

Treating Effluent Streams at Coal Power Plants Using Membranes

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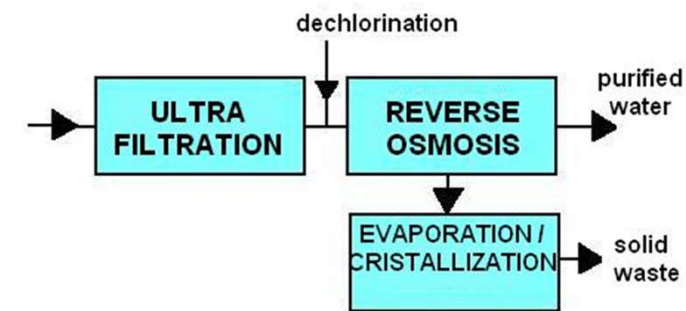
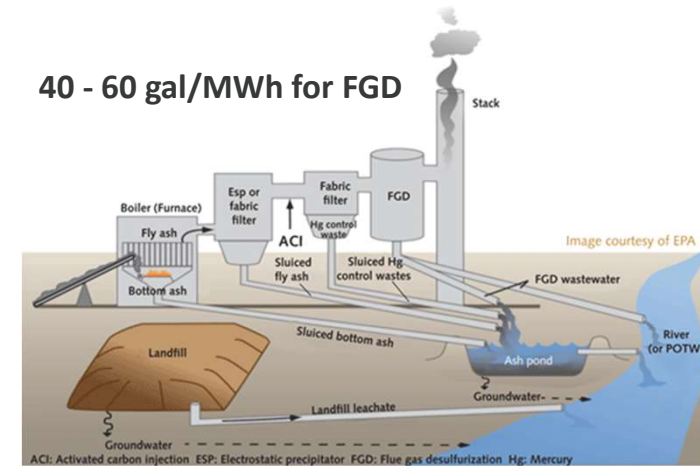


2015 EPA Regulation on Effluent Limitations



ELGs at Coal Power Plants

- September 30, 2015, finalized a rule revising the regulations for the [Steam Electric Power Generating](#) Effluent Guidelines
- Streams effected include:
 - Fly & Bottom Ash Transport Waters
 - Flue Gas Desulfurization (FGD) effluent
 - Ash Pond effluent
 - Flue Gas Mercury Control Water
- 6 regulated heavy metals (Pb, As, Hg, Se, Cr, Cd)
- Compliance Costs are expected by the EPA to be on the order of \$500M/yr across the entire U.S. fleet
- September 18, 2017 EPA announced a Postponement of Certain Compliance Dates (does not affect compliance dates for Mercury Control Water and Fly Ash Transport Water)
- Two Options for Compliance
 - Zero Liquid Discharge (ZLD) Chemical & Biological Treatment



Standard Option for ZLD

Start of the Art Technologies used in ZLD

Reverse Osmosis (RO)

- **Pros**

- High Efficiency (30%-50%)
- Low upfront capital investment

- **Cons**

- Only can concentrate brines up to 6-8 wt% of TDS
- Highly susceptible to scaling and fouling



Start of the Art Technologies used in ZLD

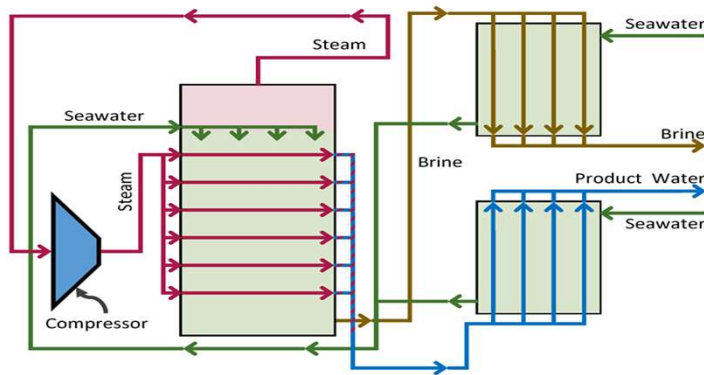
Mechanical Vapor Recompression (MVR)

• Pros

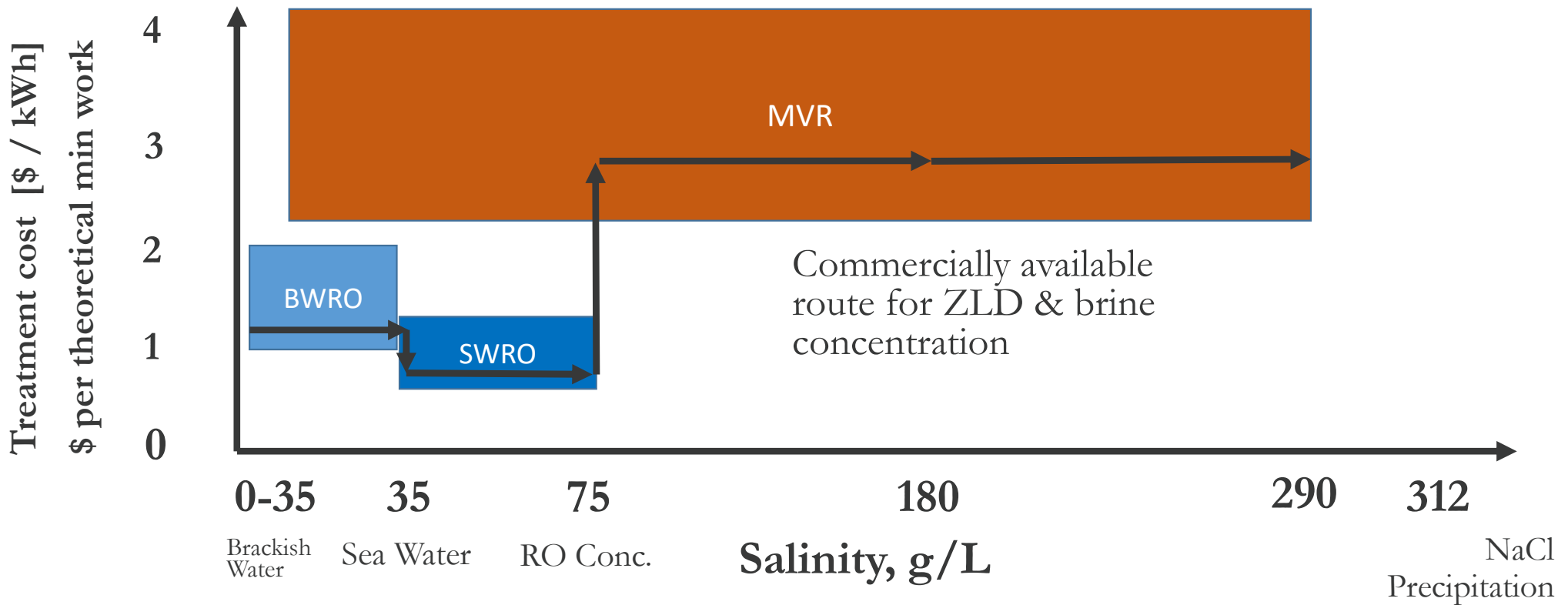
- Can concentrate brines up to 20 -25 wt% of TDS

• Cons

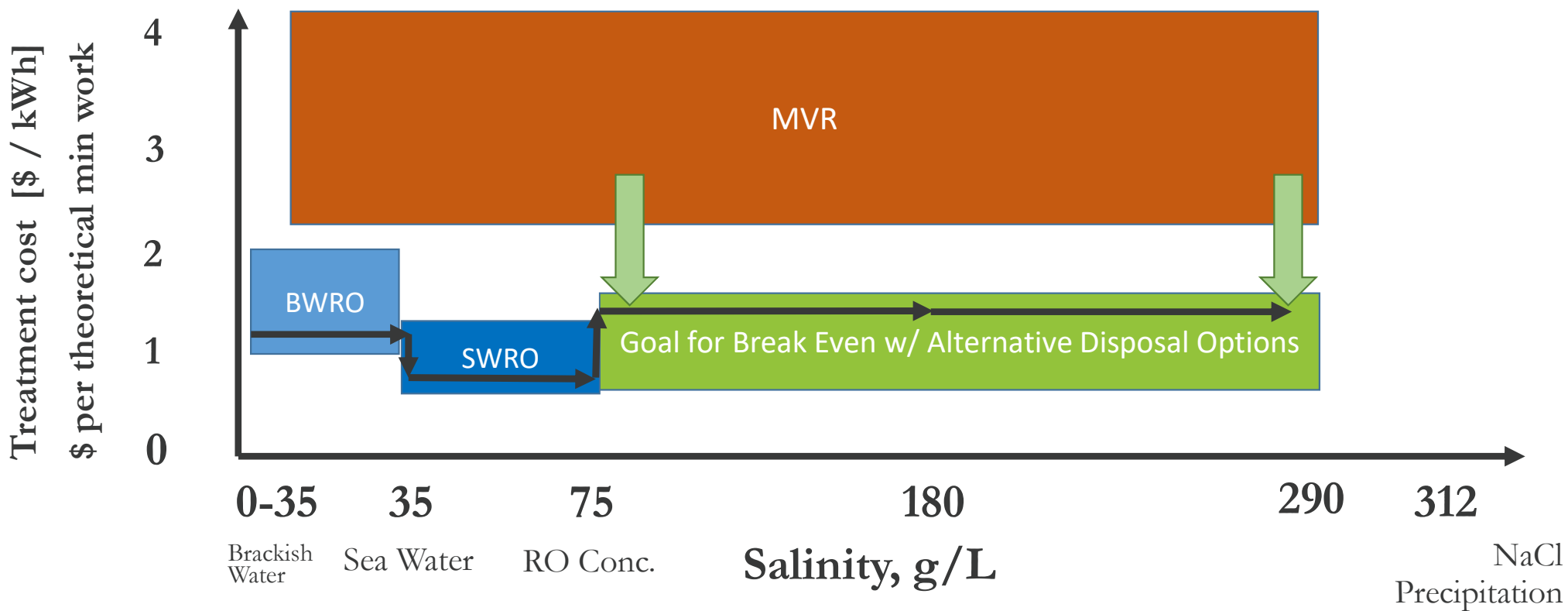
- Not particularly scalable or flexible
- Low efficiency (<10%) and high levelized costs to treat



Grand Challenge for Concentrating Effluent Streams



Grand Challenge for Concentrating Effluent Streams



Dewatering Processes

Reverse
Osmosis

- Ability to dewater high salinity brines
- Electricity driven process
- Minimal chemical handling

Mechanical
Vapor
Compression

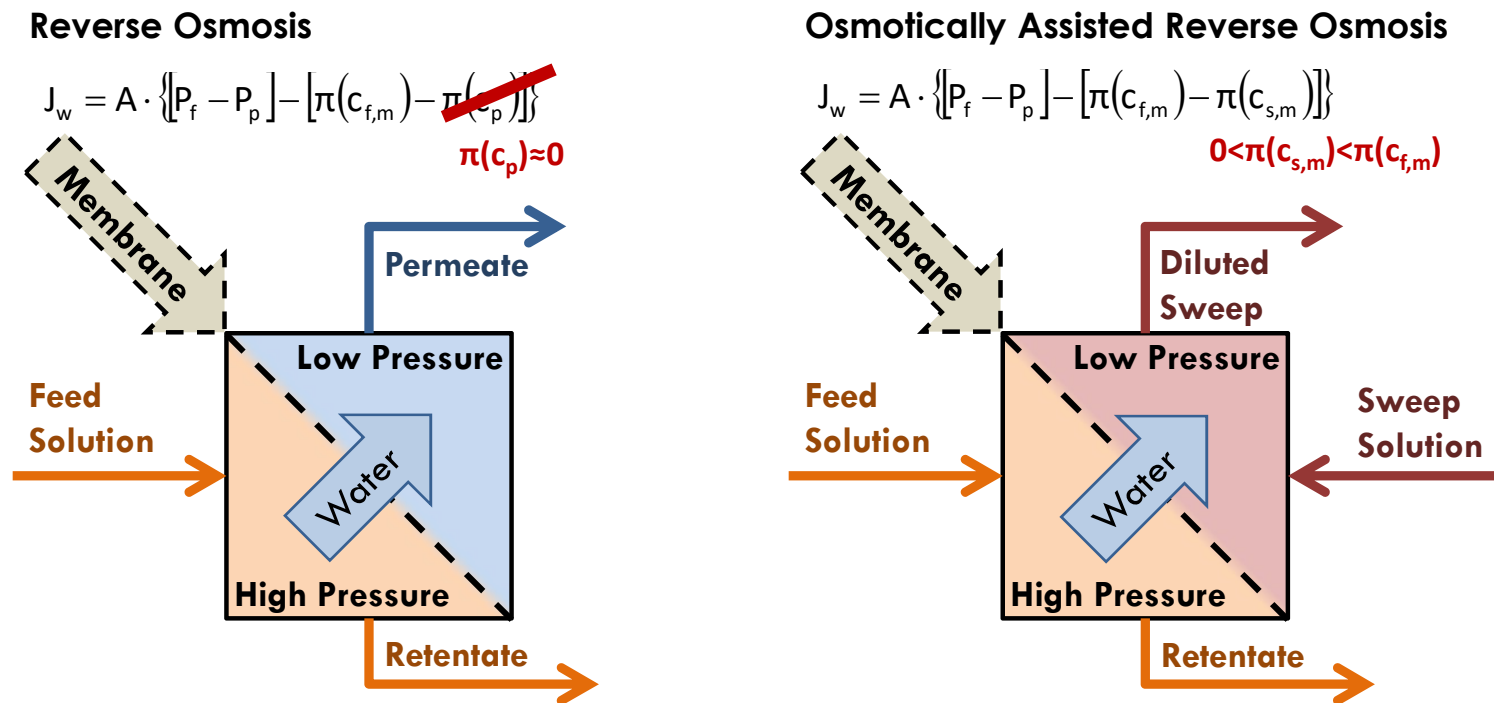
Forward
Osmosis w/
NH₃:CO₂ Draw

Membrane
Distillation

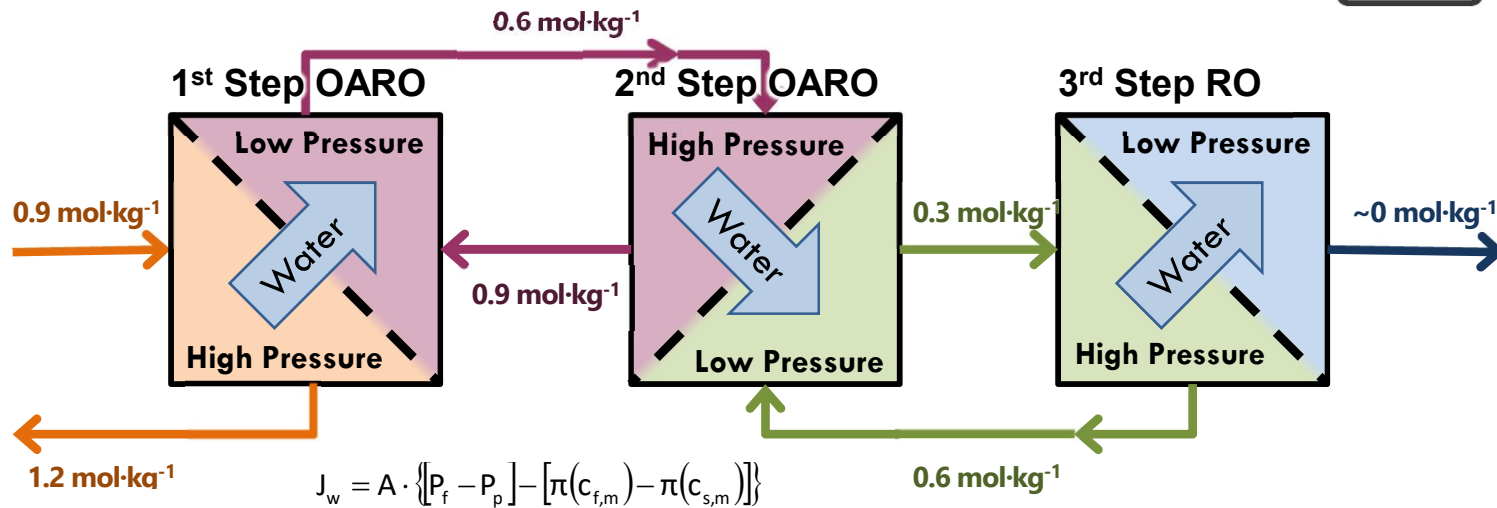
Osmotically Assisted
Reverse Osmosis

Osmotically Assisted Reverse Osmosis

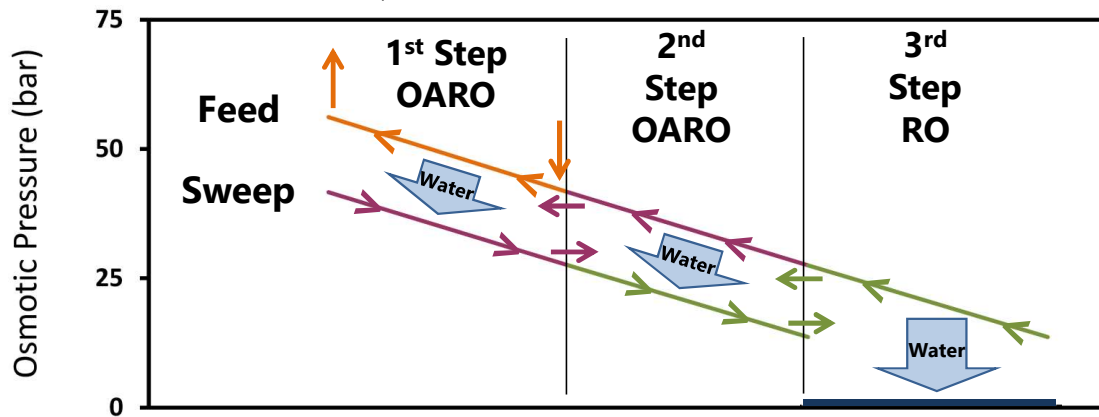
Osmotically Assisted Reverse Osmosis (OARO) differs from conventional membrane processes



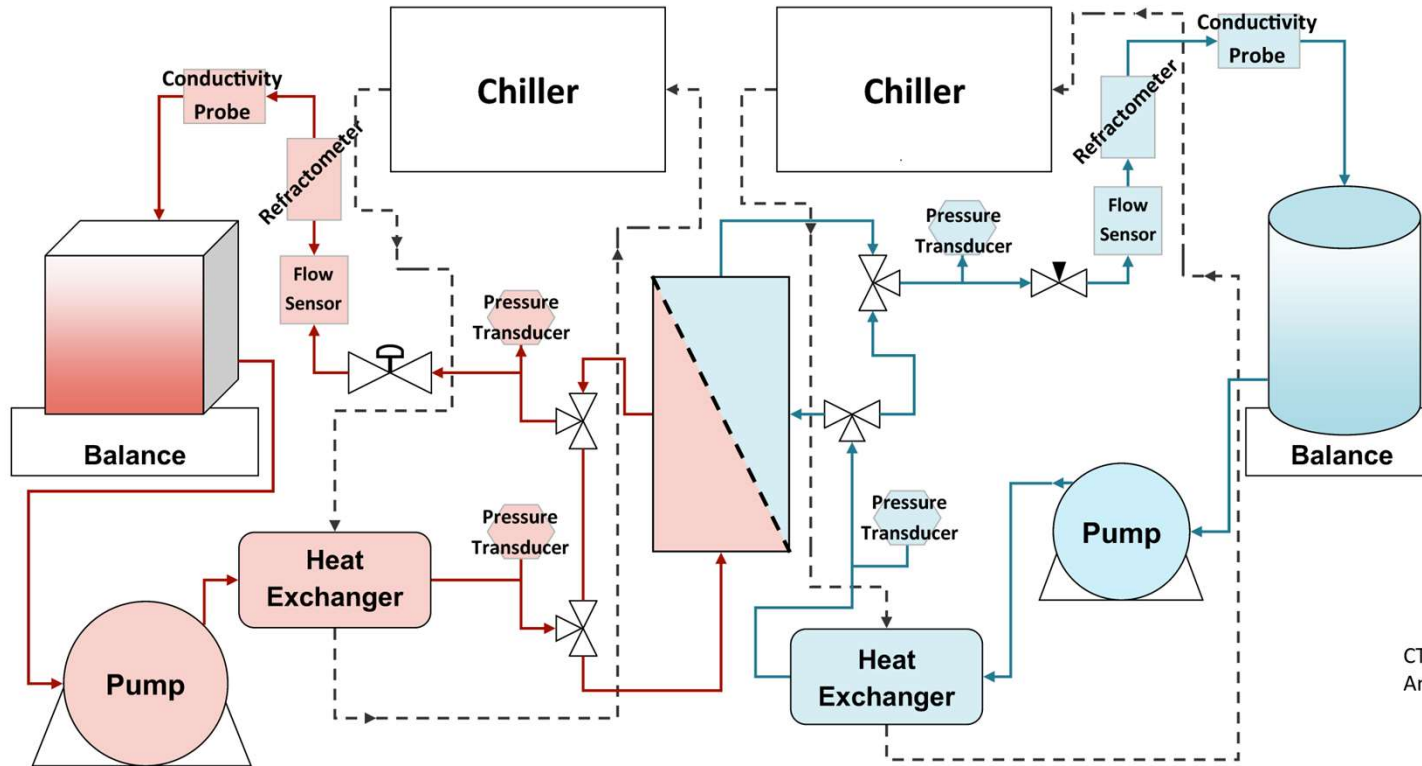
Process Configuration



$$J_w = A \cdot \{ [P_f - P_p] - [\pi(c_{f,m}) - \pi(c_{s,m})] \}$$



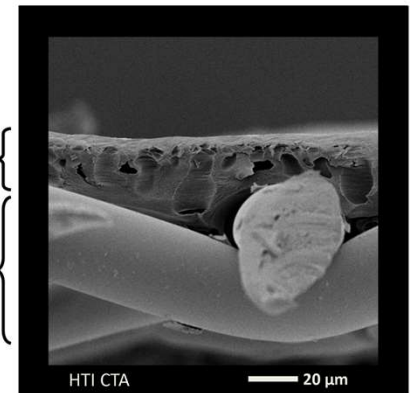
Test System at NETL



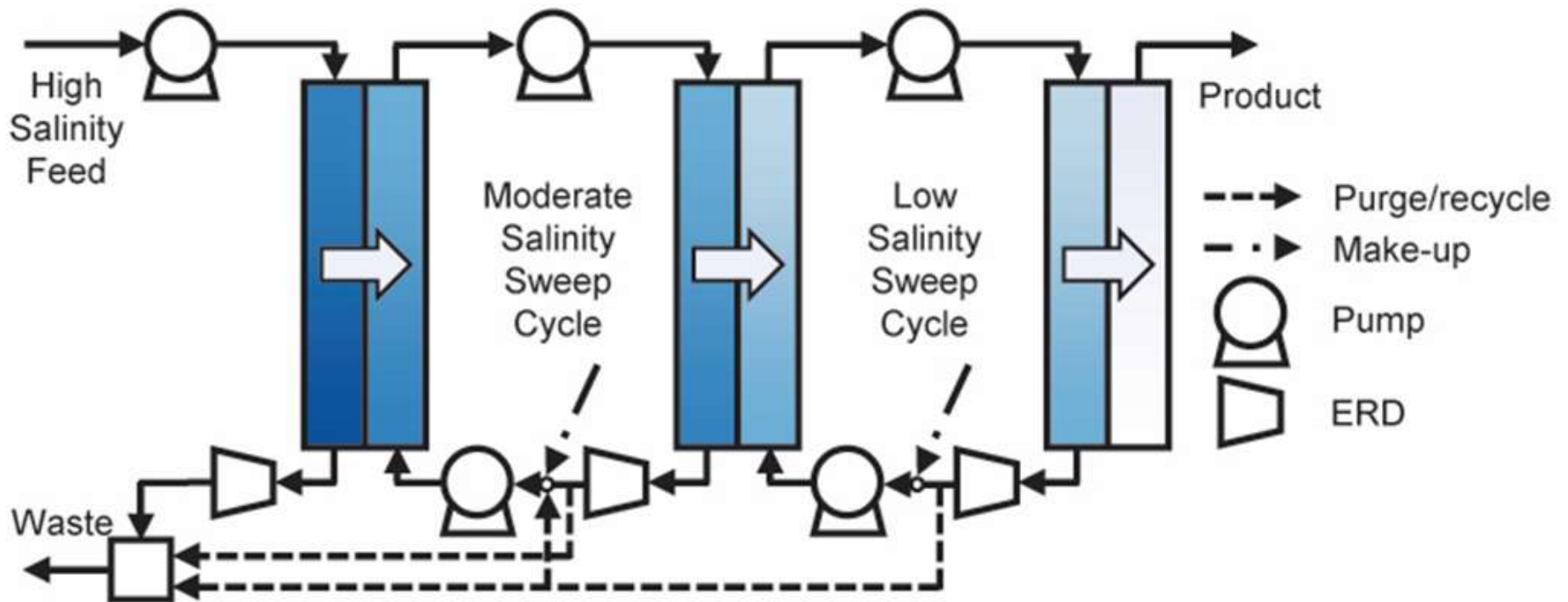
Hydrolyzes at alkaline conditions

CTA selective layer
And support layer

Embedded
hydrophilic mesh



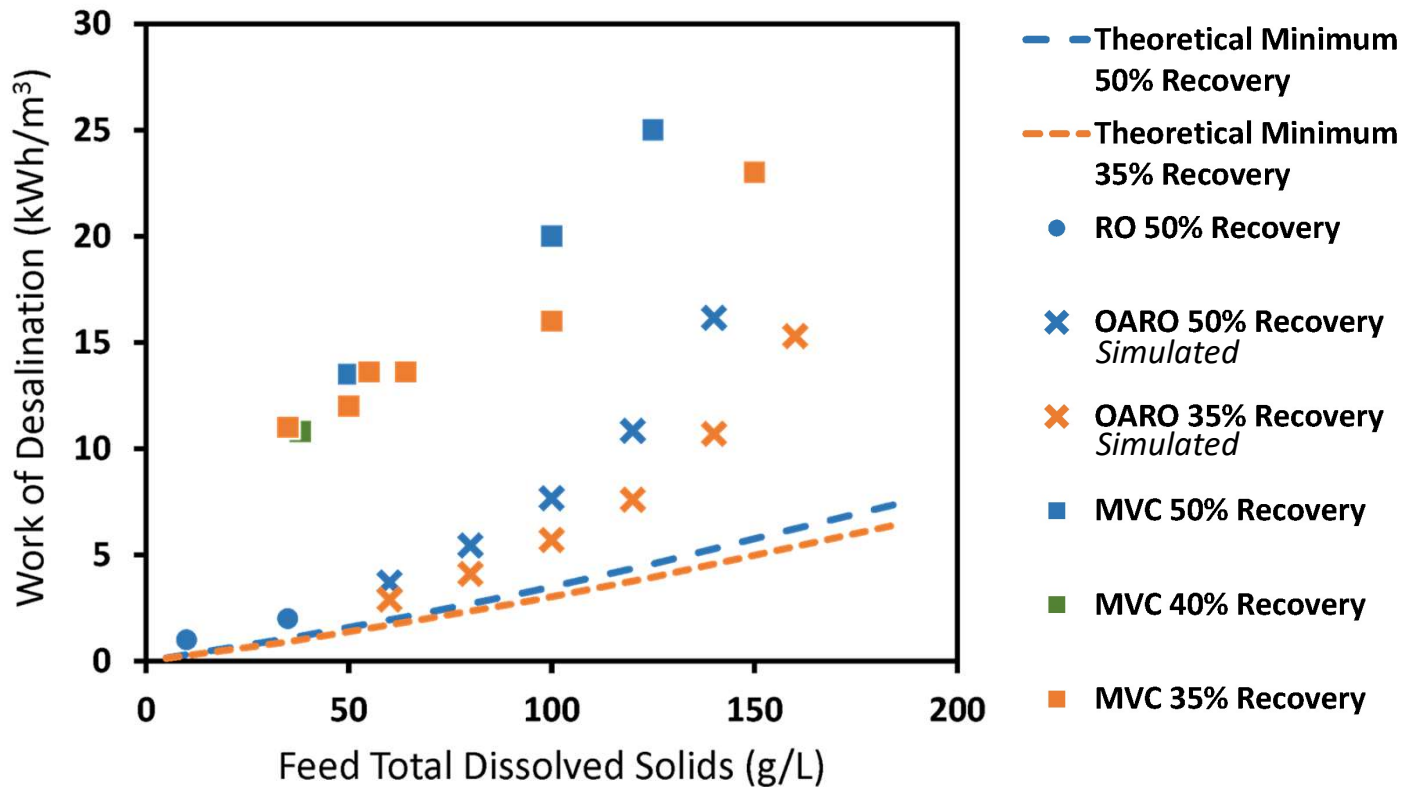
OARO Process Simulation



ERD = Energy Recovery Device Pressure Recovery assuming between 90% - 96% efficiency

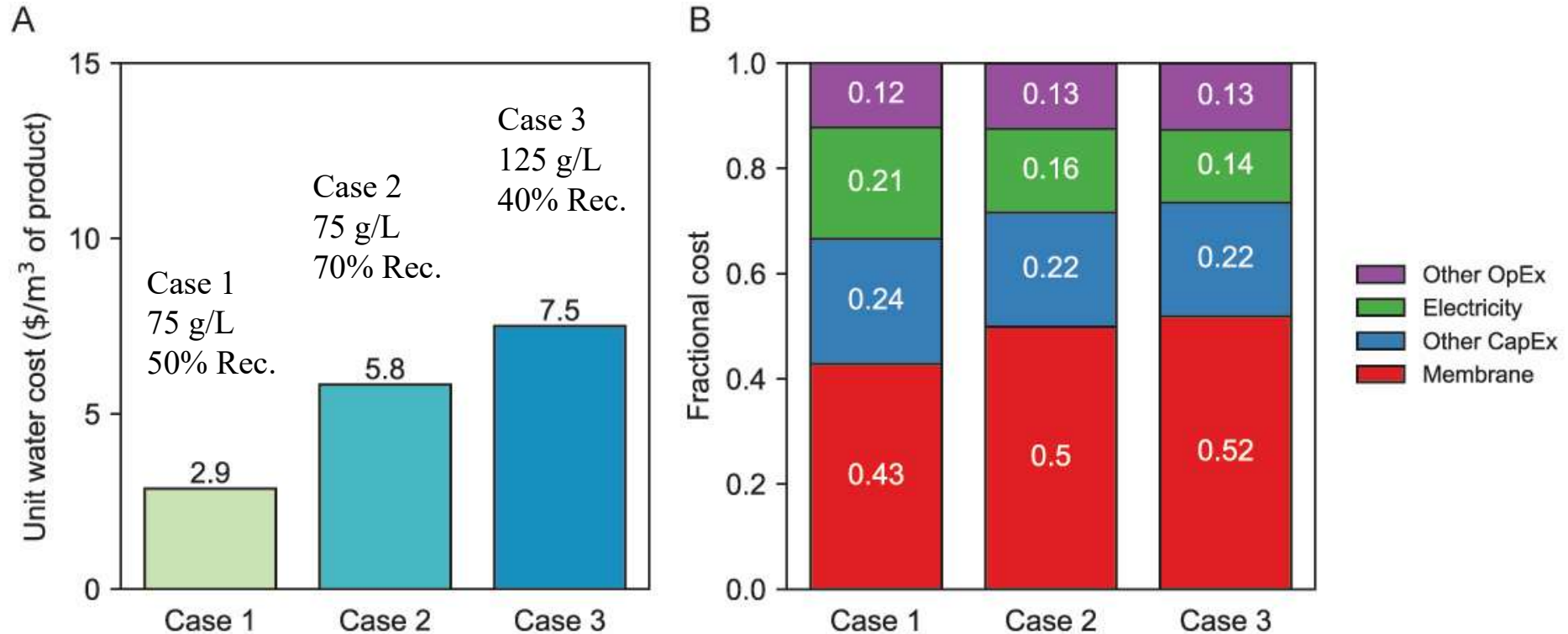
Comparison of Energy Demand

OARO has the Potential for 50% Savings in Electrical Energy



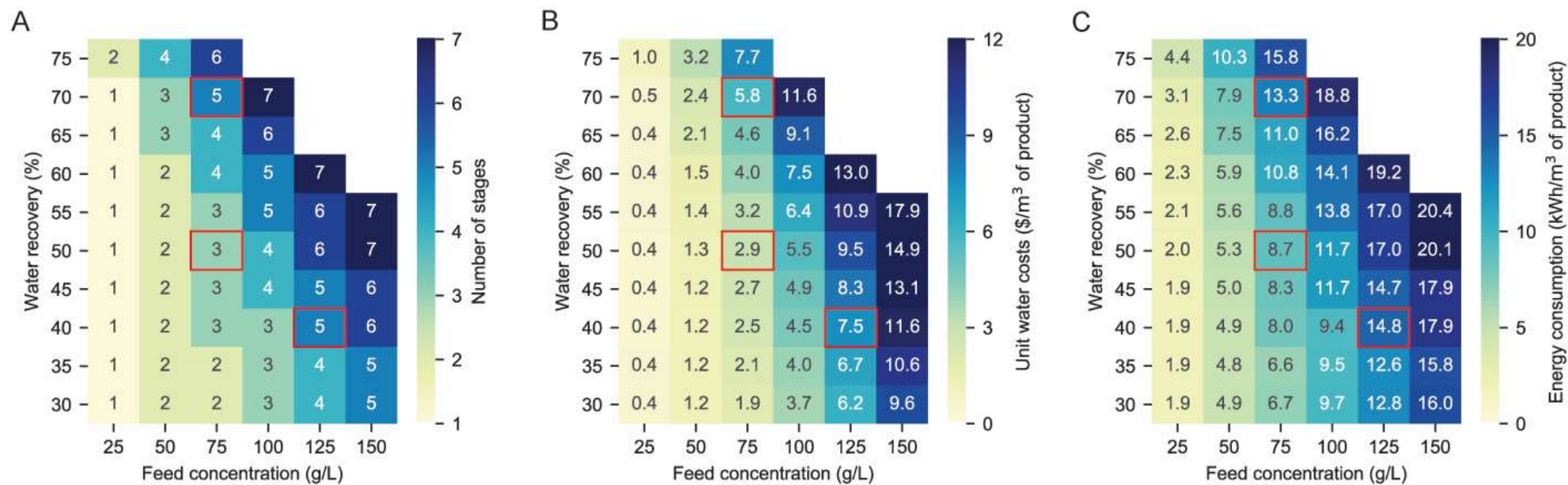
Energy consumption of RO, MVC/MVR, OARO water treatment and theoretical minimum work with respect to feed TDS concentration and recovery

Techno-Economic Analysis: Base Case



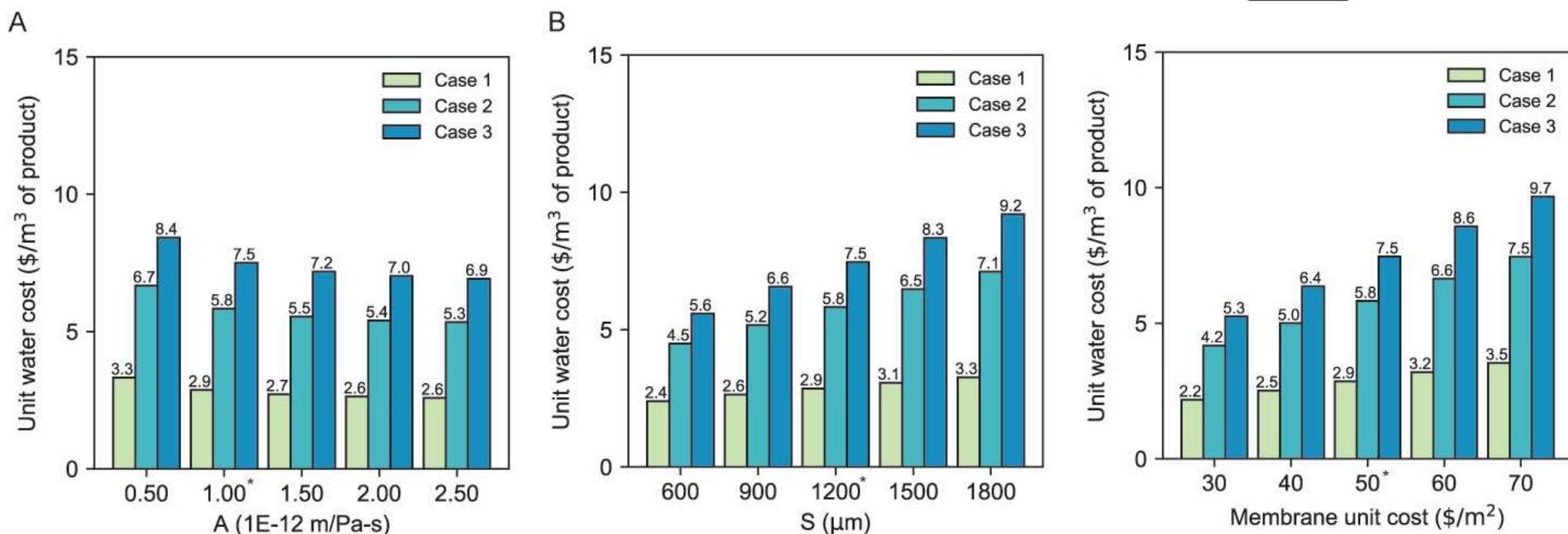
Cost optimal unit water costs (A) and normalized component costs (B) for the three high salinity brine desalination cases: Case 1: 75 g/L TDS with 50% recovery, Case 2: 75 g/L TDS with 70% recovery, and Case 3: 125 g/L with 40% recovery

Optimization within the Base Cases



Cost optimal design configurations and associated performance metrics for OARO/RO membrane-based desalination processes: A) number of stages, B) unit water costs, C) energy use. The three high-salinity brine desalination cases are denoted with a red box.

OARO cost sensitivity



OARO cost sensitivity for A) water permeability coefficient, A; B) structural parameter, S; C) membrane unit cost.

The baseline value used in modeling each of the cases is marked with an asterisk.

Conclusions & Future Work



- **OARO is a membrane process capable of concentrating effluent streams to high salinity**
- **Electrical energy cost of OARO is <50% of the electrical energy consumption of Mechanical Vapor Recompression (MVR)**
- **Preliminary Techno-Economic Analysis show modest cost savings compared with MVR using the Base Case assumptions**
- **Sensitivity Analysis shows the requirements for the structural parameter and the membrane cost that would allow for a 50% cost savings compared with MVR**

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Questions?