to validate that there is a net reduction in carbon footprint
  - To quantify any additional CO<sub>2</sub> or greenhouse gas (GHG) emissions while utilizing the CO<sub>2</sub> generated by the power plants
- The proposed technology's carbon foot print on a percent reduction basis will be compared to that of the state-of-the-art conversion technologies



## **Acknowledgements**

- DOE/NETL funding provided the DE-FE0029866 project is greatly acknowledged
- Project Manager, Steve Mascaro

