GAS TURBINE MATERIALS
LIFE ASSESSMENT AND
NONDESTRUCTIVE EVALUATION

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Project Overview

• Team member: Siemens Corp. and Argonne National Lab
• Research focus: gas turbine materials
  • For higher-temperature engine operations to improve efficiency and reduce emissions
  • For the use of unconventional fuels with more corrosion species
• Project tasks:
  • Task 1: develop predictive models for deposition, corrosion and component life assessment
  • Task 2: develop/demonstrate nondestructive evaluation (NDE) technologies for coatings
• Project duration FY2015-FY2017
NDE Objective

- Develop and demonstrate advanced thermal-imaging NDE technologies for coatings (mostly TBCs)
TBC Background – Material and Structure

- Thermal barrier coatings (TBCs) are commonly used to insulate high-temperature metallic components in gas turbines
  - TBCs may reduce metal surface temperature by >100°C

- TBCs are “prime reliant” material → nondestructive evaluation (NDE) is needed for their condition monitoring and life prediction
  - Need 100% coating surface inspection by imaging NDE

Uncoated and TBC-coated turbine blades

- TBC material: YSZ
- TBC processing: APS or EB-PVD
TBC Background – NDE Development

- Many NDE technologies were evaluated for TBCs in last few decades → generally not very successful
  - No NDE tools for industrial applications

- Current TBC analysis and quality control still relies on destructive method – microscopy:

  This research has established Pulsed Thermal Imaging – Multilayer Analysis (PTI-MLA) as a promising NDE method for entire TBC lifetime evaluation
Presentation Outline

- PTI-MLA method and capabilities
- PTI-MLA for TBC life prediction
- PTI-MLA for industrial applications
  - 3D mapping of MLA data for engine components
  - Evaluation of low-cost IR camera
Pulsed Thermal Imaging – Multilayer Analysis (PTI-MLA)

- PTI-MLA consists of a pulsed thermal imaging (PTI) experimental system and a multilayer analysis (MLA) data-processing code
- PTI-MLA images two coating properties over entire coating surface

PTI experimental setup

Thermal conductivity image

![Image: PTI experimental setup with a flash lamp, IR camera, monitor, and turbine blade.]

![Image: Thermal conductivity image with a color bar indicating 0.5 W/m-K to 1.4 W/m-K.]

Monitor

Flash lamp

IR camera

Turbine blade

0.5 W/m-K

1.4 W/m-K
PTI-MLA: Principle for Coating Analysis

**PTI system setup**

- IR camera
- Flash lamp
- Coating: $L_1$, $e_1$, $\alpha_1$
- Substrate: $L_2$, $e_2$, $\alpha_2$

$L$ – thickness
$e$ – thermal effusivity
$\alpha$ – thermal diffusivity

**Temperature profile $T(t)$ at each pixel**

- $T(t)$ vs. $t (s)$

**MLA analysis**

- Log temperature profile $\ln T(t)$
- Log slope profile $d(\ln T)/d(\ln t)$

Peak
PTI-MLA: Measurement Principle

Coating/Substrate Model

Coating: \( L_1, k_1, \rho_1c_1 \)

Substrate: \( L_2, k_2, \rho_2c_2 \)

\( L \) – thickness
\( k \) – thermal conductivity
\( \rho c \) – heat capacity
\( e = (kpc)^{1/2} \) – thermal effusivity
\( \alpha = k/\rho c \) – thermal diffusivity

- MLA method: solve governing equation for layered materials and then fit the solution with experimental data (for all pixels)

- MLA determines 3 parameters: \( e_1/e_2, L_1^2/\alpha_1, \) and \( L_2^2/\alpha_2 \) (\( e_2 \) & \( \alpha_2 \) are known)
  - For coating: (1) \( k \) & \( \rho c \) when \( L \) is known; (2) \( k \) & \( L \) when TBC porosity is known
  - For substrate: \( L \) (substrate’s \( k \) & \( \rho c \) are already known)
  - Accuracy: <3% error typical
PTI-MLA Results for typical 1-layer TBCs

Thermal conductivity $k$ images

Heat capacity $\rho c$ images

<table>
<thead>
<tr>
<th>TBC#</th>
<th>Type</th>
<th>$L$ (mm)</th>
<th>$k$ (W/m-K)</th>
<th>$\rho c$ (J/cm$^3$-K)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>EB-PVD</td>
<td>0.050</td>
<td>0.87</td>
<td>2.90</td>
</tr>
<tr>
<td>2</td>
<td>EB-PVD</td>
<td>0.138</td>
<td>1.63</td>
<td>2.22</td>
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<tr>
<td>3</td>
<td>APS</td>
<td>0.86</td>
<td>0.93</td>
<td>2.19</td>
</tr>
</tbody>
</table>
PTI-MLA Predictions for 2-layer TBCs

Double-layer TBC

La$_2$Zr$_2$O$_7$

7YSZ

Metallic substrate

Predicted layer effusivity

e: 1$^{\text{st}}$ layer (LZO)

e: 2$^{\text{nd}}$ layer (YSZ)

700µm

Predicted thickness profiles

LZO

YSZ

Substrate

5 mm

Predicted thickness profiles for a used turbine vane

Grayscale is proportional to thermal effusivity

Deposit

TBC

Substrate

500µm

~10 cm
Summary of PTI-MLA Capabilities

- PTI-MLA measures 2 coating properties:
  - \( k & \rho_c \) when \( L \) is known
  - \( k & L \) when TBC porosity (or density) is known (\( c \) is constant for TBC)

- PTI-MLA has unique capabilities:
  - Sample can be any size and geometry
  - Imaging property distribution over entire surface with desired resolution
  - Current code works for 1- & 2-layer coatings (more layers possible)
  - Also determines substrate thickness \( L \)
  - High accuracy: <3% error typical
  - Fast test (few seconds), fully automated data processing (~minute)
  - Can be miniaturized for inside engine inspection
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- PTI-MLA method and capabilities
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TBC Property Change with Life

Thermal conductivity images for a thermal-cycled TBC (@1100°C)

- Cracks initiate and increase in size with time (conductivity decrease)
- Intrinsic TBC conductivity increases with time

Crack initiation/development
TBC Life Prediction Model

- Measured overall TBC thermal conductivity $k$ is affected by two factors:
  - (1) Intrinsic TBC material conductivity $k_{TBC}$ increases with time due to sintering ($k_{TBC}$ is usually modeled by Larson-Miller parameter, or LMP)
  - (2) Interface cracking/delamination is filled by air with low conductivity $k_{air}$

\[
\frac{L_{TBC} + L_{air}}{k} = \frac{L_{TBC}}{k_{TBC}} + \frac{L_{air}}{k_{air}}
\]

where $L_{TBC}$, $k$ and $k_{air}$ are known; $k_{TBC}$ can be obtained from LMP correlation

- Air-gap thickness $L_{air}$ can be estimated from:

- TBC delaminates (or fails) when $L_{air}$ is large (value?)
Thermal Cycled APS TBC Samples

- Note: only ~10% conductivity increase in lifetime

Measured Average TBC Properties (nominal TBC thickness 0.3mm)

- Thermal conductivity $k$
- Heat capacity $\rho c$

Exposure time (% to failure)

- 0%
- 25%
- 50%
- 75%
- 100%

Thermal conductivity $k$ (W/m-K)
- 0.75
- 0.80
- 0.85
- 0.90
- 0.95

Heat capacity $\rho c$ (J/cm$^3$-K)
- 2.7
- 2.8
- 2.9
- 3.0
- 3.1
Intrinsic TBC Conductivity $k_{TBC}$ with LMP

Only these 5 points were used for $k_{TBC}$ correlation.
Air-Gap Thickness $L_{air}$ for Delamination

- Data suggest that TBC delaminates at $L_{air} \sim 2\mu m$
- This is a complete TBC life prediction model: $k \rightarrow L_{air}$
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NDE for TBCs on Engine Components

- PIT-MLA can easily obtain NDE data for entire engine part
- However, entire NDE data may be difficult to present if part is complex
- Example for a simpler part: engine blade
TBC Thickness Image for Entire Blade (total 12 sub-images)
Why 3D Mapping of NDE Image Data?

- Current NDE image data are simply compiled
- Such NDE results can be difficult to use:
  - Difficult to understand NDE images if part is complex
  - Difficult to perform dimensional analysis
  - Difficult to use NDE data for TBC life prediction
- Solution: 3D NDE data representation
Mapping NDE Data onto 3D Object

- **Input data:**
  - Surface cloud points of 3D part
  - 2D NDE images (for entire 3D part surface)

- **Step 1:** Calculating normal vectors of cloud points (if not available)

- **Step 2:** Mapping/stitching NDE images onto surface cloud points
  - Matching each NDE test image with corresponding projection image of 3D part and transferring NDE data to surface points
  - Automated weighting to eliminate data with poor or no flash heating

- **Step 3:** 3D NDE data can be displayed in any views (or videos)
Matching NDE Image with Projection Image of 3D Part

Projection image of cloud points

Matched image

NDE image

NDE data on image pixels are transferred to surface points
Weighted Data in Overlapped Areas

Surface area observed by IR camera but not illuminated by flash lamp (weight = 0)

Weight is related to flash intensity at each surface point
Final Result: TBC Thickness on Entire Blade

All 12 NDE sub-images are seamlessly mapped onto blade surface
TBC thickness for 3D blade
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PTI-MLA for Industrial Applications

- Two factors affect PTI-MLA NDE for industrial applications:
  - TBC translucency requires surface treatment (usually graphite paint)
  - High-cost and large size of high-end IR cameras

- Solution: use low-cost LWIR camera (bolometer)
  - TBC is naturally opaque at LWIR (7-13µm) (no paint required)
  - Bolometers are small and much cheaper (~10% of cooled IR camera)

State-of-the-art IR camera: SC4000 (Cooled, MWIR, 320x256, high speed)

(Bolometer)
Low-cost IR camera: A35 (RT, LWIR, 320x256, 60Hz)
Evaluation of a FLIR A35 IR camera

- Various TBC samples were tested using SC4000 and A35

- A35 results were compared with SC4000 results (as “exact”)
  - Compared parameters: TBC thickness and thermal conductivity
Measured conductivity images for 0.36mm TBC

- A35, unpainted TBC
- A35, painted TBC
- SC4000, painted TBC

- Error: +37%
- Error: -4%
- Assumed: exact

- Comparison for TBC thickness are better (+16% and -2%)
- Note: same code was used for all data processing
TBC measurement error by A35 camera

Prediction is acceptable when TBC >0.3mm with paint
PTI-MLA Development for Bolometers

- Modeling flash-heat absorption inside translucent TBCs
- Modeling bolometer response time
Optical Model for TBC Heat Absorption

**Painted TBC**

From flash lamp (<2.5µm) to IR camera

7YSZ

Metallic substrate

**Unpainted TBC**

To LWIR camera (7-13µm) to MWIR camera (3-5µm)

**Flash heating as a function of coating depth \(q(z)\):**

\[
q(z) = q_{i1}(1 - \rho_0) \frac{e^{-\alpha z} - \rho_1 e^{-\alpha(L-z)}}{1 - \rho_0 \rho_1 e^{-2\alpha L}}
\]

\(\alpha\) = optical attenuation coefficient

\(\rho_0\) & \(\rho_1\) = surface reflectivity

\(L\) = coating thickness
Modeling Bolometer Response Time

- In bolometer, pixel temperature change from absorbed incident thermal energy is used to sense radiation intensity.

- This process is modeled by:

  \[ P(t) = G\Delta T + H \frac{d\Delta T}{dt} \]

  - \( P(t) \) = incident power,
  - \( G \) = thermal conductance of thermal link
  - \( H \) = pixel heat capacity
  - \( \Delta T \) = relative pixel temperature (bolometer reading)

- When \( P(t) \) changes abruptly from 0 to a constant \( P \) at \( t=0 \), \( \Delta T \) follows:

  \[ \Delta T = \frac{P}{G} \left( 1 - e^{-\frac{G}{H}t} \right) \]

  - \( \frac{H}{G} \) = bolometer response time

- Response time for A35 is 12ms (\( \Leftarrow \) reason for poor NDE results for thin TBCs)
TBC measurement error by A35 camera - with heat absorption and response time models

Prediction is acceptable for all data
Typical Measured TBC Thickness on Blade

A35, unpainted TBC ($\alpha = 3.9 \text{ mm}^{-1}$)

A35, painted TBC

SC4000, painted TBC

- Error: - 7.2%
- Error: - 6.5%
- Assumed: exact

- Error for measured TBC conductivity is similar (+7.7% and +7.4%)
  - Note: errors of <10% are generally considered acceptable
  - Note: same bolometer code was used for all data processing

- Errors in A35 results are mostly due to noise $\rightarrow$ higher flash heating will reduce them! (especially for unpainted and thicker TBCs)
Summary

- PTI-MLA can accurately measure TBC properties
- PTI-MLA can nondestructively evaluate TBCs in their entire lifetime
  - For TBC life prediction
  - For industrial applications
- PTI-MLA has essentially solved the TBC NDE issue!
  - PTI-MLA is a turn-key technology and can be licensed from Argonne