Development of Spallation-Resistant Coatings: Preliminary Results

University Turbine Systems Research Workshop Irvine, California October 4, 2012

Matthew N. Cavalli and John P. Hurley





Project Overview

- University of North Dakota Mechanical Engineering and the UND Energy & Environmental Research Center (EERC) are working with Siemens Power Generation to test a new method for joining high-temperature alloys for use in advanced high-hydrogen-gas-burning turbines.
- Will bond thin plates of oxidation- and spallation-resistant Kanthal APMT[™] to high-strength CM247LC and Rene[®] 80 using evaporative metal (EM) bonding.
- Bonded parts, with and without thermal barrier coatings (TBCs), will be tested for oxidation, corrosion, and spallation resistance.





Alloy Compositions

Composition of Kanthal APMT in wt % – Dispersion-Strengthened												
	Cr	Al	Мо	Mn	Si	Fe						
APMT	22	5	3	0.4	0.7	Bal.						

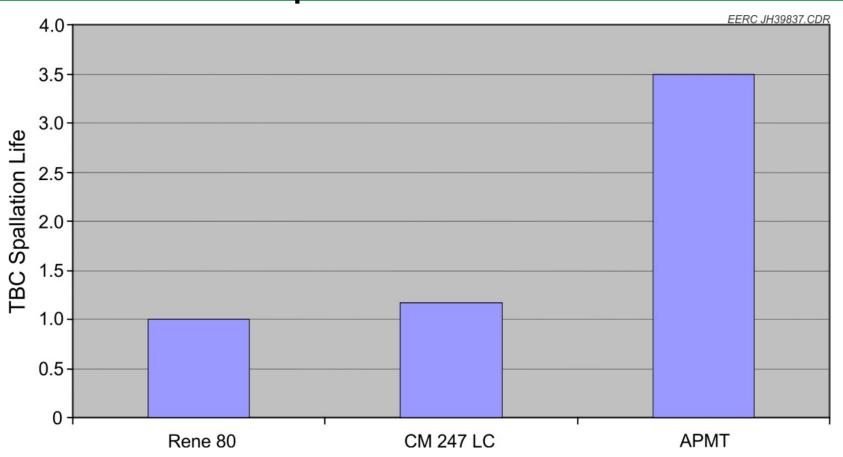
	Composition of CM 247 LC in wt % – Gamma Prime-Strengthened														
	Fe	Ni	Cr	Al	Ti	Co	Мо	Та	W	Nb	Hf	Mn	Si		
CM247LC	_	Bal.	8.1	5.6	0.7	9.5	0.5	3.2	9.5	0.1	1.4	_	_		

	Composition of Rene 80 in wt% – Gamma Prime-Strengthened														
	Cr	С	Мо	W	Ti	Nb	Со	Al	В	Fe	Zr	Ni			
Rene 80	14.2	0.16	4.0	4.1	5.1	0.03	9.4	3.0	0.02	0.10	0.04	Bal.			





Prior Work: TBC Spallation Lifetimes



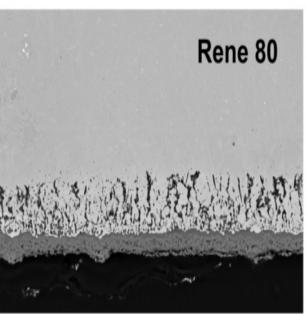
Testing at Siemens Energy Inc. shows that the spallation lifetime of TBCs on APMT is three times that of a similar coating on Rene 80 or CM247LC.

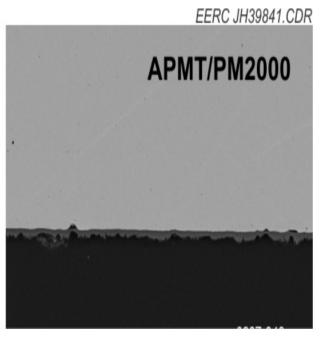




Prior Work: Alloy Oxidation Rates





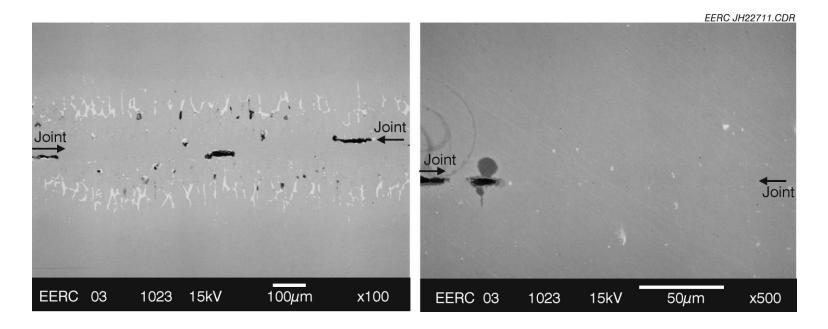


The oxidation rate of APMT is much lower than for CM247LC or Rene 80.





Prior Work: Transient Liquid Phase (TLP) Bonding



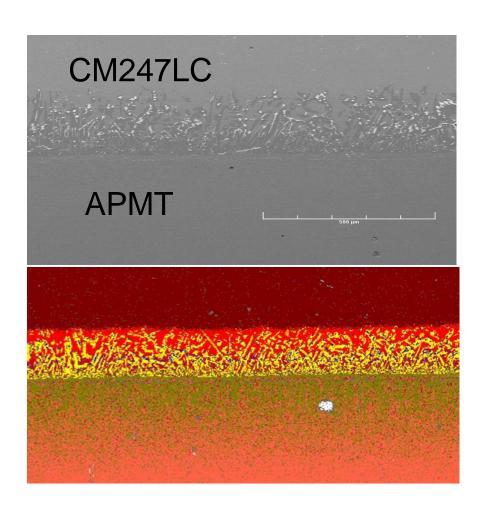
- Welding of advanced alloys is not possible because critical structures are destroyed.
- TLP bonding uses a reactive braze that diffuses away from the joint.
- Bonding alloys need to have low melting points, be soluble, and not form intermetallics.
- Evaporative metal (EM) bonding is an alternative





Prior Work: Joining Complex Geometries

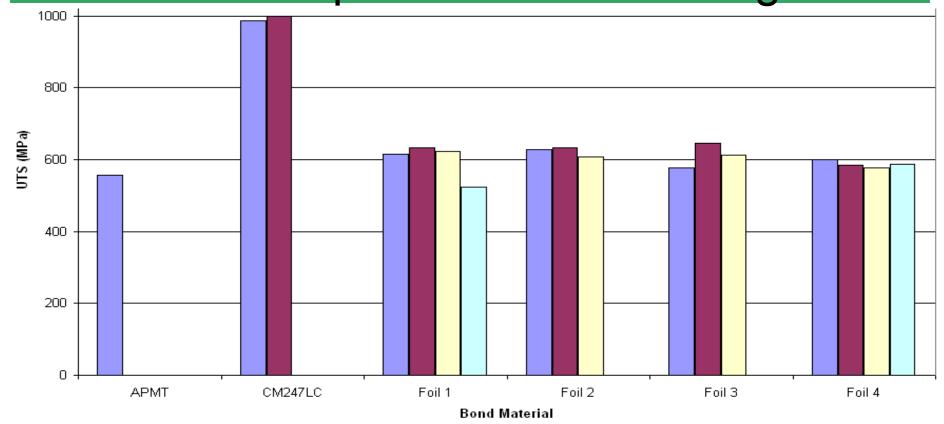
- Scanning electron microscopy photo top, x-ray map on bottom.
- Needle growth and interdiffusion create a joint stronger than the APMT.
- Nickel diffuses up to 700 µm into APMT.
- Iron diffuses 200 µm into the CM247LC.







Prior Work: Room Temperature Joint Strengths



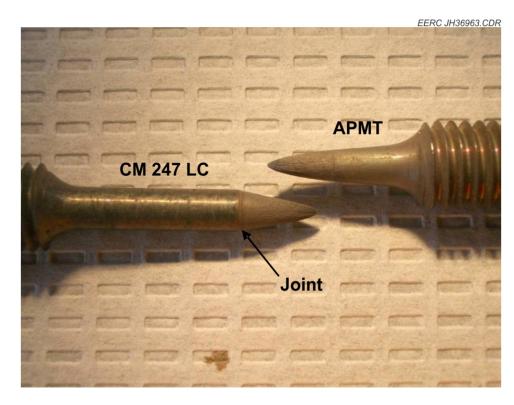
- Room-temperature ultimate tensile strength results for joints made with four joining alloys.
- All samples broke within the APMT, showing the joints are stronger than the APMT.





Prior Work: 950°C Stress Rupture Test

- Stress rupture tests done at 950°C using 20 MPa, the 100-hour APMT rupture stress.
- Samples broke within the APMT, not the joint.
- APMT was much weaker than anticipated.

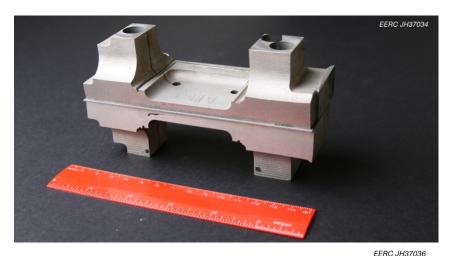






Prior Work: Joining Complex Geometries

- Joined actual turbine ring segments of CM247LC with APMT sheet in between.
- Demonstrates the ability to cover large areas of superalloys with oxidation- and spallation-resistant APMT using EM bonding.
- Joints were stronger than the APMT.









Articulated Clamping System

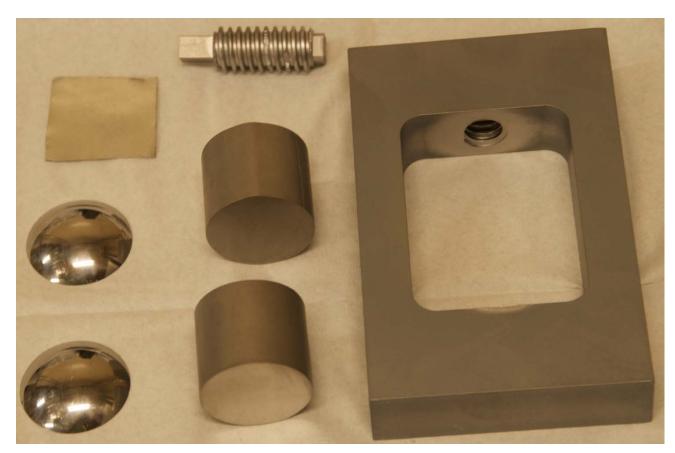
- Specimens electro-discharge machined to shaped and then polished
- Bonding surface blasted with silica beads.
- Clamp made from low-CTE metal (Mo).
- Steel hemispheres (E52100) used to articulate the pieces, which is necessary because of the thinness of the foils. Steel used to facilitate modeling.
- Joints of APMT to CM 247 and APMT to Rene 80







Articulated Clamping System





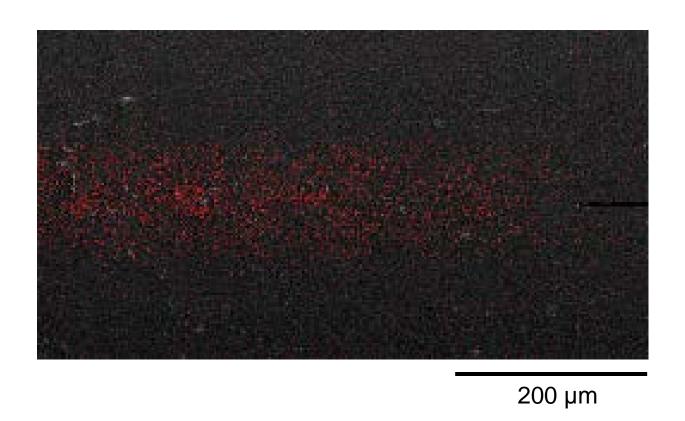




- Task 1 Determine diffusion rates of evaporative metal through APMT, CM247LC, and Rene 80 as functions of temperature.
 - Prepare bonded rods at different temperatures and times.
 - Cross-section bonded rods, and measure bonding metal concentration gradients.
 - Develop diffusion rate equations as functions of temperature.
 - October 2011 March 2013



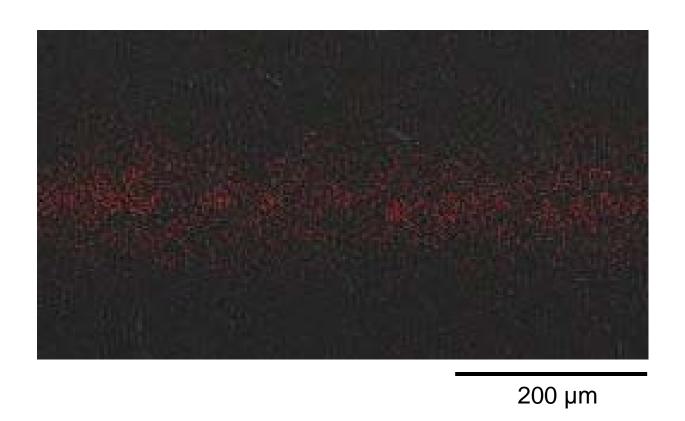




Elemental Map of Zn – CM 247 bonded at 1214°C for 1 hour (joint edge)



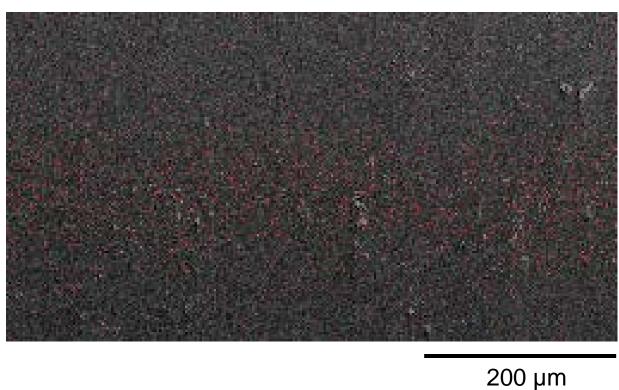




Elemental Map of Zn – CM 247 bonded at 1214°C for 1 hour (joint center)



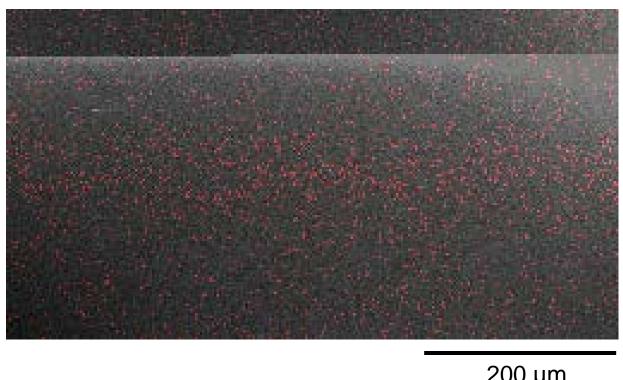




Elemental Map of Zn – CM 247 bonded at 1214°C for 3 hours (joint center)





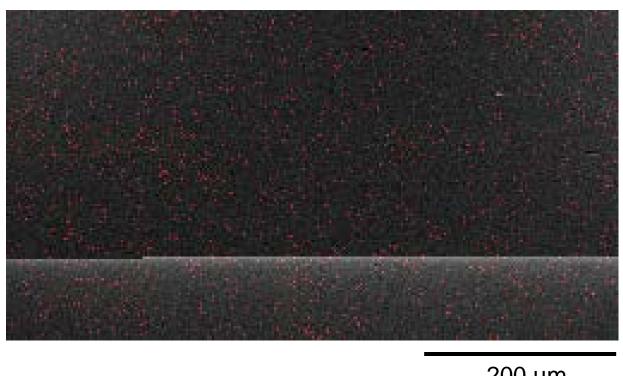


200 µm

Elemental Map of Zn – APMT bonded at 1214°C for 1 hour (joint center)





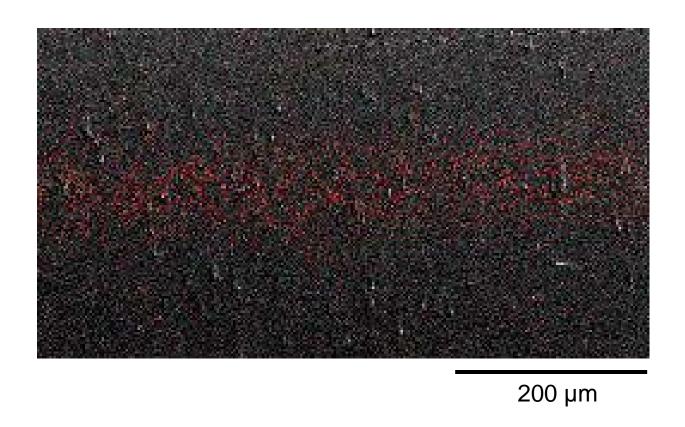


200 µm

Elemental Map of Zn – APMT bonded at 1214°C for 3 hours (joint center)







Elemental Map of Zn – Rene 80 bonded at 1214°C for 1 hour (joint center)





- Task 2 Model bonding pressure distributions in complex joints.
 - Measure bonding pressures in actual joints.
 - Measure high temperature properties of substrate metals (E, α)
 - Model pressures at the bond line at temperature.
 - Design clamping system.
 - October 2011 March 2013

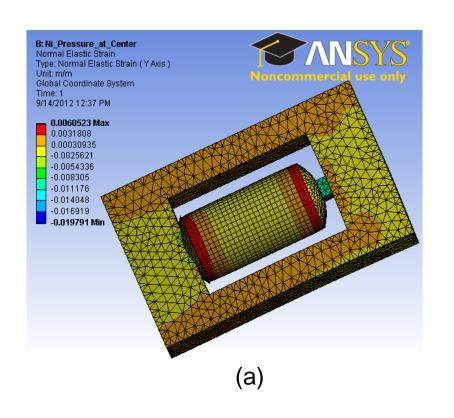


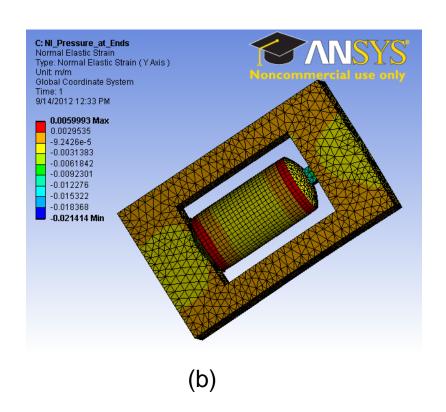












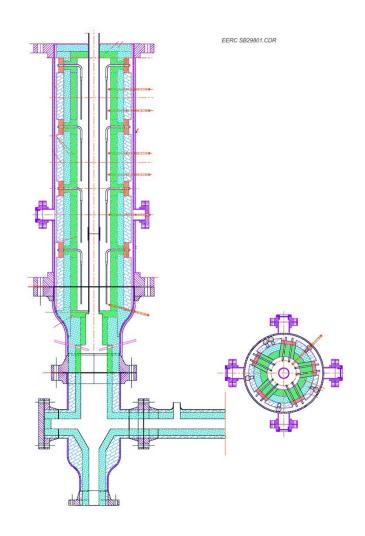
Comparison of strains in the bonding assembly when loads applied at a) joint center or b) joint ends.





Task 3 – Characterization of combusted syngas contaminants.

- Information to be used in designing later corrosion testing – contaminants will not be similar to gasifier fly ash.
- Collection of microcontaminants in combusted syngas created in a pilotscale gasifier.
- Analysis of captured microcontaminants by SEM.
- Data will be made available to other researchers.









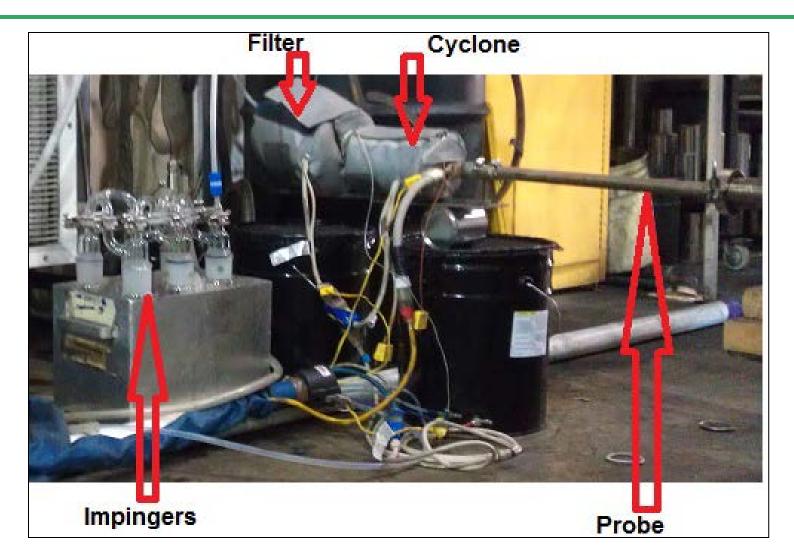
EERC entrained flow gasifier test rig



EERC fluidized bed gasifier test rig











- Sampling method follows EPA methods 26A and 29
- Flow enters probe at about 750°C and cools to 100°C
- Flow passes through a polycarbonate filter (0.1 micron diameter holes)
- Flow enters water-filled impingers

Trace Metal	As	Ве	Cd	Со	Cr	Mn	Ni	Pb	Sb	Se	Hg
LLQ (µg/L)	0.5	0.1	0.1	0.5	0.1	0.1	0.2	0.1	0.1	1.0	0.02
Conc.(µg/L)	0.4	0.2	0.2	0.4	8.2	63.80	7.53	0.76	0	1.1	0.99
Conc.(µg/m³)	0.12	0.06	0.06	0.12	2.39	18.58	2.19	0.22	0	0.32	0.29

Trace Metal	K	Mg	Ca	Na	Fe	Ti	V	Мо	Zn	Ge
LLQ (μg/L)	20	20	20	20	20	20	20	20	20	20
Conc.(µg/L)	140	128.8	670.4	243.5	354.6	15.84	0.777	3.959	13.42	1.881





Spectrum	0	Si	S	Cr	Fe	Ni	Total
Spectrum 1	63.83	3.74	18.98	2.06	11.40		100.00
Spectrum 2	62.65	2.68	19.45	2.01	12.15	1.06	100.00
Spectrum 3	70.25		17.28		12.47		100.00
Spectrum 4	65.51	3.26	18.11	2.54	10.58		100.00
Spectrum 5	72.48		17.11		10.41		100.00
Max.	72.48	3.74	19.45	2.54	12.47	1.06	
Min.	62.65	2.68	17.11	2.01	10.41	1.06	

Comp	Composition of 316L Stainless Steel in wt % (max)													
С	Р	S	Cr	Al	Мо	Mn	Si	Fe						
0.03	0.045	0.03	16-18	10-14	2-3	2	0.75	Bal.						





- Task 4 Preparation of APMT-plated superalloy turbine parts.
 - Use data from Tasks 1 and 2 to design clamping system and time—temperature heat treatment.
 - April 2013 September 2014
- Task 5 Environmental testing of plated turbine parts.
 - Oxidation and spallation testing at Siemens Energy.
 - Corrosion testing at the EERC.
 - October 2013 September 2014
- Task 6 Reporting (ongoing).





Acknowledgements

- This work funded by the Department of Energy, Award #DE-FE0007325
- Briggs White, Program Manager
- Serges Tatsinkou-Nguelo
- Joshua Braband





Disclaimer

This presentation was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government, nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.



