Commercial Scale CO₂ Injection and Optimization of Storage Capacity in the Southeastern United States

Project Number: DE-FE0010554

George J. Koperna, Jr.
Advanced Resources International
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Carbon Storage R&D Project Review Meeting
Developing the Technologies and
Infrastructure for CCS

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Presentation Outline

- Benefit to the Program
- Project Overview
- Technical Status
- Accomplishments to Date
- Summary
- Appendix
 - Organization Chart
 - Gantt Chart
 - Bibliography

Benefits Statement

The project will model **commercial-scale CO₂ storage capacity** optimization strategies to effectively manage the CO₂ plume and pressure field **within stacked reservoir systems**. These strategies will utilize geologic and performance data collected from SECARB's Anthropogenic Test Site, and will be high-graded based on cost and storage efficiency, considering reservoir geomechanics (pressure field) and laboratory-derived cap rock data.

Major advances:

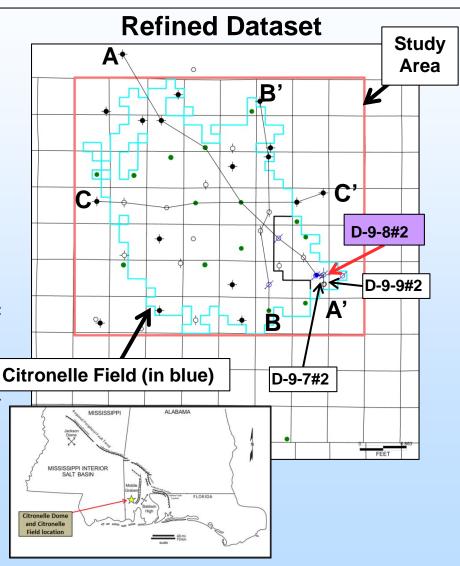
- Estimating commercial scale storage efficiency factors (Support industry's ability to predict CO₂ storage capacity in geologic formations to within ±30 percent)
- Detailed confining unit core characterization
- Generation of reduced order models
- Stacked Reservoir System Best Practices Manual

Project Objectives

- Optimize capacity and ensure storage containment in stacked Gulf Coast saline and oil bearing reservoirs
- Leverage modern and historical geologic characterization and injection performance data to develop detailed geologic models
- Overlay economic and risk management scenarios for each simulation case to determine the overall feasibility of commercial scale storage.
- Conduct detailed cap rock core analysis testing
- Develop new storage efficiency factors based on these project results
- Develop reduced order models to approximate the 'super computer' results
- Summarize the results in a Best Practices Manual

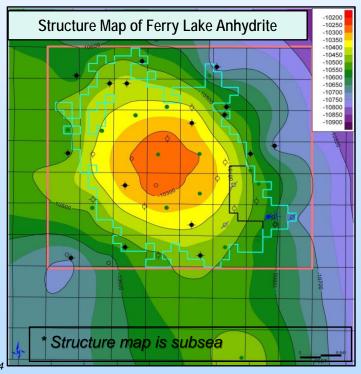
Project Status: Study Area & Well Data Set

- 400+ total wells in Citronelle Field on 40-ac spacing
- Study area for geologic model = 56 sq. miles
- Geologic model characterizes injection zones and confining units from surface though the Donovan sandstones at depths >12,000 ft.
- D 9-8 #2 well in Citronelle Southeast
 Unit selected as Type Log for geologic correlations of injection zones & confining units.
- Multiple cross-sections constructed for geologic correlation of model layers.
- Digitized the SP & resistivity curves for 36 well logs. These data input to neural net software to estimate
 5 SPOB1414 porosity.



Project Status: Building the Geologic Model

- Potential storage and confining layers were identified and correlated laterally
- Structural closure is present at all horizons from surface through the Donovan (Rodessa) sandstone

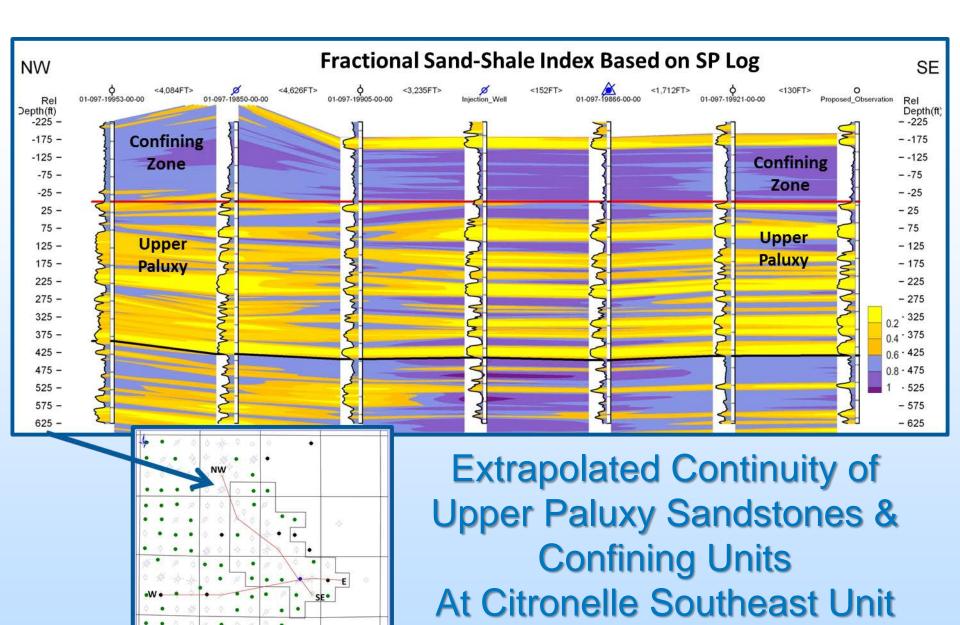


Stratigraphic Column

| Stratigraphic Column | | | | | | | |
|----------------------|-------------------|----------------------------------|---|------------------------------|--|---------------|--|
| System | Series | Stratigraphic Unit | Major Sub Units | | Potential Reservoirs and Confining Zones | | |
| Tertiary | Plio- Pliocene | | Citronelle Formation | | Freshwater Aquifer | | |
| | Miocene | Undifferentiated | | | Freshwater Aquifer | | |
| | Oligocene | Vicksburg Group | | casawhay Fm. catunna Clay | Base of USDW Local Confining Unit | ļ | |
| | Eocene | Jackson Group Claiborne Group | Talahatta Fm. | | Minor Saline Reservoir Saline Reservoir | | |
| | e Paleocene | Wilcox Group | Hatchetigbee Sand Bashi Marl Salt Mountain LS | | Saline Reservoir | | |
| | | Midway Group | Porters Creek Clay | | Confining Unit | | |
| | Upper | Selma Group | | | Confining Unit | | |
| 0 | | Eutaw Formation | | | Minor Saline Reservoir | | |
| Cretaceous | | Tuscaloosa Group | Upper Tusc. | | Minor Saline Reservoir | g | |
| ëo | | | Mid. Tusc | Marine Shale | Confining Unit | <u> Q</u> | |
| us | | | Lower Tusc. | Pilot Sand Massive sand | Saline Reservoir | ed | |
| | Lower | Washita- | _ | antzler sand | Saline Reservoir | | |
| | | Fredericksburg | Basal Shale | | Primary Confining Unit | <u> </u> | |
| Cretaceous | | Paluxy Formation | 'Upper' 'Middle' 'Lower' | | Proposed Injection Zone | ogged Interva | |
| | | Mooringsport Formation | | | Confining Unit | <u>a</u> | |
| | | Ferry Lake Anhydrite | Rodessa Fm. | | Confining Unit | | |
| | | | | 'Upper' | Oil Reservoir | | |
| | | Donovan Sand | 'Middle' | | Minor Saline Reservoir | | |
| | | | | 'Lower' | Oil Reservoir | | |

Assessed Zone

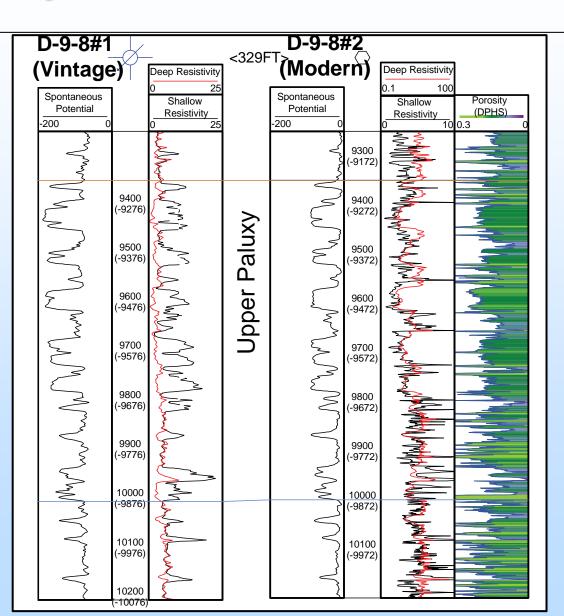
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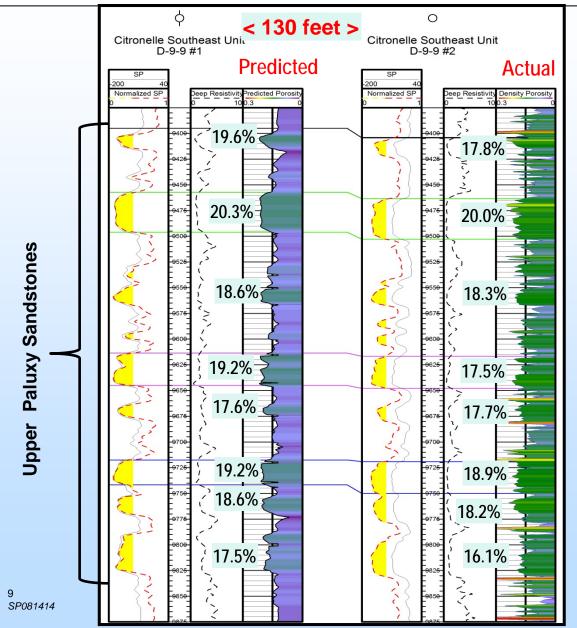
NW - SE Example

Porosity Prediction

- Most of the legacy wells have resistivity logs only and no porosity logs.
- 3 new wells with modern porosity logs were drilled on well pads with existing abandoned wells.
- These paired wells offer a unique opportunity for using a neural network approach to predict porosity.



Porosity Prediction Results

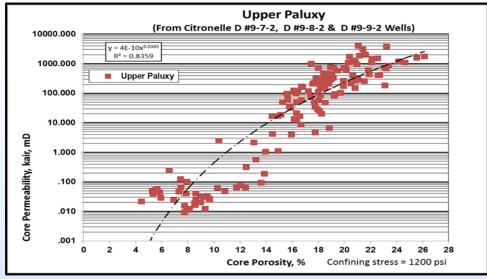


- Porosity predicted from Neural Net for D-9-9 #1 compared to actual density porosity from D-9-9 #2 well.
- Average porosity values for selected Upper Paluxy sandstones are shown.
- Average porosity values for Paluxy sandstones for "predicted" and "actual" are very close.
- Larger range between min and max values and finer vertical resolution for actual porosity than for "predicted" porosity.

Upper Paluxy Permeability Prediction

- 60 Model Layers
- Three whole cores from the injection and observation wells, SECARB Phase III Anthropogenic Test at Citronelle Field
- Porosity range: 4.4% 26.1%;
- Max permeability of 145 samples
 = 4,020 mD
- Mean porosity = 16.3%
- Mean k_{air} = 373.9 mD (arithmetic)
- Mean k_{air} = 19.3 mD (geometric)





Examples of Predicted Permeability for Upper Paluxy

| Core Porosity, | Upper Paluxy | Core Porosity, | Upper Paluxy | |
|-------------------|-----------------------|-------------------|-----------------------|--|
| % | Core Permeability, mD | % | Core Permeability, mD | |
| 6 | 0.004 | 24 | 1,186.7 | |
| 8 | 0.058 | 26 | 2,446.1 | |
| 12 | 2.26 | 28 | 4,778.6 | |
| 16 | 30.4 | 30 | | |
| 20 | 228.5 | 32 | | |
| 22 | 540.6 | 34 | | |

Porosity and Permeability Extrapolated for Each Model Layer

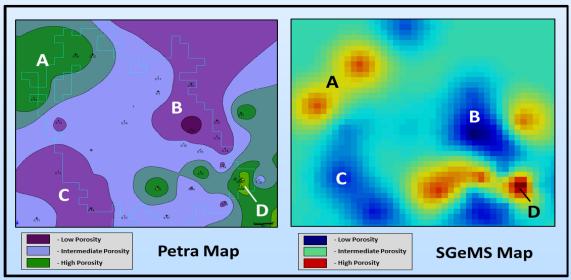
- Tertiary/ Quaternary Model Layers (Midway-Surface):
 - Predicted porosity from neural net not successful due poor log data quality/ missing data.
 - A single porosity and permeability value applied for each model layer over the entire study area
- Cretaceous Model Layers (Donovan to Selma):
 - Apply geostatistics to interpolate predicted porosity
 - Apply porosity-permeability transforms from core data to extrapolate reservoir permeability from predicted porosity

| Formation | # Model Layers |
|-------------------------|----------------|
| Alluvium | 1 |
| Citronelle | 1 |
| Miocene | 1 |
| Chickasawhay | 1 |
| Vicksburg | 1 |
| Jackson | 1 |
| Claiborne | 3 |
| Wilcox | 5 |
| Midway | 5 |
| Selma | 20 |
| Eutaw | 20 |
| Upper Tuscaloosa | 50 |
| Tuscaloosa Marine Shale | 10 |
| Lower Tuscaloosa | 30 |
| Washita | 60 |
| Fredericksburg | 60 |
| KWF Confining | 5 |
| Upper Paluxy | 60 |
| Lower Paluxy | 20 |
| Mooringsport | 5 |
| Ferry Lake Anhydrite | 1 |
| Donovan | 40 |

Heterogeneity Modeling

- Heterogeneity was modeled over the study area using geostatistics.
 - Generating realizations was tedious
 - (least squares) Kriging methods within Petra approximated geostatistics.

Porosity Interpolation for the Paluxy (Layer 7)

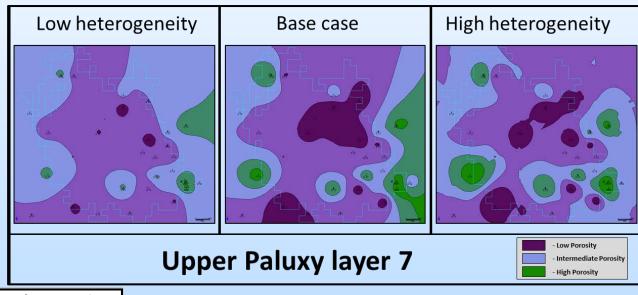


Letter markings on the maps highlight the corresponding low and high porosity regions that are spatially and morphologically similar.

Heterogeneity Modeling

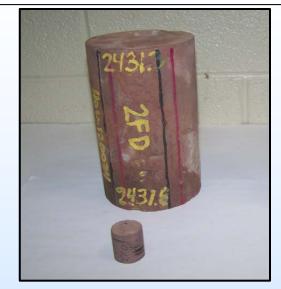
 Moving forward, Petra (Kriging) was used to generate the heterogeneity cases for each layer, proving more flexible and

efficient.



| Heterogeneity Scenario | Surface Style Contouring |
|------------------------|---------------------------|
| Base Case | Highly connected features |
| Low Heterogeneity | Minimum Curvature |
| High Heterogeneity | Disconnected Features |

Laboratory Results Confining Layer in the Paluxy Formation, Citronelle Field



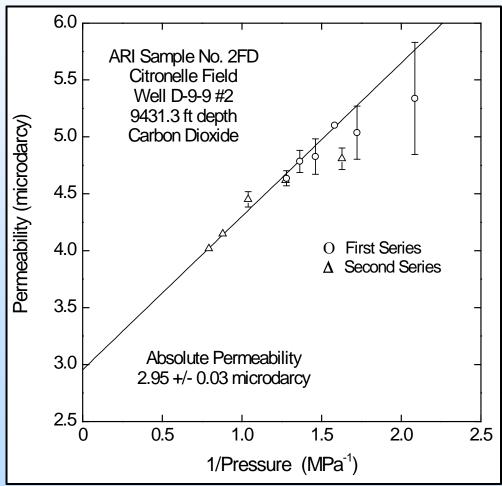
4" dia. core 1" dia. plug

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Absolute permeability of Sample 2FD from the SECARB Phase III Anthropogenic Test.

Core from Well D-9-9 #2, 9431.3 ft depth.



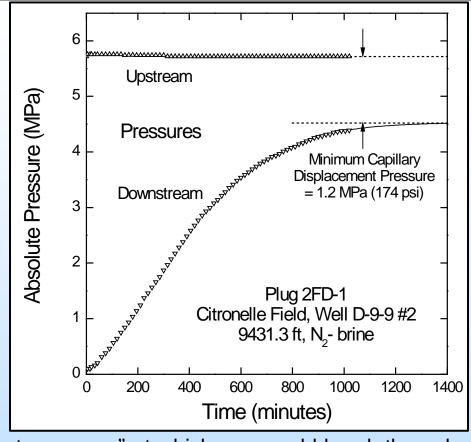
Determination of Minimum Capillary Displacement Pressure*†

Sample from the SECARB Phase III Anthropogenic Test, Paluxy Formation, Citronelle Field.

Plug 25 mm in diameter by 27 mm long. Single-phase permeability, 3 microdarcy.

Decay of a pressure pulse imposed across the plug, initially saturated with brine. Upstream pressure, 815 psig.

Upstream-downstream pressure difference approaches an asymptotic value equal to the capillary pressure at the narrowest throat in the highest conductivity pore.



Determines the "minimum capillary displacement pressure," at which gas would break through brine-saturated rock, given enough time.

Provides a better estimate of breakthrough pressure than obtained by increasing the upstream pressure until gas appears at the downstream face.

^{*}Hildenbrand, A., S. Schlömer, and B. M. Krooss, "Gas breakthrough experiments on fine-grained sedimentary rocks." *Geofluids*, **2002**, 2, 3-23.
*Hildenbrand, A., S. Schlömer, B. M. Krooss, and R. Littke, "Gas breakthrough experiments on pelitic rocks: comparative study with N₂, CO₂ and CH₄," *Geofluids*, **2004**, *4*, 61-80.

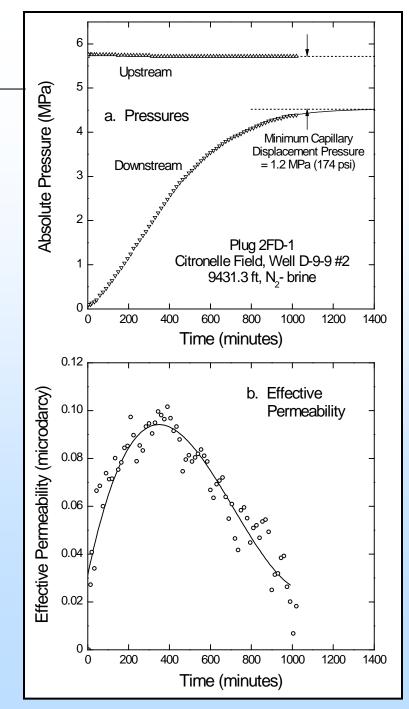
Effective Permeability*†

During the approach to the minimum capillary displacement pressure, the effective permeability to the gas phase can be obtained from the derivative of the downstream pressure with respect to time.

The effective permeability first increases, as brine drains and gas phase saturation increases, then decreases as brine returns, closing off open pores, from smallest to largest.

The maximum effective permeability, 0.09 to 0.10 microdarcy, ~ 1/30th of the absolute permeability, determines the maximum gas flow rate through a confining layer following breakthrough.

[†]Hildenbrand, A., S. Schlömer, B. M. Krooss, and R. Littke, "Gas breakthrough experiments on pelitic rocks: comparative study with N_2 , CO_2 and CH_4 ," *Geofluids*, **2004**, *4*, 61-80.



^{*}Hildenbrand, A., S. Schlömer, and B. M. Krooss, "Gas breakthrough experiments on fine-grained sedimentary rocks." *Geofluids*, **2002**, *2*, 3-23.

Effective Permeability vs. Pressure

Dependence of the effective permeability of the brinesaturated plug on upstream to downstream pressure difference, following breakthrough.

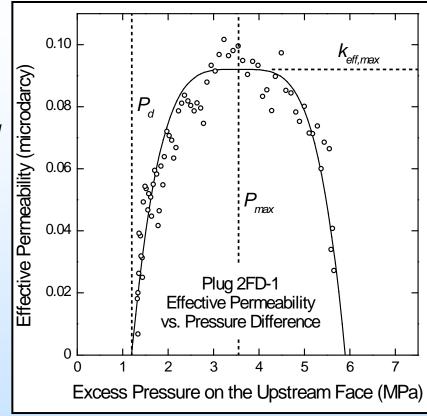
The minimum capillary displacement pressure, P_d (1.2 MPa, 174 psi) is the pressure at breakthrough, on the left.

The effective permeability varies from 0 at the minimum capillary displacement pressure to a maximum of 0.09 to 0.10 microdarcy at $P_{max} = 3.55$ MPa (515 psi), at the minimum brine saturation and maximum gas saturation.

The dependence of the effective permeability on pressure, above the minimum capillary displacement pressure, can be described by:

$$\frac{k_{eff}}{k_{eff,max}} = 1 - \left(\frac{P_{max} - P}{P_{max} - P_d}\right)^4 \qquad P_d \le P \le P_{max}$$

The effective permeability is expected to remain at its maximum value, $k_{eff,max}$, with further increase in excess gas pressure above P_{max} .



The "excess pressure" in the laboratory set-up is the upstream to downstream pressure difference across the plug. In the field it would be the difference between the pressure in stored CO₂ at the interface with a confining layer and the local hydrostatic pressure.

Size Distribution of Conducting Pores Derived from the Dependence of Effective Permeability on Pressure

Dependence of effective permeability on pressure:

$$\frac{k_{eff}}{k_{eff,max}} = 1 - \left(\frac{P_{max} - P}{P_{max} - P_d}\right)^4 \tag{1}$$

Relationship between pore radius and capillary pressure:

$$P_{capillary} = \frac{2 \gamma \cos \vartheta}{r} \tag{2}$$

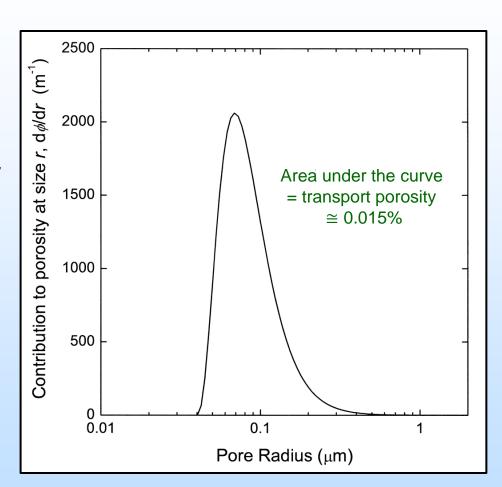
Washburn (1921).

Rate of change of porosity, ϕ , with increase In radius, r, of N parallel monosize pores:

$$\frac{d\phi}{dr} = \frac{8}{r^2} \frac{dk}{dr} \tag{3}$$

Hildenbrand et al., Geofluids, (2002) 2, 3-23.

Substitute Eq. (2) into Eq. (1), then differentiate Eq. (1) with respect to *r*, and substitute the result into Eq. (3).



Volume-based size distribution of conducting pores.

Leakage through a Confining Layer

Injected CO₂ is treated as a simple column having uniform cross section and depth.

Rate of CO_2 storage (mass per unit time per unit plan area) = injection rate – leakage rate.

Excess pressure at the confining layer/reservoir interface = (density brine - density CO_2)

x g x height of CO_2 column

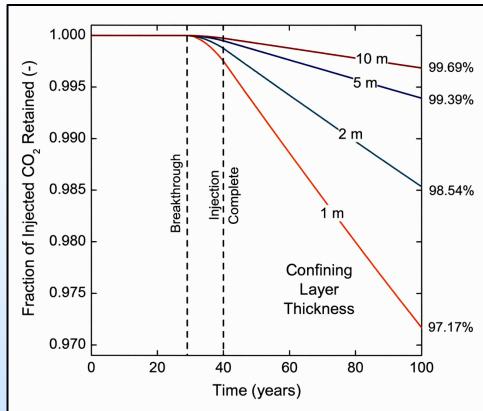
Leakage begins when the excess pressure exceeds the minimum capillary displacement pressure.

The dependence of effective permeability on excess pressure, following breakthrough, is described by the equation fit to the measurements.

CO₂ is injected at a rate of 500 metric tons/day for 40 years into wells on 40-acre centers.

Breakthrough occurs 29 years after the start of CO_2 injection.

For confining layers thicker than about 5 m, ${}_{29}99\%$ of CO_2 is retained at 100 years.



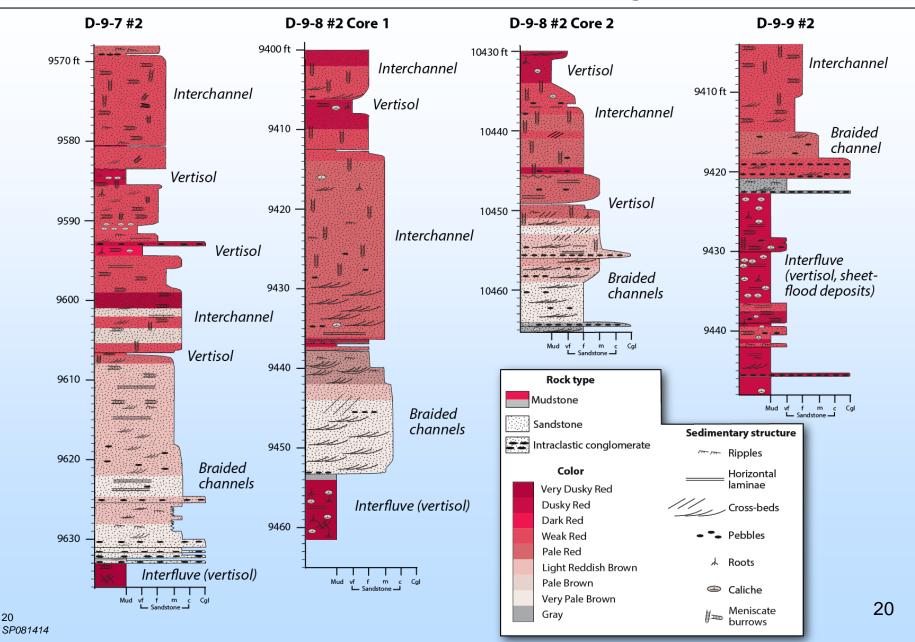
Porosity of the storage reservoir: 19%

Minimum capillary displacement pressure: 174 psi

 CO_2 column height at breakthrough: 273 m Maximum permeability of the confining layer: $k_{eff,max} = 0.095$ microdarcy at 515 psi

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Graphic Core Logs



Reservoir Sandstone

Cross-beds



Ripple cross-laminae



Core width = 10 cm

Meniscate burrows



Geological Highlights

- Reservoir: Multistorey bedload-dominated fluvial deposits.
- ✓ Baffles, barriers, and seals: Interfluvial mudstone with caliche.
- ✓ Sandstone is very fine- to coarse-grained subarkose and arkose.
- Diagenesis reflects dominant influence of soil development.
- ✓ Grain dissolution, quartz overgrowth, illuvial clay coating, carbonate cement influence reservoir quality.
- ✓ Reservoir porosity commonly >20%.
- ✓ Permeability up to 3.8 Darcies.
- ✓ Similar deposits are widespread in Lower Cretaceous of Gulf of Mexico region.



Accomplishments to Date

- Completed geologic model
- Successful implementation of the Neural Network approach to predict porosity
- Generated low, base and high heterogeneity cases
- Completed simulation models, handed over to UAB for testing, debugging and execution
- Laboratory measurements/estimates of
 - effective permeability,
 - minimum capillary displacement pressure, and
 - leakage impact
- OSU is underway with Paluxy core, petrographic and x-ray diffraction







Key Findings/ Lessons Learned

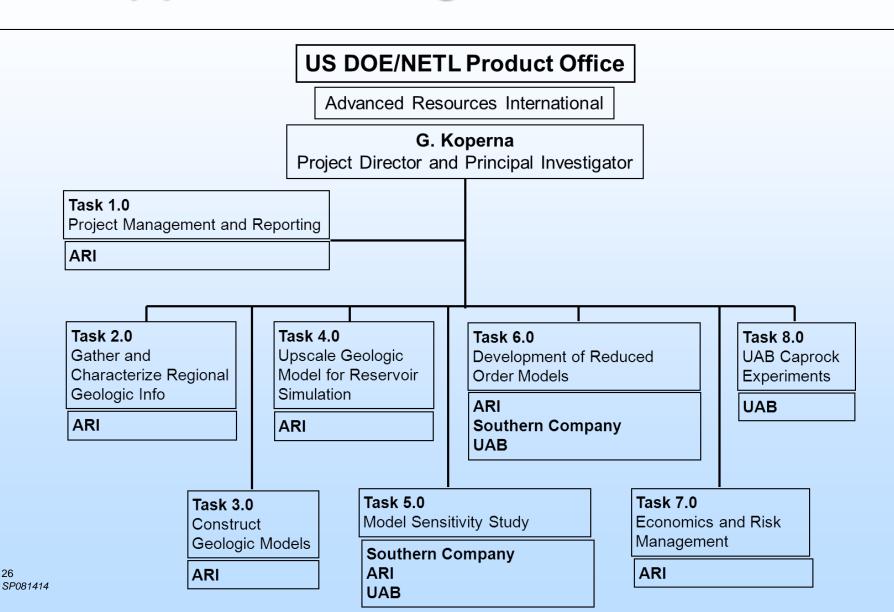
- The Project Team is able to successfully characterize a subsurface volume of 1.9E+13 ft³ for reservoir simulation (56 square miles x 12,000 vertical feet), by combining legacy geophysical log data with modern log data, core data, and state of the art interpretive tools like neural net and geostatistics software.
- Neural network tools were extremely effective in "modernizing" the vintage geophysical well logs to ascertain spatial variations in porosity and, by proxy, permeability.
- Kriging, in lieu of full geostatistical analyses may greatly improve the workflow of the project when reviewing heterogeneity variability.
- Effective permeablities through brine-filled confining units appear to be on the order of 1/30th of the absolute permeability.
- CO₂ containment through significantly thick and low permeability confining units appears to be >99%, based on Paluxy data.

Future Plans

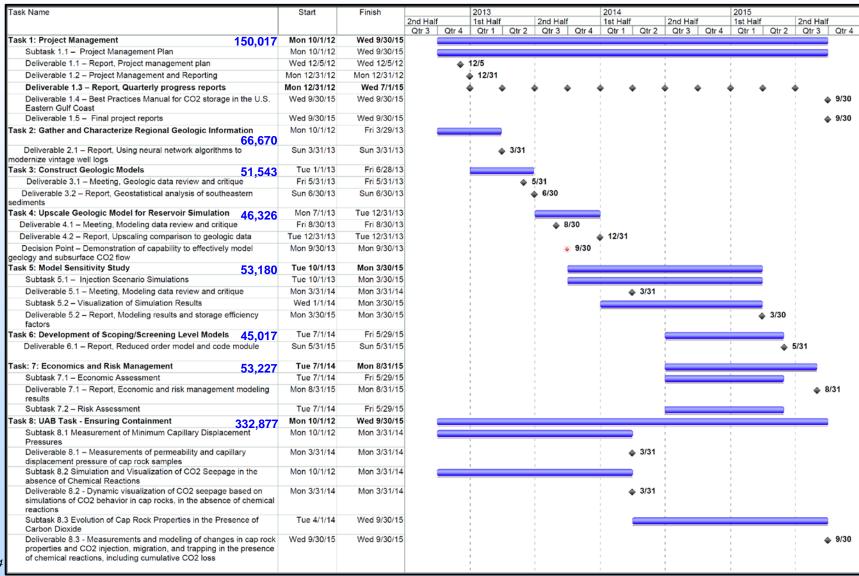
- **Sensitivity Study**: Will explore sensitivities such as well design and lateral heterogeneity to maximize storage capacity while minimizing the operation's footprint.
- Optimization: Will incorporate economic and risk management considerations which will be overlain on the modeling results to ascertain their financial impact.
- Cap Rock Analysis: Caprock analysis will provide regional seal characteristic data to be used in numerical modeling.
- New Storage Efficiency Factors: Will develop new commercial storage efficiency factors.
- **Screening Models**: Will develop simplified screening models to cost effectively identify potential commercial storage sites.
- Scoping Level Models: Will develop a scoping level model to provide baseline storage capacity and injectivity and estimate ground deformation, plume extent and pressure build-up.
- **Best Practices Manual**: Will produce a Best Practices Manual for optimized commercial-scale storage.

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Appendix: Organization Chart



Appendix: Gantt Chart



Appendix: Bibliography

- Geologic Characterization for the U.S. SECARB Anthropogenic Test; Combining Modern and Vintage Well Data to Predict Reservoir Properties, Shawna R. Cyphers, Hunter Jonsson, and George J. Koperna, Jr., poster presentation, American Association of Petroleum Geologists, Annual Convention & Exhibition, Pittsburgh, PA, May 19-22, 2013.
- Constructing a Geologic Model to Simulate Commercial Scale CO₂ Injection and Optimization of Storage Capacity in the Southeastern United States, Hunter Jonsson, Shawna Cyphers, George Koperna, Robin Petrusak, presentation abstract accepted for Carbon Management Technology Conference, CMTC 2013, Alexandria, Virginia, October 21 – 23, 2013
- Constructing a Geologic Model to Simulate and Optimize the Commercial Scale Injection and Storage of CO₂ at Citronelle Field, Mobile County, Alabama, J. MacGregor, R. Petrusak, S.R. Cyphers, H. Jonsson, A. Oudinot, and G.J. Koperna, poster presentation, 2014 AAPG Annual Convention & Exhibition, Houston, Texas, April 6- 9 2014.