

the Energy to Lead

Pilot Test of a Nanoporous, Super-hydrophobic Membrane Contactor Process for Post-combustion CO₂ Capture

DOE Contract No. DE-FE0012829

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Introduction to GTI and PoroGen



- Not-for-profit research company, providing energy and natural gas solutions to the industry since 1940s
- Facilities
 - 18 acre campus near Chicago
 - 200,000 ft², 28 specialized labs






- Materials technology company commercially manufacturing products from high performance plastic PEEK (poly (ether ether ketone))
- Products ranging from membrane separation filters to heat transfer devices



Project overview

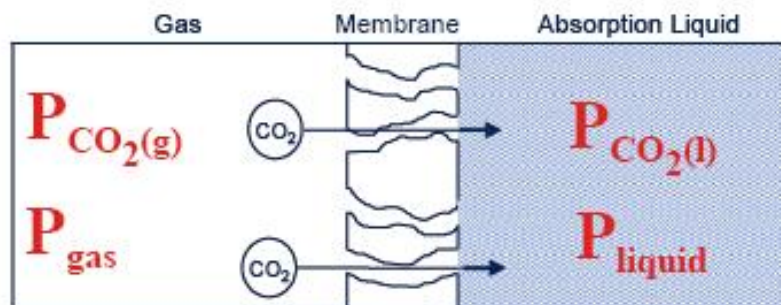
- **Performance period**: Oct. 1, 2013 – June 30, 2018
- **Total funding**: \$12.5 MM (DOE: \$10MM, Cost share: \$2.5MM)
- **Objectives**:
 - Build a 0.5 MW_e pilot-scale CO₂ capture system and conduct tests on flue gas at the National Carbon Capture Center (NCCC)
 - Demonstrate a continuous, steady-state operation for ≥ 2 months
- **Goal**: Achieve DOE's goal of 90% CO₂ capture rate with 95% CO₂ purity at a cost of \$40/tonne of CO₂ captured by 2025

- **Team**:

Member	Roles
	<ul style="list-style-type: none"> • Project management and planning • Process design and testing
	<ul style="list-style-type: none"> • Membrane and module development
 TRIMERIC CORPORATION	<ul style="list-style-type: none"> • Techno-Economic Analyses (TEA)
NCCC	<ul style="list-style-type: none"> • Site host

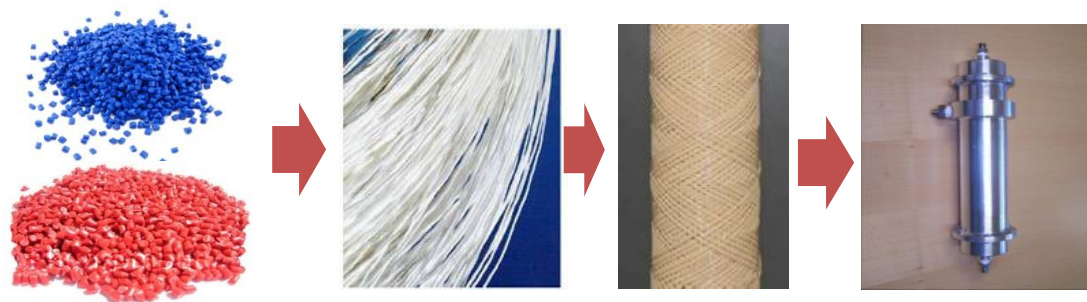
What is a membrane contactor?

- High surface area membrane device that facilitates mass transfer



- Separation mechanism:** CO_2 permeates through membrane and reacts with the solvent; N_2 does not react and has low solubility in solvent
- Why **PEEK HFMC**?

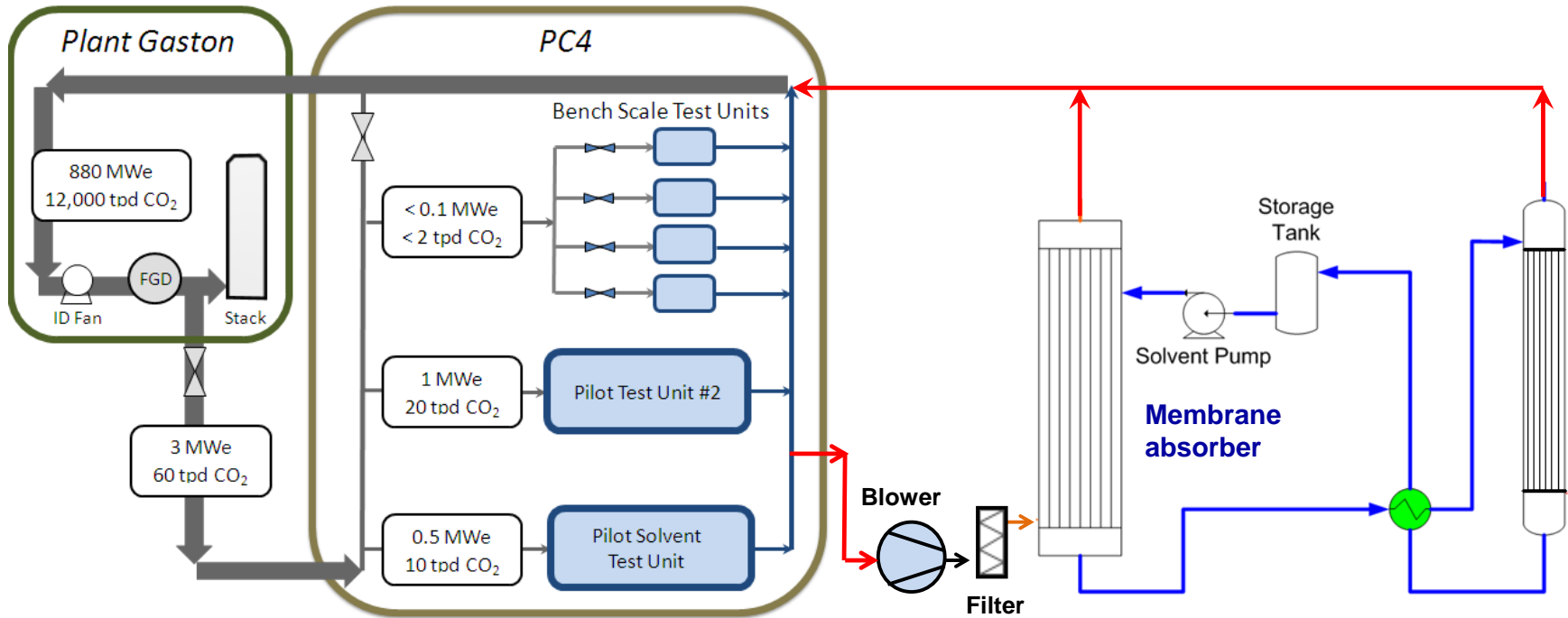
Polymer	Max service temperature (°C)
Teflon™	250
PVDF	150
Polysulfone	160
PEEK	271



PEEK= Polyether ether ketone

HFMC= Hollow Fiber Membrane Contactor

Process description



NCCC's PC4

HFMC plant

Membrane contactor for flue gas CO₂ capture compared to conventional membrane process

Membrane technology	Need to create driving force?	CO ₂ /N ₂ selectivity (α)	Can achieve >90% CO ₂ removal and high CO ₂ purity in one stage?
Conventional membrane process	Yes. Feed compression or permeate vacuum/sweep gas required	Determined by the dense "skin layer"	No. Limited by pressure ratio, multi-step process required*
Membrane contactor	No. Liquid side partial pressure of CO ₂ close to zero	Determined by the solvent, $\alpha > 1000$	Yes

* DOE/NETL Advanced Carbon Dioxide Capture R&D Program: Technology Update, May 2011

Technical and economic challenges of applying membrane contactor to existing PC plants

- **Performance**

- Maximize overall mass transfer coefficient to reduce absorption system size

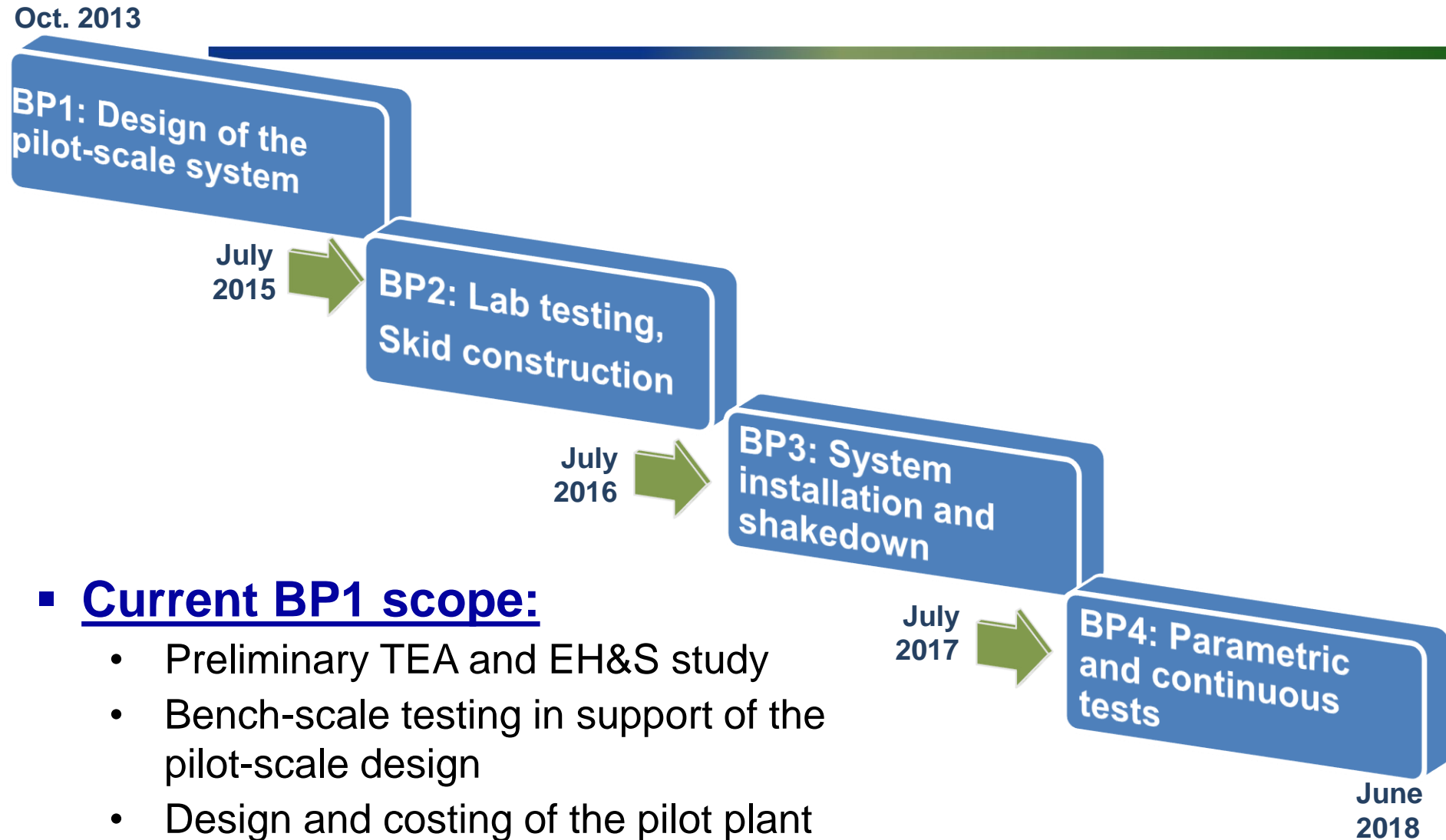
- **Durability** – Long-term membrane life in contact with solvent

- Improve membrane hydrophobicity

- Contactor **scale-up** and **cost reduction**

- Make larger diameter module, module packaging to reduce cost

Timeline and scope



■ Current BP1 scope:

- Preliminary TEA and EH&S study
- Bench-scale testing in support of the pilot-scale design
- Design and costing of the pilot plant

Preliminary Techno-Economic Analysis completed in September 2014

- Preliminary TEA was based on bench scale field test results at Midwest Generation's (IL) coal fired power station

- Flue gas feed

Feed element	Concentration
CO ₂	7.4-9.6 vol%
NO _x	40-60 ppmv
SO ₂	0.4-0.6 ppmv
CO	100-600 ppmv
O ₂	8.5-11 vol%
Balance: N ₂ , water vapor, trace elements	

- Mass transfer coefficient of 1.2 (sec)⁻¹ achieved with aMDEA solvent at 93.2% CO₂ removal

aMDEA = Activated methyldiethanolamine

Preliminary TEA shows HFMC technology with aMDEA solvent can cost 25% less than DOE Case 12

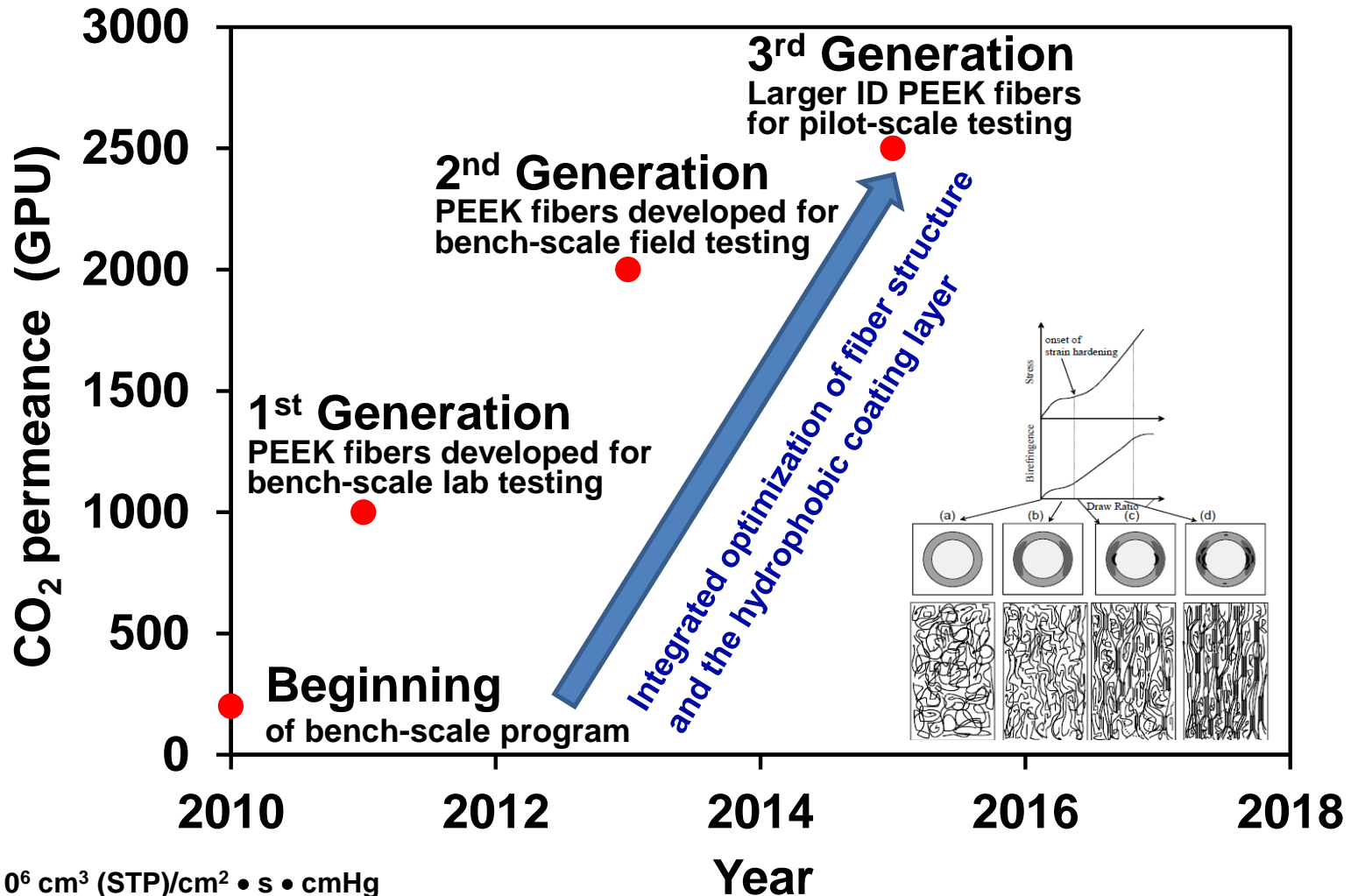
Mass transfer coefficient target of the current pilot program: **1.7** sec⁻¹

Item	Unit	DOE Case 12	Bench scale field test data	Target mass transfer coefficient achieved
LCOE - No TS&M	mills/kWh	137.3	127.1	122.1
Increase in LCOE - No TS&M	%	69.6%	57.0%	50.9%
Cost of CO ₂ Capture - No TS&M	\$/tonne	56.47	47.53	42.48

LCOE = Levelized Cost Of Electricity

TS&M = Transportation, Storage and Monitoring

PEEK membranes continue to improve, larger inner diameter fibers with high CO₂ permeance developed



1 GPU = 1 x 10⁶ cm³ (STP)/cm² • s • cmHg

New larger ID fibers have intrinsic CO₂ permeance as high as 2,600 GPU, surpassing our target of 2,000 GPU

- Achieved in January 2015 with testing conditions:
 - 2-inch diameter modules
 - Pure CO₂ gas
 - ~3 psig feed pressure
 - Room temperature (22 °C)

Cartridge No.	Number of fibers	Active fiber area (cm ²)	Pure CO ₂ permeance (GPU)
2PG-664	448	3,161	2,580
2PG-665	448	3,161	2,500

Why larger inner diameter (ID) fibers?

- During bench-scale field test, pressure drop (ΔP) between flue gas Inlet and outlet was 5 psi
- Current pilot program target: decrease ΔP to ≤ 2 psi because the lower the ΔP the more saving on operating costs
- The Hagen–Poiseuille equation: ΔP very sensitive to ID

$$\Delta P = \frac{8Q\eta L}{\pi \cdot r^4}$$

- Q : volumetric flow rate, η : absolute viscosity of the fluid, L : length of the hollow fiber, and r : radius of the hollow fiber
- Fiber ID is being increased from 13 mil to 20 mil

The 2,500 GPU 20-mil-ID-fiber module showed high CO₂ capture performance in contactor mode

- aMDEA solvent
- 90% CO₂ removal

	Mass transfer coefficient, (sec) ⁻¹	gas-side ΔP, psi
Tested in 2-inch module	1.6	0.28

Predicted ΔP for 8-inch module:
0.74 psi

Material compatibility confirmed/resolved before module scale-up

- No problems with O-ring seals were noted through tests of multiple 2-inch diameter modules
- Resolve tubesheet adhesion issues



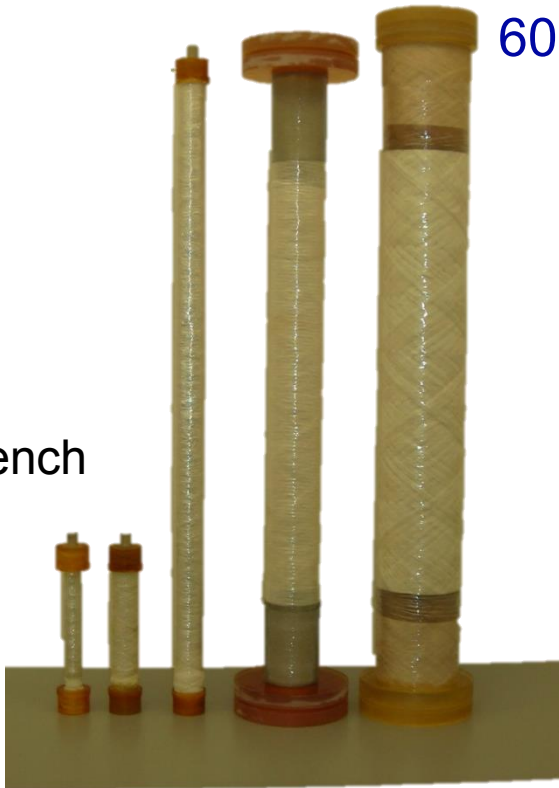
- No wet out of hydrophobic membrane surface after long-term operation based on single-gas CO₂ permeation measurements before and after contactor testing

Membrane module scaled to 8-inch diameter

8" diameter
60" long

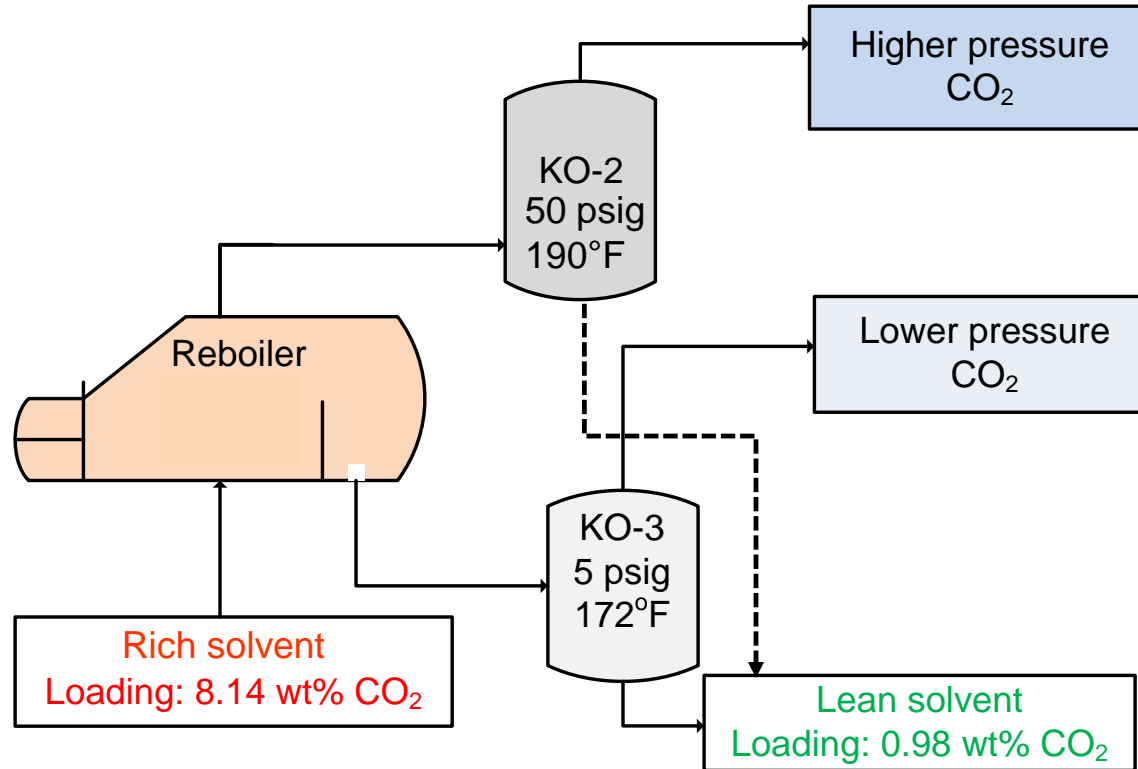
8-inch module constructed

2" bench

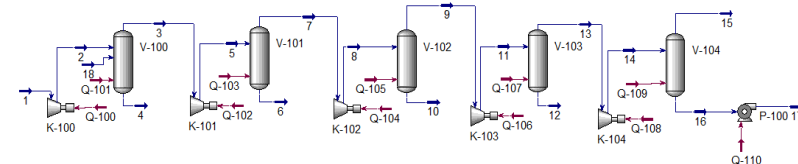


Measured intrinsic CO₂ permeance
for the 8-inch module: **2,300 GPU**

New regeneration process developed from process modeling during TEA study, validated by lab testing



- One stage of high pressure flash combined with one stage of low pressure flash
- Power required for compression can be reduced by as much as **20%**



Pilot plant design

- **Design bases:**

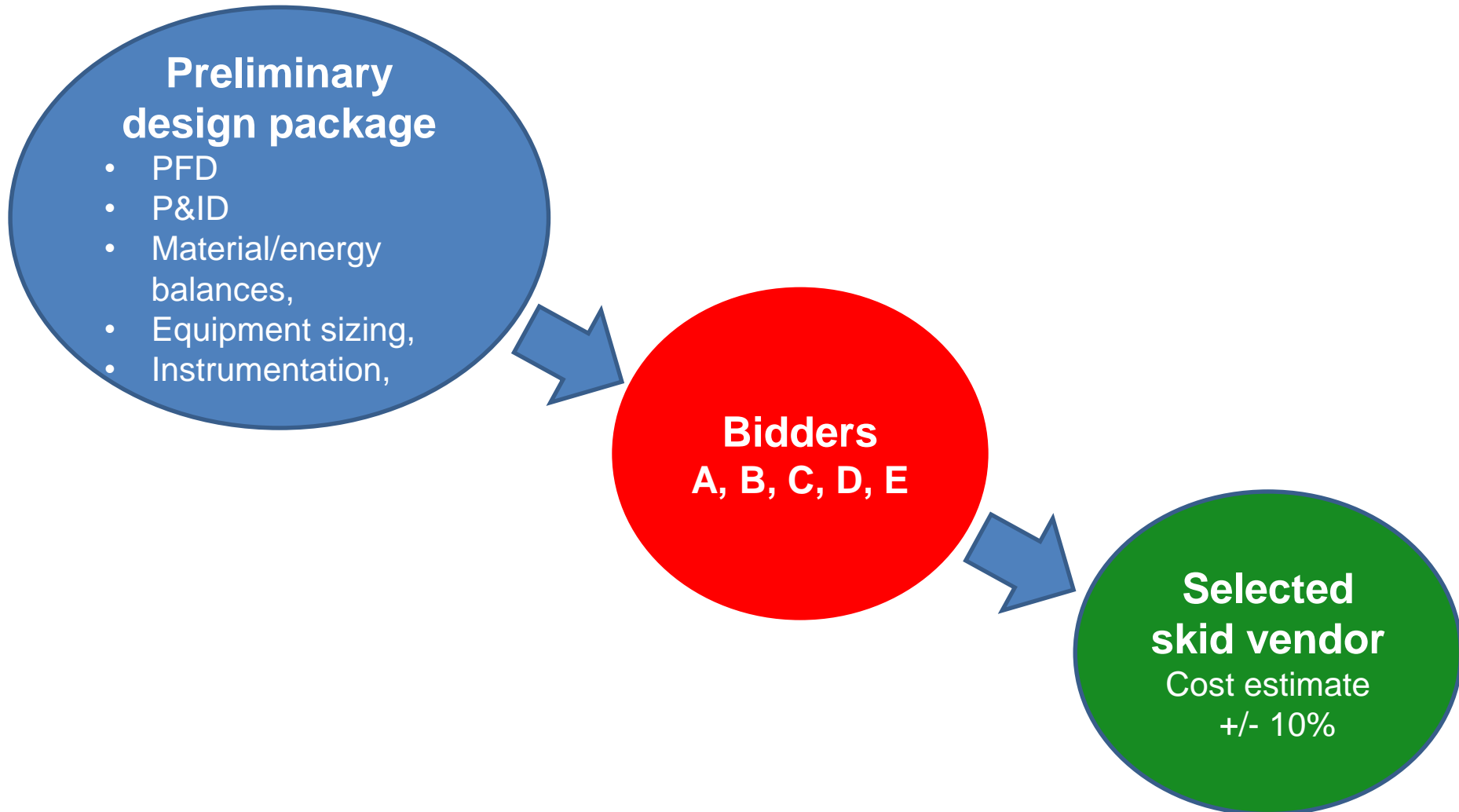
- Bench scale PFD, P&ID and testing results
- Process modeling
 - **Mass and energy balances**
 - **Equipment sizing**
 - **Process conditions**

Preliminary design completed, HAZOP reviewed at NCCC in February 2015

- **Major HAZOP review outcome**
 - No “show-stopper” or “major” modifications were identified
 - Valuable insights from NCCC engineers → revised design

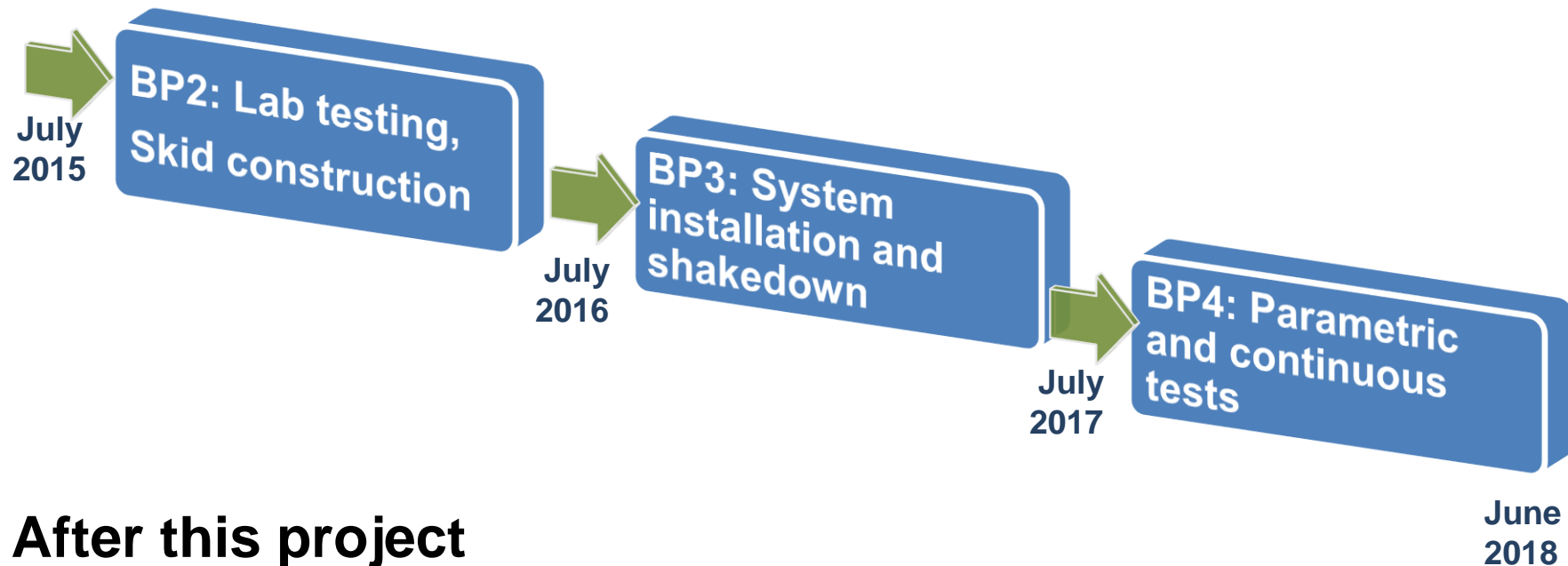


Revised design package sent to bidders, one will be selected to construct the plant



Plans for future testing/development/commercialization

- In this project**



- After this project**

Time	Development	CO ₂ capture, Ton/day
By 2018	0.5 MWe pilot scale (in progress)	10
By 2022	10 - 25 MWe demonstration	200 - 500

Summary

- PEEK HFMC: promising based on bench-scale field tests
 - $\geq 90\%$ CO₂ removal in one stage
 - Mass transfer coefficient of 1.2 (sec)⁻¹, which is over one order of magnitude greater than conventional contactors
- Pilot-scale development in progress
 - TEA: projected costs 25% lower than benchmark technology
 - PEEK membranes continue to improve, new developed larger ID fibers showed high CO₂ permeance and low pressure drop
 - Module scaled to 8-inch diameter with CO₂ permeance of 2,300 GPU
 - New regeneration process designed and validated experimentally
 - Design and costing near completion

Acknowledgements

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gti[®] JIP Partners

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