Ni-Based Alloys for Advanced Ultrasupercritical Steam Boilers

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## **ORNL's Role in the A-USC Boiler Effort**



Inconel 740

- Generate high quality creep-rupture data using accepted test methods
  - Nickel-base alloys, including code case for Inconel 740
  - Supplement minimum required data for code-approved alloys, e.g., alloy 617, Inconel 740
  - Identify fabrication & welding issues on creep strength
- Understand microstructural underpinnings of creep strength and failure
- Predict life with confidence



## **Nature of Work Has Changed**





## **Focus of Work Has Been on Ni-Based Alloys**

	Ni	Cr	Со	ΑΙ	Ti	Nb	Мо	Fe	Mn	Si	С	В
740	Bal.	25	20	0.9	1.8	2.0	0.5	0.7	0.3	0.5	0.03	-
740H	Bal.	25	20	1.4	1.4	1.5	0.5	1.0	-	0.2	0.03	0.001
282	Bal.	20	10	1.5	2.1	-	8.5	1.5	0.3	0.15	0.06	0.005
617	Bal.	22	11	1.2	0.4	-	8.6	0.7	0.03	0.1	0.06	0.003

- Both Inconel 740 and Haynes 282 form γ' (Ni<sub>3</sub>Al, Ni<sub>3</sub>Ti) and carbides
- Alloy 617CCA (617B) is mainly solid solution strengthened
- Only Inconel 740 forms η (Ni<sub>3</sub>Ti), with 740H having significantly less susceptibility to its formation (several studies)
- Vol% η that forms during exposure seems to have little effect on creep rupture (Shingledecker and Pharr, Tortorelli et al.)
- Alloys have elements that promote internal oxidation (Pint et al., Wright et al.)



## Long-Term Creep-Rupture Data for 740/740H Build Confidence in A-USC Boiler Use



## High Density of Cavities After 56,550 h





## **Grain Boundary Cavitation**





## Little $\gamma'$ Depletion Noted at GBs





## 740H Long-Term Creep-Rupture Specimen Showed "Good" Microstructural Stability





## Despite ~46,000 h at 750°C under Load, Little Eta Phase Observed for Inconel 740H





## γ' Size Measurements Show Coarsening But Little Change in Later Stages





## Boiler-Relevant Creep-Rupture Data for Haynes alloy 282

- Interest in Haynes 282 for boiler application triggered by turbines part of A-USC program
- Work to date has shown Haynes 282 may be preferred to 740
  - better creep-rupture resistance
  - minimal debits due to welding (and, possibly, cold work)
- Recommended 2-stage aging protocol (1010°C/1h+788°C/8h) deemed problematical by boiler manufacturers
- 2013: determined a one-step aging treatment (800°C/4h)
- FY15: Completed a creep-rupture test campaign for one-step aged Haynes 282



• Code case test campaign starting (different project)



## Little Difference in Creep-Rupture Lifetimes for the Two Aging Treatments



## Significant γ' Coarsening Observed for Haynes 282 Creep Specimens





## Spherical y in Haynes 282 Contrasts with Cuboidal y in Inconel 740





## Differences in Shape Can Be Explained by Respective y/y Lattice Mismatches



Larger misfit results in greater interfacial energy

- Cuboidal shape of precipitates
- Larger driving force for coarsening



# Median 282 $\gamma'$ Size Falls Above that of 740 But within Scatter





## **Particle Strengthening in Haynes 282**





## **Similar Behavior as Load Varied**





## Creep-Rupture Testing of Alloy 617CCA Completed Earlier in Program



### 617 Bend Tests Followed Approach Used for Inconel 740 Shingledecker and Pharr, J. Mater. Eng. Perf., 2013

Cold-forming:

76.2 mm bend 33% OFS (outer fiber strain)





### 127.0 mm bend 20% OFS

171.4 mm bend 15% OFS



- 775° C, 38.6 MPa
- Strain Tracked by Diameter Increase With Time
- Outer Diameter measured at 0, 45, 90, 135° along tube length L



## First alloy 617 Failure at ~32,800 h Recorded in Past Year

775°C, 38.6 MPa, 33% OFS





## **Cold Work by Tube Bending Had No Effect on Creep-Rupture Lifetime for 617CCA**



## In Contrast, Inconel 740 Showed a Significant Debit due to Cold Work of Tube Bends



Creep rupture of solid solution Ni-based alloys like 617CCA thought to be less susceptible to cold work effects than precipitation-strengthened alloys such as Inconel 740



## Milestones

### <u>FY14</u>

Prepare a summary report analyzing all results to date on creep behavior of alloy 282 (Completed)

Complete a report or paper on oxidation effects on Ni-based superalloys under creep conditions (Completed)

Complete a summary report on all alloy 617 data produced by the A-USC program with a comparison to other 617 databases. (Now May 2015)

Complete a proof-of-principle creep test of a co-extruded pipe (Now June 2015)

<u>FY15</u>

Complete a report or paper on the long-term high-temperature microstructural stability of Inconel 740 (Completed)

Issue final reports by alloy type on ORNL work for the A-USC boiler project (September 2015, probably December 2015)



## Remaining Work Before End of A-USC Boiler Consortium Project in Dec. 2015

- Completion of microstructural analyses of specimens with longest rupture times and use of such data in advanced lifetime models for Ni-based superalloys
- Increasing max temperature in Inconel 740/740H code case to 825°C
- Multiple summary reports/papers on the different alloys tested and analyzed during the course of the A-USC boiler project



## Summary

- Creep testing and microstructural analysis were used to assess thermal stability and time-dependent deformation behavior of precipitationstrengthened Inconel<sup>®</sup> alloy 740 and Haynes<sup>®</sup> 282<sup>®</sup> alloy, both alloys meet A-USC goal with single-step heat treatments
- Alloy 617CCA shows no effect of cold work on creep-rupture life
- Work is focused on remaining data and microstructural analyses and documentation in a set of final reports







## **STEM Measurements Used For Aging Data**

### Haynes 282 – 750°C, 320MPa 1462h

**DF-STEM** 















## $\gamma/\gamma'$ misfit reduces as Mo increases

	Alloy element, wt%										
Alloy	Ni	Cr	Со	Мо	Ti	AI	Nb				
282	Bal.	20	10	8.5	2.1	1.5					
740	Bal.	24	19.9	0.5	1.5	1.3	1.6				



- Mo promotes formation of TCP phases,  $\mu \& \sigma$
- TCP phases can be linked to premature creep cavitation

