

# ***MSC.Marc 2003<sup>+</sup>***

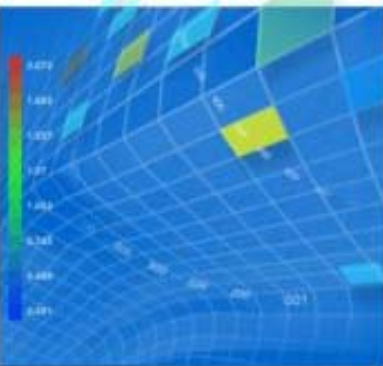
## **Fuel Cell Applications**

# ***Contents***

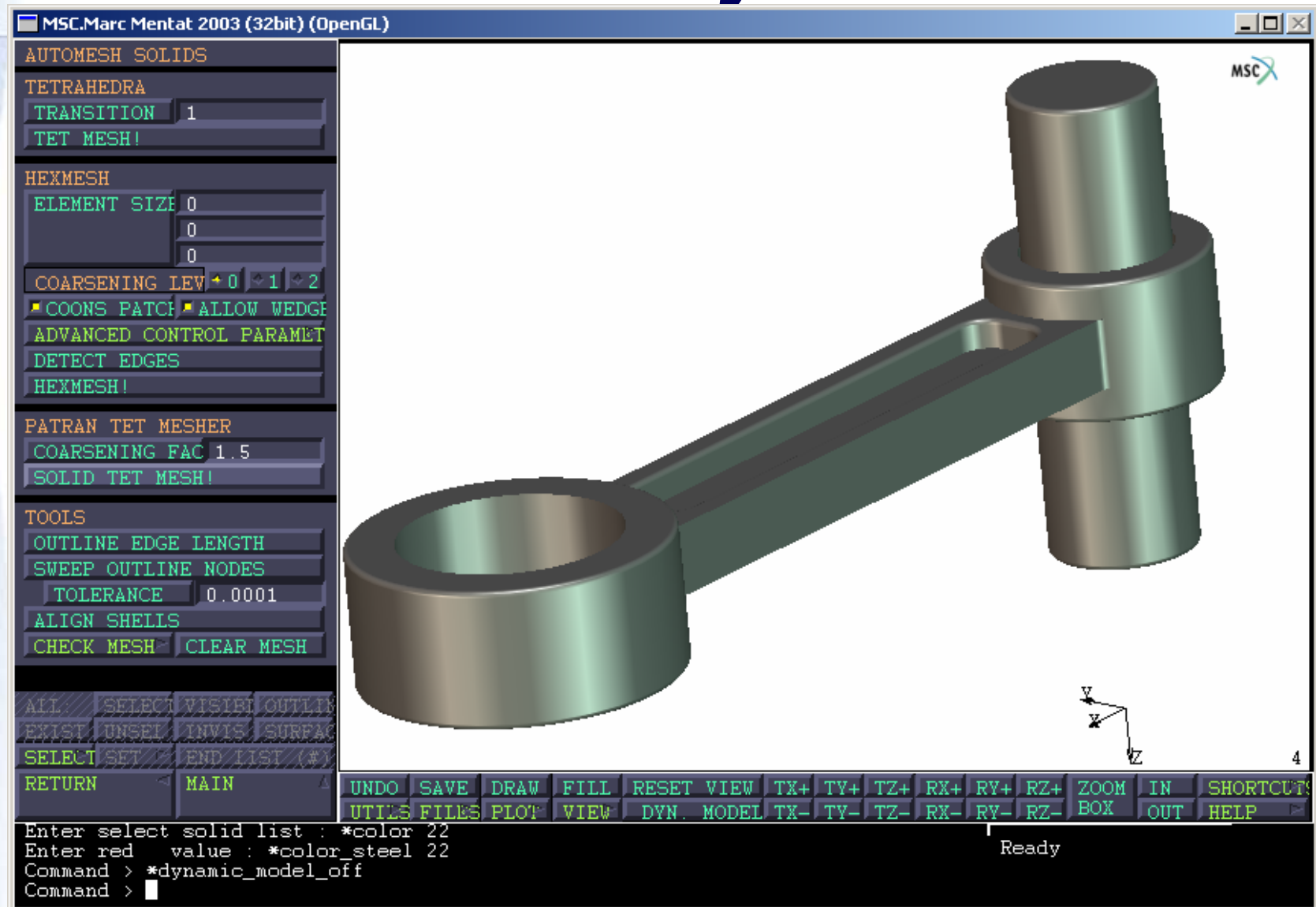
- **Meshing/Remeshing**
- **Analysis of Composite Materials (shell/solid)**
- **Fracture Mechanics Capabilities**
- **Heat Transfer and Coupled Thermal Stresses**
- **Running Jobs in Parallel**
- **Fluids**
- **User Subroutines**
- **Future Work**
- **PEN Fuel Cell Modeling**



# ***Meshing/Remeshing***



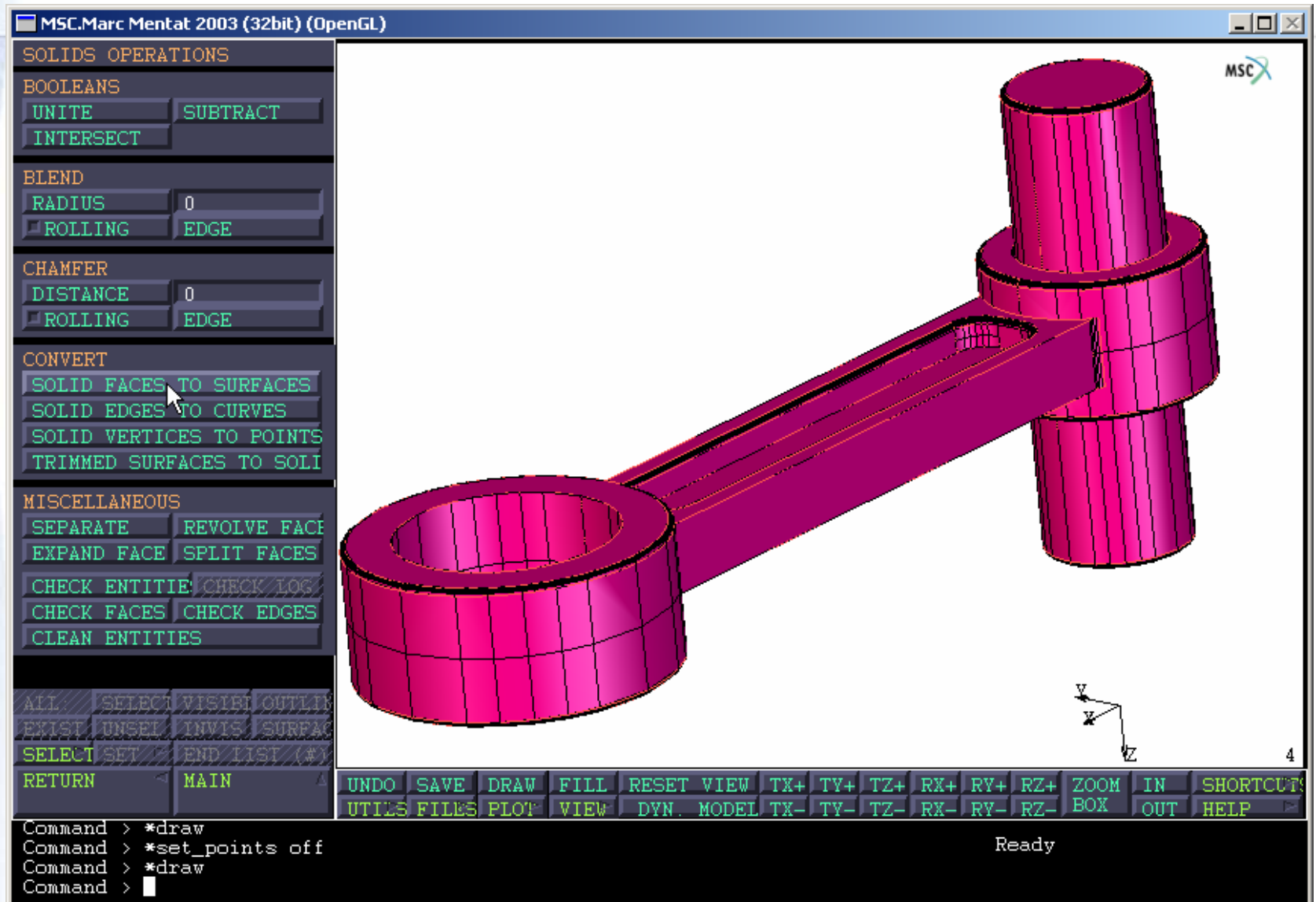
# CAD Connectivity: ACIS Solid



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# Convert to Surfaces

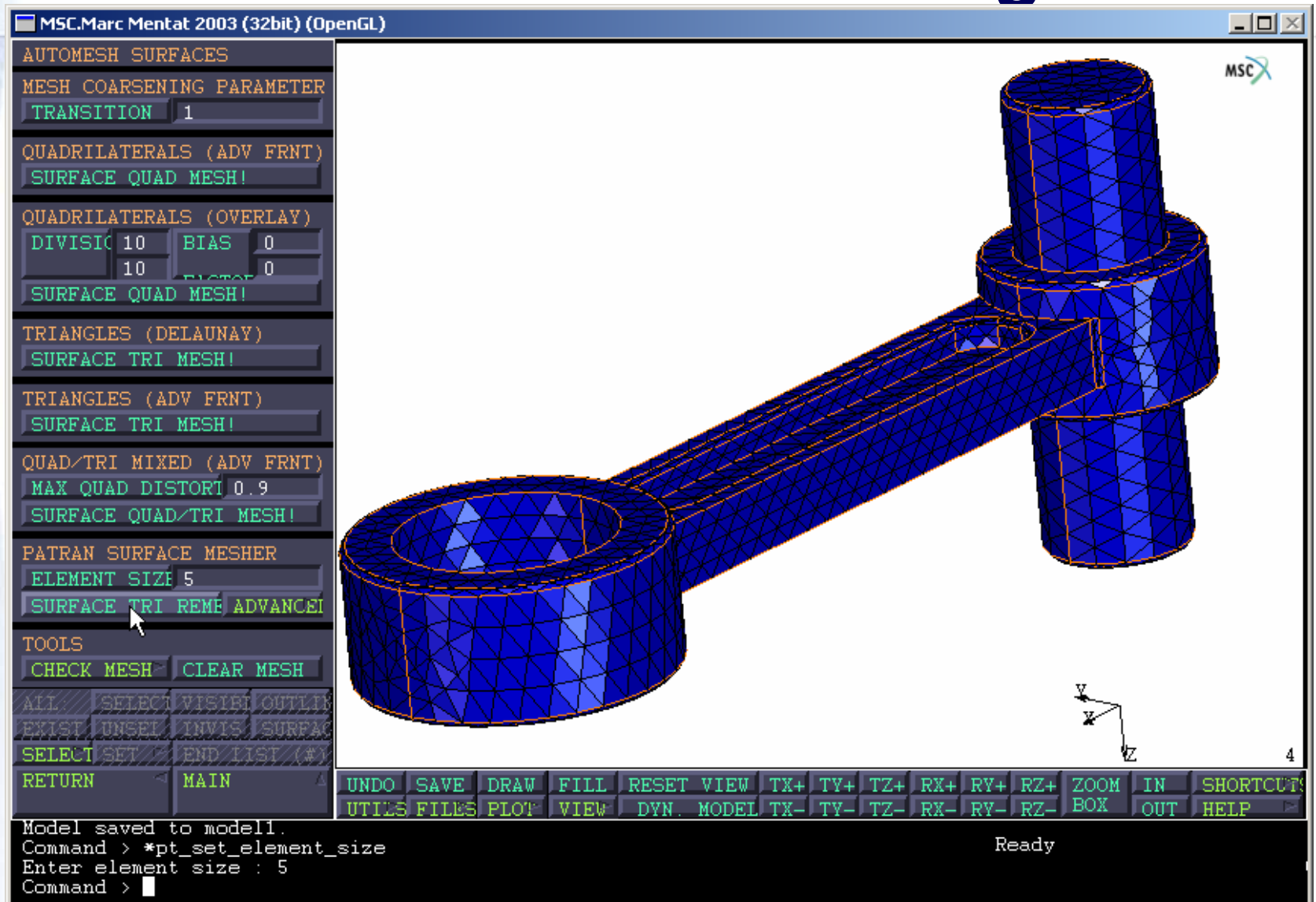


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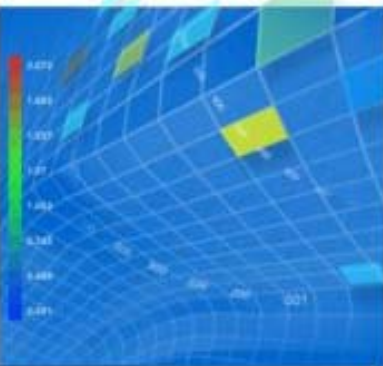
# Automatic Meshing



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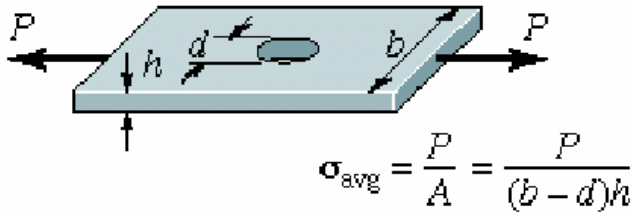
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# ***Local Remeshing***



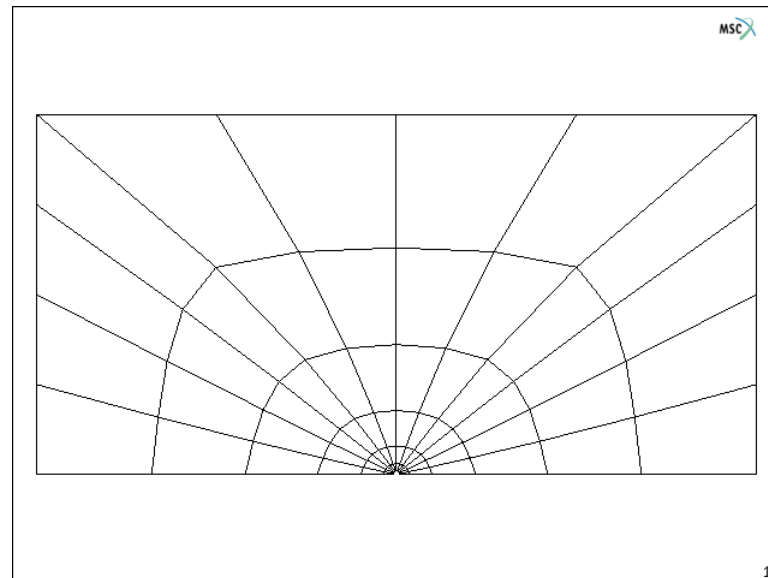
**Stress Concentration – Plate with Hole**

# Uniform Axial Load



$$\sigma_{max} = K_c \sigma_{avg}$$

$$\begin{aligned} h &= 1 \\ b &= 10 \\ d &= .1 \end{aligned}$$



1

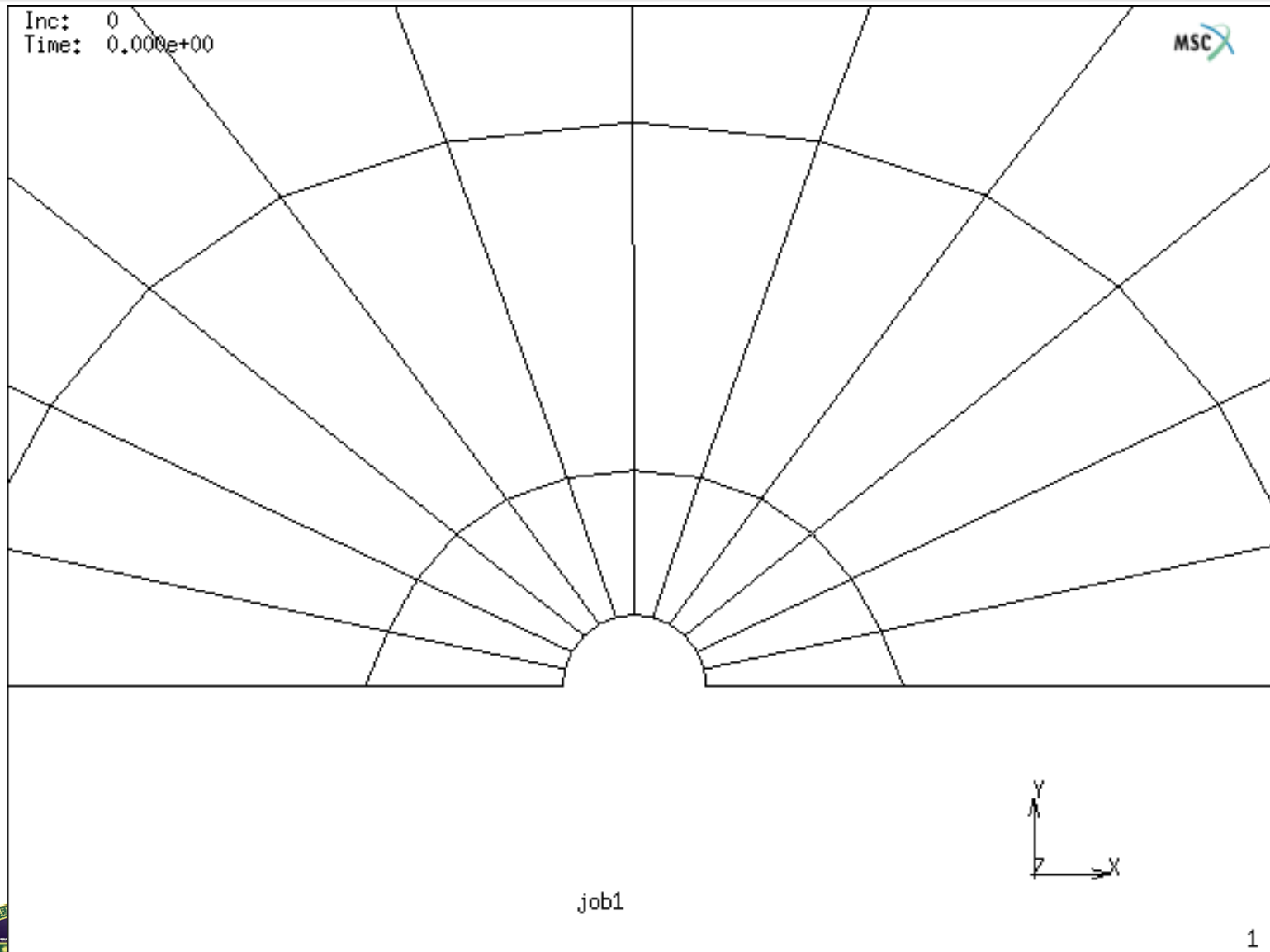


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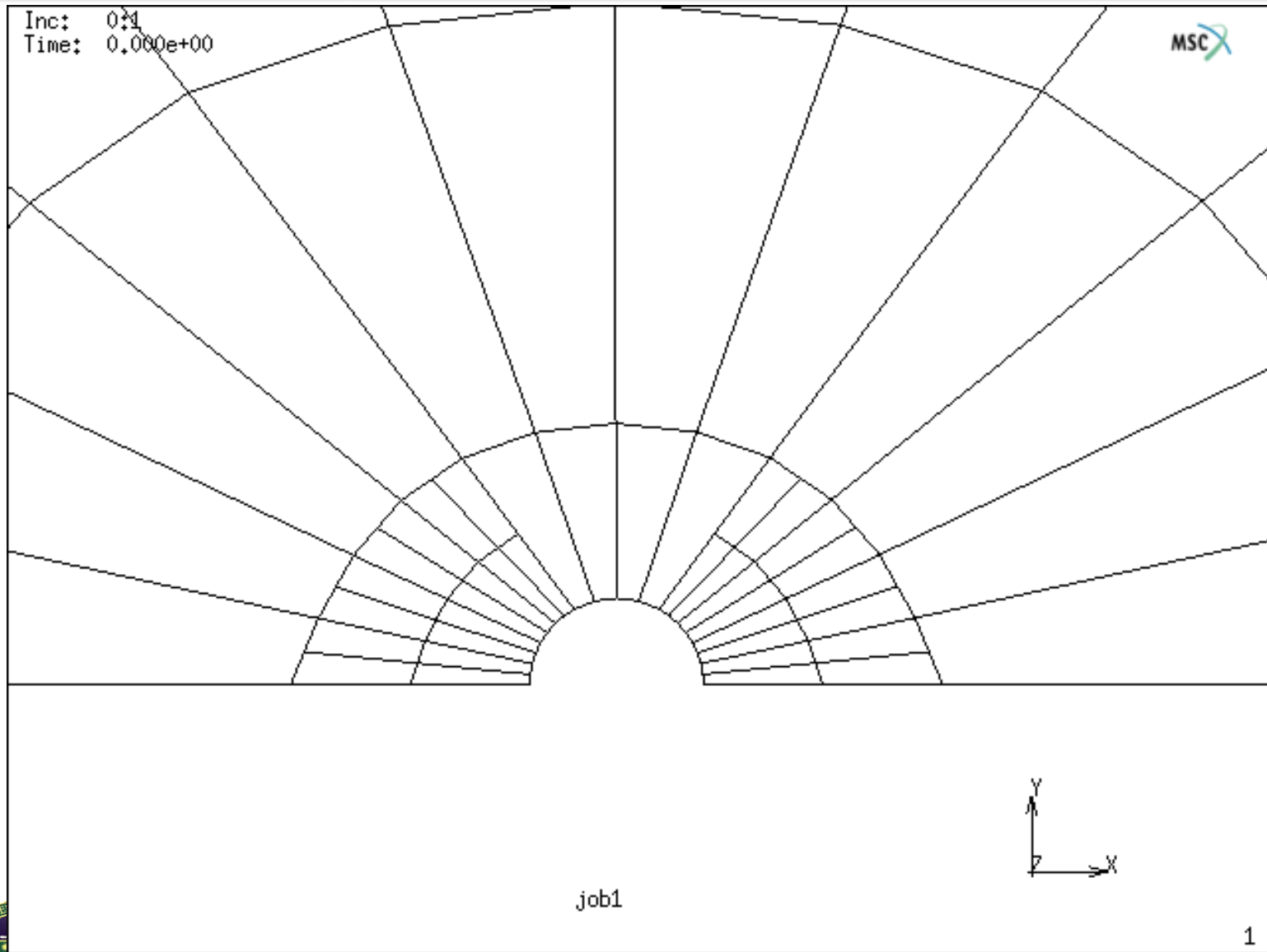
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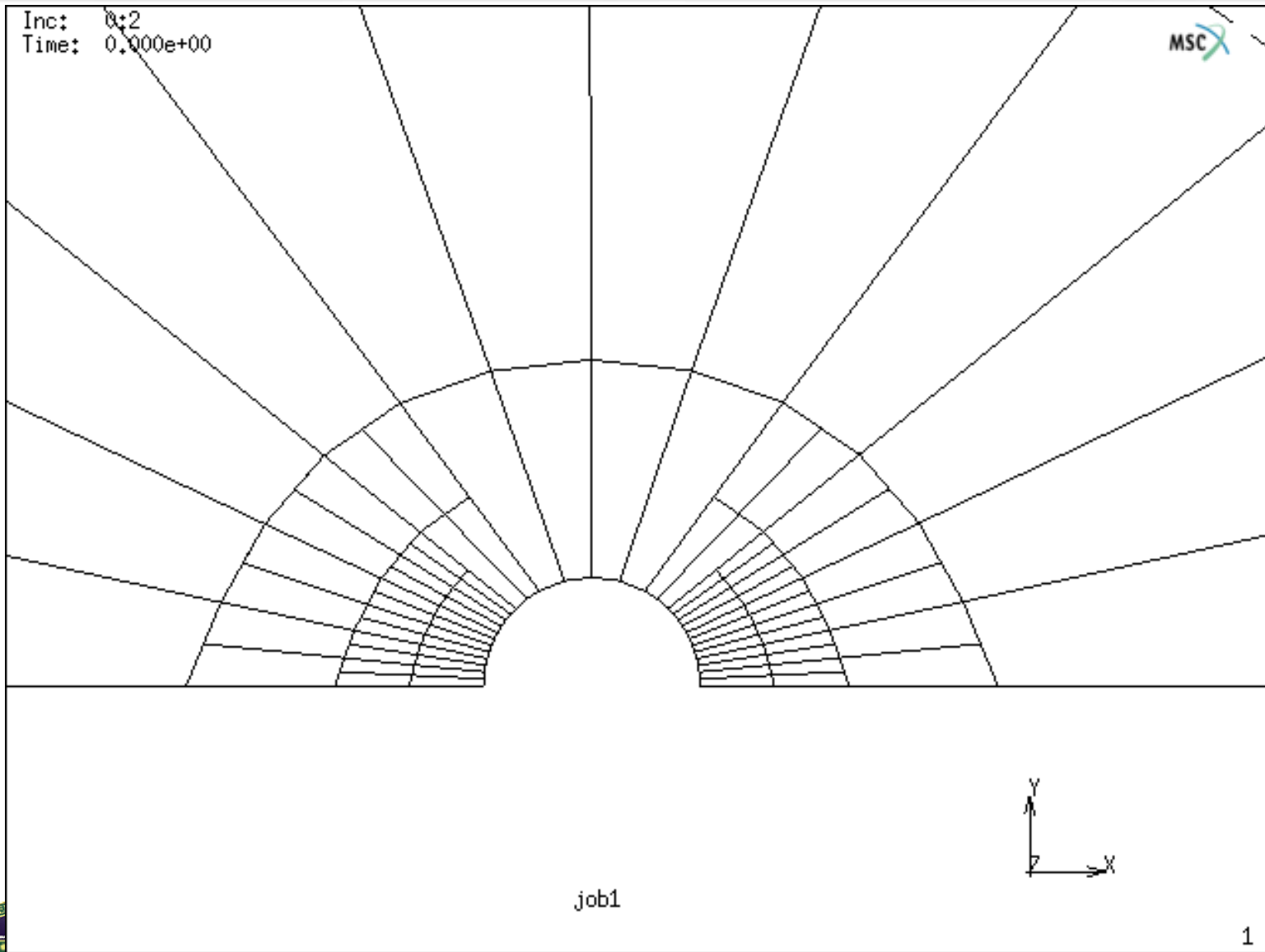
# 72 Elements, $K_c = 1.84$



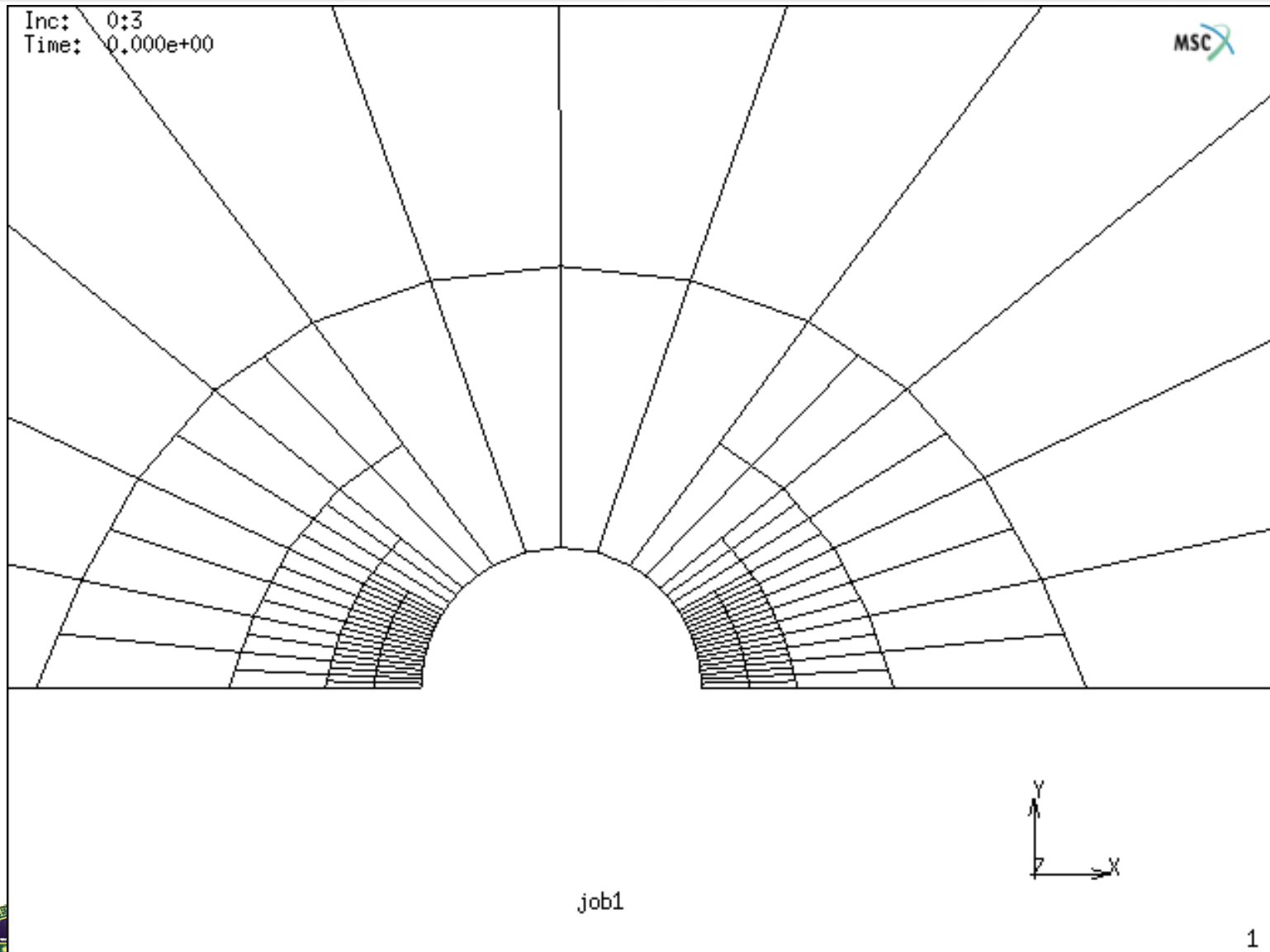
# 96 Elements, $K_c = 2.26$



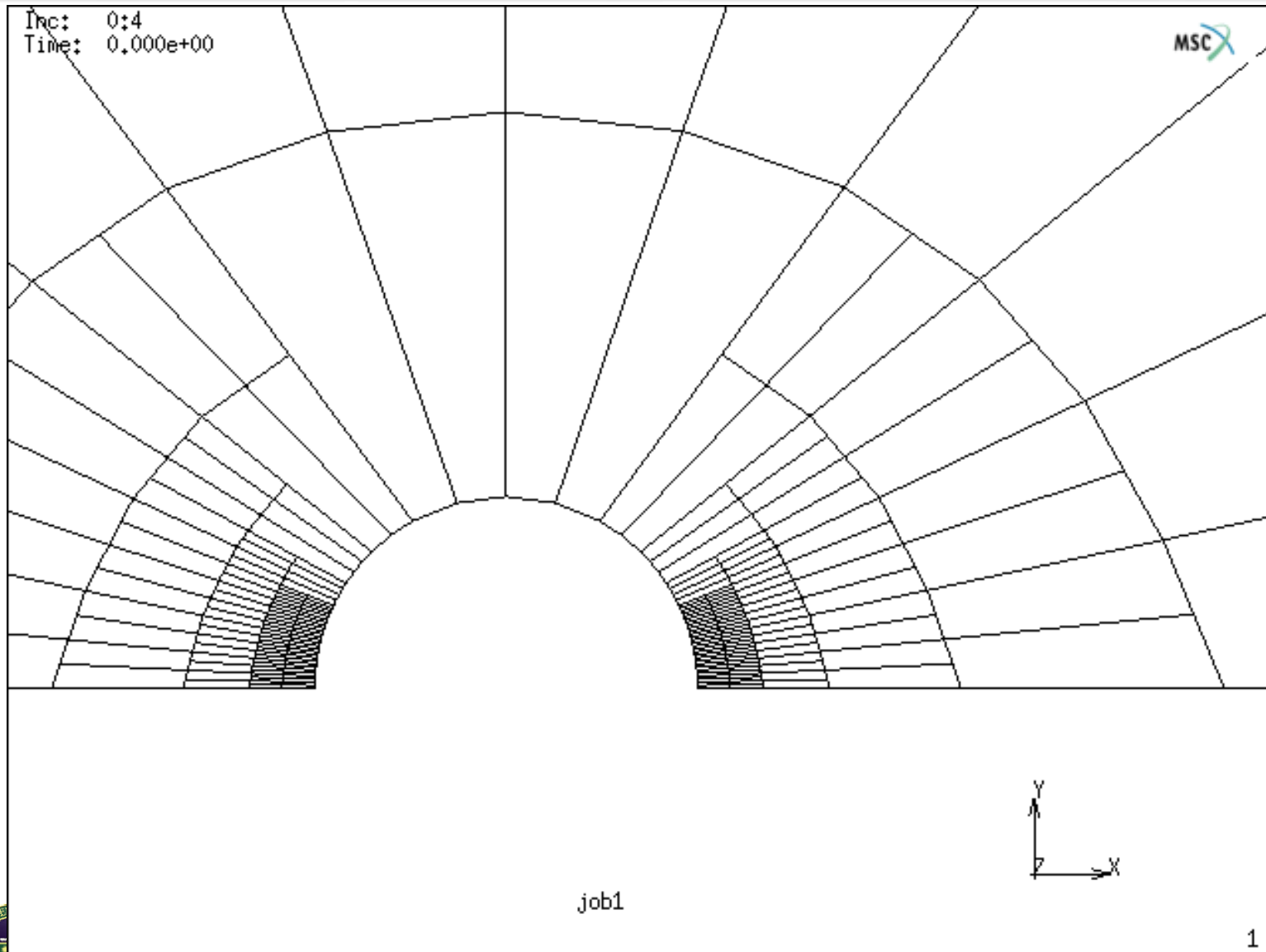
# 132 Elements, $K_c = 2.63$



# 186 Elements, $K_c = 2.89$

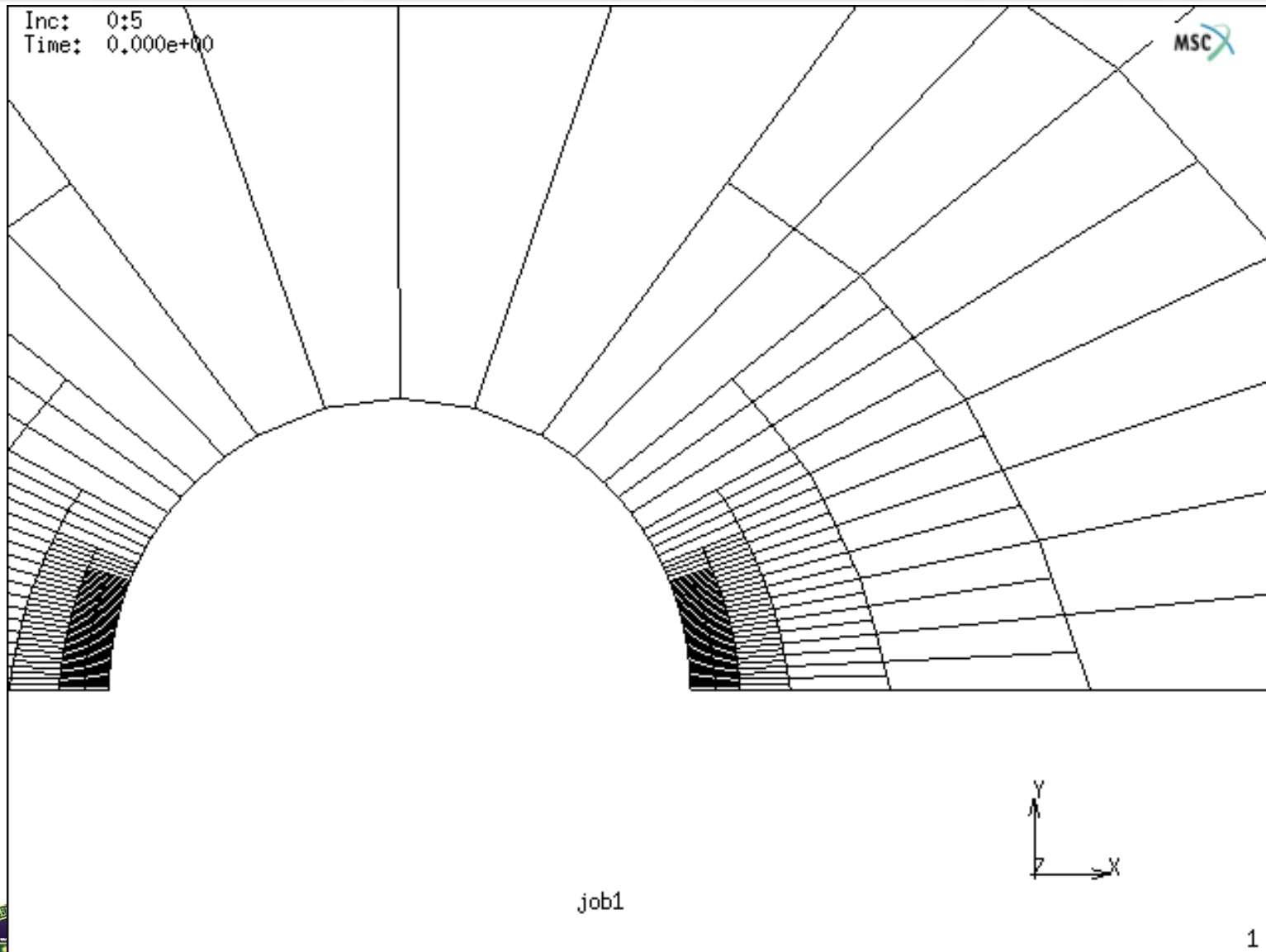


# 270 Elements, $K_c = 3.01$

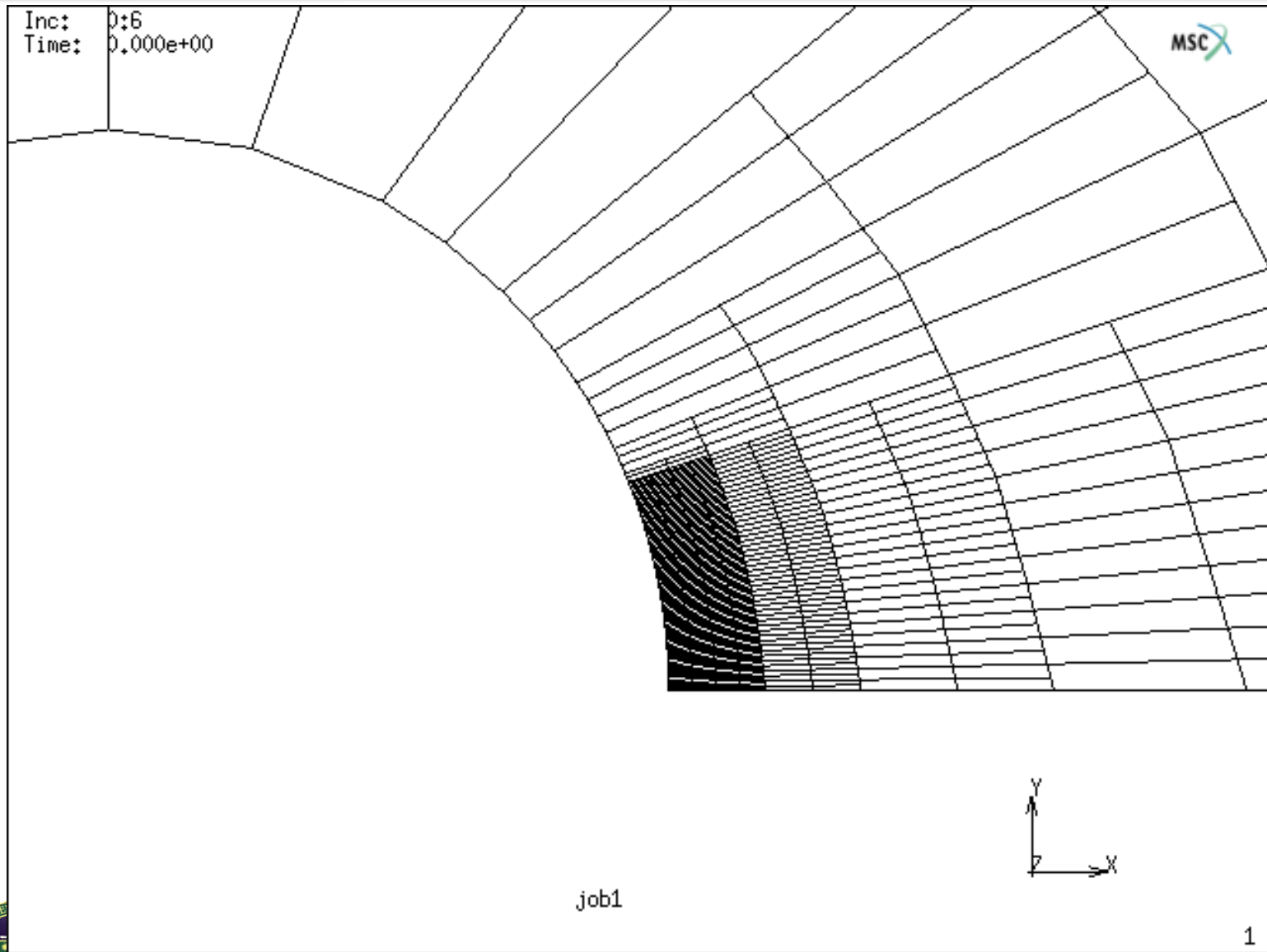




# 414 Elements, $K_c = 3.03$

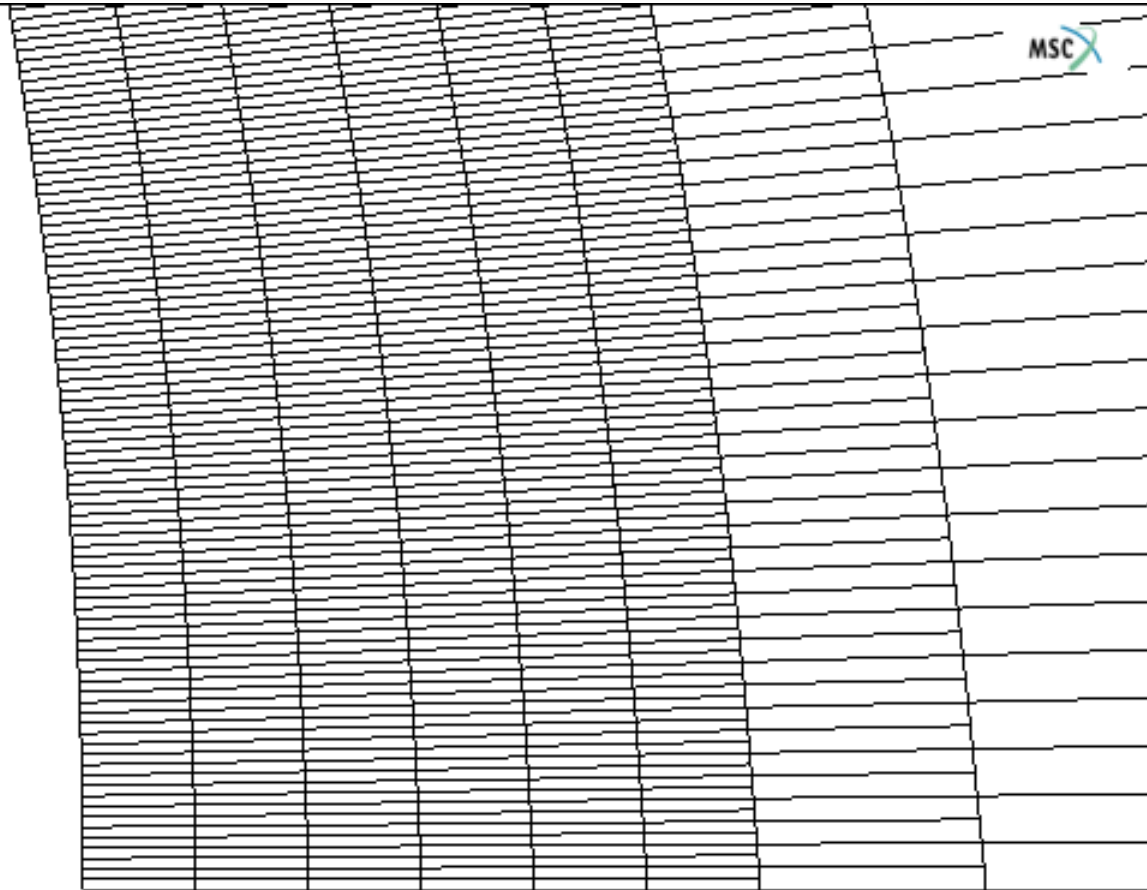


# 1278 Elements, $K_c = 3.03$



# 2715 Elements, $K_c = 3.03$

Inc: 0:7  
Time: 0.000e+00



job1

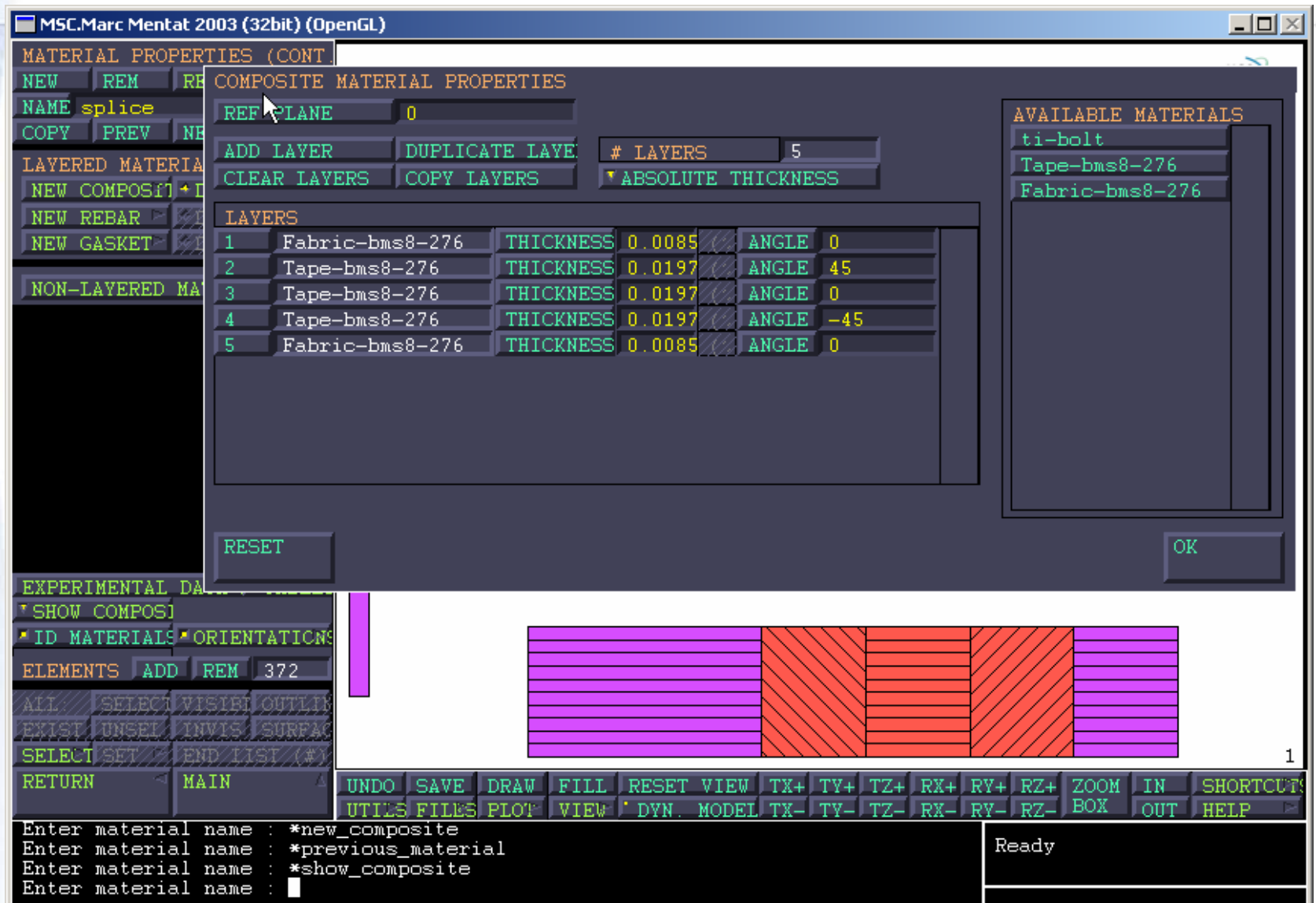


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# ***Analysis of Composite Materials***

**Shells and Solids**

# Composite Shell and Bricks

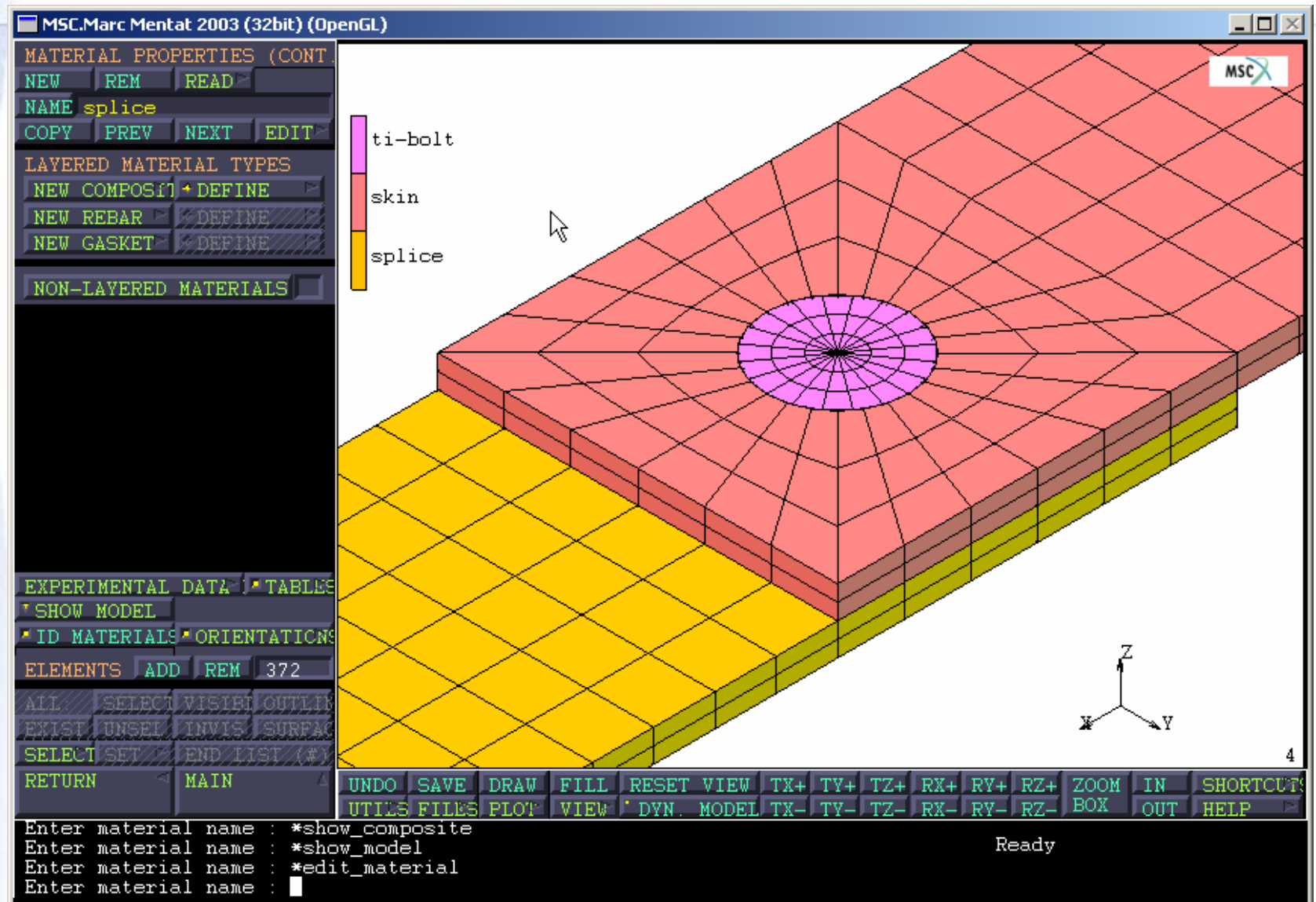


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# Composite Bricks

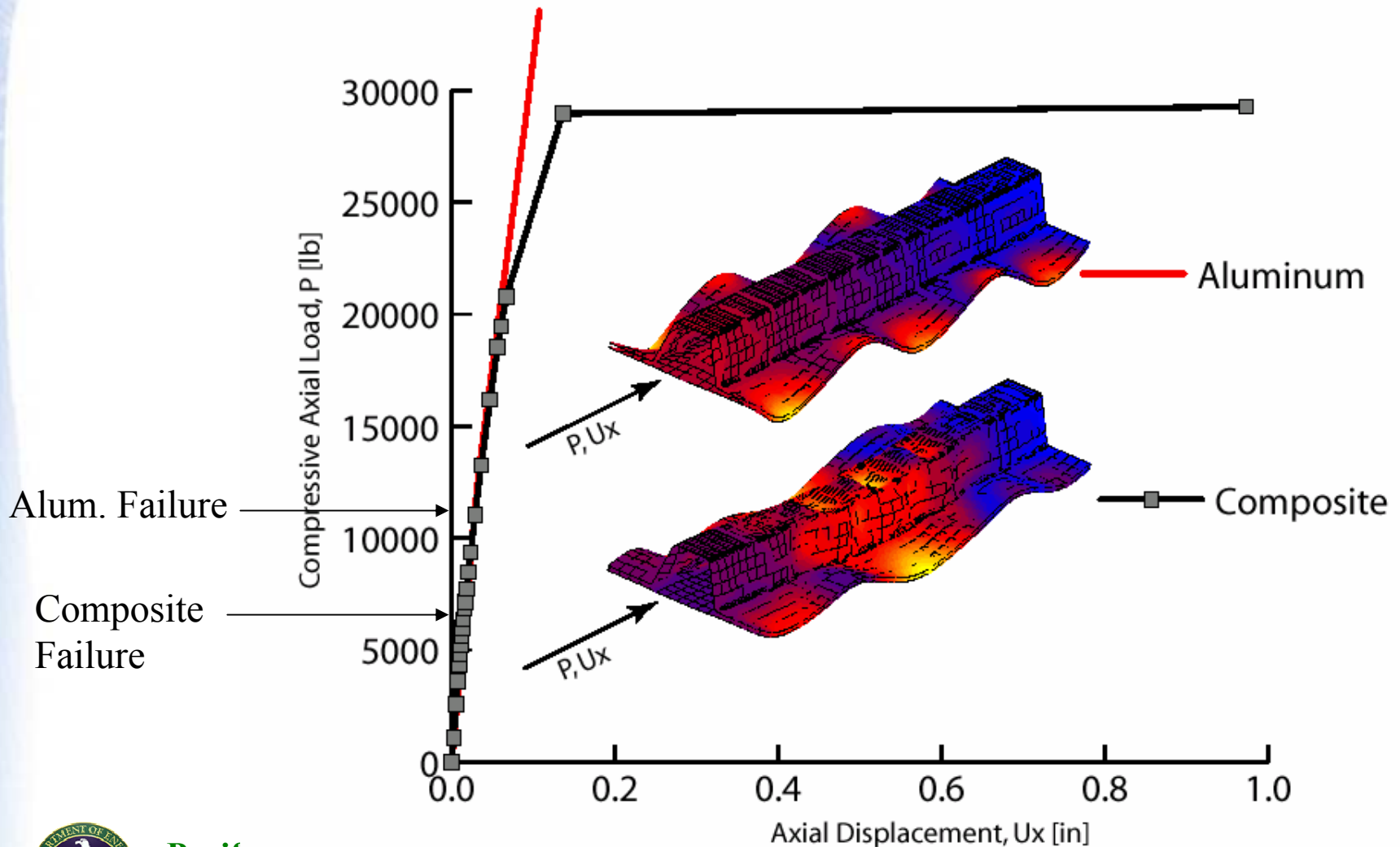


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# 7E7 Mid Skin Buckling

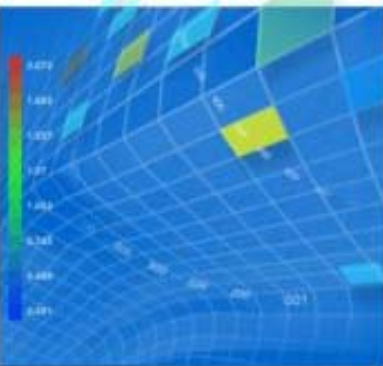
Results from 3d-hat1.mud and 3d-hat1AL.mud



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# ***Fracture Mechanics***



# J-Integral Estimations

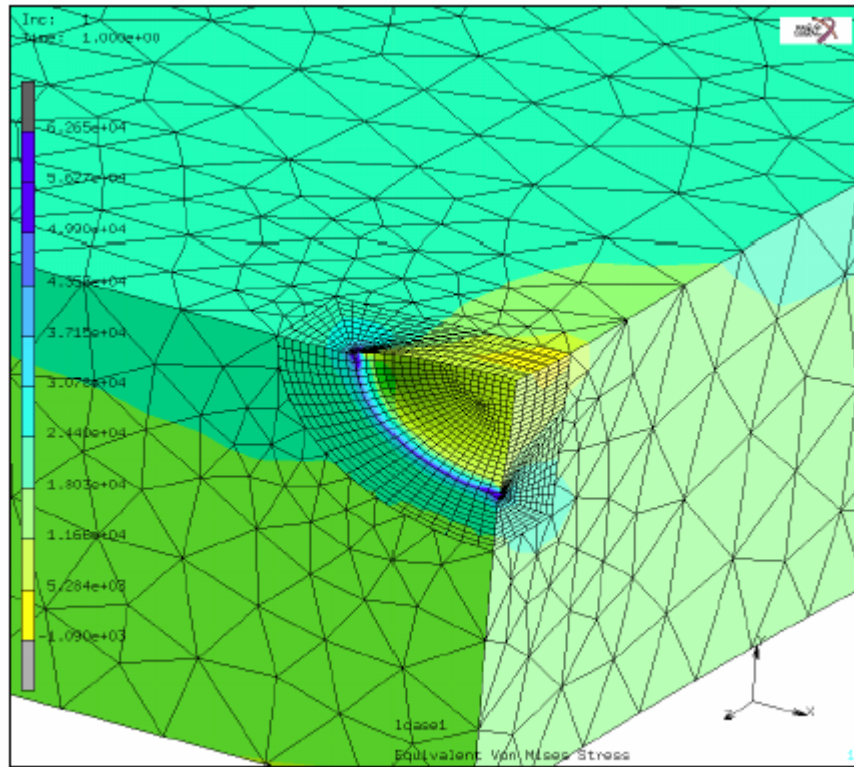


Figure 19-6 Equivalent von Mises Stress Contours

Table 19-1 J-integral Estimations

Crack Tip Node	Path Radius	J-integral Value
1235	1.1180E-01	3.1508E+03
1235	2.2361E-01	3.2027E+03
1235	3.3541E-01	3.1918E+03
1235	4.4721E-01	3.1984E+03
1235	5.5902E-01	3.1961E+03
1235	6.7082E-01	3.1947E+03
1235	7.8262E-01	3.1934E+03
3656	1.1187E-01	3.1553E+03
3656	2.2375E-01	3.2247E+03
3656	3.3562E-01	3.2335E+03
3656	4.4750E-01	3.2378E+03
3656	5.5937E-01	3.2338E+03
3656	6.7125E-01	3.2276E+03
3656	7.8312E-01	3.2216E+03

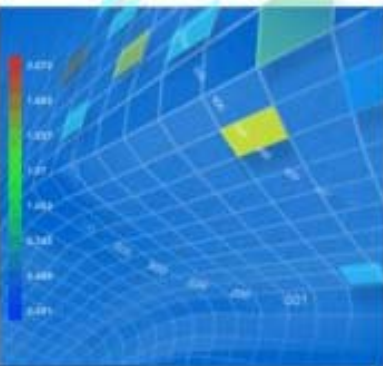


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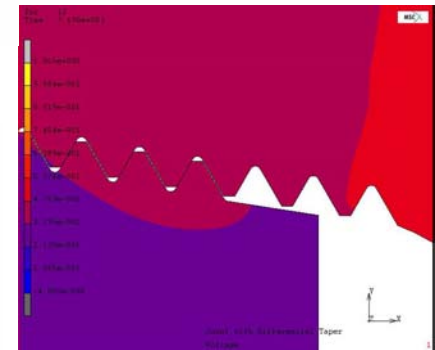
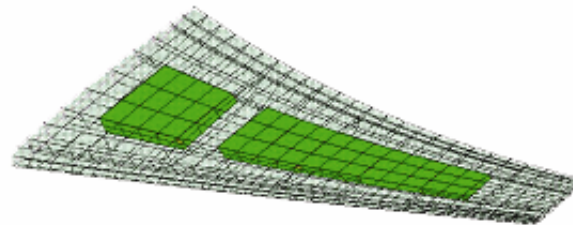
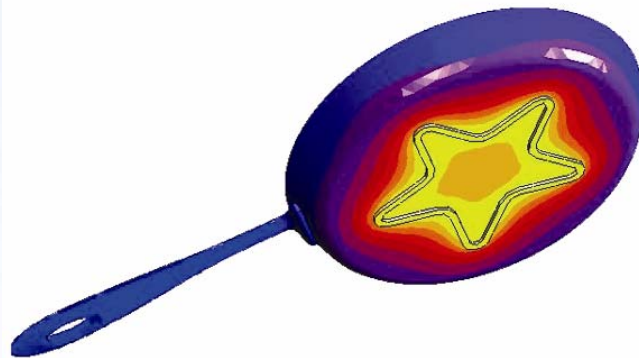
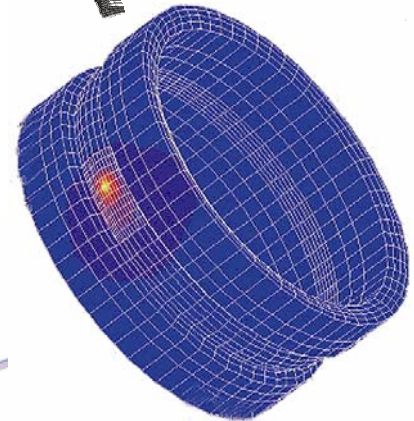
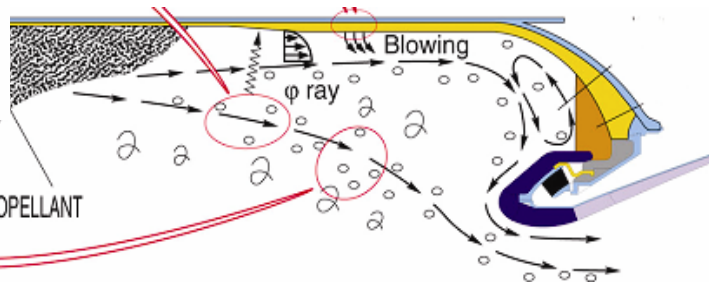
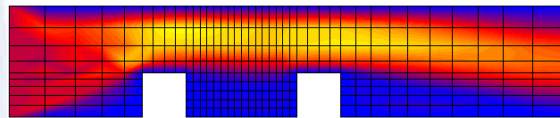
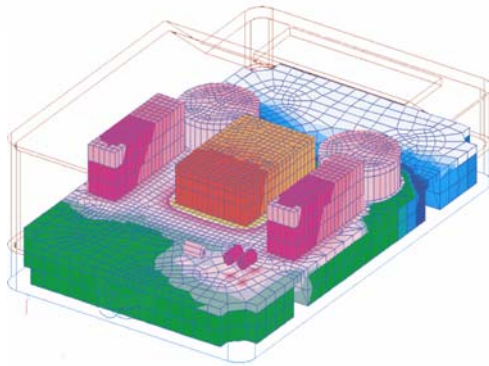
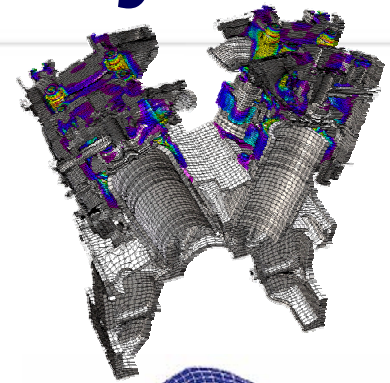
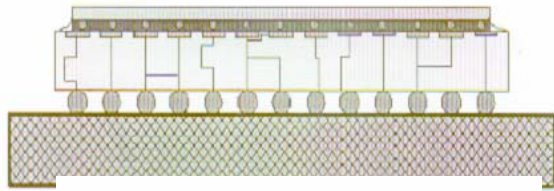


# ***Heat Transfer and Coupled Thermal Stress***





# The World of Thermal Analysis



# *Capabilities*

- **Steady State Simulation**
- **Transient Simulation**
- **Temperatures can be easily used in uncoupled thermal stress analysis**
- **Coupled Thermal-Structural Analysis**
- **Coupled Thermal-Electric (Joule Heating)**
- **Coupled Thermal-Electric-Structural**
- **Choice of Time Step Procedures**
  - **Fixed Time Steps**
  - **Adaptive Time Steps**



# *Capabilities*

- 1-d
- 2-d (planar and axisymmetric solid and axisymmetric shells)
- 3-d (solid, and shells)
- Heat transfer shells may have any number of layers, temperature varies either linearly or quadratically through layer
- Nonlinear Transient Cyclic Symmetry
- All heat transfer elements have comparable structural elements for thermal stress analysis or coupled analysis



# ***Capabilities***

- **Isotropic , Orthotropic or Anisotropic thermal properties.**
- **All properties may be function of temperature.**
- **Latent heat effects included to model phase changes**



# *Capabilities*

- **Point or Distributed Fluxes**
- **Convective Boundary Conditions**
- **Radiative Heating**
- **View Factor Calculations efficiently done using Monte Carlo method**
- **Internal Heating due to plasticity or friction in coupled structural analysis.**
- **Thermal Contact in coupled structural analysis.**





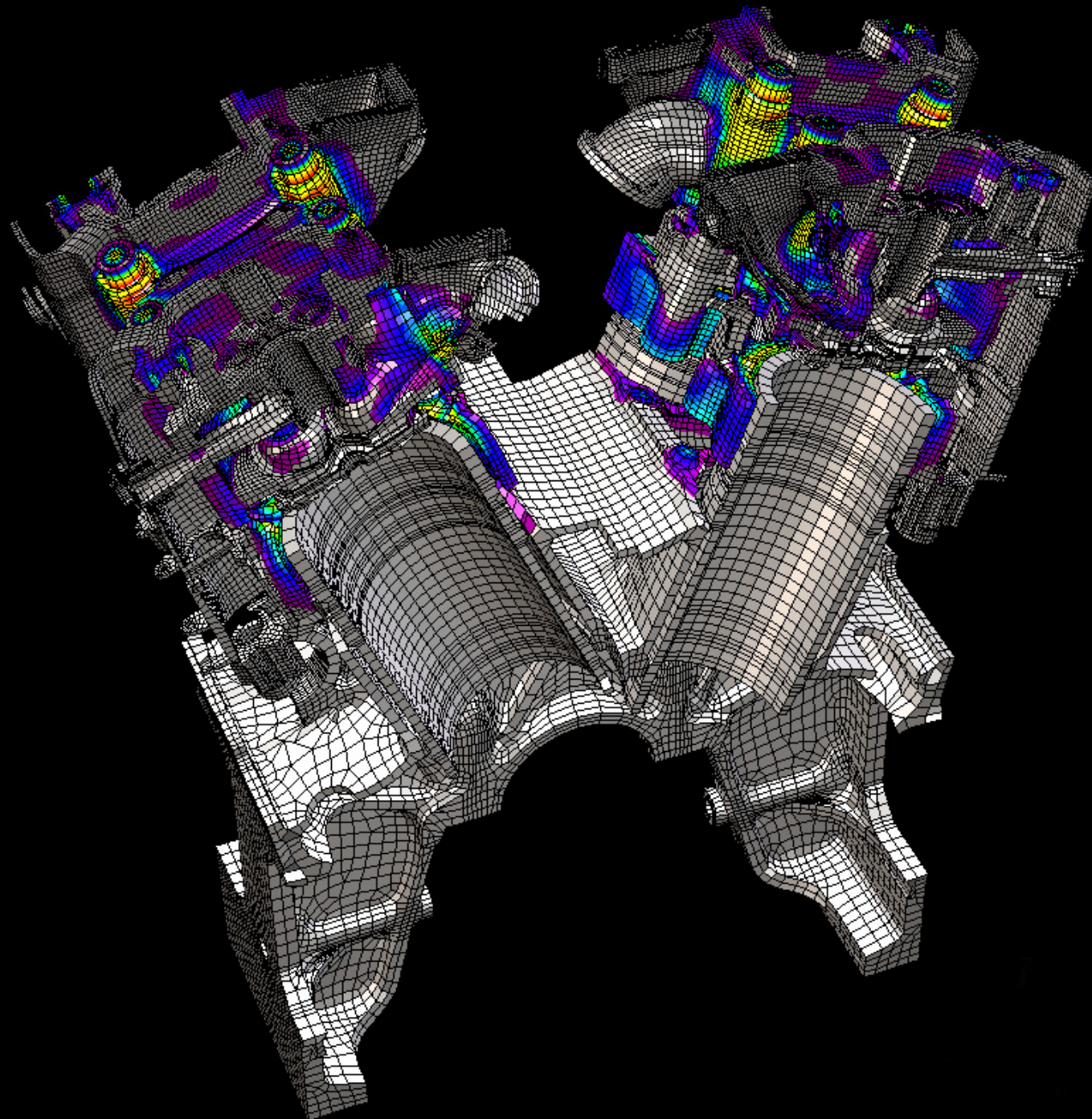
# ***Applications***

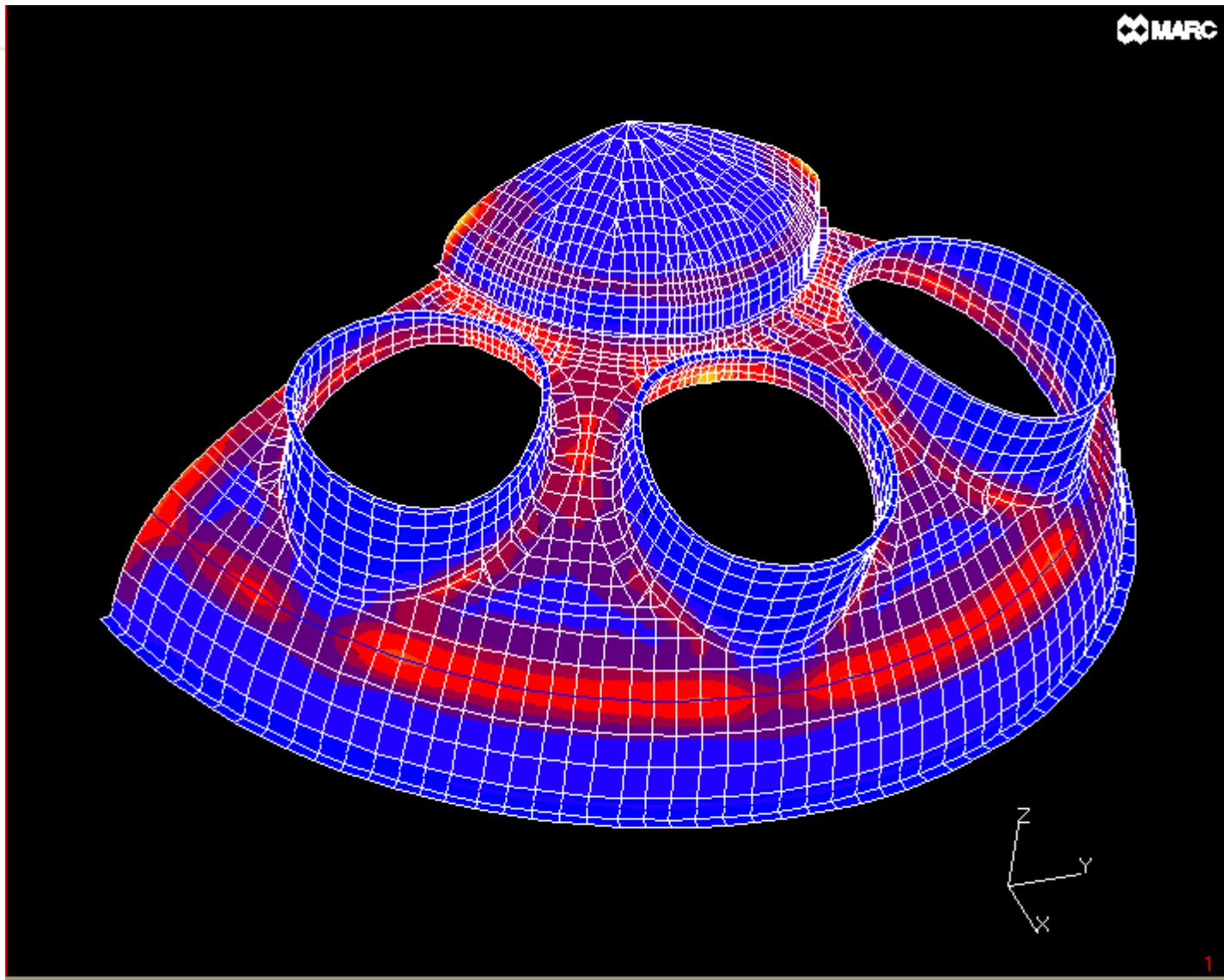
- **Energy Industry**
- **Engines (Gas Turbine, Diesel, Automotive)**
- **Rockets**
- **Electronics**
- **Fire Safety**
- **Manufacturing**
- **Welding**



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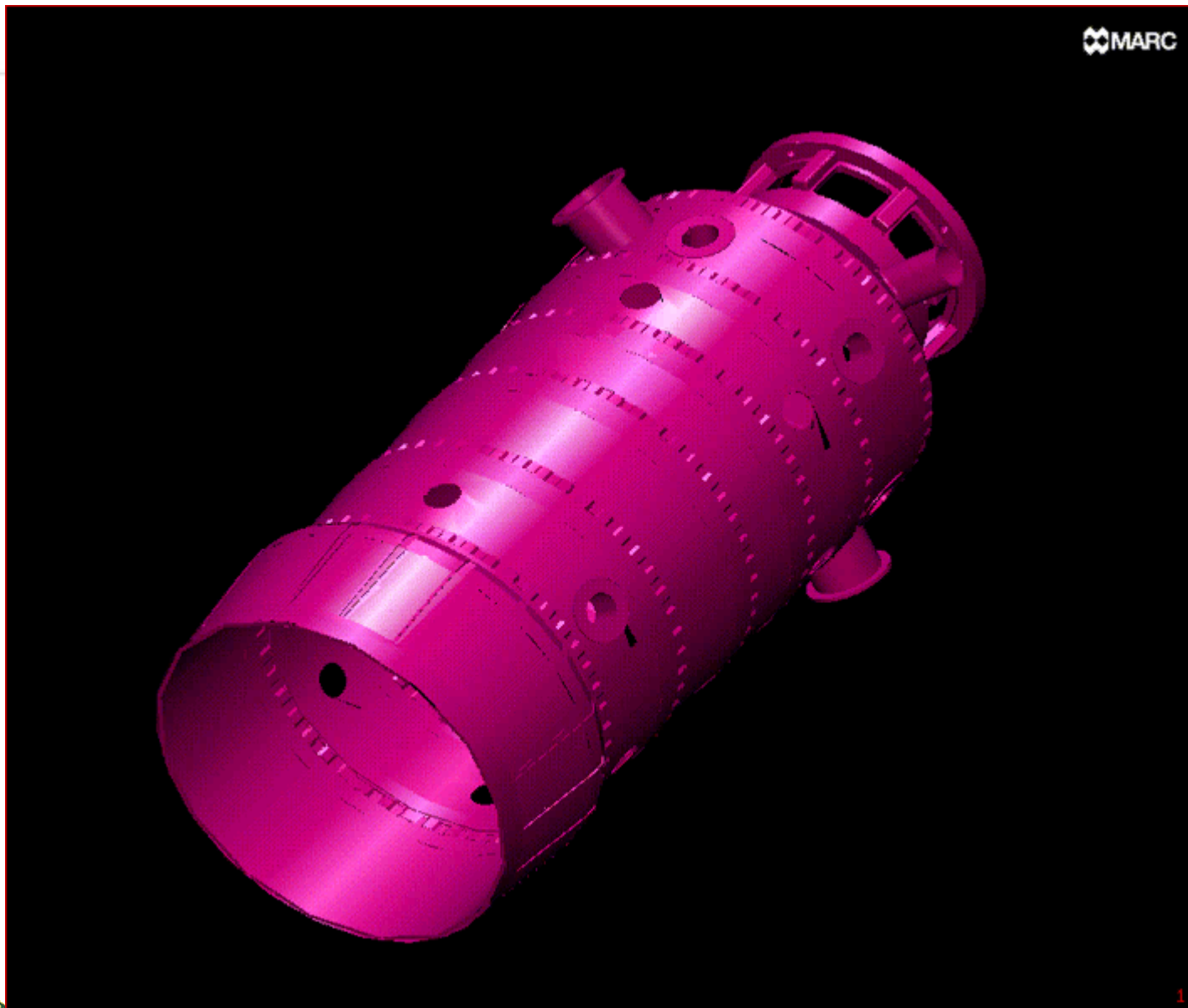




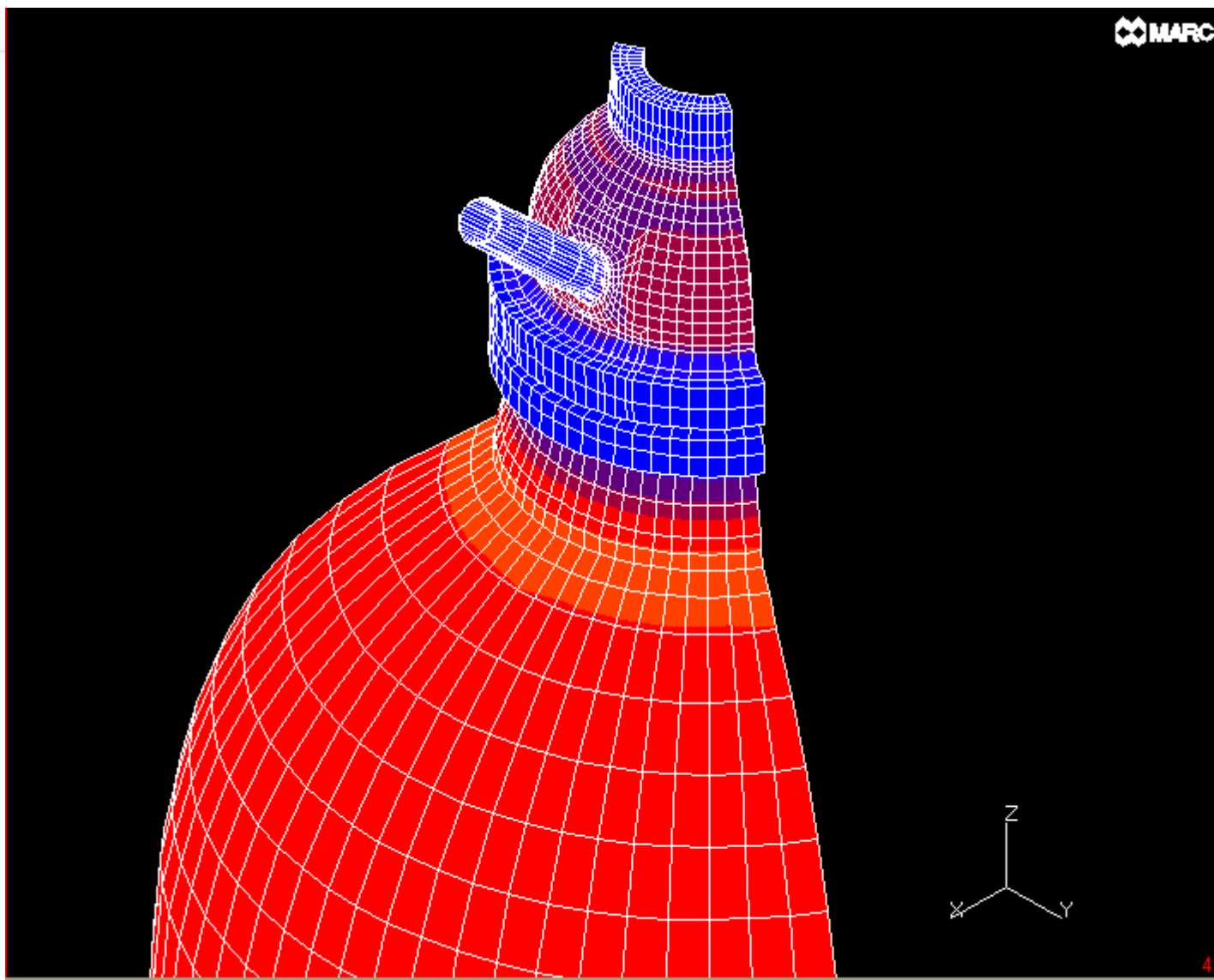
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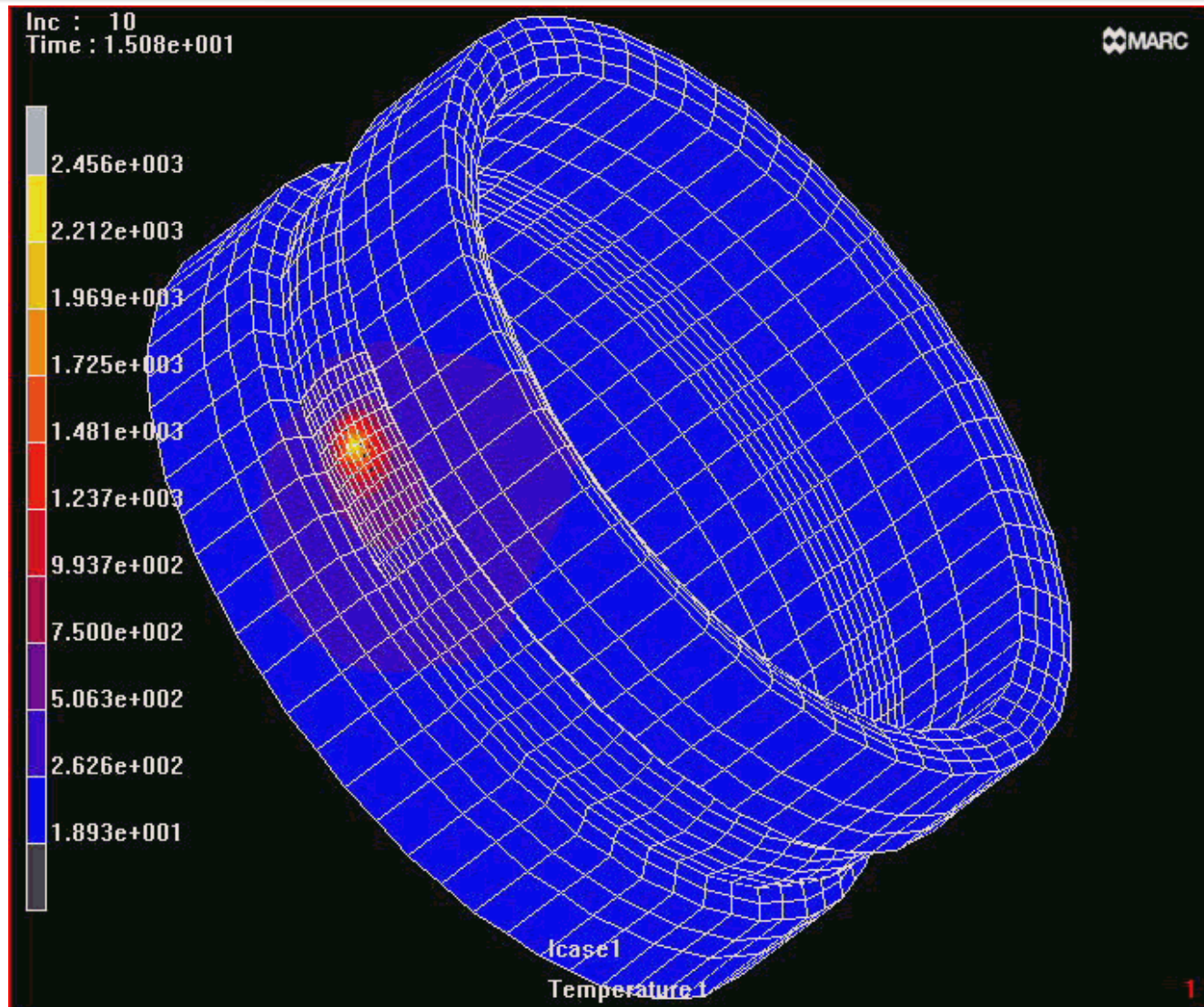


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# Welding Simulation



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# ***Channel***

- **Special Modeling techniques to represent fluid flow in channels**
- **Special modeling techniques to model convection and radiation across small gaps.**



# ***Computationally Efficient Solution Methods***

- **Direct Sparse Solvers**
- **Iterative Solvers**
- **Parallel Processing using Domain Decomposition**



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# ***Turbine Blade Structural Analysis***

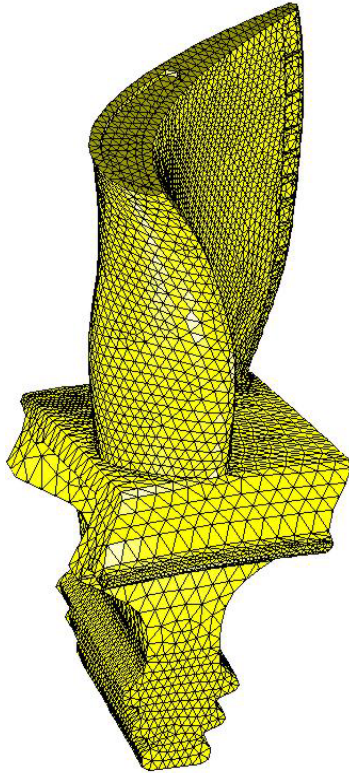
- **Number of Domains: 4**
- **Number of Elements: 72K**
- **Degrees of Freedom: 55K**
- **Scaling: 4.2X**



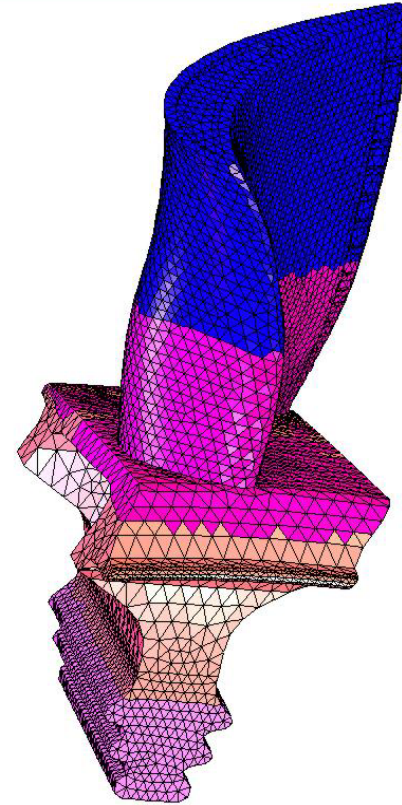
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# ***Turbine Blade Structural Analysis***



1



1



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# ***Thermal Contact***

- If  $\text{dist} < d1$  then thermal conduction
- If  $d1 < \text{dist} < d2$  then simplified thermal radiation
- If  $d2 < \text{dist}$  then no contact



# *Near Contact*

- Convection
  - Natural convection
  - Radiation
  - Distance dependent convection
- 
- $Q = hcv*(T2-T1)+hnt*(T2-T1)ent +$
  - $\sigma*eps*(T2^4-T1^4) +$
  - $(hct - (hct-hbl)*gap/dqnear)*(T2-T1)$



# ***Thermal Contact Input***

- **Hct** – contact thermal coefficient
- **Hcve** – environment thermal coefficient
- **Tsink** – sink temperature
- **Hcv** – near convective coefficient
- **Hnc** – near natural convection coefficient
- **Bnc** – exponent for natural convection
- **Em** – emissivity
- **Hbl** – lower limit of distance dependent convection coeff
- **Dqnear** – distance below which near thermal behavior is applied



# ***Coupled Joule Heating***

- **Weak coupling between mechanical, thermal, and electrical fields**
- **Typical application: high voltage electrical switch**
- **Electronic circuits**



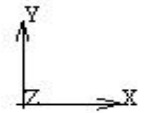
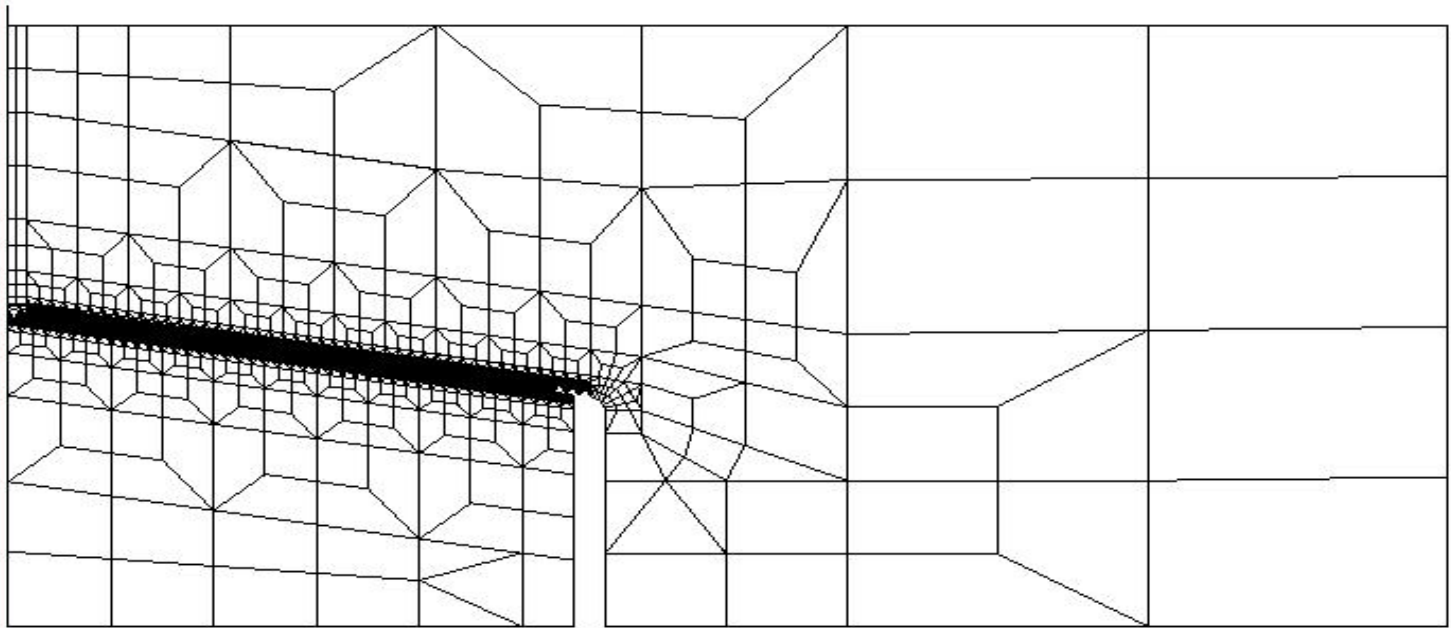
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# High Voltage Device

Inc: 0  
Time: 0.000e+000

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Joint with Differential Taper

1

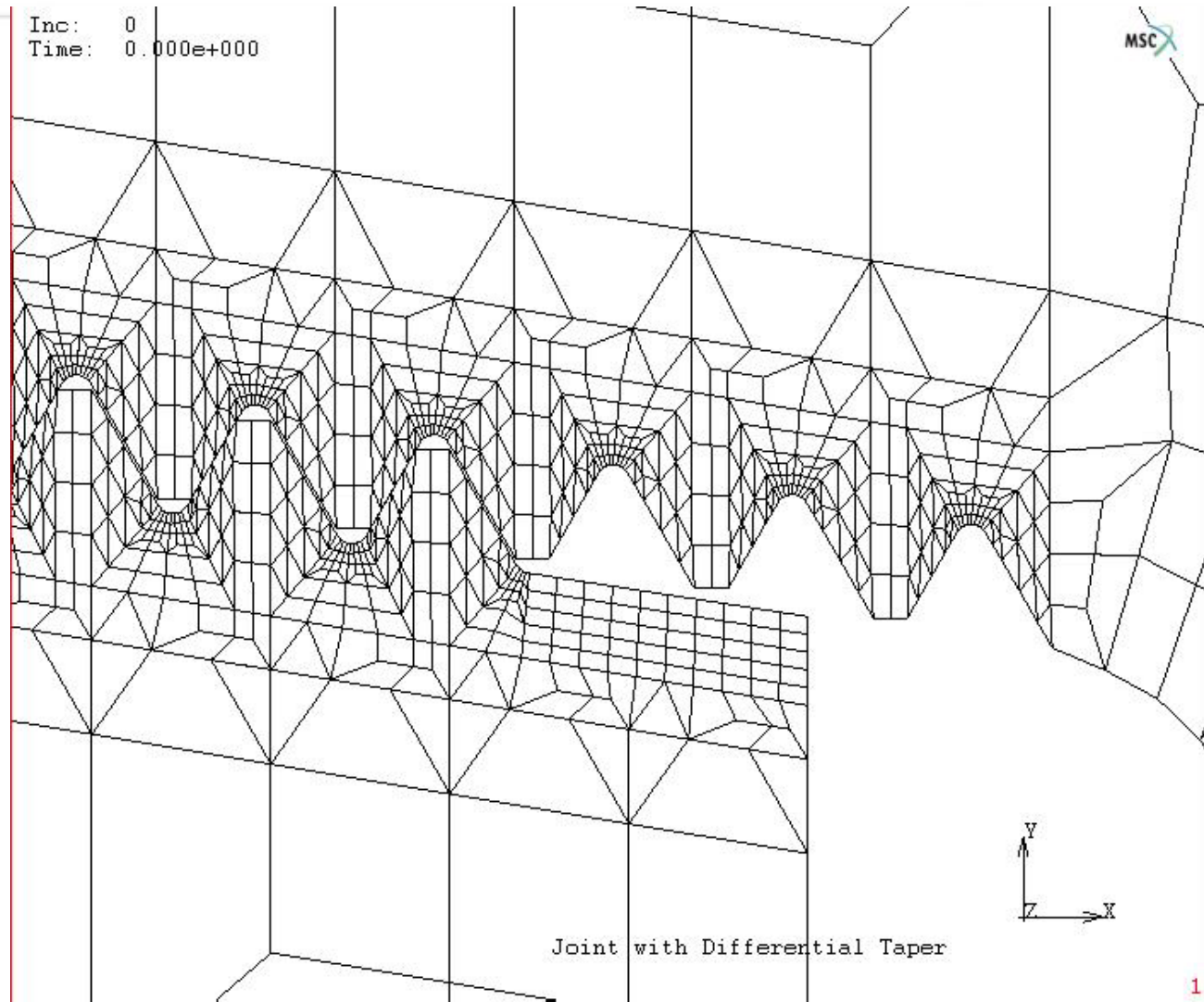


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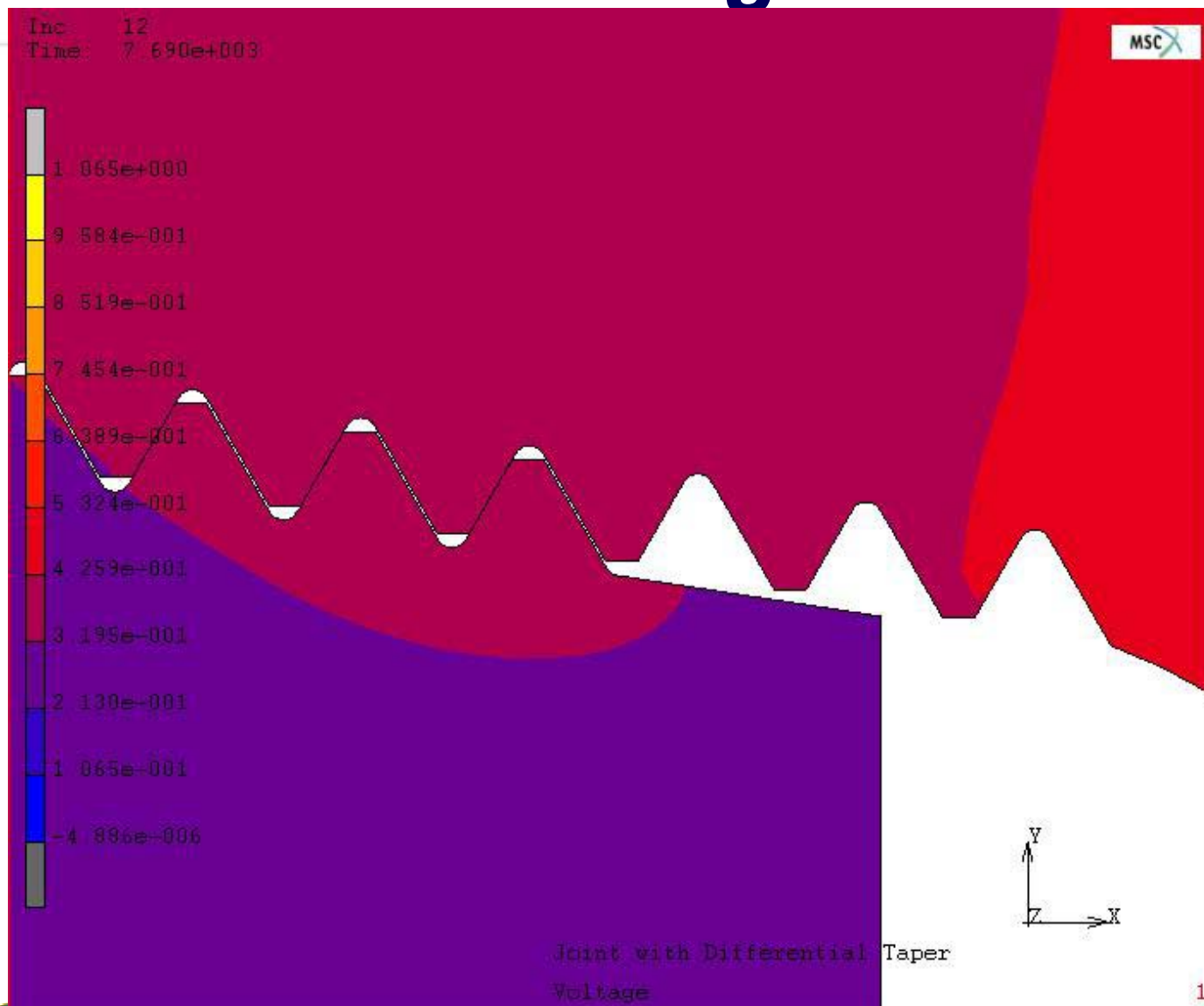
# Close up of Threads



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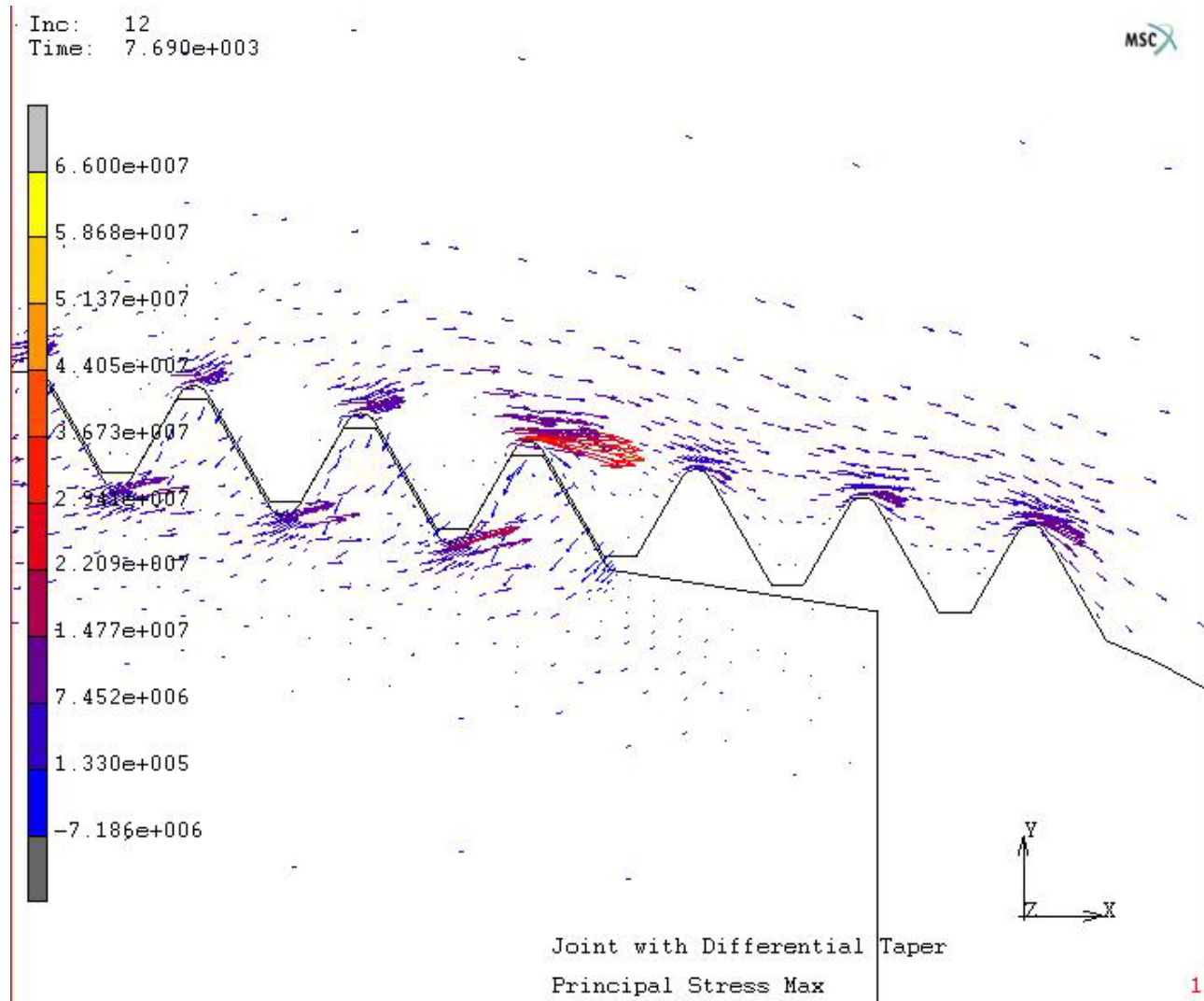
# Voltage



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# Induced Stress Due to Contact and Thermal Strains



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# ***Fluid – Thermal Analysis***

- **Navier Stokes Finite Element Procedure Used**
- **Tightly Coupled Analysis**
- **Incompressible Fluid**
- **Laminar Flow**
- **Newtonian or Non-Newtonian Fluid**
- **2D or 3D fluid flow with any type of element**
- **Forced or Free Convection**



# ***Fluid-Thermal Applications***

- **Electronic Packaging**
- **Quenching**
- **Fuel Cells**

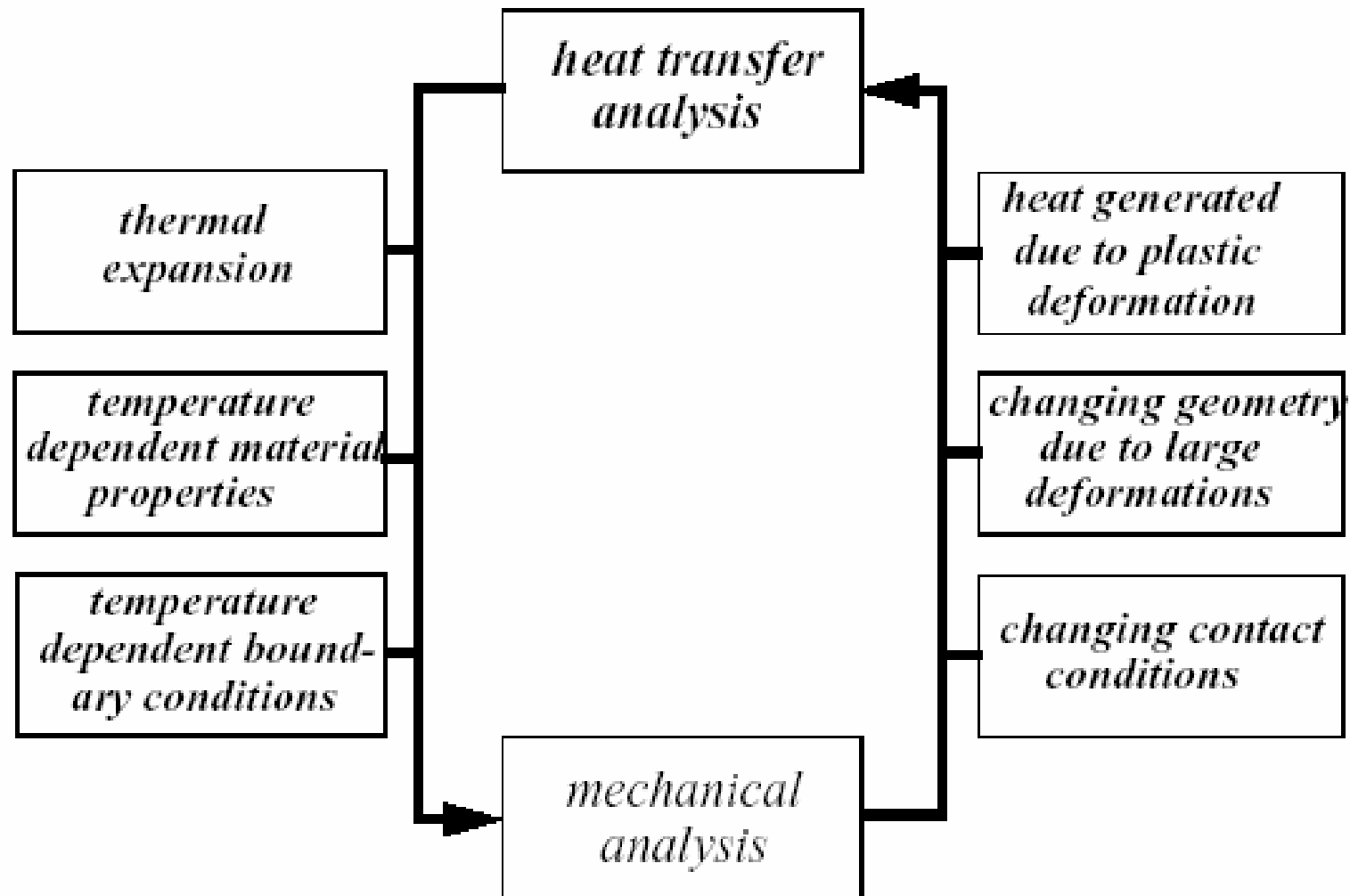


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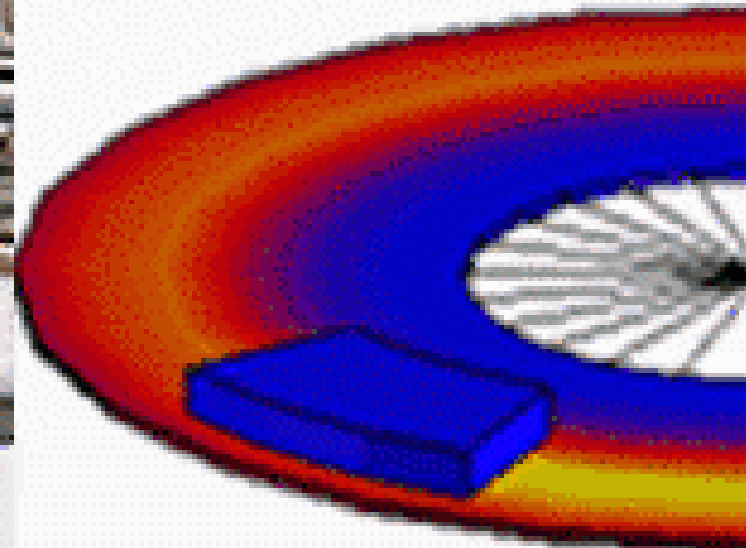


# Coupled Thermal Stress



# ***Disc Brake***

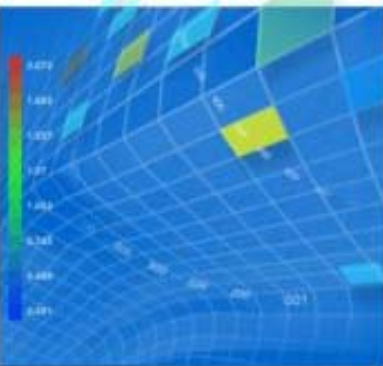
## **Disc Brake Dynamics Coupled Contact**



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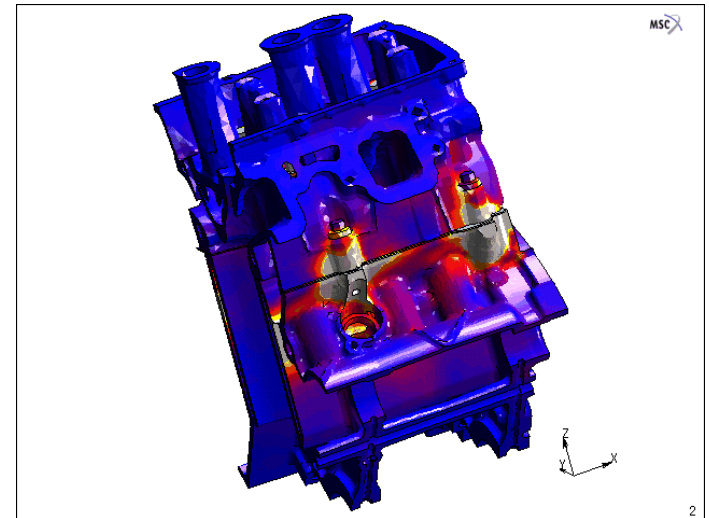
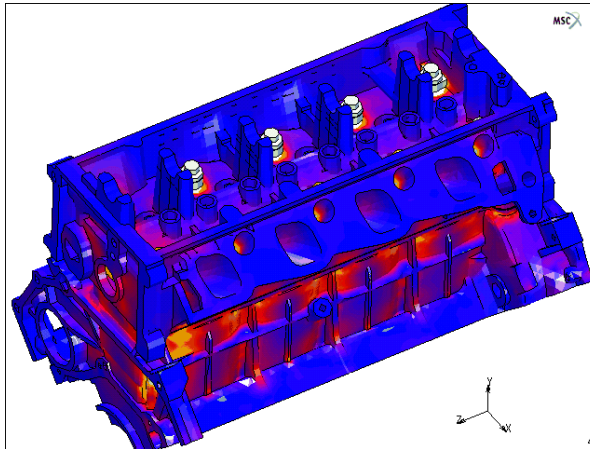
# ***Parallelization***



# Super Scalable Parallel

Number Of CPU's	1	2	4
CPU Time (sec)	6429	2491	1128
Speedup	1.0	2.6	5.7

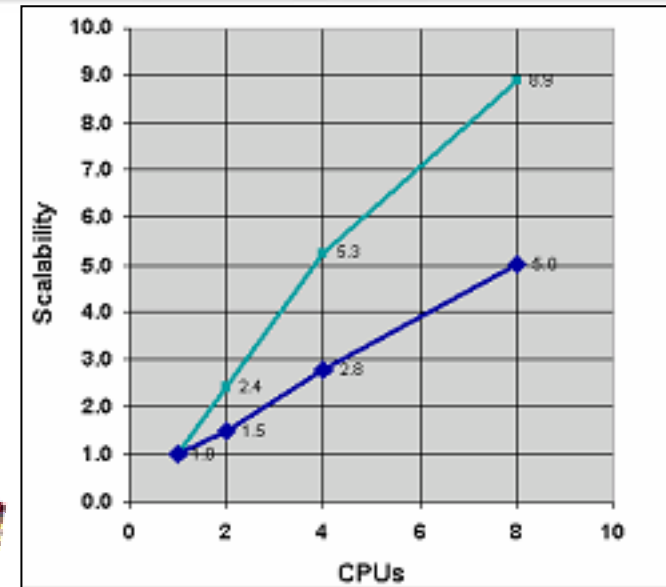
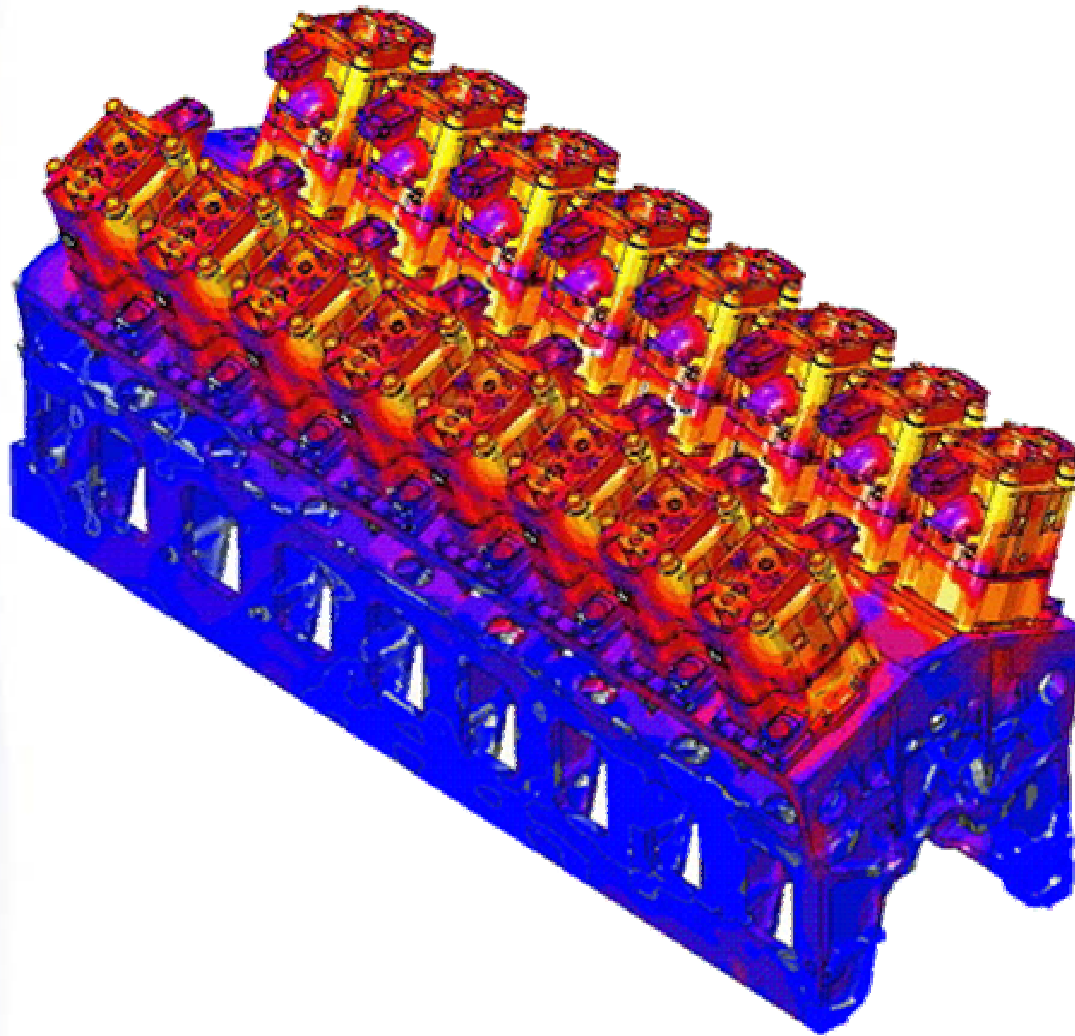
Linux cluster of 4 HP workstation xL-class  
with two of Intel's® Pentium® III 1GHz  
processors and 4GB of RAM/CPU



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# Parallel for Engine Assemblies

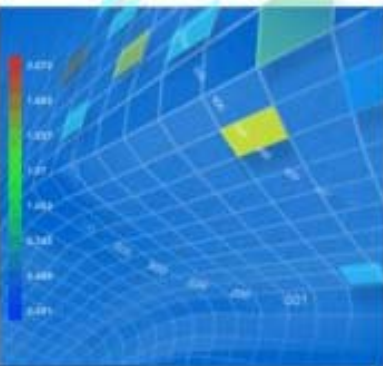


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# *Fluids*



# ***MSC.Marc Volume E: Fluid Demonstration Problems***

- 9.1 Planar Couette Flow, 9.1-1
- 9.2 Poiseuille Flow, 9.2-1
- 9.3 Fluid Squeezed Between Two Long Plates, 9.3-1
- 9.4 Driven Cavity Flow, 9.4-1
- 9.5 Flow Past a Circular Cylinder, 9.5-1
- 9.6 Flow Over Electronic Chip, 9.6-1
- 9.7 Natural Convection, 9.7-1
- 9.8 Flow Around Tubes, 9.8-1



# Plot of the Couette Flow Velocity Field

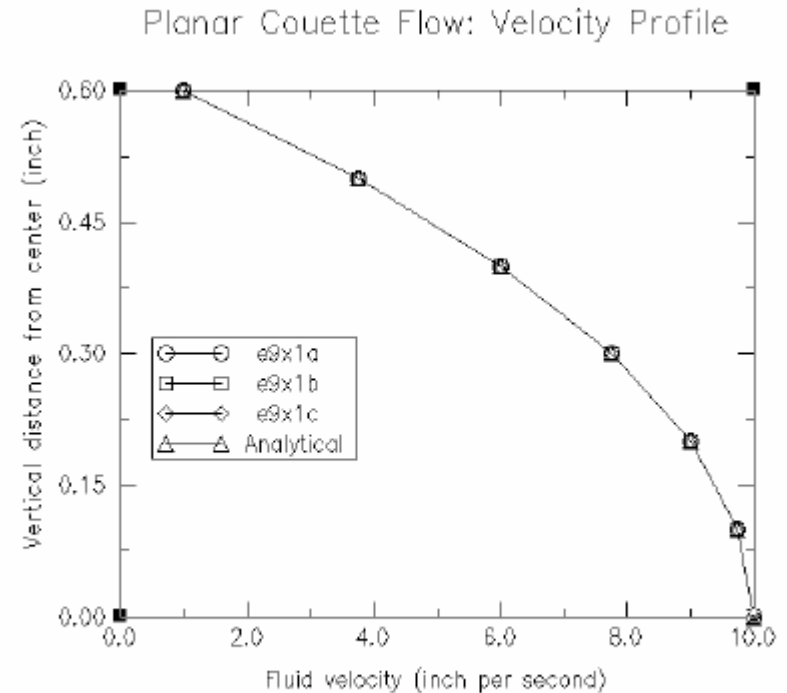
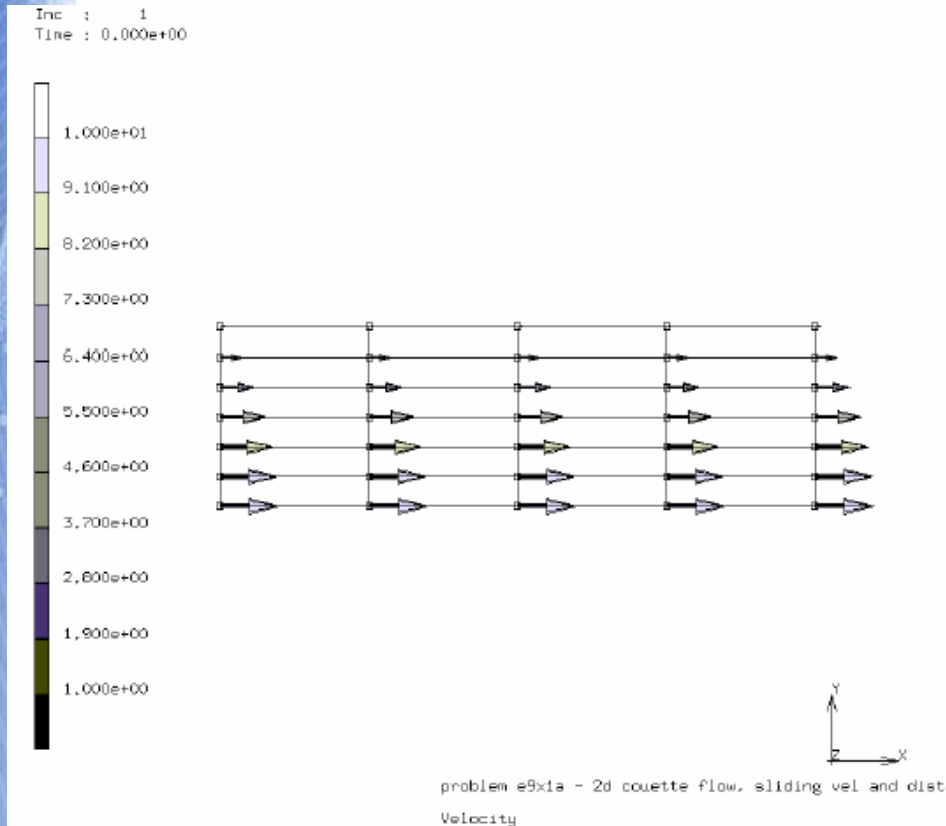


Figure 9.1-4 Comparison of Computation and Analytical Results



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# Plot of the Poiseuille Flow Velocity Field

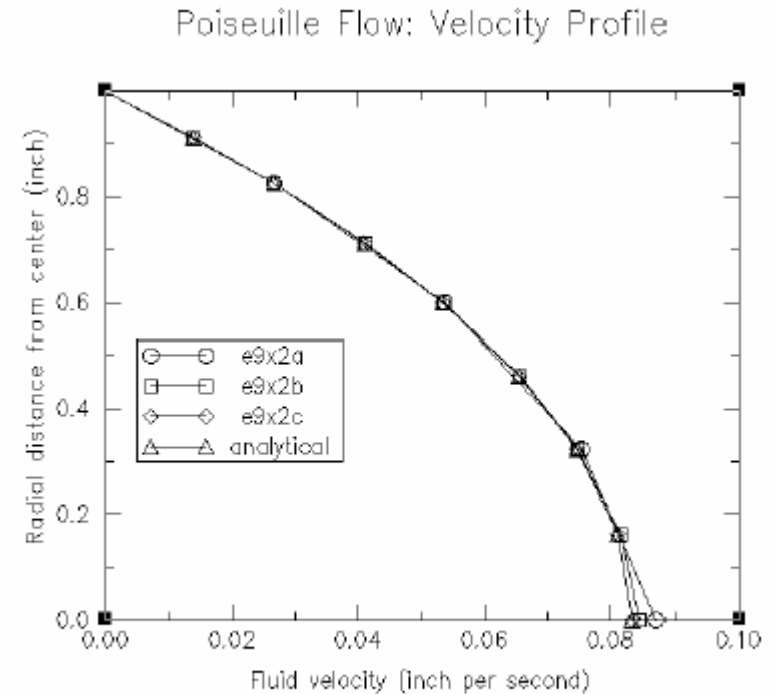
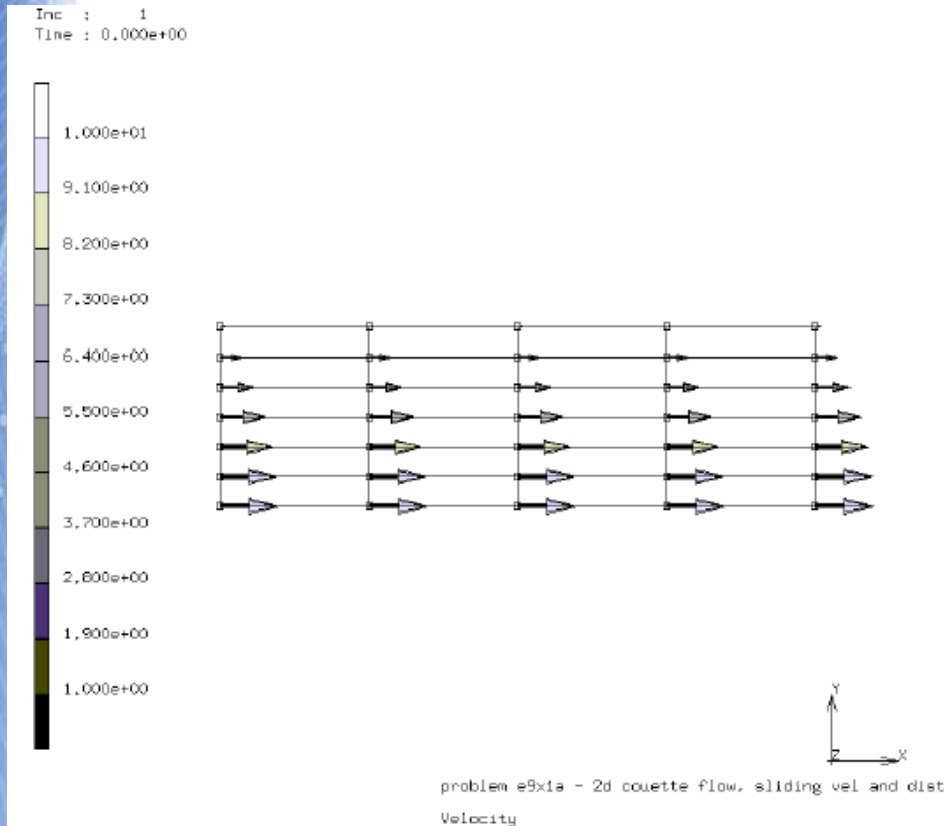


Figure 9.2-4 Comparison of Computation and Analytical Results



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# Fluid Squeezed Between Two Long Plates

Inc: 1  
Time: 0.000e+00



blem e9x3a: 2D fluid squeezed between plates, element type  
Velocity



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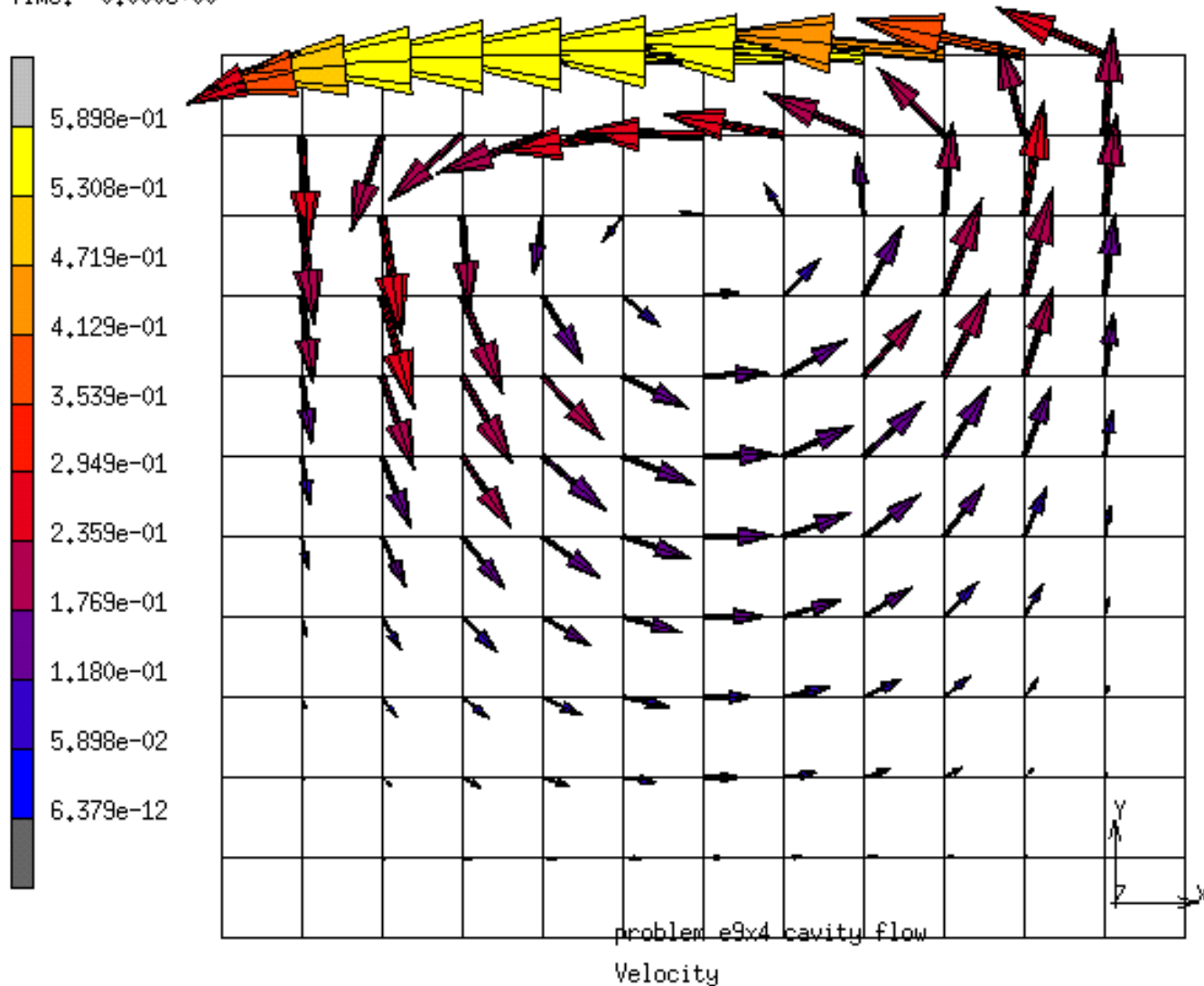
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# Vector Plot: Driven Cavity Flow Velocity Field

Inc: 1  
Time: 0.000e+00

MSC



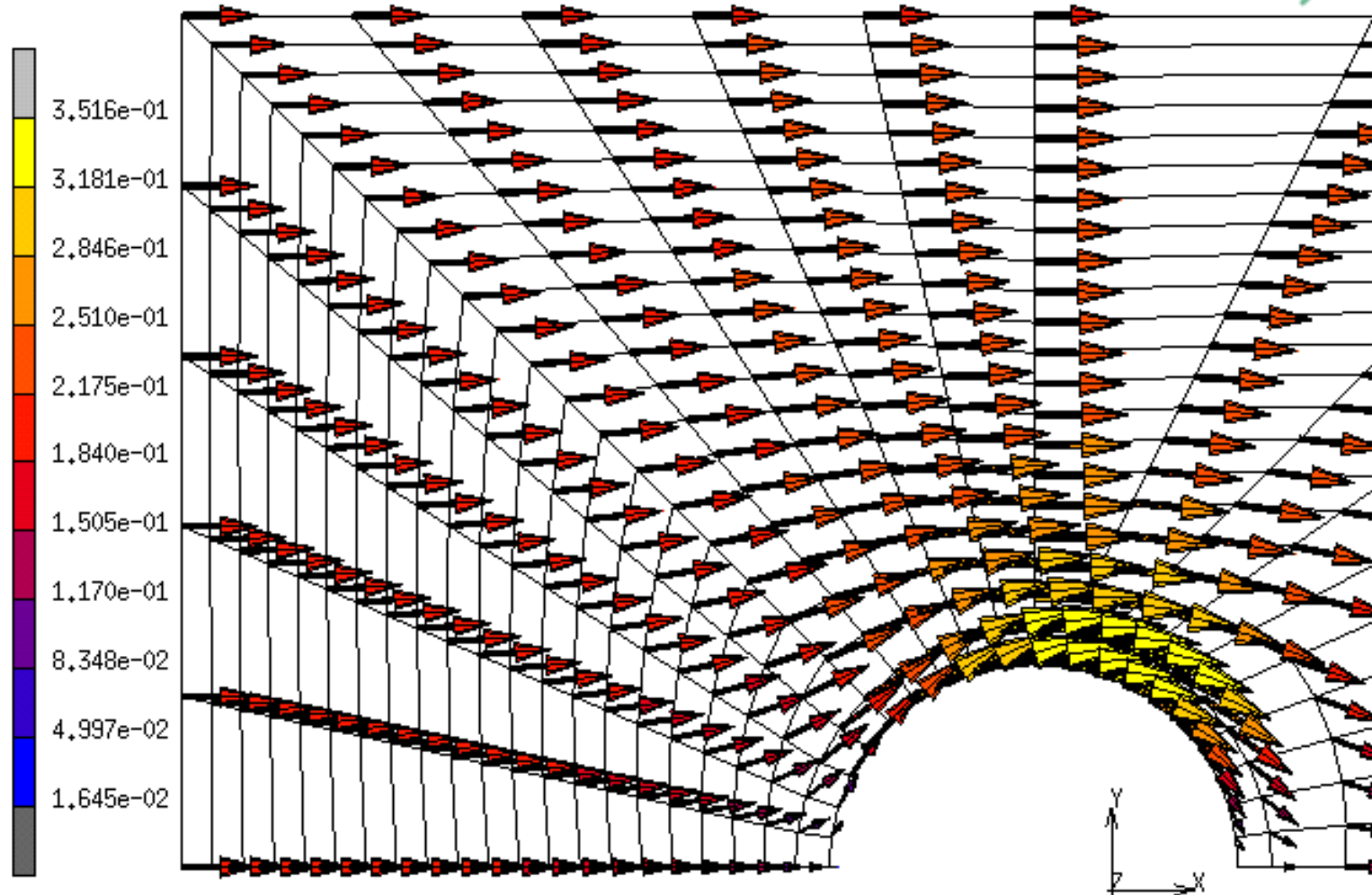
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# Flow Over Cylinder Transient Velocity Field

Inc: 10  
Time: 1.000e+00

MSC



e9x5e - fluid around a cylinder, no 3rd (P) B.C.  
Velocity

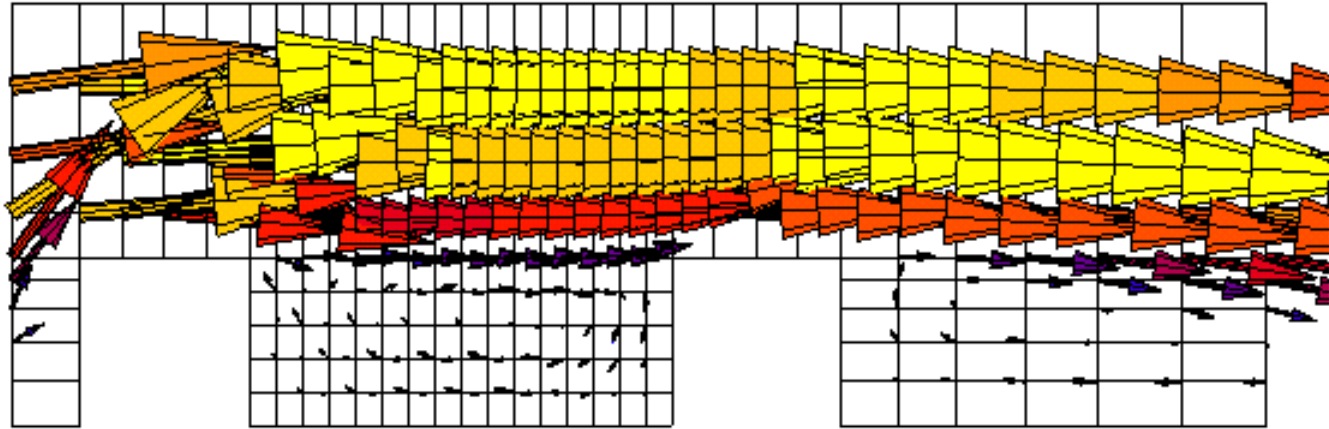


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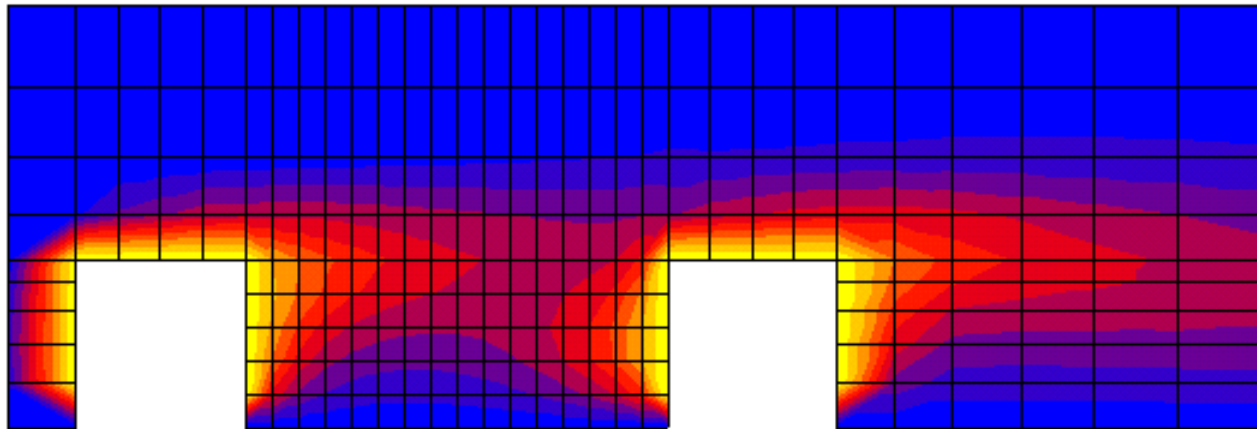
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# Flow Over Electronic Chip

Velocity Vector



Temperature

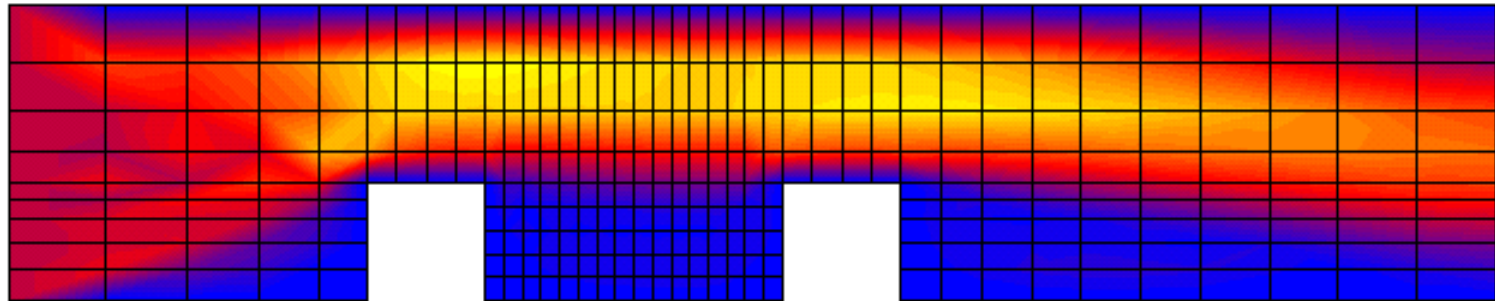


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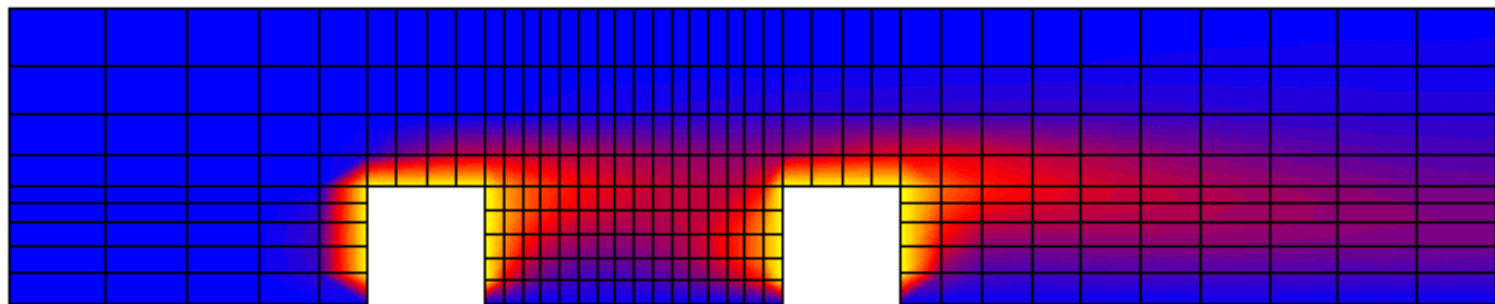
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# Flow Over Electronic Chip

Velocity Magnitude



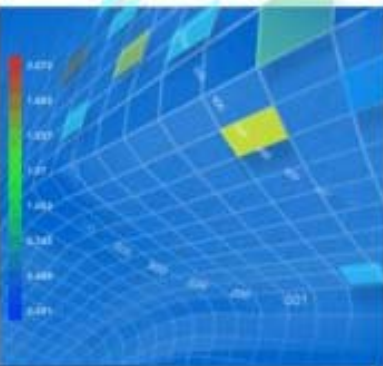
Temperature



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# ***User Subroutines***





# Over 100 User Subroutines

## Output Quantities Subroutines

User Subroutine	Required Parameters or Model Definition Options	Purpose
ELEVAR	UDUMP	Allows postprocessing of element results.
ELEVEC	UDUMP	Allows postprocessing of element results in harmonic analysis.
INTCRD		Makes available integration point coordinates.
IMPD	UDUMP	Allows postprocessing of nodal vector results.
PLOTV	POST	Defines element quantity to be written to post file.
UBGINS		Dummy routine available at the beginning of each increment.
UBGTR		Dummy routine available at the beginning of
UEDINC		
UELOOP		
UPOSTV	POST	

## Loads and Boundary Conditions Subroutines

User Subroutine	Required Parameters or Model Definition Options	Purpose
CREDE	THERMAL LOADS	Definition of state variable including temperature.
CUPLFX	COUPLE DIST FLUXES (flux type 101)	Heat generated due to inelastic behavior in coupled analysis.
DIGEOM	CONTACT (2D) CONTACT (3D)	Definition of rigid surface.
FILM	HEAT or COUPLE FILMS (Model Definition) FILMS (History Definition)	Definition of convective heat transfer coefficient and sink temperature.
FLOW	HEAT CHANNEL	Definition of mass flow rate.
FLUX	HEAT or COUPLE DIST FLUXES (Model Definition) DIST FLUXES (History Definition)	Definition of distributed flux.
FORCDF	FORCDT FIXED DISP or DISP CHANGE	Definition of point load or kinematic boundary condition in a harmonic analysis.



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# Example

```

c*****
      subroutine flux(f,ts,n,time)
c*****
      implicit real*8 (a-h,o-z)
c dimensions for FLUX subroutine
      dimension ts(6),n(7),thick(5)

c
c dimension of arrays for passing data to the Electrochemistry Module
c
      integer ncell,ngridx,ngridy,ngridair,ngridz,ivchange
      integer i,j,k,l,m,ivflag,iu,iv
      integer ngridzi(4),ivflag,nd,nfueltype,nspecies,iflowtype
      .....
c
c initialize parameters
      call ini_set(lxcell,lycell,ivflag,lair,lfuel,
& vtot,itot,ufuel,
& pin,iflowtype,nfueltype,ngridair,
& ncell,ngridx,ngridy,ngridz,nspecies,txyzn,qxyzn,pxyn,
& up,fuelvxn,tfuelxn,ap,thick,
& lzcell,airvn,tairn,tairxyn,tfuelxyn)

      nbhb = 999
      .....
c FOLLOWING SECTION CALCULATES INTEGRATION POINT TEMPERATURES
c
c Code is valid for any kind of problem where temperature at
c integration points is available
c Following code is set up for continuum elements (number of layers = 1)
c icode = 9 = temperatures at integration points
c
      layer = 1
      icode=9
c average temperatures for number of integration points per element
      ttl = 0.0
c nn= integration point number
      do nn=1,numip
          call elmvar(icode,m,nn,layer,var)
          tmp = var
          ttl = ttl + tmp
      enddo
      .....
c run EC code once per increment and update state variables
      call udf_qiv(ivflag,itot,vtot,ufuel,nd,ivpower,heattot,
& iflowtype,nfueltype,nspecies,
& lxcell,lycell,lzcell,

```

dp



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# ***Future Work***

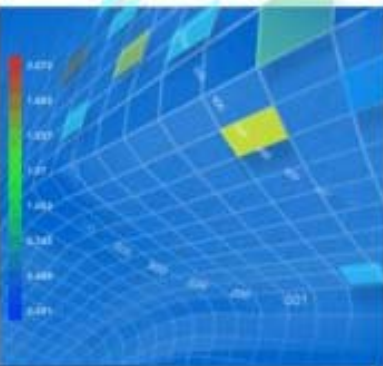
**On Fuel Cells**

# ***Proposed Development***

- **To develop a customized graphical user interface for fuel cell stacks.**
- **To integrate an EC module currently used by PNNL into MSC.Marc to be able to analyze the thermal stresses arising as a consequence of the heat production due to chemical reaction in the fuel cell and heat transfer due to convection effects.**
- **To conduct a feasibility study of the accuracy and efficiency of MSC.Marc for simulating flow fields in a typical fuel cell stack and to use the results of this feasibility study to determine areas of possible improvement in MSC.Marc's fluid capabilities.**



# ***PEN Fuel Cell Modeling***



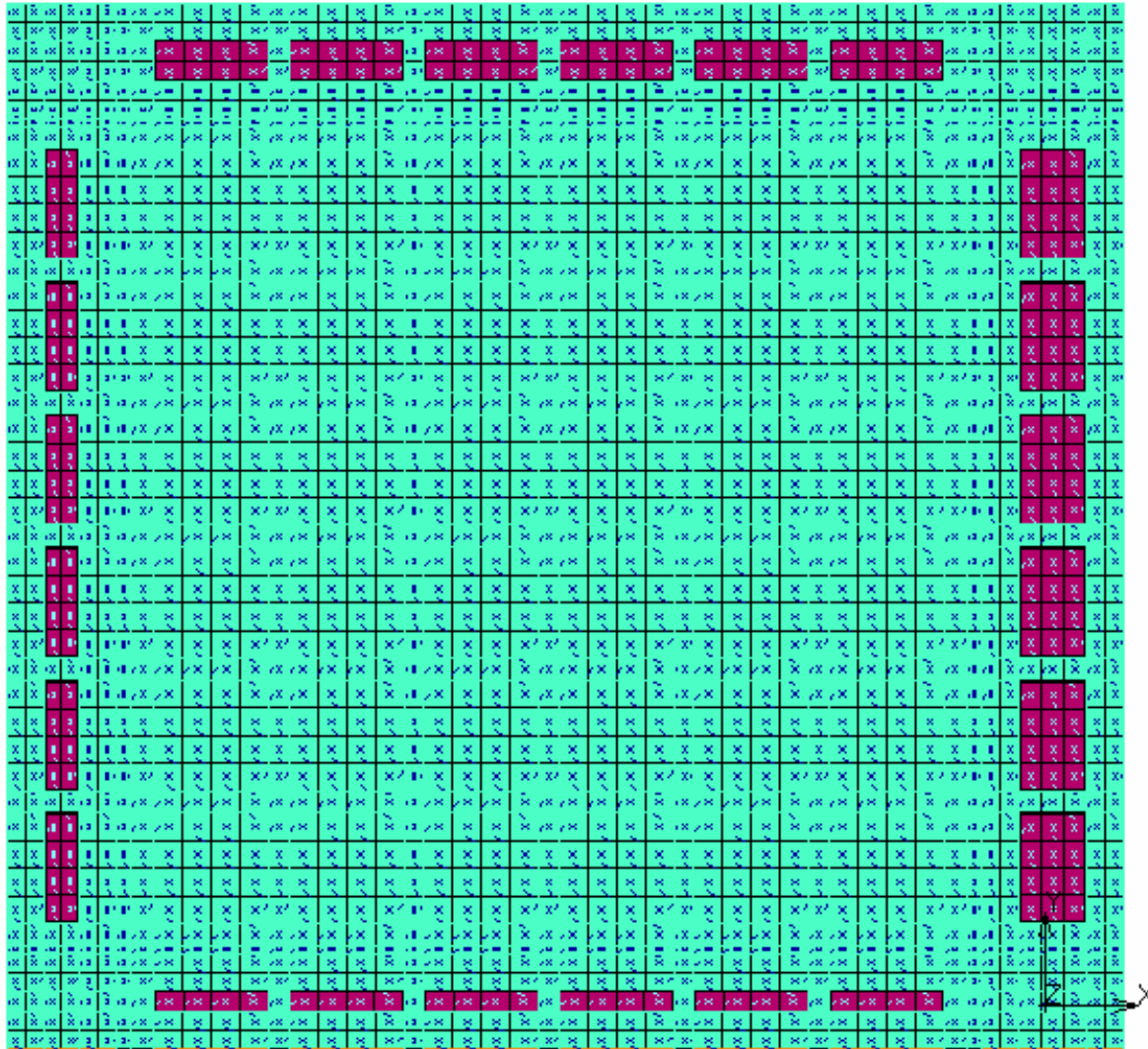


# ***Fuel Cell Layer Configuration***

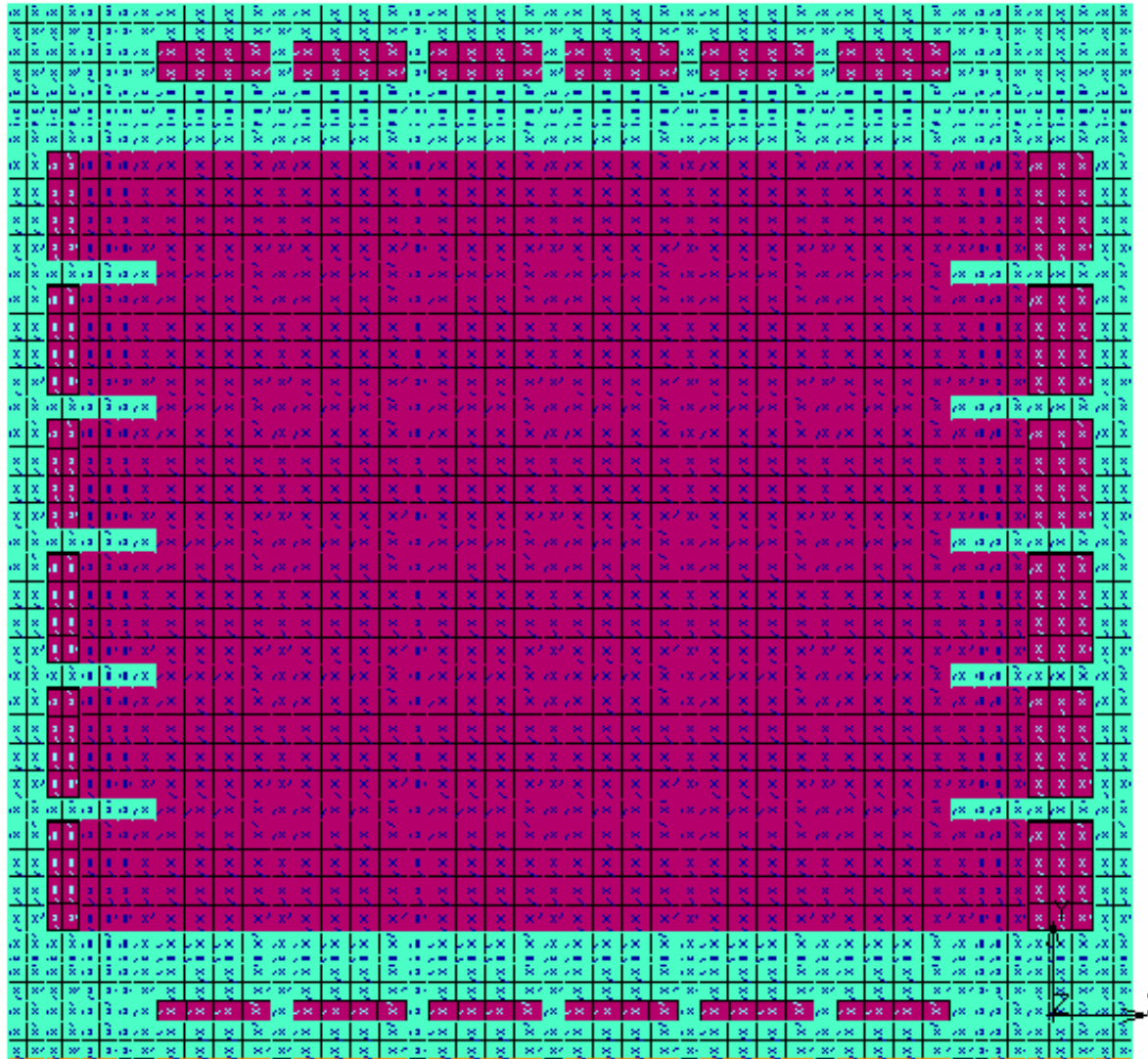
- The following slides show the layers of a typical planar fuel cell design.
- In the example design, the layers stack up to make up air and fuel flow channels on each side of the PEN.
- The PEN has 3 layers, Cathode (air-side), Electrolyte, and Anode (fuel-side). The center area (inside where the PEN seals to the picture-frame) is where the electrochemistry occurs.
- The following slides show “footprints” of the various layers (the selected areas show in the blue-green color).
- The layers are listed in the order from the interconnect (conductive layer between stacked cells), to the cathode-side layers, the PEN, anode-side layers, to the interconnect on the anode-side.
- The last 2 slides show the layers from bottom (cathode) and top (anode) views with the interconnect layers removed.
- The flow/ heat transfer/EC/stress model must have the necessary connectivity through all these layers, including through the flow channels where no mesh is shown in the last 2 slides.



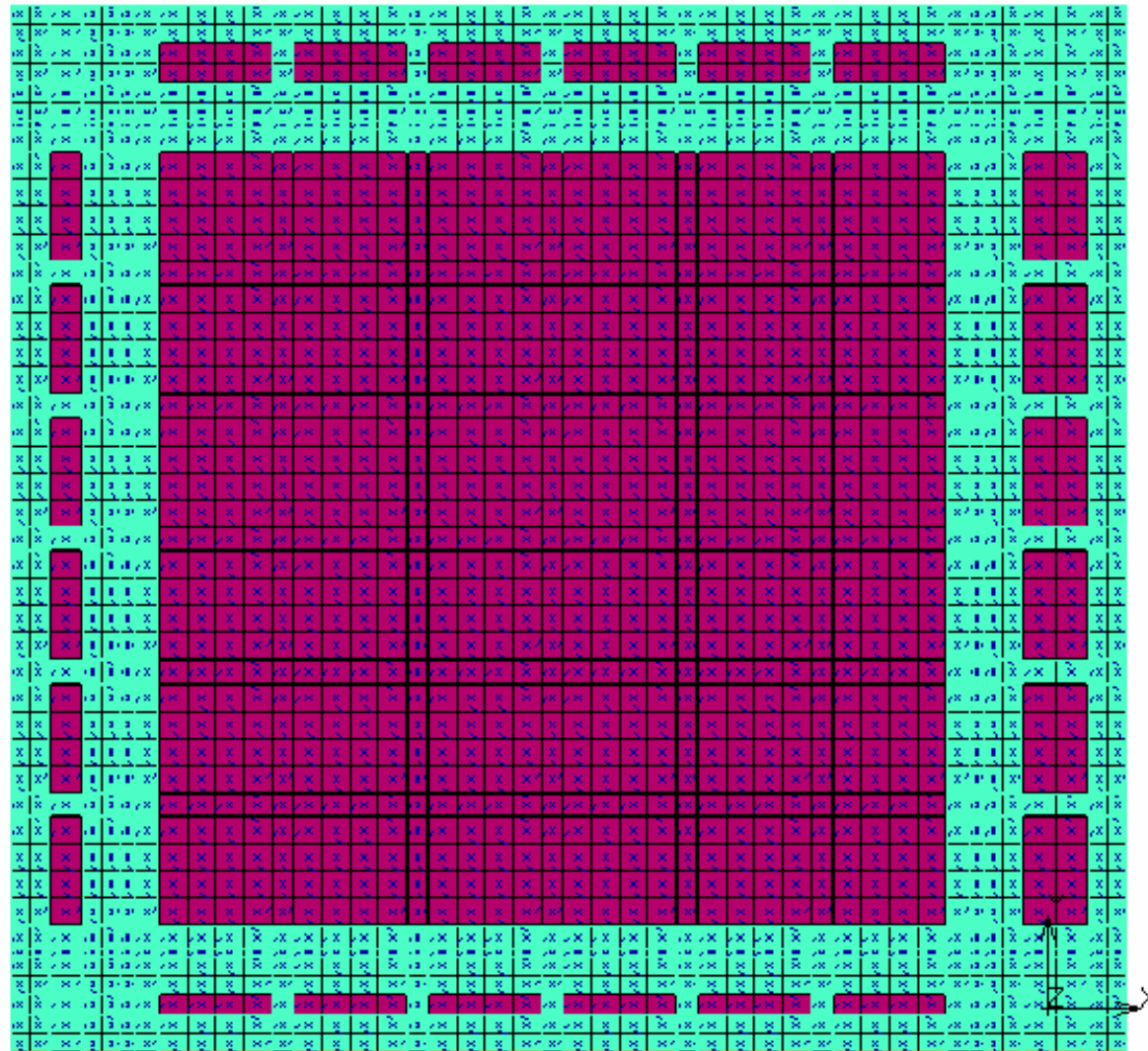
# Interconnect



# Cathode Spacer



# Picture Frame

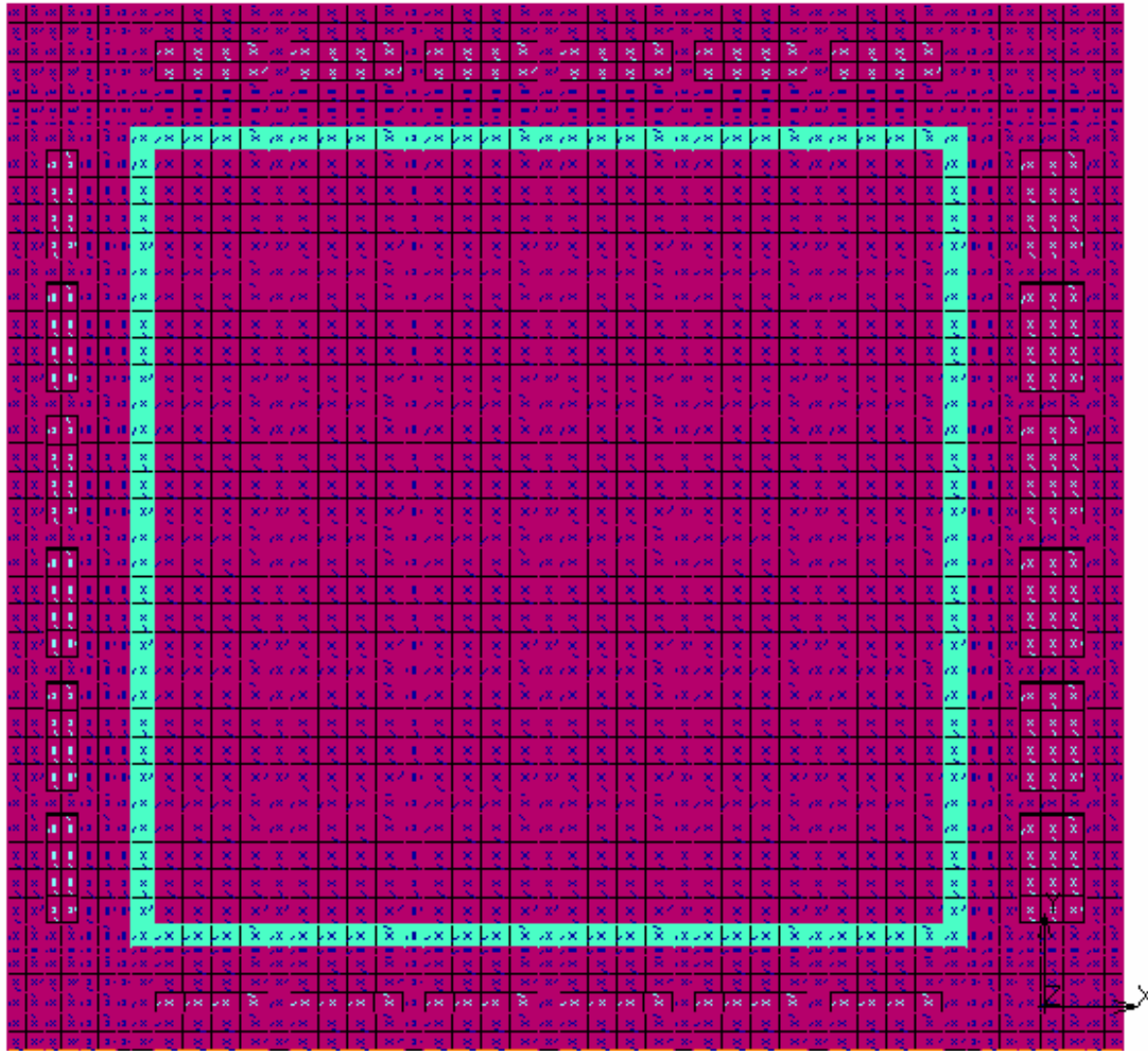


1





# PEN Inactive Area



Pen  
Inactive  
Area,

Pen-to-  
Picture  
frame  
Seal

(both same  
Footprint)

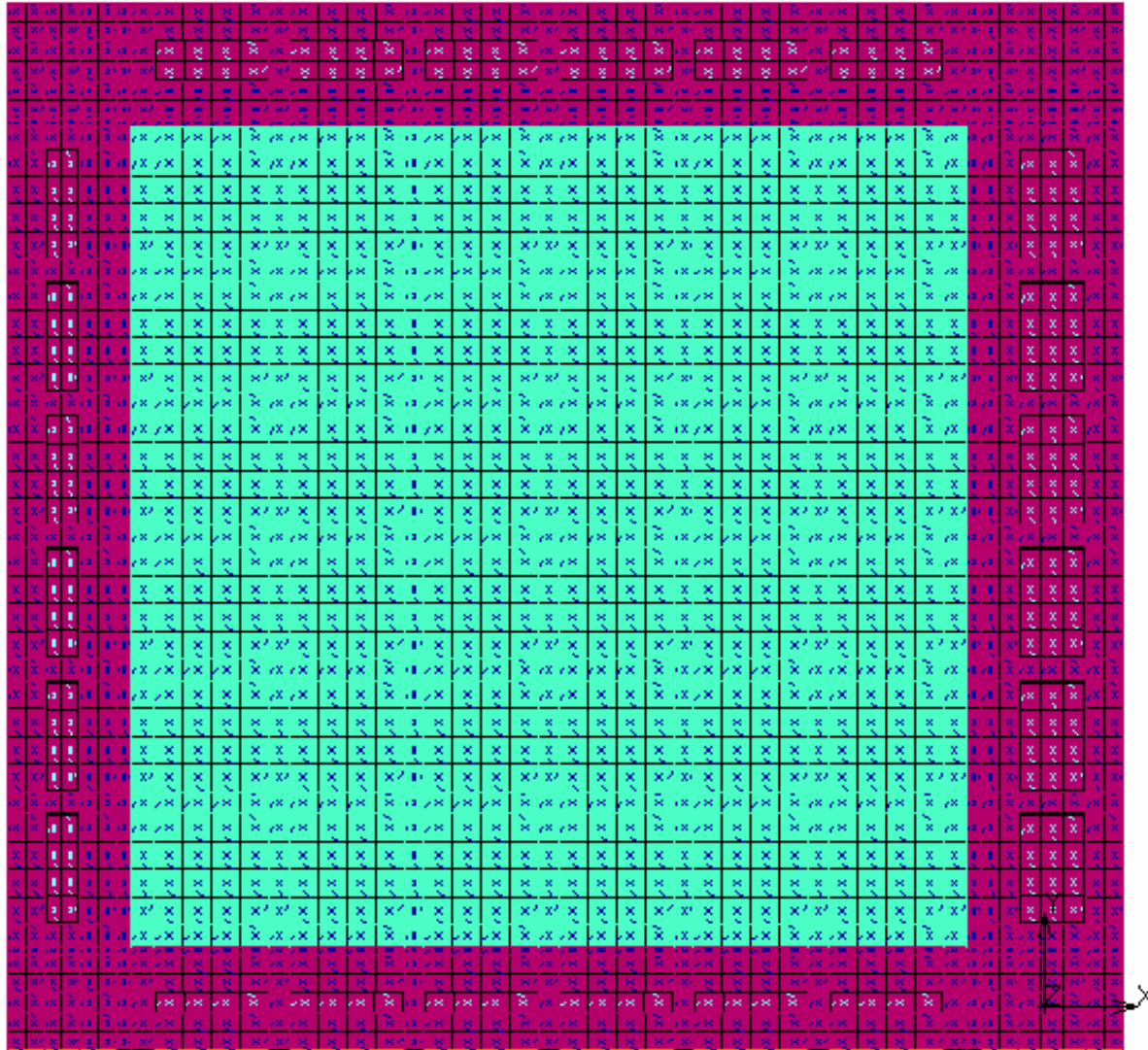


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# PEN



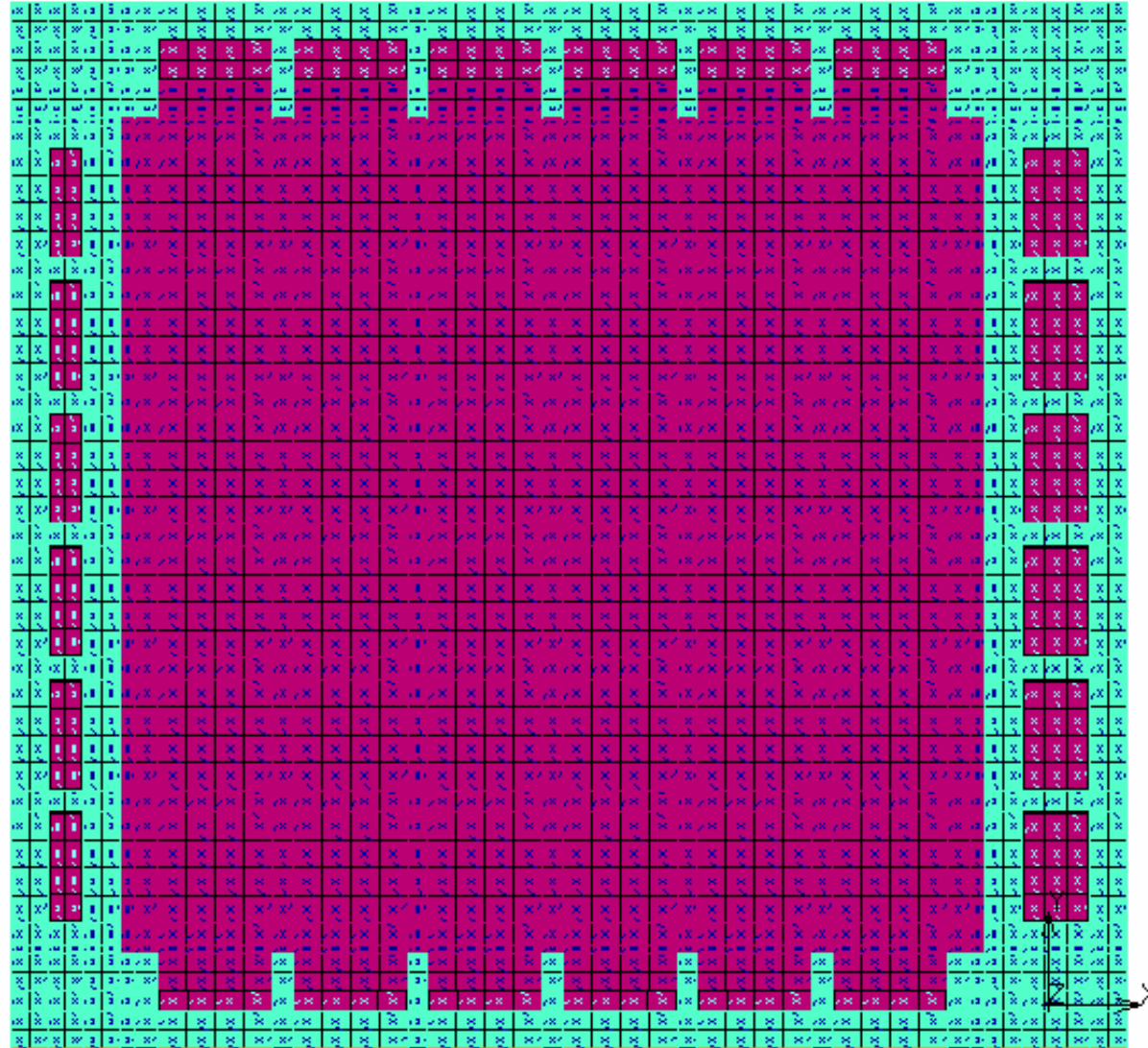
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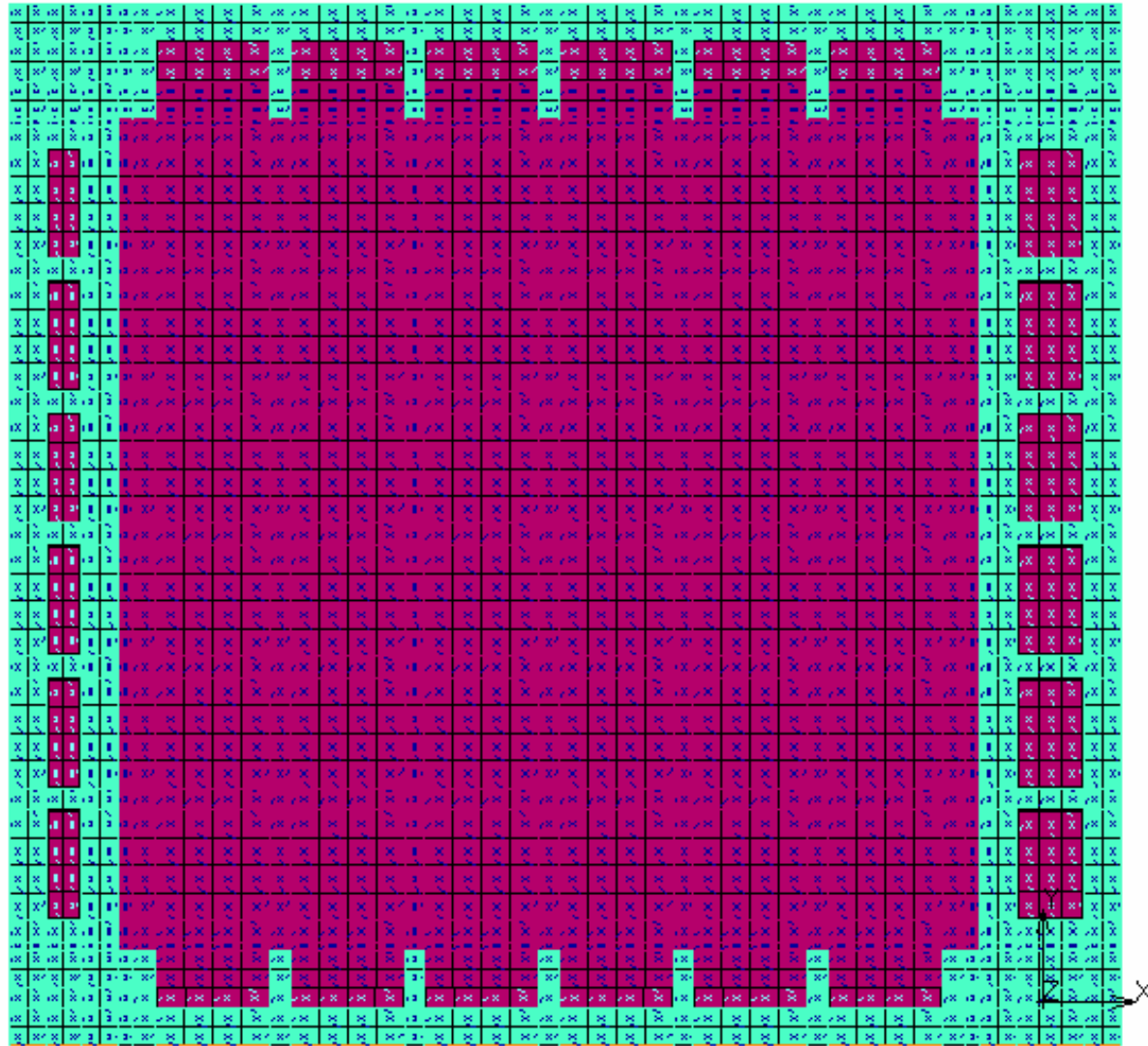
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# Anode Spacer



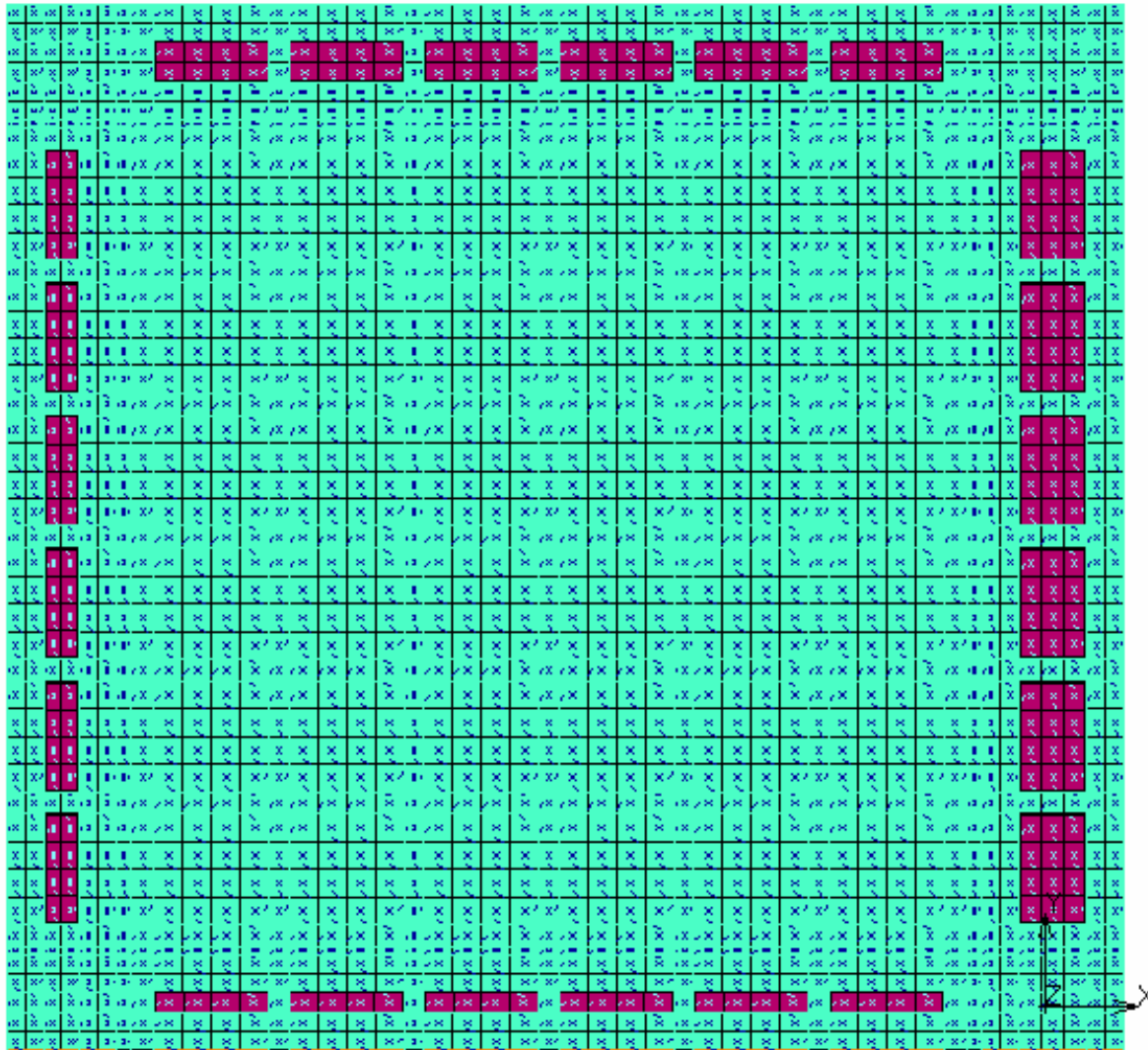
# Seal to Interconnect



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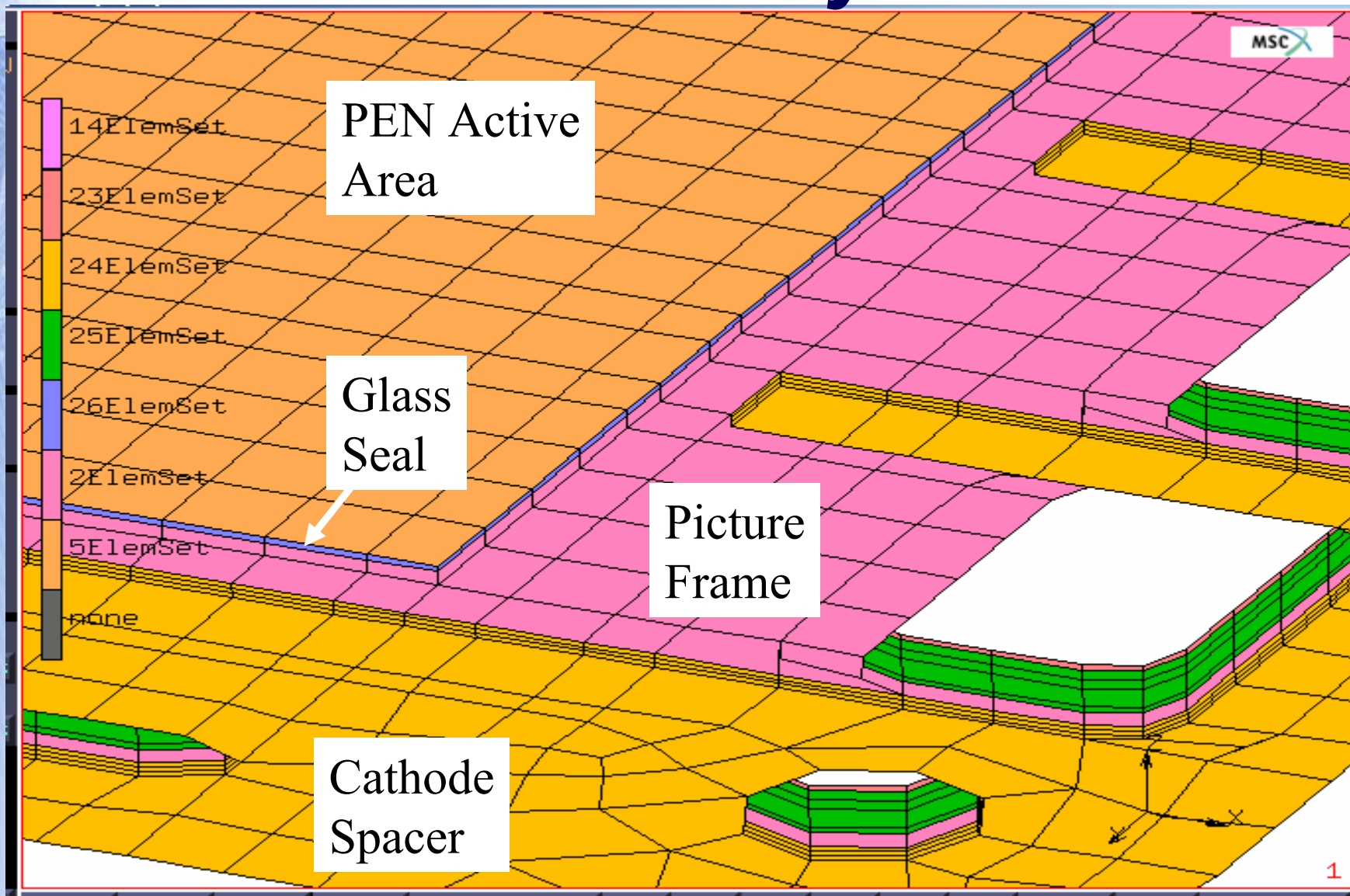


# Interconnect





# Assembly

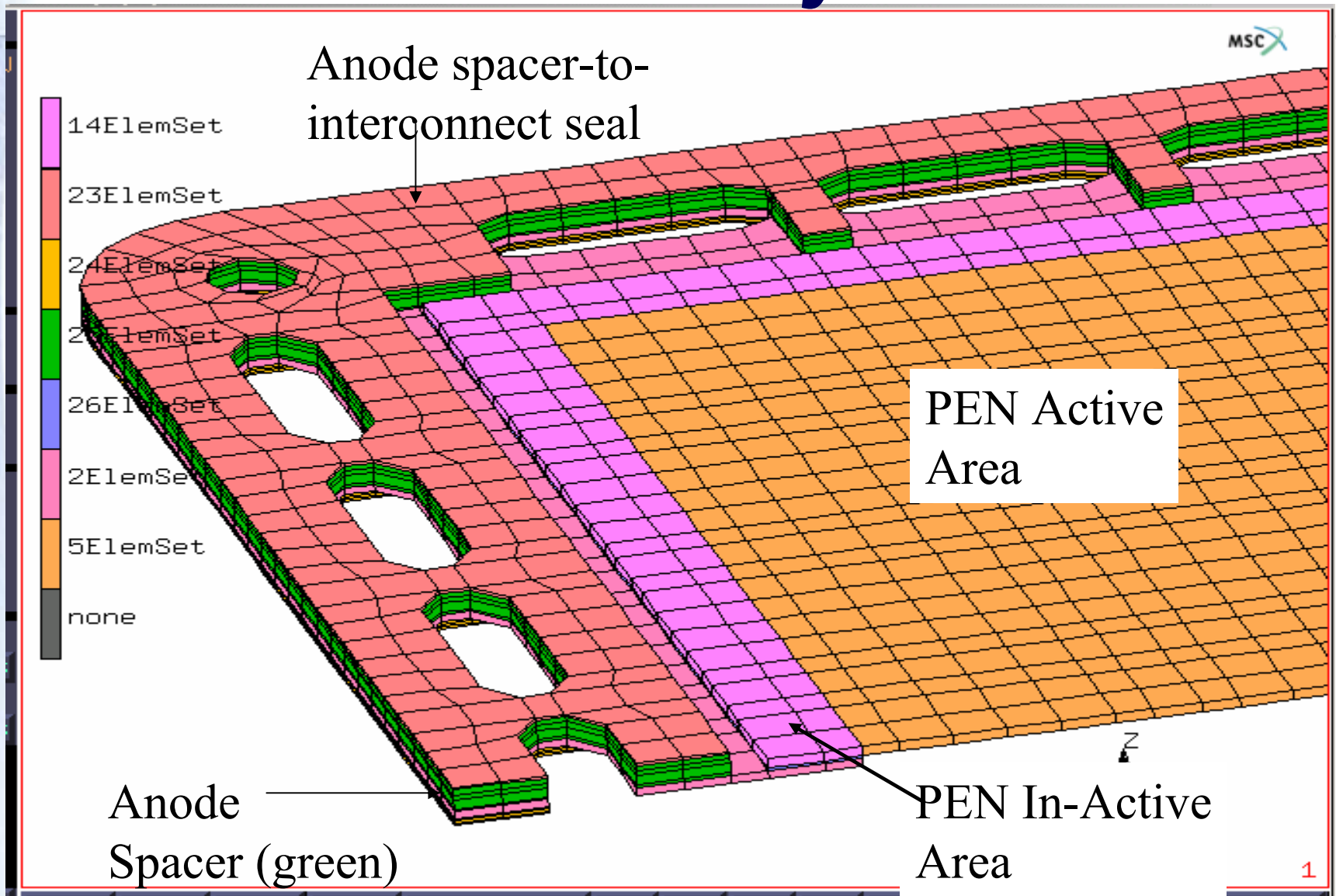


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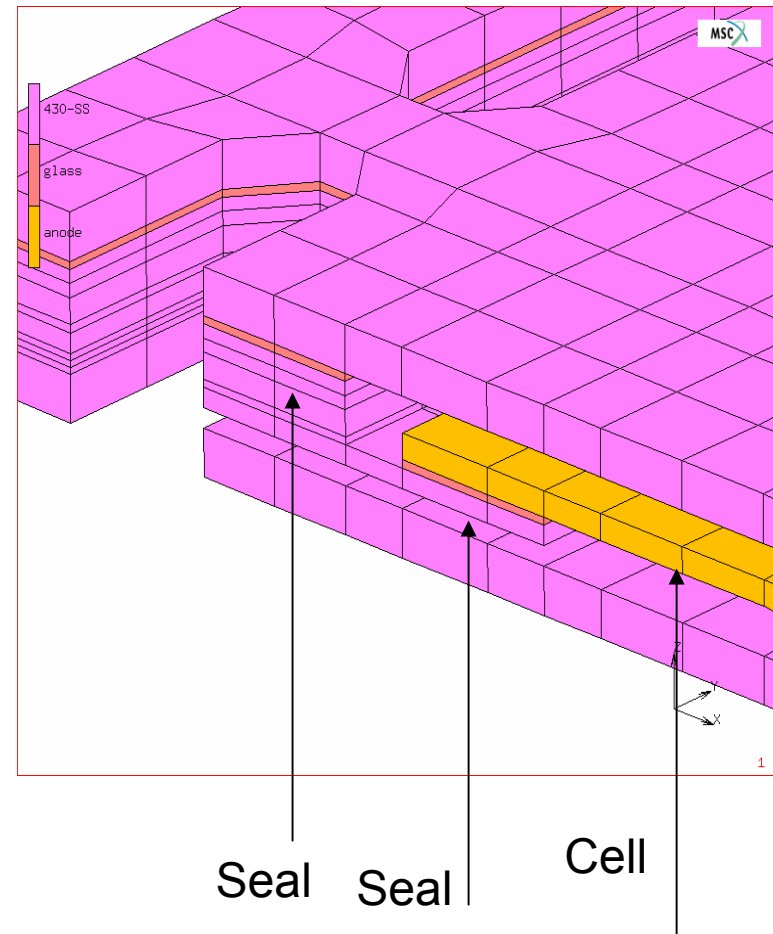
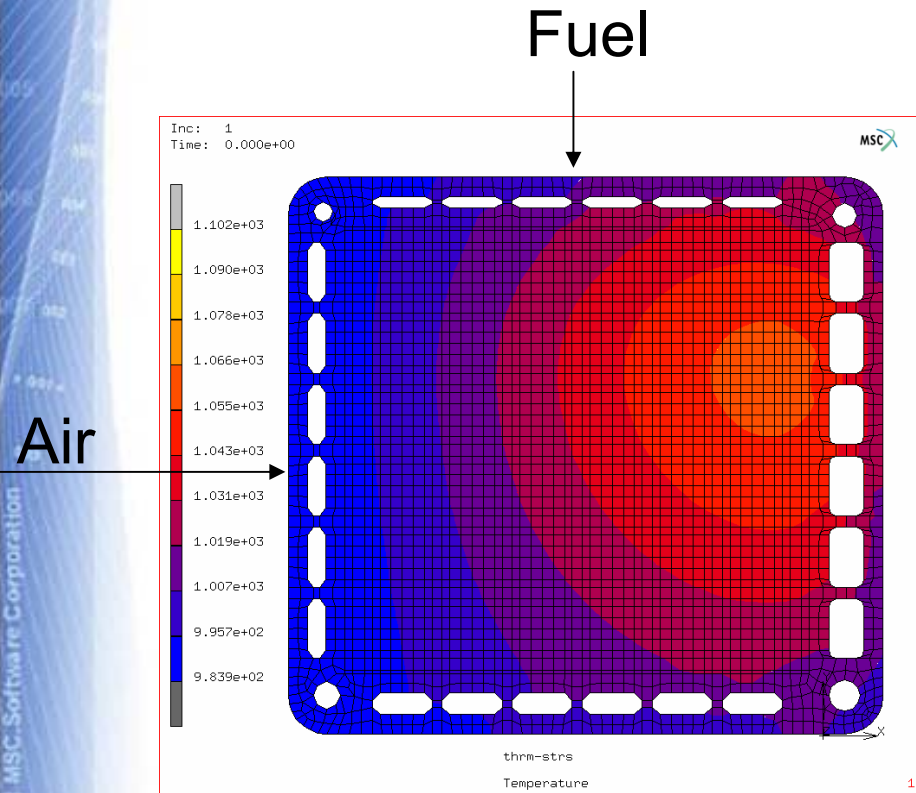
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# Assembly



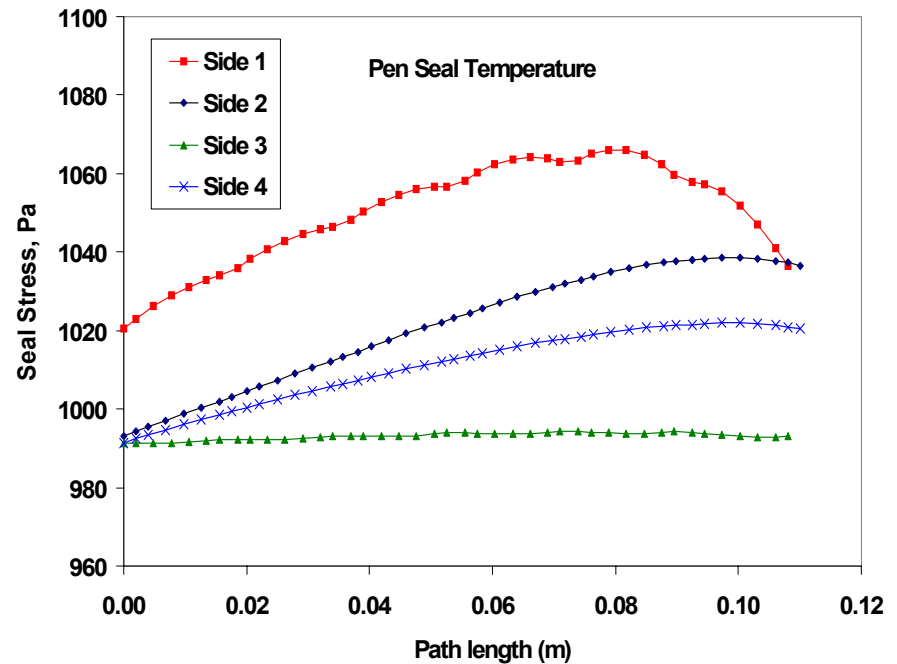
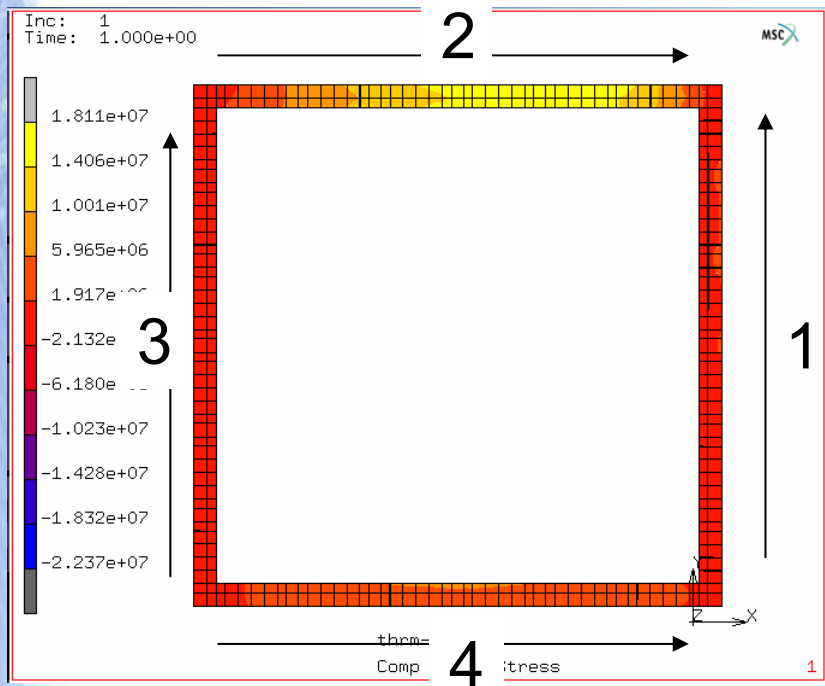
# Fuel Cell Geometry



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# Seal Temperature Profiles



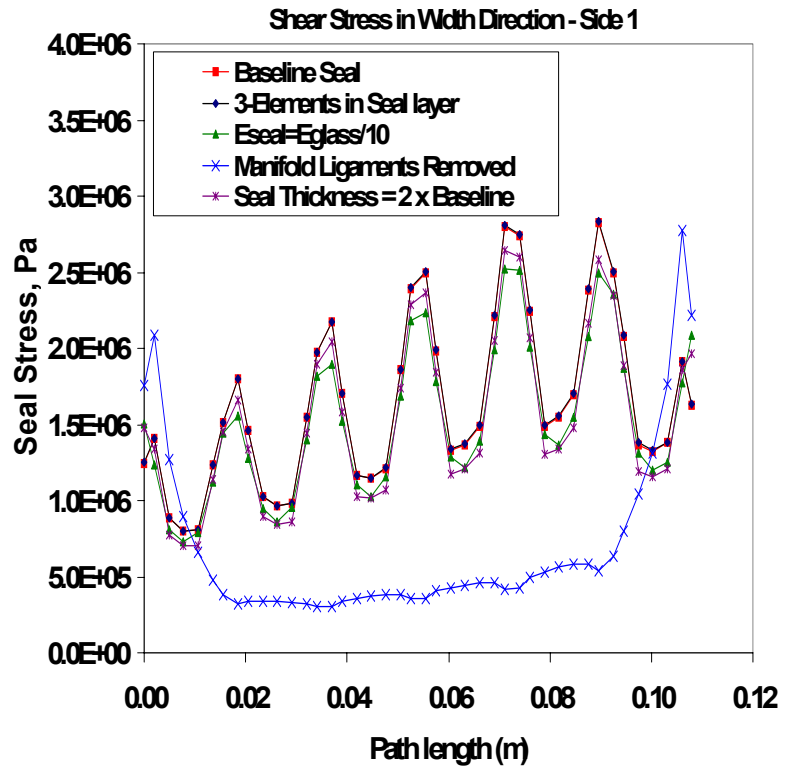
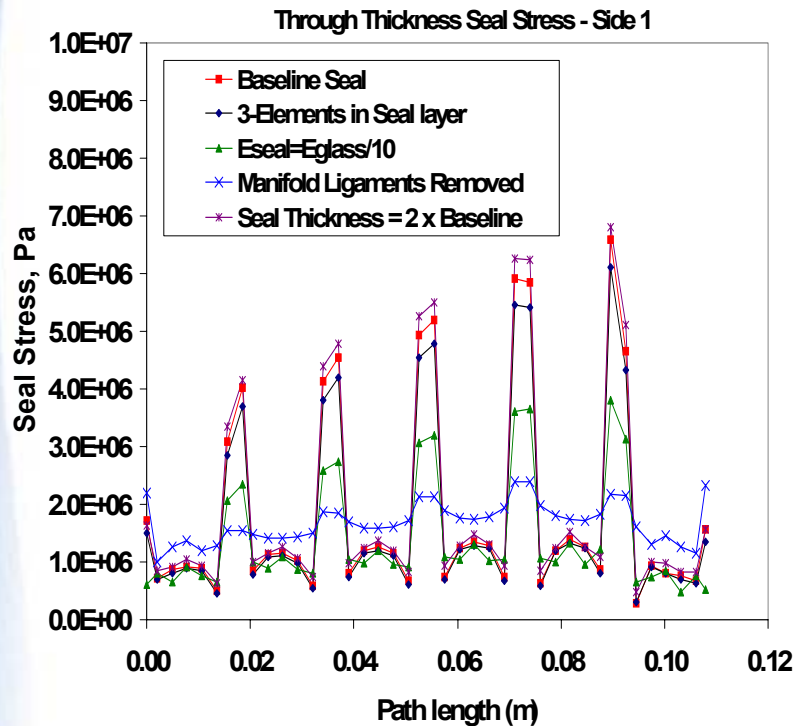
Glass Seal Temperature



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# Through Thickness Stress

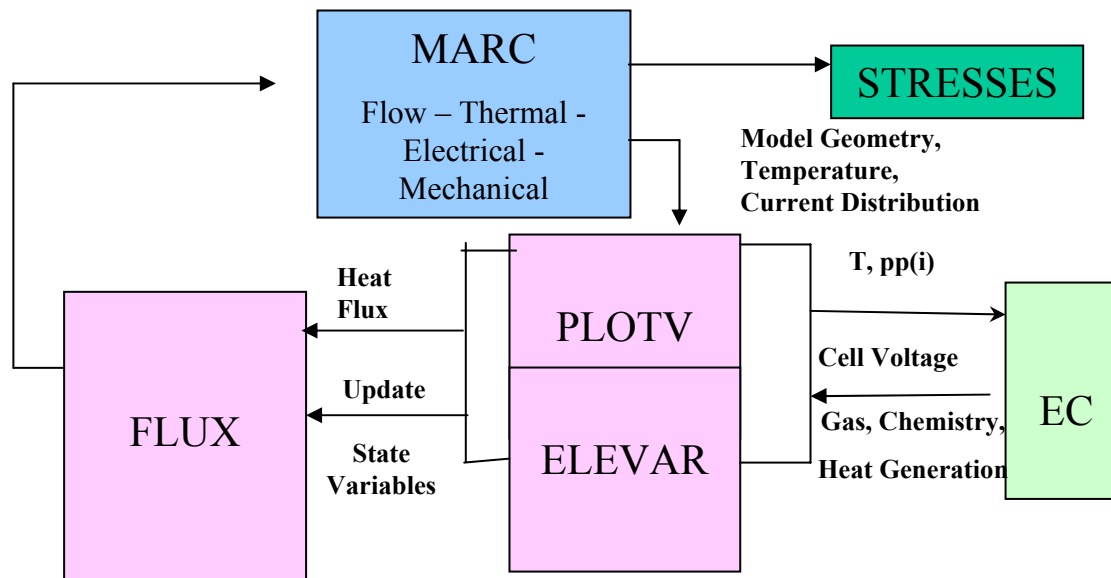


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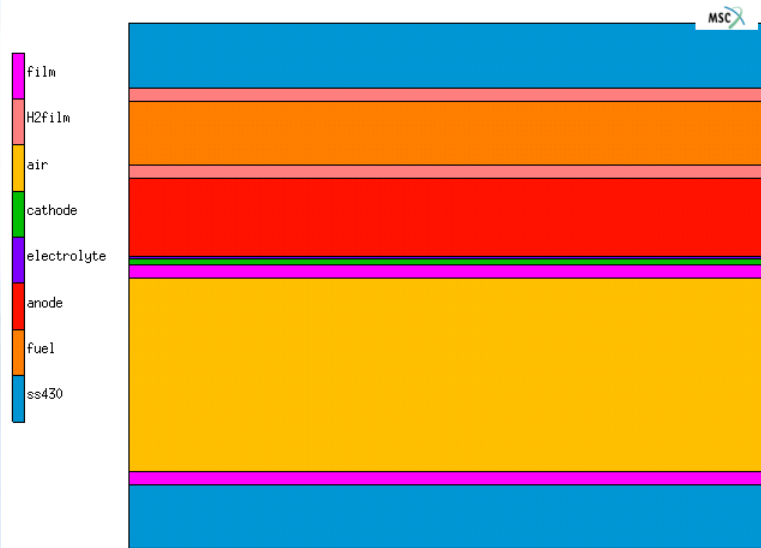
# EC in FEA Framework

- Fuel cell operations involve multi-physics processes; the constitutive thermal, chemical, electrochemical and transport processes are strongly coupled => requiring versatile multi-physics tool for realistic description
  - Technology development involves design optimization of various geometric, material and operation parameters; the cost of such parametric studies increases exponentially with the number of the working parameters and there are many such parameters involved
- => Computational efficiency is critically important

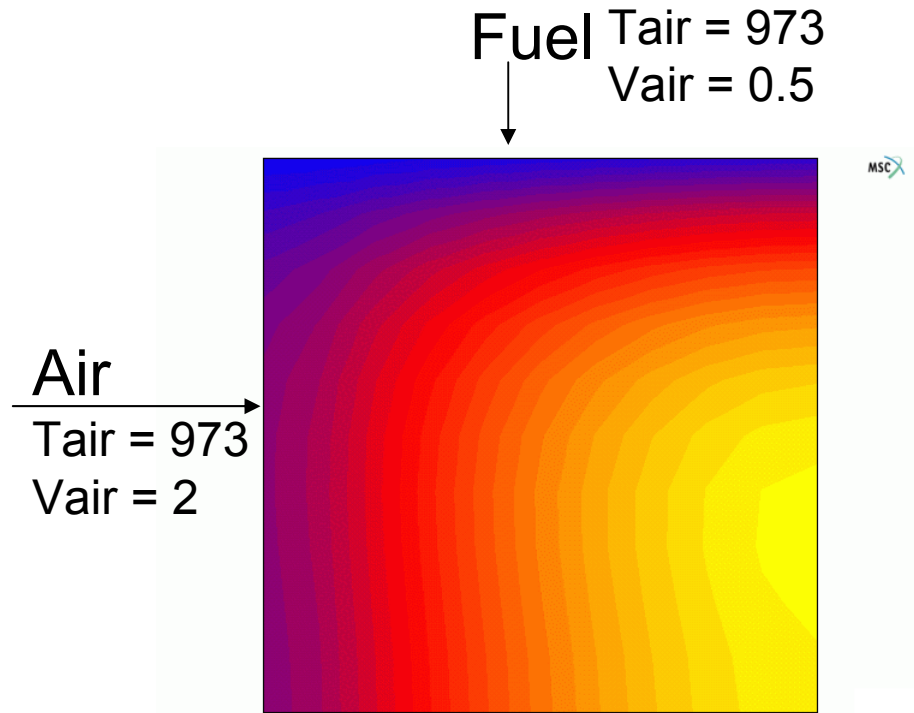




# EC in FEA Framework



Material Layers Thickness 4mm



.11m square



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