

# Computational Tools for Additive Manufacture of Tailored Microstructure & Properties

*Annual Project Meeting Presentation: Simulation Based Engineering*

## Raytheon Technologies Research Center

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# Background & Introduction

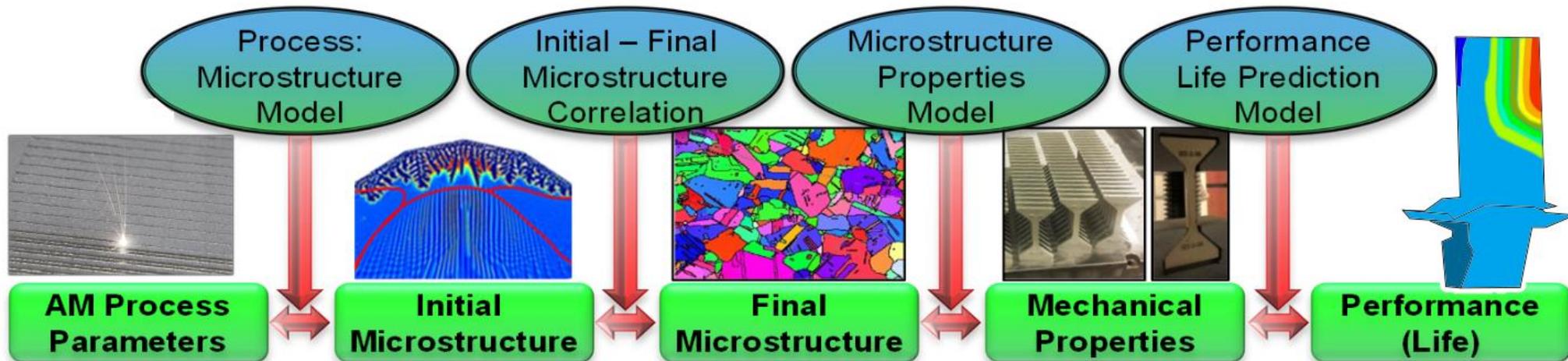
**Purpose:** Establish computational tools to link AM parameters to material properties to enable parts with spatially varying microstructure for enhanced performance

Project seeks to demonstrate the application of computational methods & tools on microstructure evolution and prediction of mechanical behavior for nickel based superalloy parts.

**Current State:** use “standard parameters” to print parts with a homogenous microstructure; limited control over grain size, morphology, etc.

**Desired State:** a predictive thread of AM input parameters through to tailored property placement

**Challenge:** AM parts go through multiple steps, each with strong impact on finished part



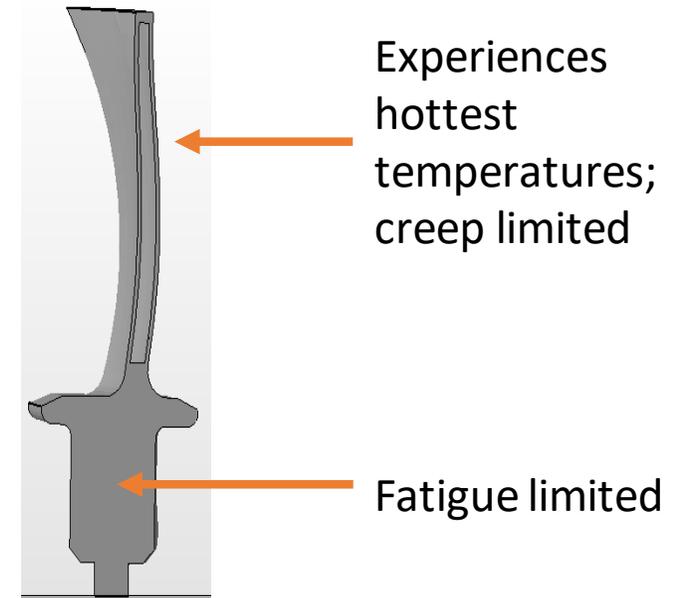
# Core Questions

Successful implementation of thread that links AM process parameters through to part performance requires answers to the following:

- What AM process parameters can be readily be controlled & modeled to manipulate deposit microstructure?
- Do differences in as-deposited microstructure get erased with post processing thermal treatments (e.g. stress relief)?

## Motivating / Target Case Study for the Program

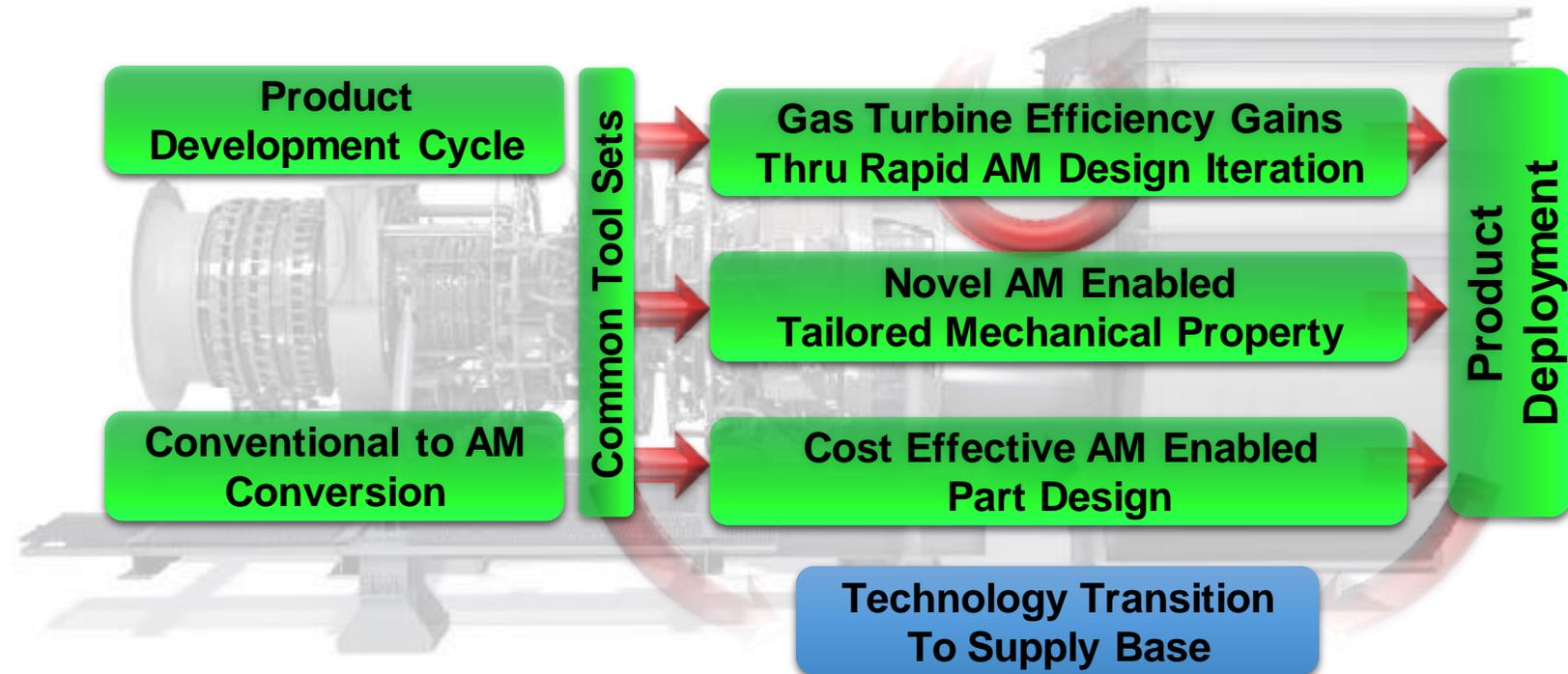
- AM of a turbine blade with coarse grains in the air foil and fine grains at the root
- Platform: Laser Powder Bed Fusion
- Material: IN718, Ni-superalloy



# Fossil Energy Impact

## Revolutionize hardware via additive manufacturing (AM)

- Process efficiency gains through new component design can be gained by rapid concept iteration as casting development cycle times are erased.
- Enhanced part lifetime/performance through AM enabled spatially varying microstructures.
- Upend part replacement supply chains with new processing developments impacting a large existing base including F-Class turbines.
- AM applicable to all Industrial Gas Turbines as well as derivative power generation systems such as aerospace turbines.



# Project Outline & Status

## Key Tasks & Progress

A. Models to link AM Process Parameters to As-Deposited Microstructure



B. Initial to Final Microstructure Evolution Correlation (Post Processing Effects)



C. Microstructure-Properties-Performance Model

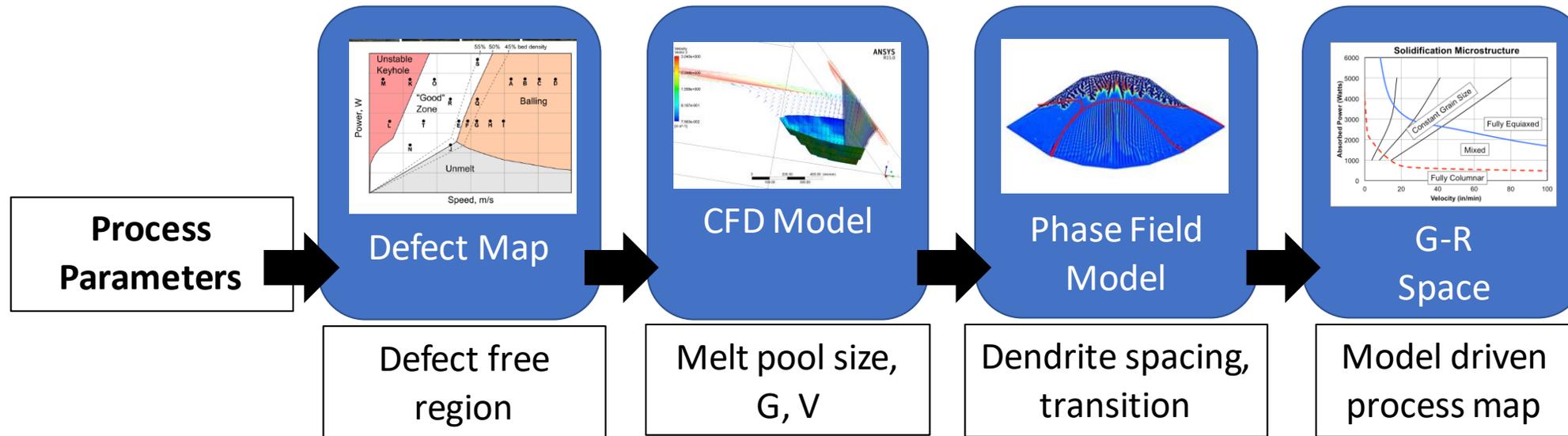
*In Progress*

D. Demonstration of Spatially Varied Microstructure Via AM



# Update: Link AM Parameters to Microstructure

## Microstructure influenced by thermal history of the melt pool



Approaches to control melt pool solidification

1. Increase layer thickness → requires sufficient laser power
2. Laser scan path → need control over scan strategy

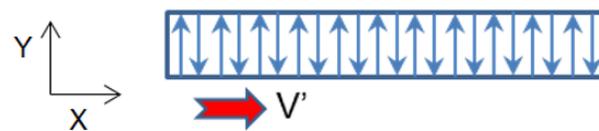
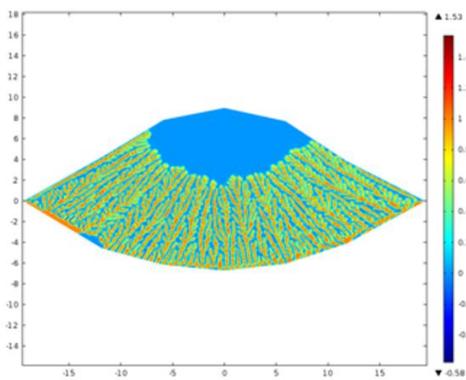
RTRC's COTS powder bed systems are too limited in laser power to take advantage of Approach 1 so focus was placed on manipulating laser scan vectors.

# Update: Link AM Parameters to Microstructure

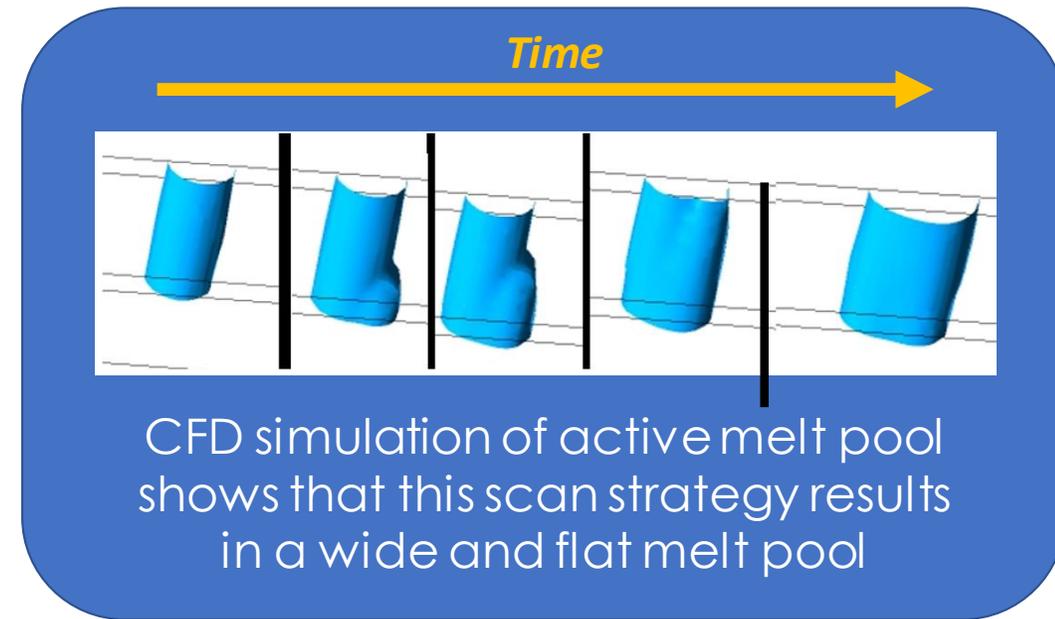
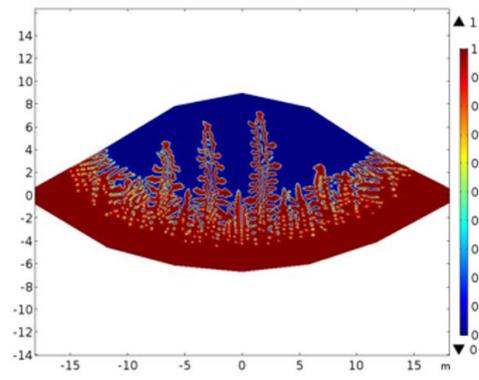
Use an “Active Melt Pool” scan whereby the melt pool is active for longer time thus lowering cooling rate & making a flatter pool to promote a 2D microstructure for larger columnar grains



Standard or default scan strategy



Active melt pool scan strategy



CFD simulation of active melt pool shows that this scan strategy results in a wide and flat melt pool

Phase field simulations indicate active melt pool results in larger dendrites

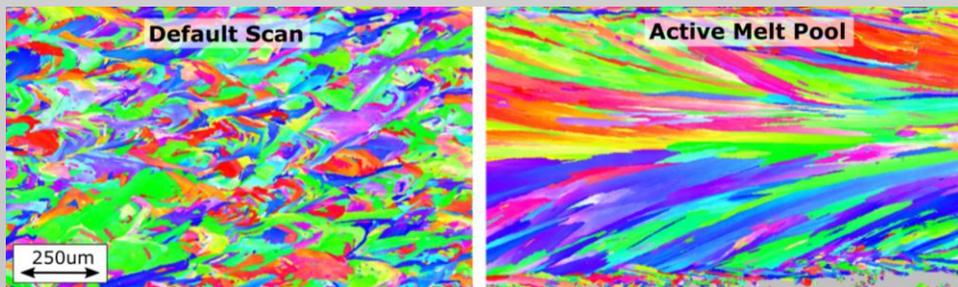
# Update: Link AM Parameters to Microstructure

Active melt pool technique experimentally validated to result in larger, more columnar like, grains

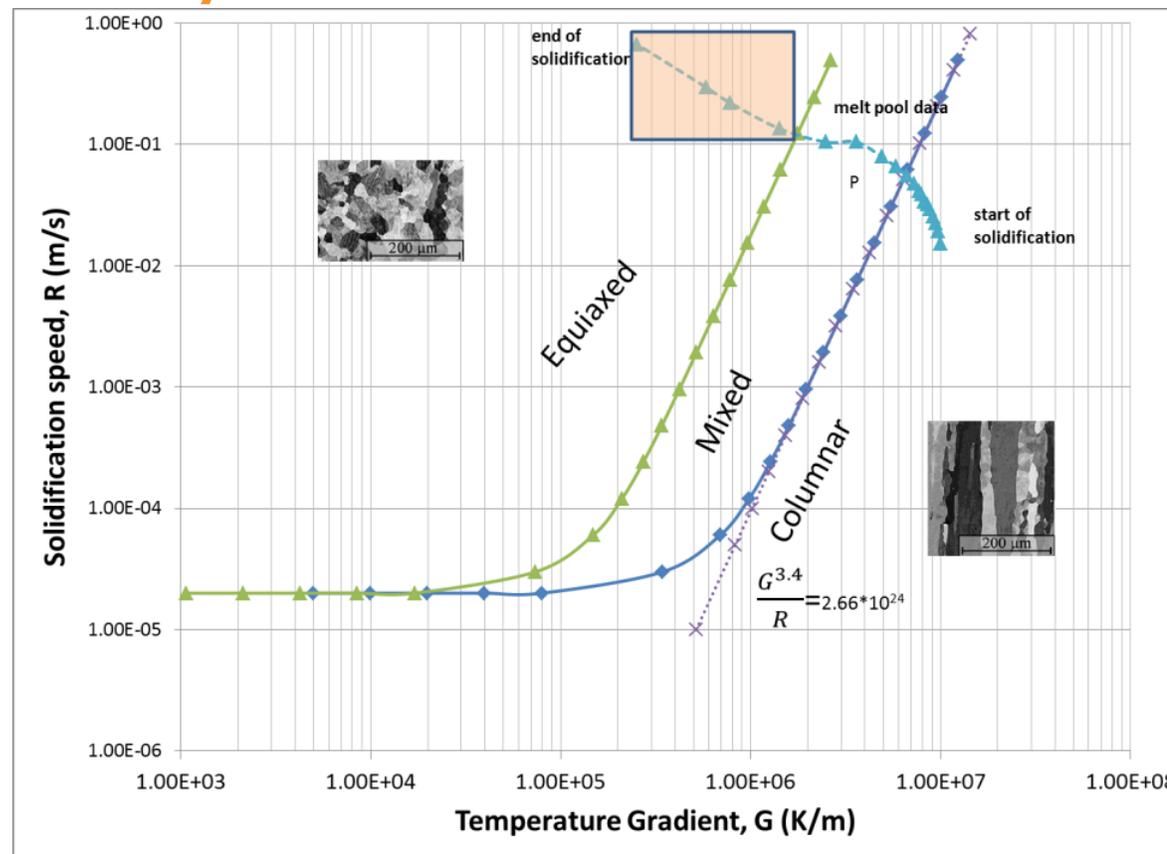
CFD simulation provides thermal gradient  $G$ , & solidification speed ( $R$ ) that can be plotted on a microstructure solidification map.



## Validation



EBSD scans of IN718 additive coupons made with default and active melt pool scan strategy

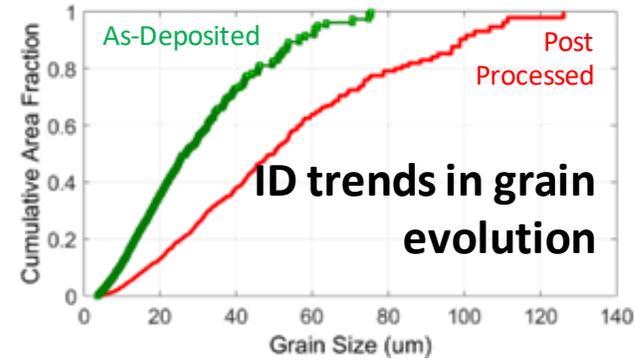


Active melt pool solidification primarily in the columnar zone. The top of the melt pool (orange zone) may be equiaxed but this is erased when the next layer during AM is processed.

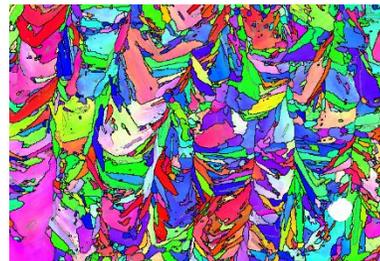
# Update: Microstructure Evolution Trends

## Insights for Microstructural Evolution

While custom heat treatments could be employed to influence grain structure evolution, this work follows industry standard post-processing thermal treatments.



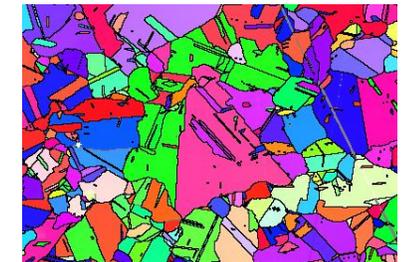
Track trends in the evolution of **grain size**, **shape**, and **orientation distribution** that are key inputs to the microstructure sensitive performance model.



Quantify grain size with EBSD



- Stress Relief (ASTM F3055)
- HIP (ASTM F3055)
- Solution + Age (AMS 5663M)

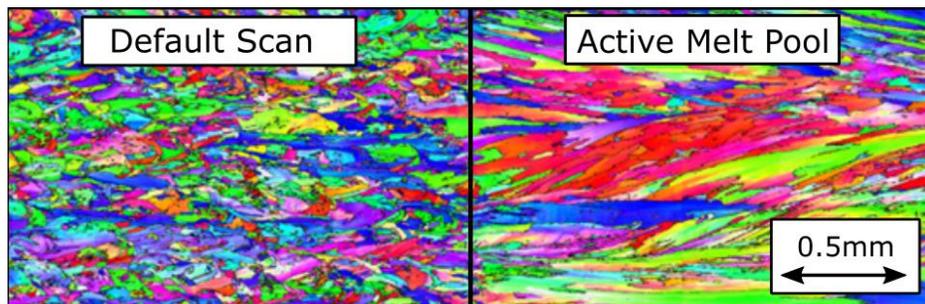


Quantify final grain size with EBSD

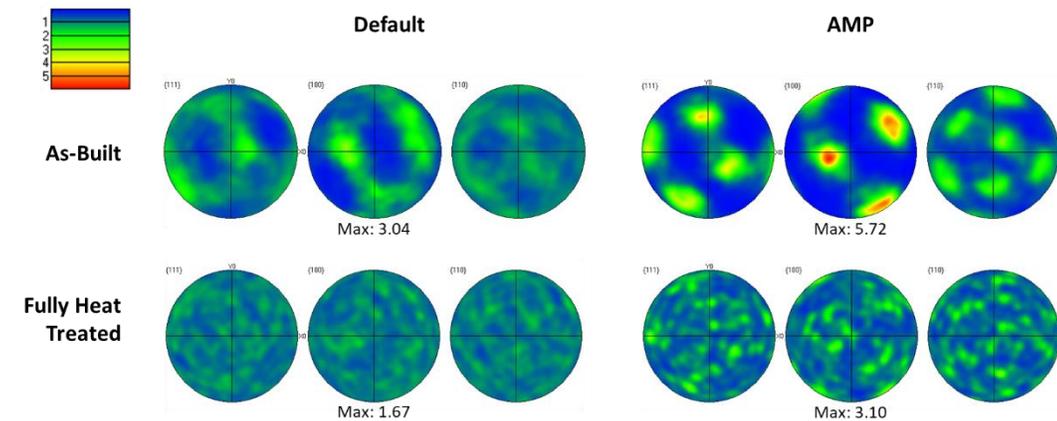
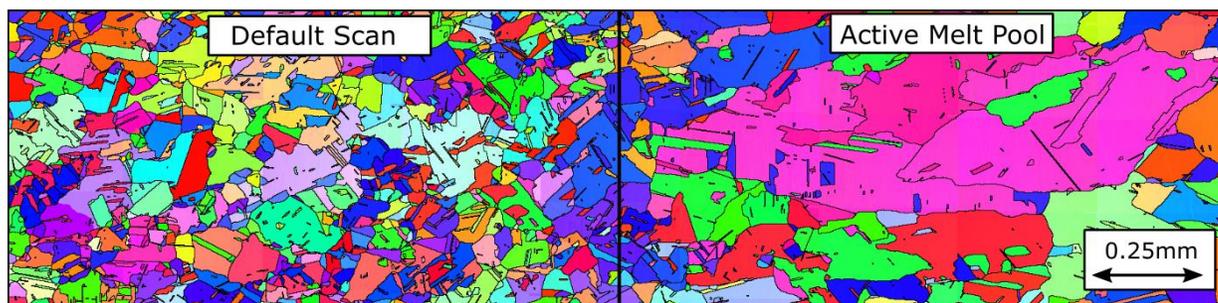
# Update: Microstructure Evolution Trends

Larger grains from active melt pool approach retained through post processing.

As-Deposit



Post Processed



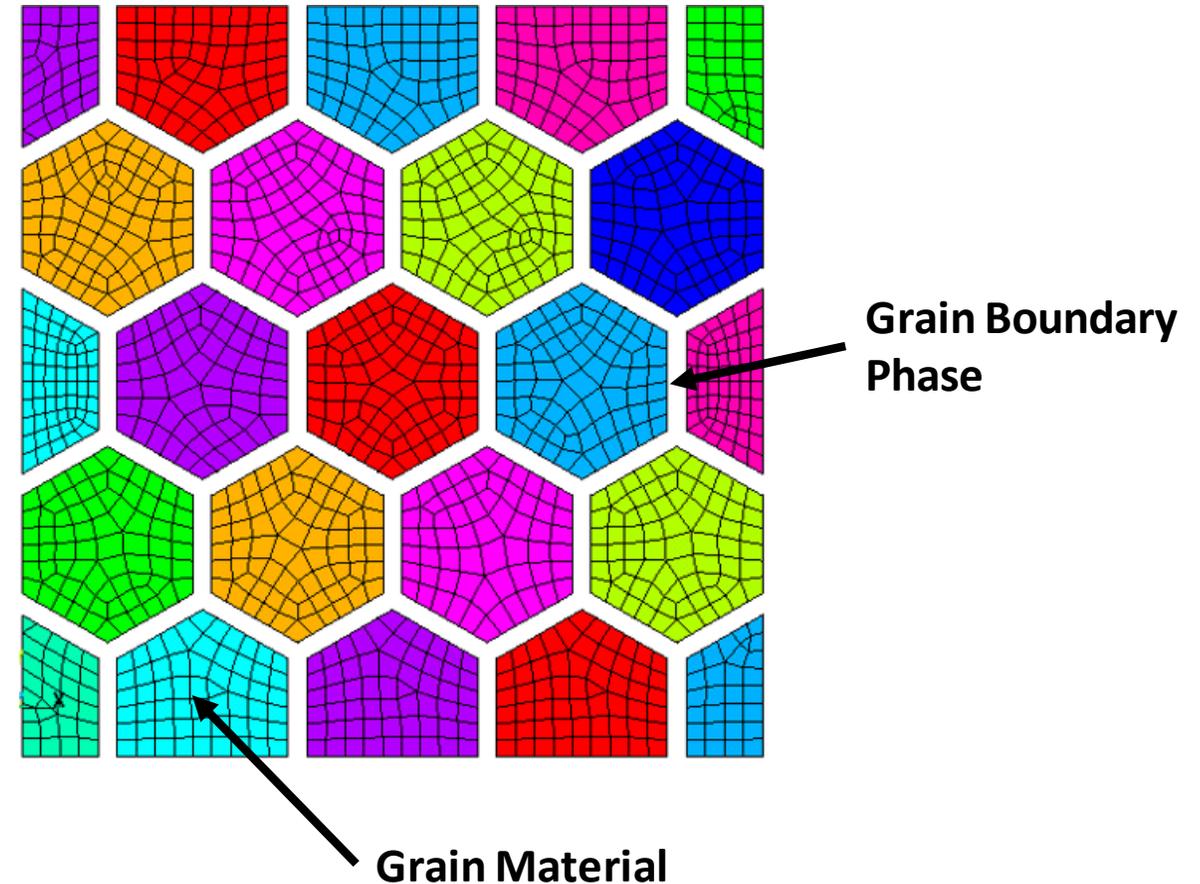
Overall, texture is random for both default & active melt pool (AMP) deposits in post processed state

Scan Strategy	Grain Size ( $\mu\text{m}$ )		Trends
	As-deposit	Post Processed	
Default	27	70	~2.5X increase in grain size, more equi-axed
Active Melt Pool	44	365	~8X increase in grain size, elongated grains

# Update: Microstructure Performance Models

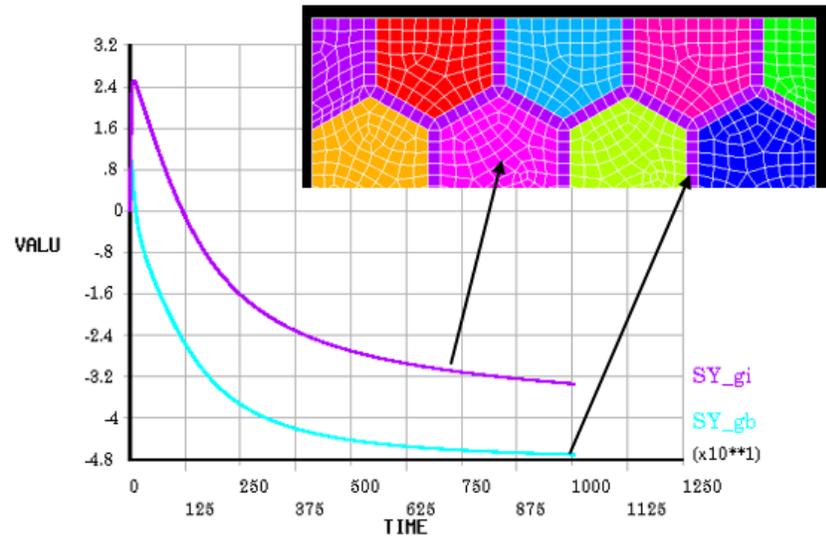
## Grain-scale simulations to predict global creep behavior governed by bulk grain & grain boundary mechanisms

- Additive IN718 modeled as a connected 2 phase system
  1. Grain Material modeled with crystal plasticity
  2. Grain Boundary Phase modeled by Norton's Law
- Microstructure sensitivity → smaller grains means more grain boundary phase influence in the material response.

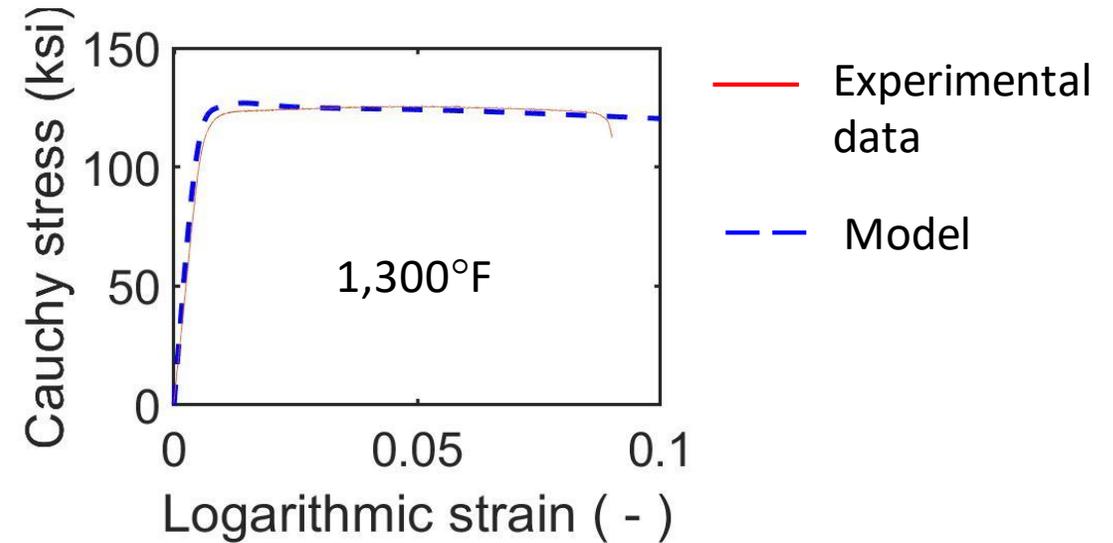


# Work In Progress

- Model is de-bugged and operational with surrogate material calibration factors



- Model calibrated for time independent quasi-static tensile/compressive behavior



- Collection of time-dependent creep data for additively manufactured coarse grain and fine grain deposits are in progress & required for model calibration to predict creep performance.

# Update: Spatially Varied Microstructure Demo

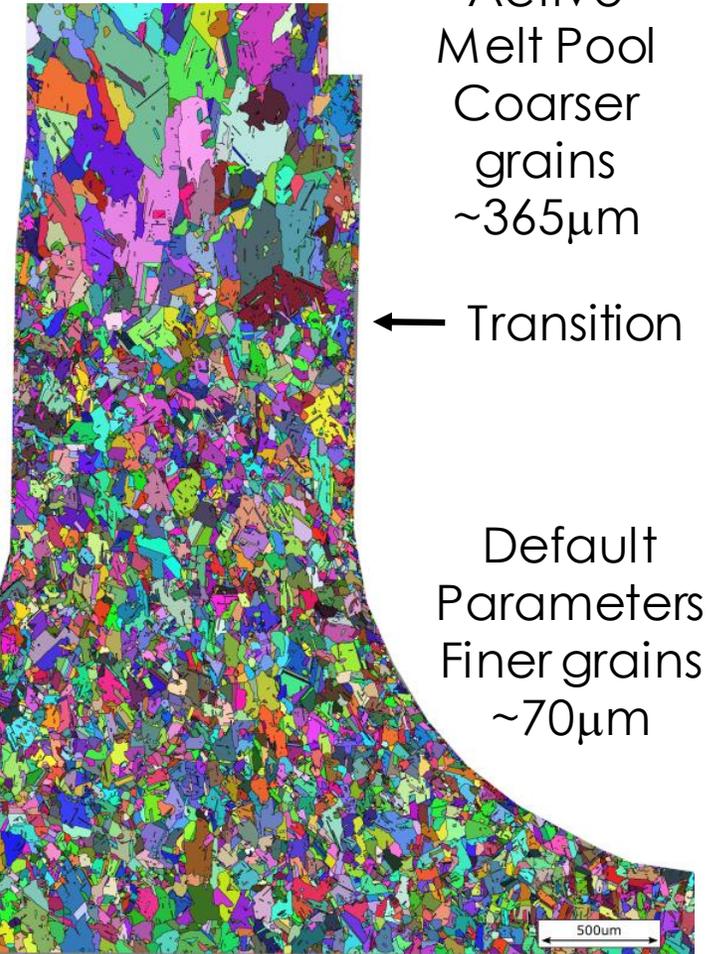
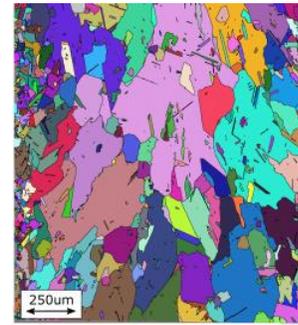
Successfully printed a turbine blade surrogate with coarse grains in the air foil (creep resistance) and fine grains at the root (fatigue resistance)

## Strategy

- Print blade using powder bed system with “default” parameters in the root & active melt pool scan strategy for the airfoil.

## Key Accomplishments

- Retention of spatially tailored microstructure after full post processing (Stress relief → HIP → Solution → Age thermal treatments).
- No egregious defects such as cracks, pores, etc.



Active Melt Pool  
Coarser grains  
~365µm

← Transition

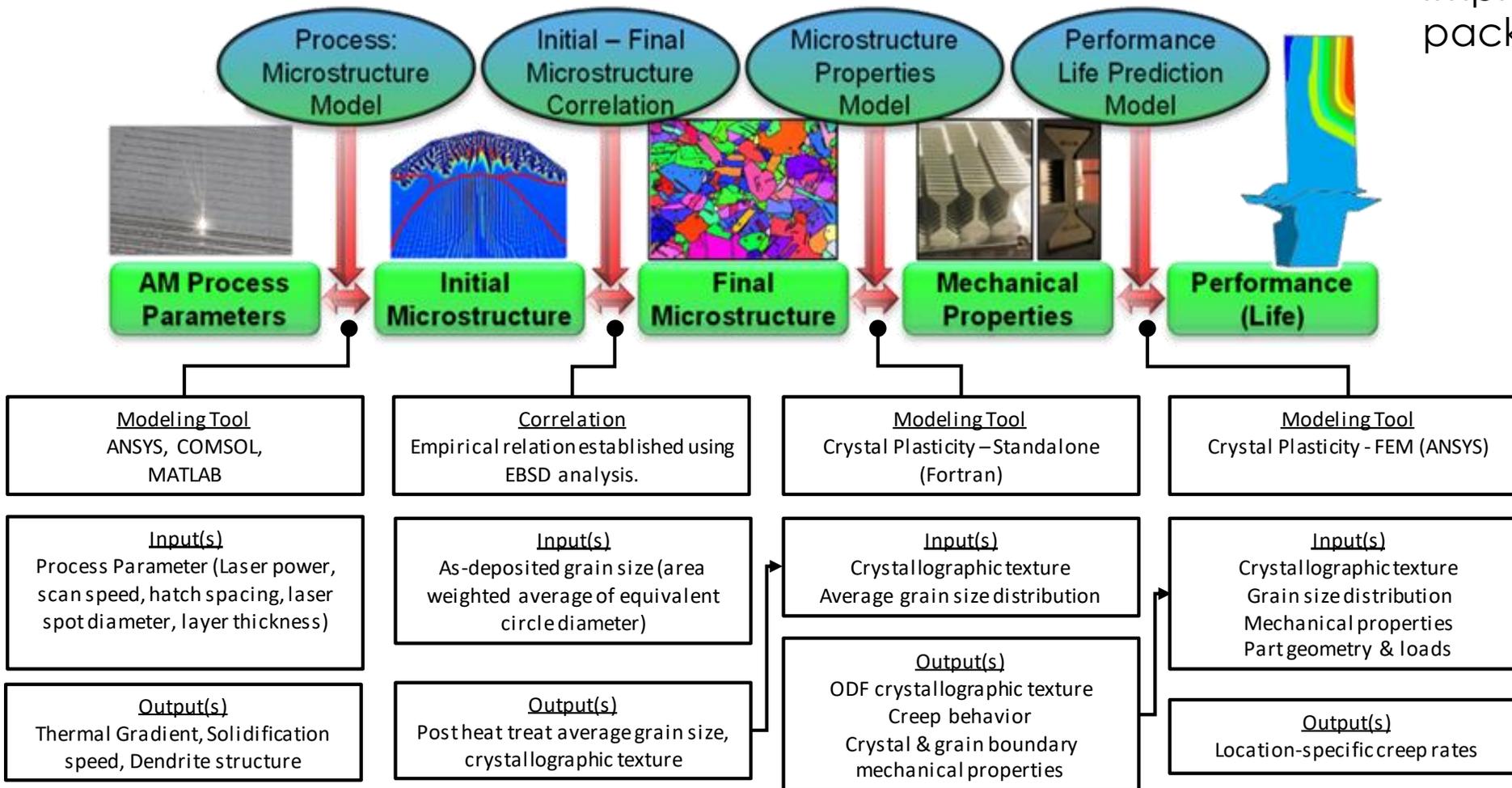
Default Parameters  
Finer grains  
~70µm

*EBSD scan with random color assigned to individual grains*

# Preparing for Next Steps

## Assembling the Full Framework Connecting Process-Structure-Properties-Performance

- Implementation with software packages common to industry



### Directions Beyond the Program

Coordinate with AM platform providers to offer systems with features to enable more microstructural control

Methods to connect across the different models in the tool chain

# Concluding Remarks

## Summary

- Employed modeling to understand the impact of AM process parameters on the as-deposited microstructure → results in the ability to influence material properties & performance in 3D printed parts by intentionally adjusting scan vectors, laser power, speed, etc.
- Confirmation that spatially varied microstructure can be retained with post processing.
- Employed lessons learned to demonstrate AM of a turbine blade with spatially varying microstructure having coarse grains in the air foil for creep resistance and finer grains at the root for fatigue resistance.

## Next Steps

- Finalize the microstructure sensitive property model for prediction of creep performance. Awaiting the collection of long duration (500+ hr) creep data for coarse and fine grain AM Ni-superalloy to use for model calibration.
- Complete program with documentation of all technical progress.

# Acknowledgements



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