

the Energy to Lead

Hybrid Membrane/Absorption Process for Post-combustion CO₂ Capture

DOE Contract No. DE-FE-0004787

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NETL CO₂ Capture Technology Meeting
July 9, 2012

Introduction to GTI and PoroGen

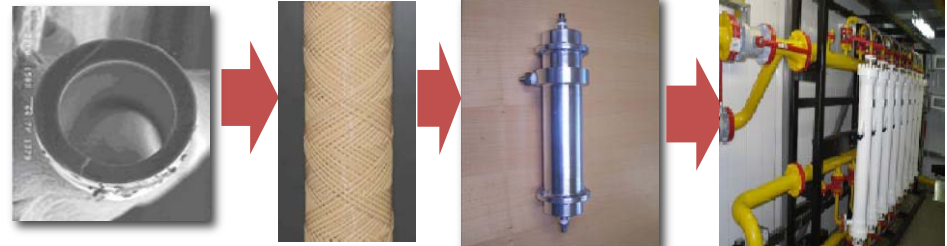


- Not-for-profit research company, providing energy and natural gas solutions to the industry since 1941
- Facilities
 - 18 acre campus near Chicago
 - 200,000 ft², 28 specialized labs



- Materials technology company commercially manufacturing products from high performance plastic PEEK (poly (ether ether ketone))
- Products ranging from membrane separation filters to heat transfer devices

PEEK Fiber + Cartridge + Module = Separation system



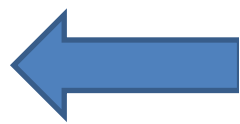
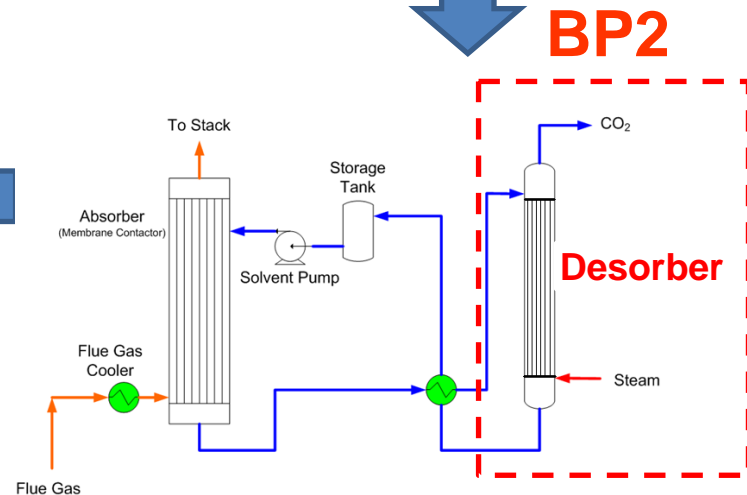
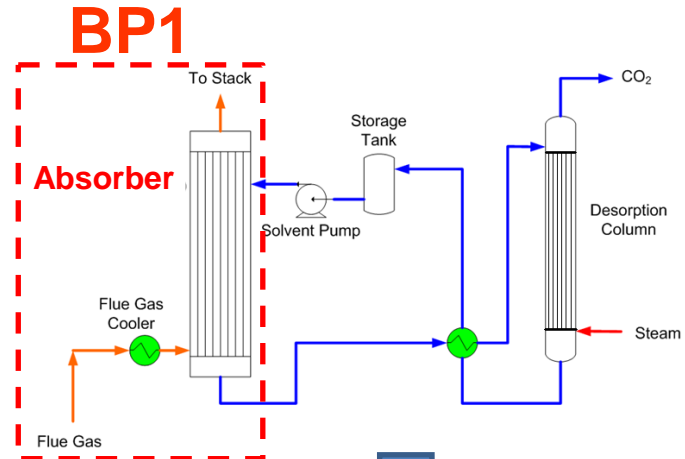
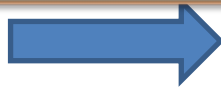
Project overview

- **Funding**: \$3,736 K (DOE: \$2,986 K, Cost share: \$750 K)
 - BP1 budget: DOE: \$799 K, Cost share: \$200 K (20%)
 - BP2 budget: DOE: \$1,036 K, Cost share: \$262 K (20%)
 - BP3 budget: DOE: \$1,149 K, Cost share: \$287 K (20%)
- **Performance period**: Oct. 1, 2010 – Sept. 30, 2013
- **Project participants**:
 - **GTI**: process design and testing
 - **PoroGen**: membrane and membrane module development
 - **Aker Process Systems**: economic analysis
 - **Midwest Generation**: providing field test site

Objective and scope

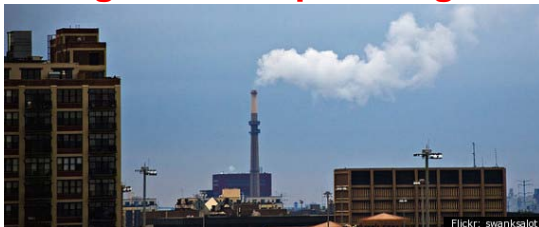
2010

Objective: develop PEEK membrane contactor technology to meet DOE's target of $\geq 90\%$ CO₂ capture, < 35% increase in COE



BP3

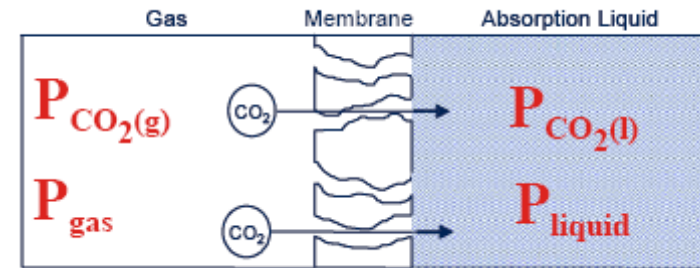
Integrate absorption/regeneration



Field testing for **25 KW** equivalents of CO₂ capture (**0.5 ton/day**)

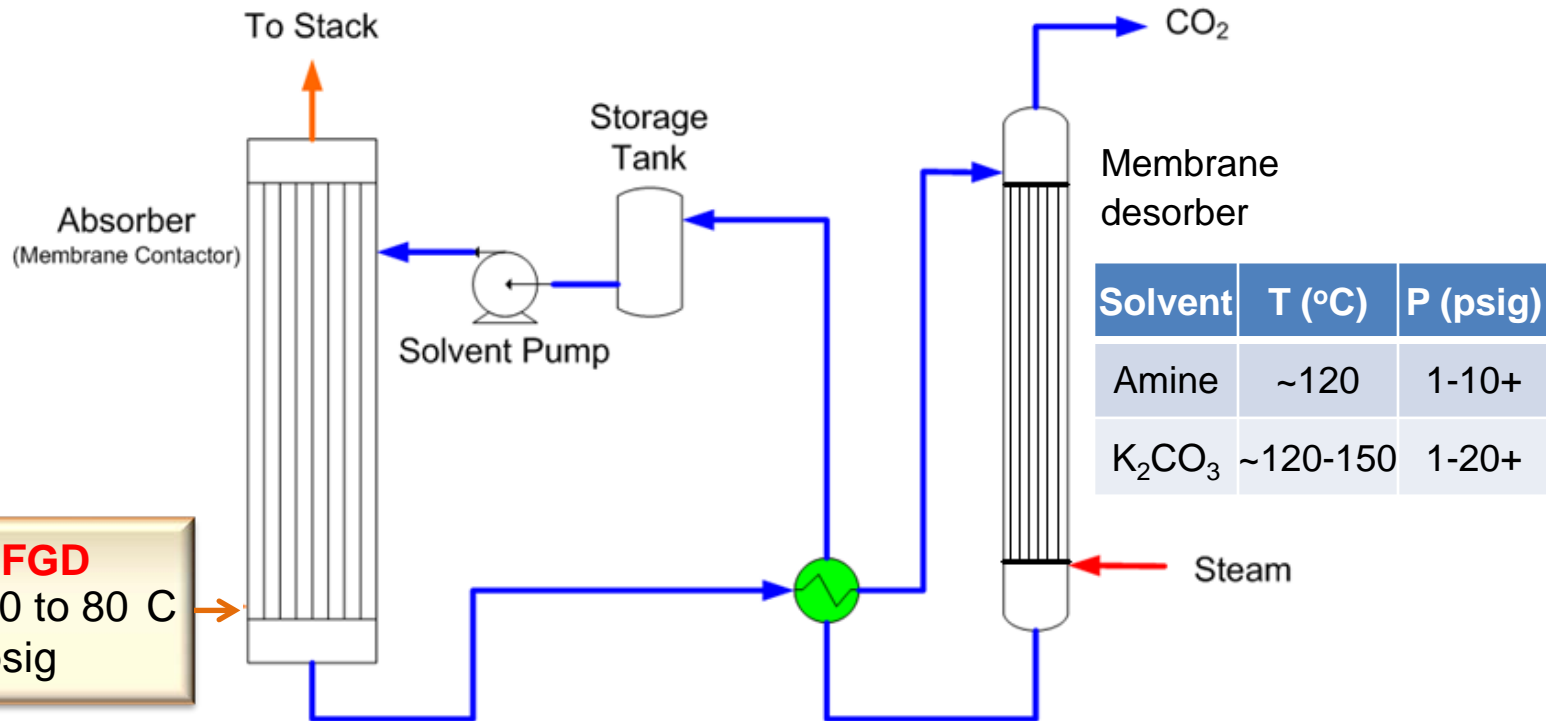
What is a membrane contactor?

- High surface area membrane device that facilitates mass transfer
- Gas on one side, liquid on other side
- Membrane does not wet out in contact with liquid
- Separation mechanism:** CO₂ permeates through membrane and reacts with the solvent; N₂ does not react and has low solubility in solvent
- Comparison to conventional membrane process**



Membrane technology	Need to create driving force?	CO ₂ /N ₂ selectivity (α)	Can achieve >90% CO ₂ removal and high CO ₂ purity in one stage?
Conventional membrane process	Yes. Feed compression or permeate vacuum required	Determined by the dense "skin layer", typically $\alpha = 50$	No. Limited by pressure ratio, multi-step process required*
Membrane contactor	No. liquid side partial pressure of CO ₂ close to zero	Determined by the solvent, $\alpha > 1000$	Yes

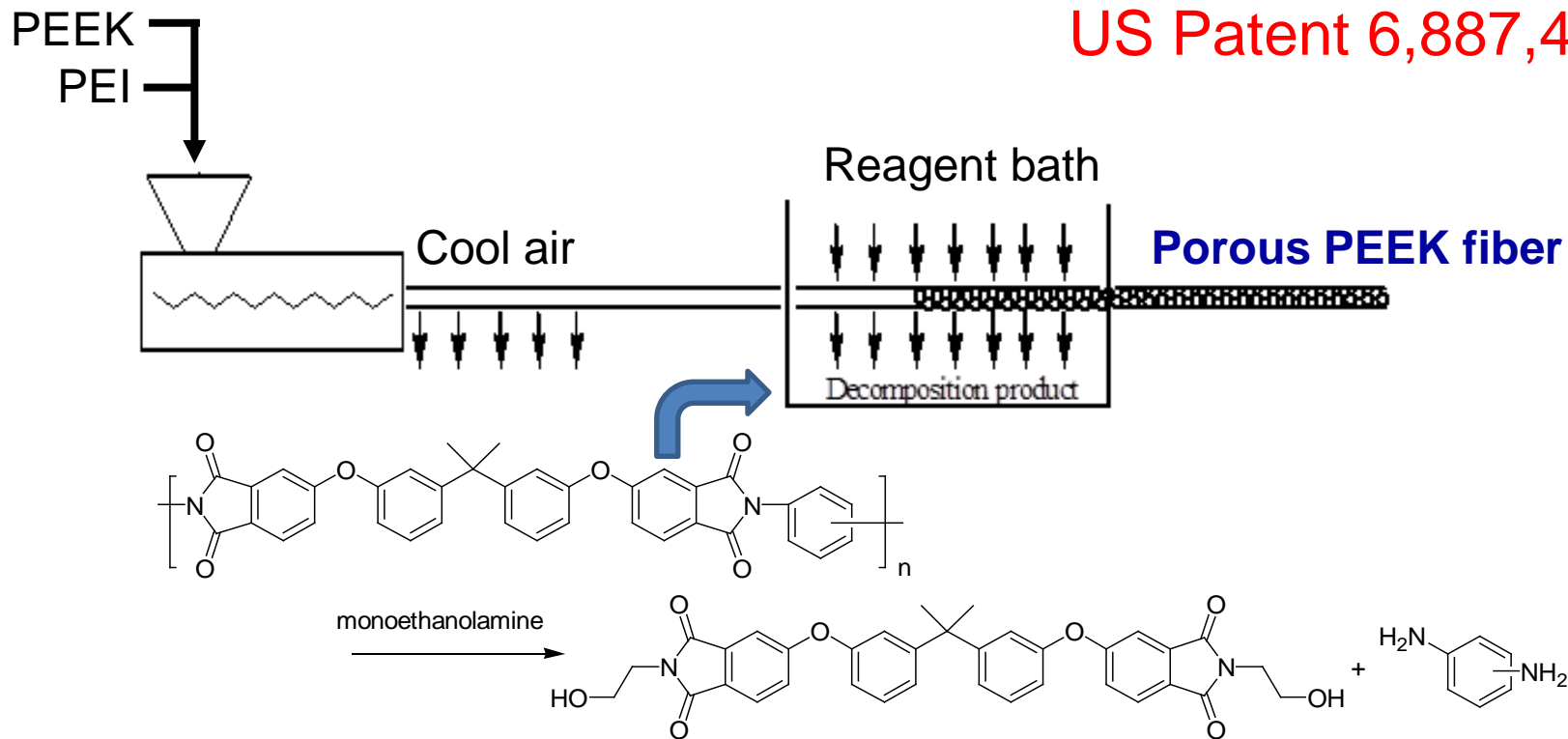
Process description



Process identical to DOE's benchmark technology amine plant except membrane absorber and desorber are used instead of absorption and regeneration towers

PoroGen has a patented process for preparation of nano-porous PEEK hollow fiber membrane

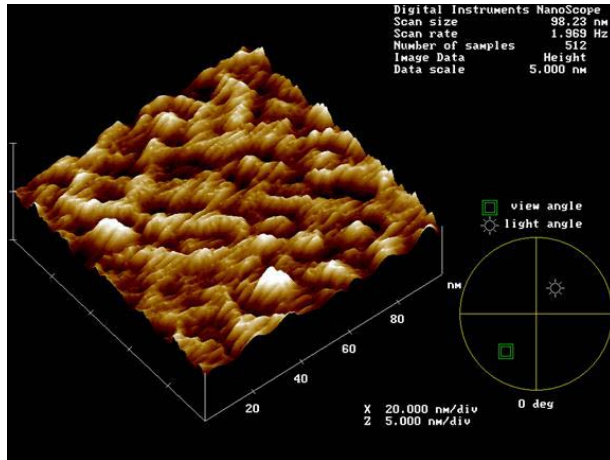
US Patent 6,887,408



Hollow fiber morphology, and pore size are continuously improved to meet membrane contactor operating requirements

Two types of super-hydrophobic membranes under development

a) Nano-porous PEEK hollow fiber membrane

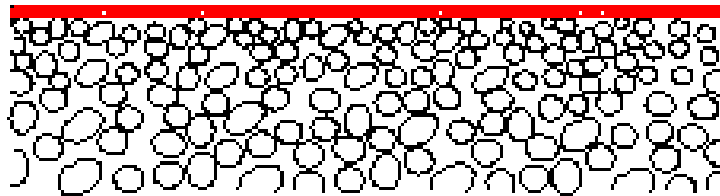


Super-hydrophobic surface not wetted by alcohol



Alcohol droplet

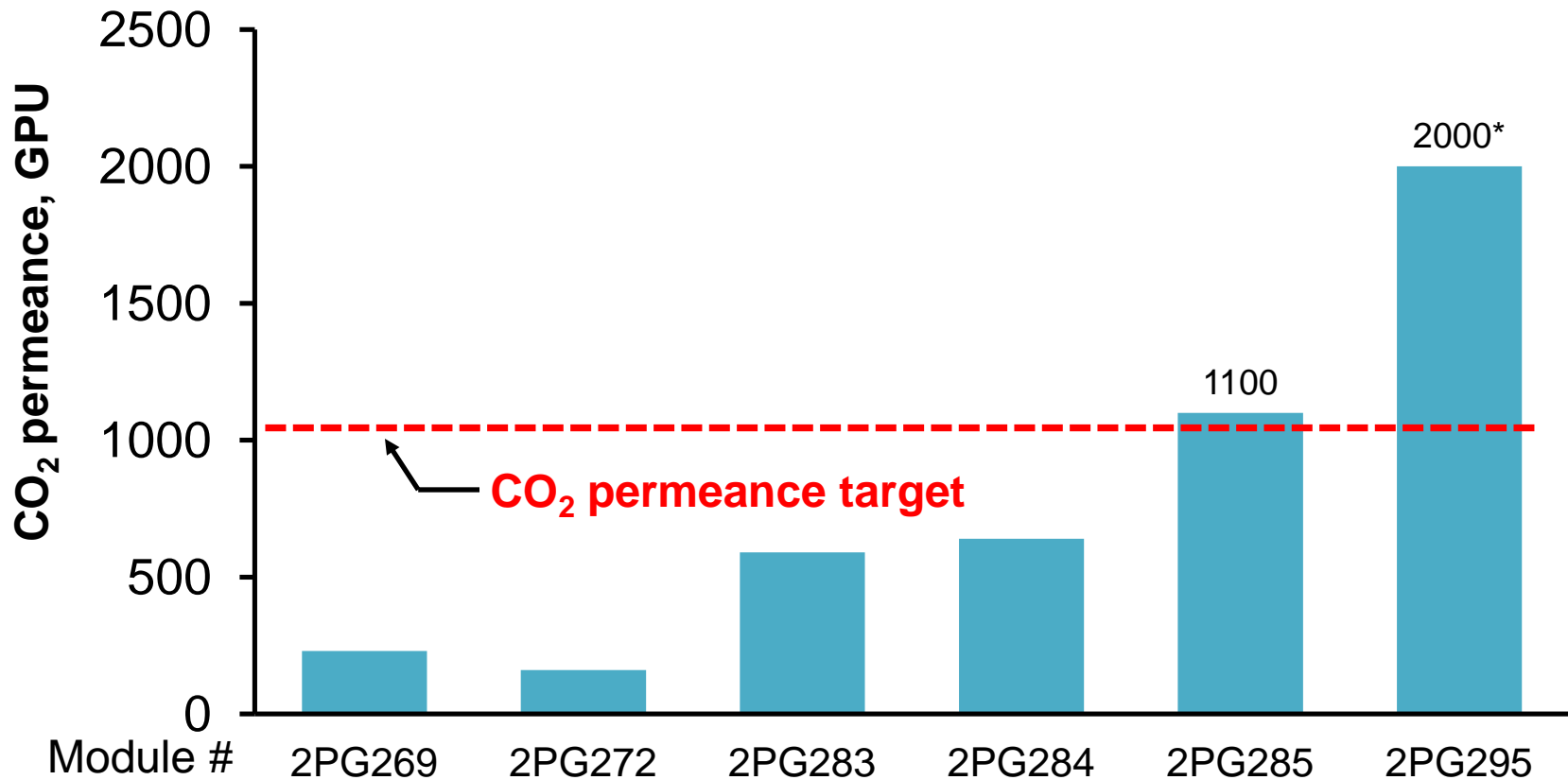
b) Composite PEEK hollow fiber membrane Thin layer (0.1 μm) of smaller surface pores



Asymmetric porous structure

Membrane intrinsic CO₂ permeance exceeded initial target for commercial performance

More than **40 modules** constructed by PoroGen

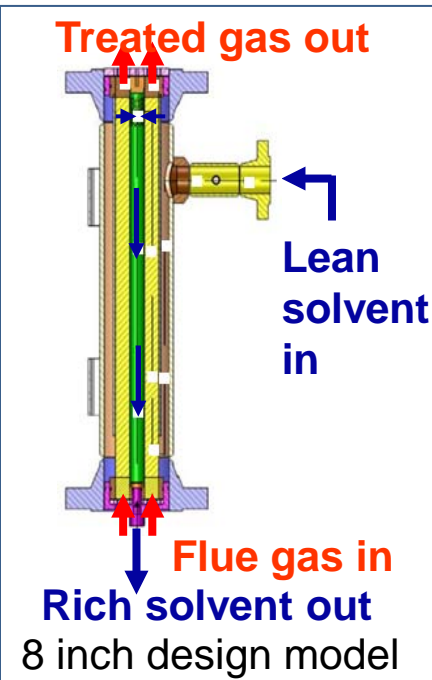


Beginning of the project

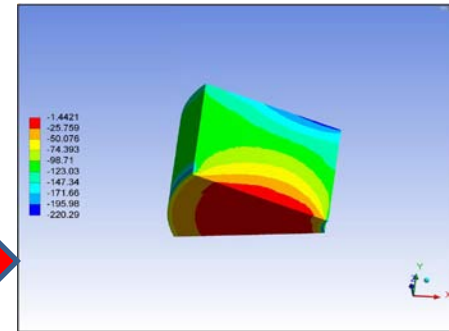


Now

Membrane module design and scale-up

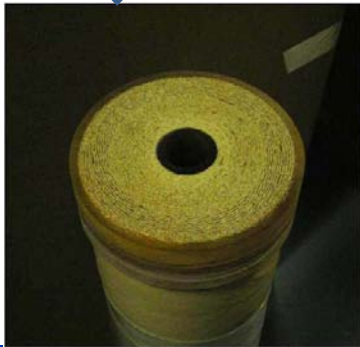


- Design of commercial size, flue gas CO₂ capture module completed
- Design validated through CFD modeling
- Scaling up from 1 m² (lab-scale) to 100 m² (8-inch commercial module)
- Production capability of 8" diameter module on commercial scale equipment established



Tubesheet CFD stress analysis

Cartridge tubesheet for Ø8" x 60" long module



8-inch structured packing module produced



BP1: Membrane Absorber Study

Bench-scale membrane **absorber** CO₂ capture performance demonstration

- **Feed**: Simulated flue gas compositions (N₂ + CO₂ saturated H₂O, SO_x, NO_x, O₂) at temperature and pressure conditions after FGD.
- **Membrane module**: Performance can be essentially linearly scaled to commercial size modules.
 - Uncertainty exists because gas/liquid contactor interface issues
 - Additional factors affect mass transfer coefficient
- **Solvents**: Commercial aMDEA (40 wt%) and activated K₂CO₃ (20 wt%), testing of advanced solvents planned.
- **Use of design of experiment test matrix**: totally **over 140 tests**.



Module for lab testing
(Ø2" x 15" long, 1m²)

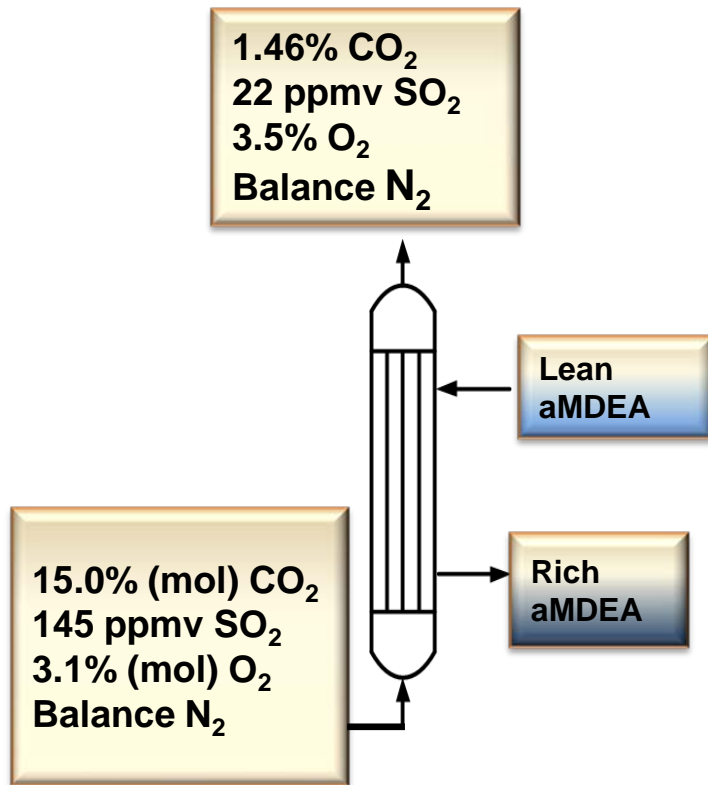
Technical goal achieved with commercial aMDEA and K_2CO_3/H_2O

Module 2PG285, 1100 GPU

Parameters	Goal	aMDEA	K_2CO_3
CO ₂ removal in one stage	$\geq 90\%$	90%	94%
Gas side ΔP , psi	≤ 2	1.6	1.3
Mass transfer coefficient, (sec) ⁻¹	≥ 1	1.7	1.8

CO₂ removal rate is not affected by O₂, SO_x, and NO_x contaminants in feed

Module 2PG286, 1000 GPU



Measured results:

CO ₂ removal	91%
Mass transfer coefficient, (sec) ⁻¹	1.6
Gas side ΔP, psi	1.6
CO ₂ capture rate, kg/h/m ²	0.5

Compared to conventional amine scrubber

- 15% less of the inlet SO₂ was absorbed by the solvent as compared with conventional column. The formation of heat-stable salts will be reduced.

Another test showed CO₂ removal rate is not affected by NO_x

BP2: Membrane Desorber Study

Bench-scale membrane **desorber** CO₂ stripping performance demonstration

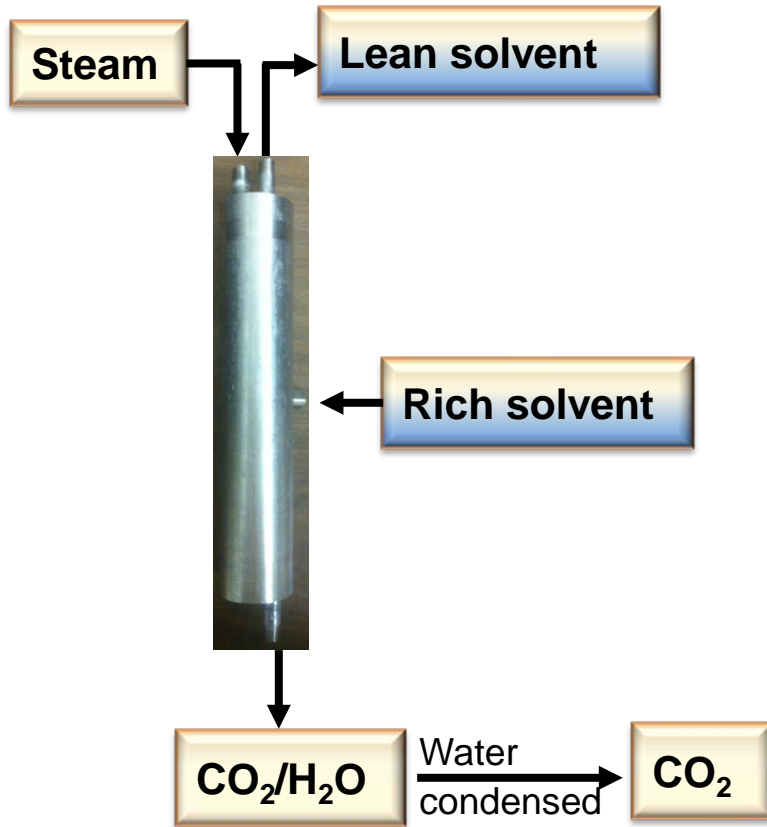
- **Membrane module**: Performance can be essentially linearly scaled to commercial size modules
- **Liquid feed**: CO₂ loaded aMDEA and activated K₂CO₃ rich solvents, flow rate: 0.2-0.7 L/min
- **Four flow configurations (Modes)** investigated: **over 60 tests**



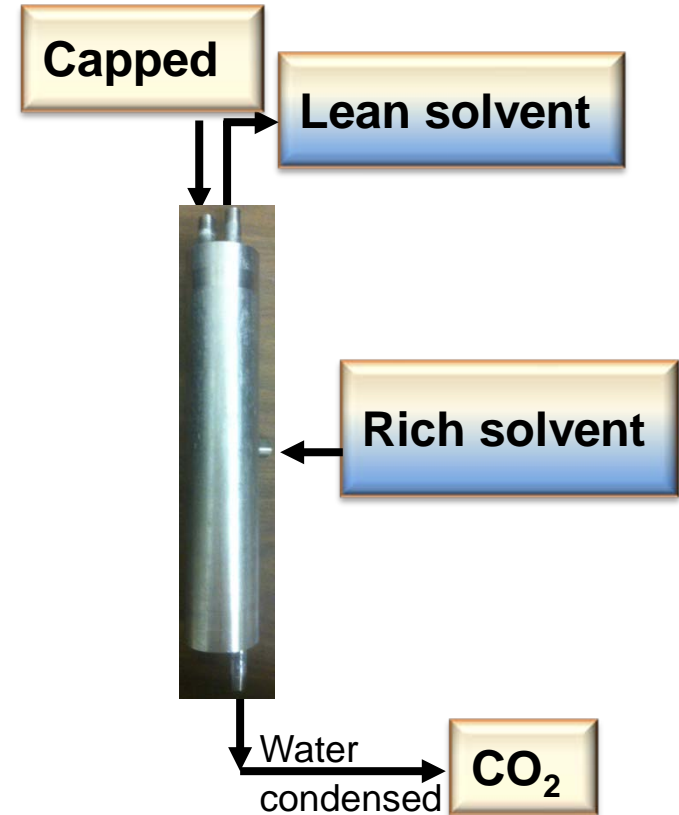
Module for lab testing
(Ø2" x 15" long, 1m²)

Examples of Modes for solvent regeneration

Mode I (Steam Sweep)



Mode II (No Sweep)



High CO₂ stripping rate and high regeneration efficiency obtained

- CO₂ stripping rate: 4.1 kg/m²/h, 10 times higher than the absorption rate. Thus, only 10% membrane area is required for regeneration.
- CO₂ purity: **97%** (target is 95%), 3% is water vapor, can be further condensed.
- Regeneration efficiency: 66% in one stage, and can be further increased by increasing operation temperature and optimizing process design.

Phase II technical goal achieved

Parameters	Goal	Mode III	Mode IV
CO ₂ purity	≥ 95%	97%	97%
CO ₂ stripping rate (kg/m ² /h)	≥ 0.25*	2.8	4.1

* Calculated based on a mass transfer coefficient of 1.0 (sec)⁻¹ for regeneration

Updated COE and increase in COE when use of membrane regeneration is considered

Case	COE, mills/kWhr	Increase in COE
DOE Case 9 no capture	64.00	--
DOE Case 10 state of the art (amine plant)	118.36	85%
BP1 status: membrane absorber	100.11	56%
BP2 status: membrane desorber	98.67	54%

R&D strategy to meet DOE's target

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DOE Case 10 state of the art (amine plant)	118.36	85%
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BP2 status: membrane desorber	98.67	54%
R&D strategy to meet DOE's target		
1) Module cost ↓ from \$80 to \$30/m ²	95.64	48%
2) Advanced solvent	On trajectory to meet DOE target	

Plan for the rest of BP2

#	Plans for future testing in BP2
1	Further membrane development based on regeneration testing results so far.
2	Modes III and IV are currently down selected for further study. Operation conditions will be further optimized to down select one mode for Phase III.
3	After regeneration mode is down selected, use of reflux in membrane desorber to improve regeneration efficiency (target: "lean" solvent lean enough for membrane absorber).
4	Refinement of the process economics based on the lab test data .
5	Finalize testing plan for Phase III.

Readiness and Plan for BP3: Integrated Absorber/Regeneration

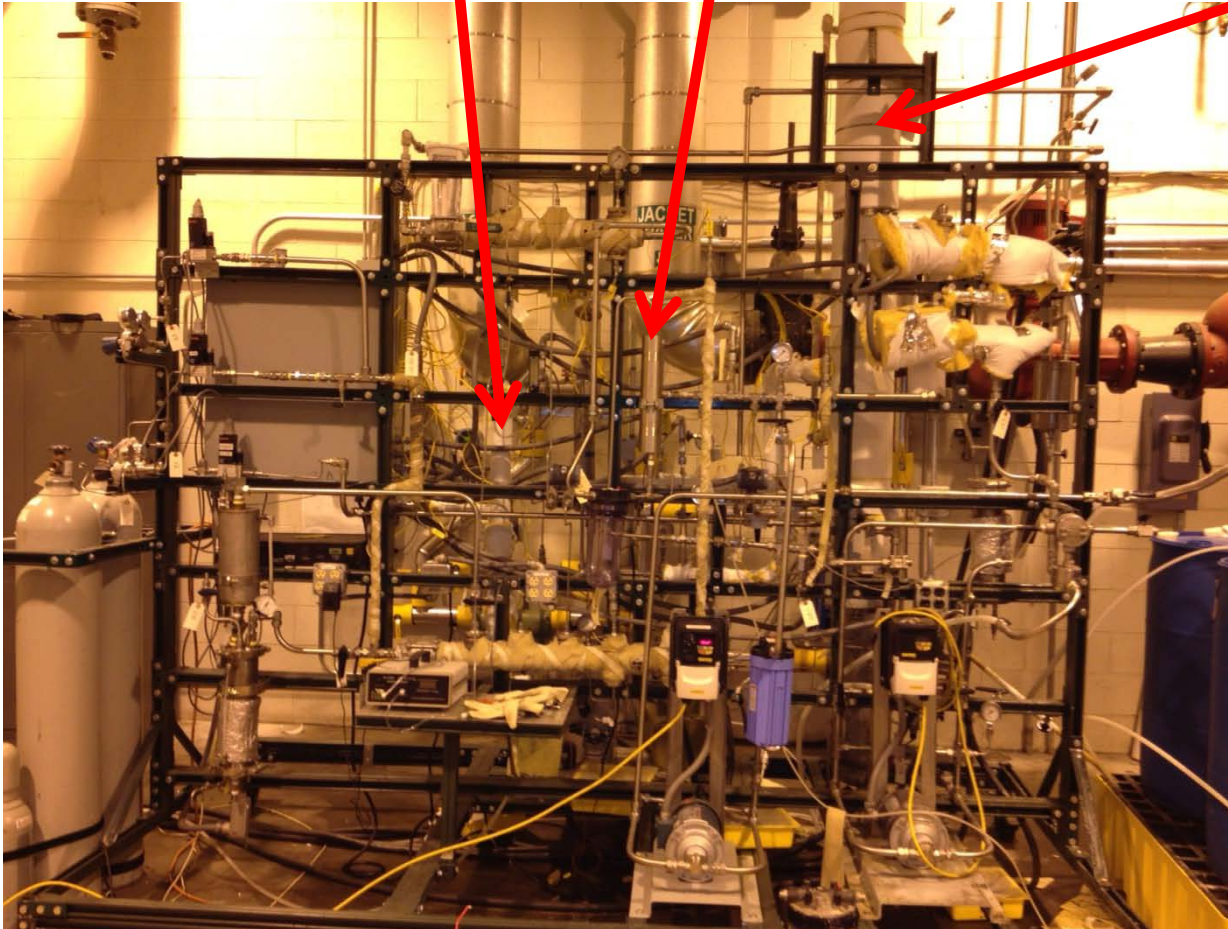
Membrane contactor skid constructed

Membrane desorber

Membrane absorber

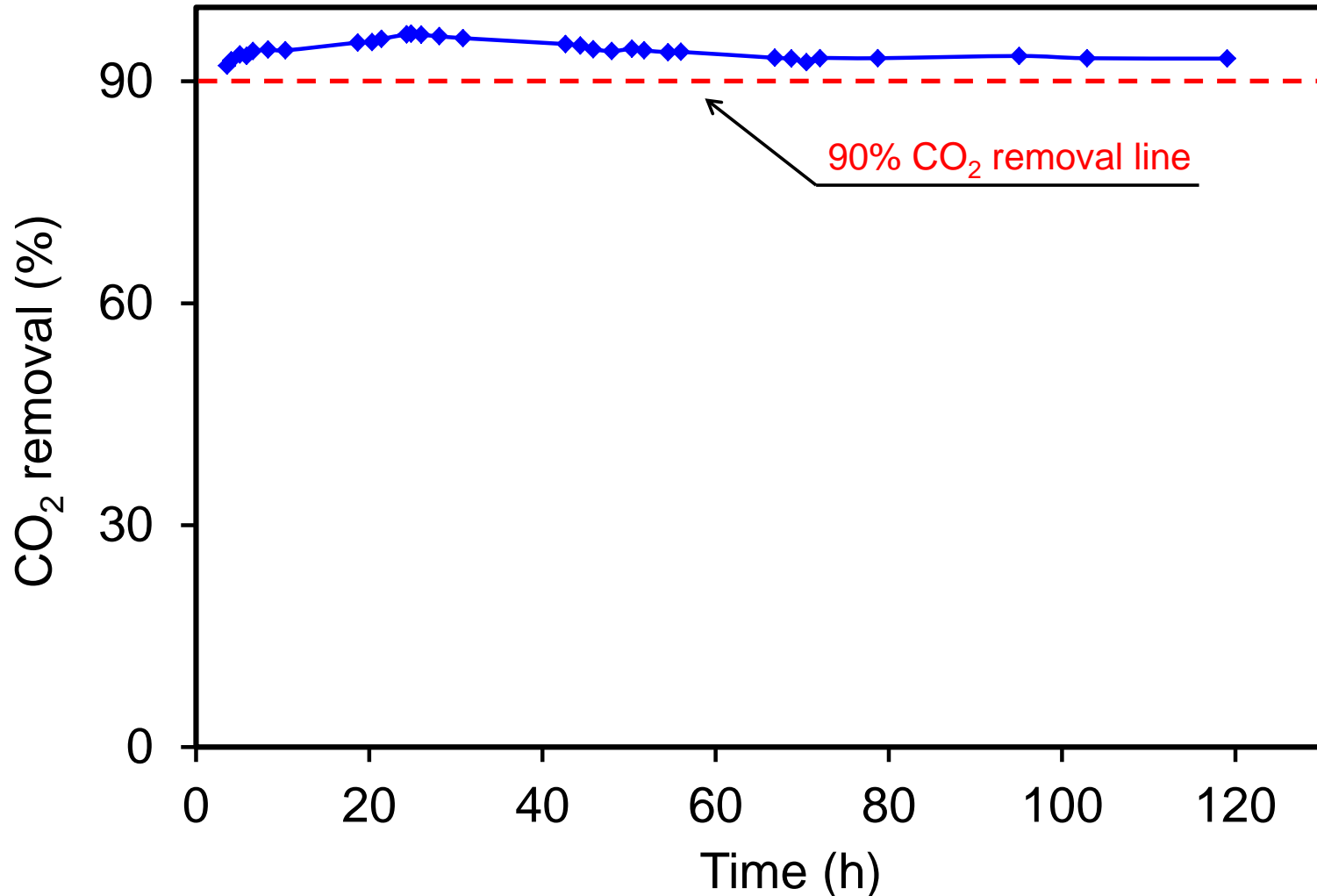
Desorption tower

(backup plan)

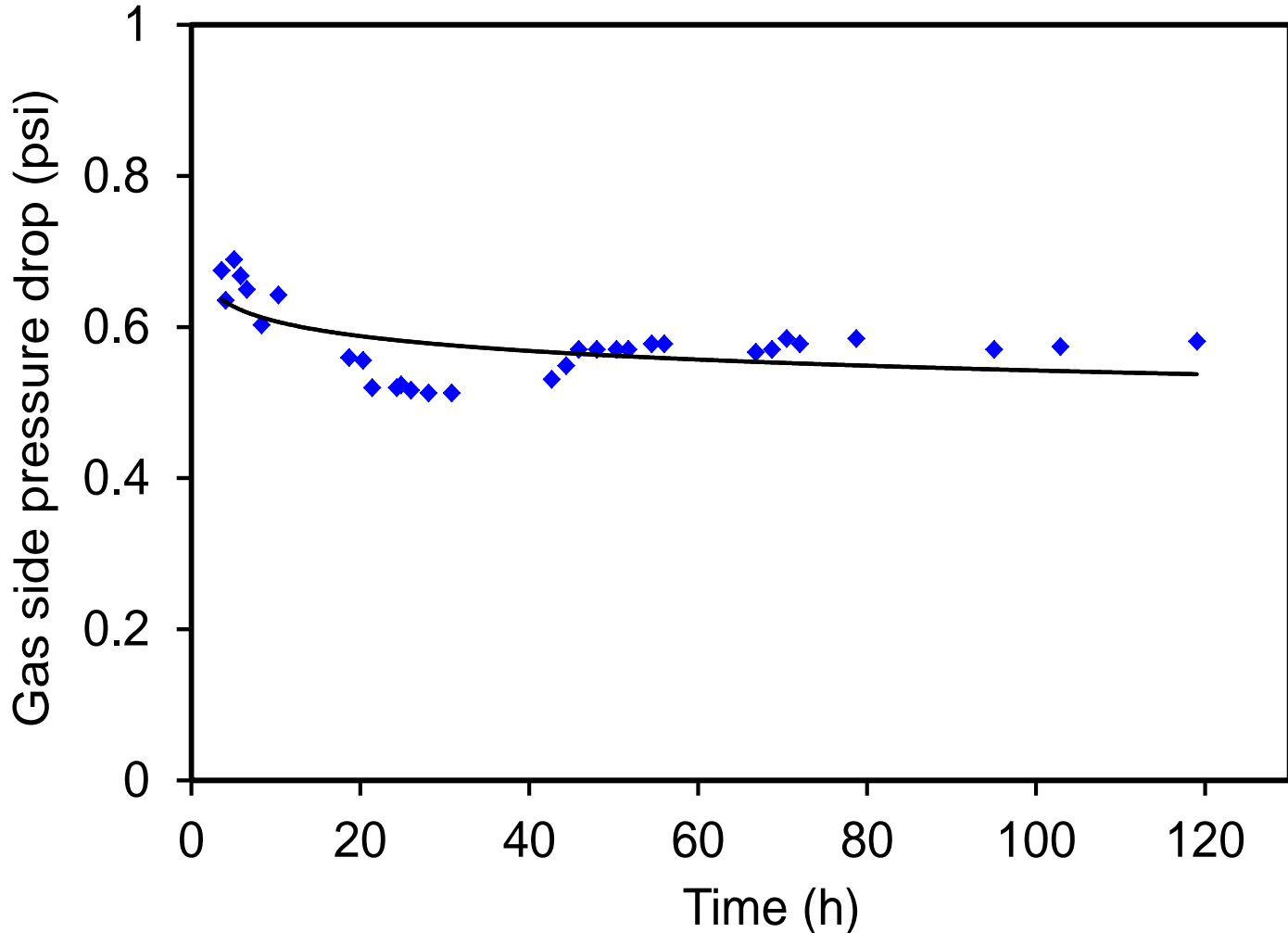


- Designed for **25 KW** equivalents of CO₂ capture (0.5 ton/day)
- **Phase I**: absorption
Phase II: regeneration
Phase III: Integrate absorption/regeneration for field testing

CO₂ removal rate > 90% during the time investigated (120 hours)



Gas side pressure drop stable and remained less than 0.7 psi (target is less than 2 psi)



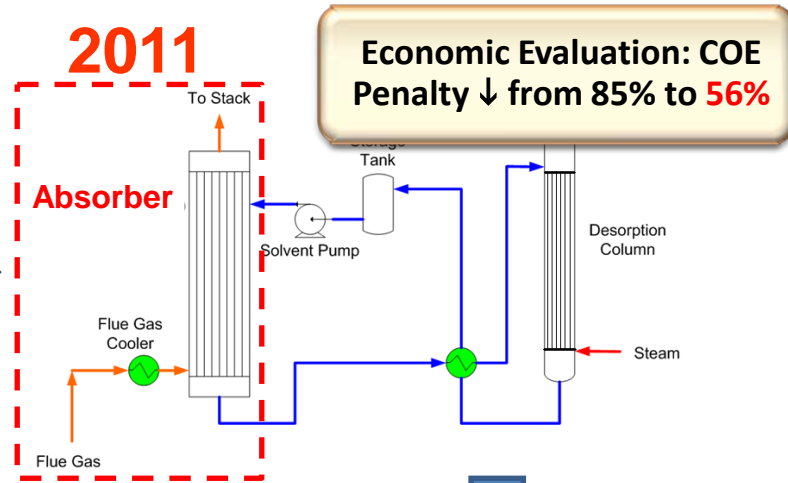
Plans for Future Testing and Development

Plans for future testing and development in this project

2010



2011

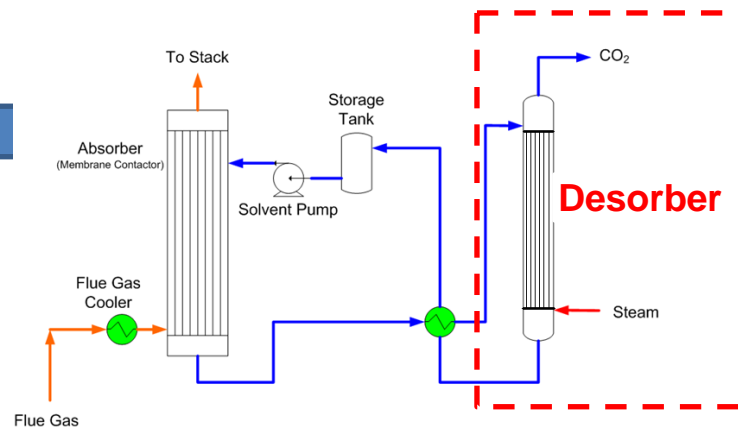


2013

Approach DOE's target:
 ≥ 90% CO₂ capture,
 < 35% increase in COE



2012



1) Optimize membrane and system design to improve regeneration efficiency

2) Refine economic evaluation based on optimized sorption and desorption test results

3) Integrate absorption and regeneration

4) Field testing for **25 kW** equivalents of CO₂ capture (**0.5 ton/day**)

Technology implementation timeline after this project

Time	Development	CO ₂ capture, Ton/day	Module diameter	Projected # of modules*
By 2013	25 kWe bench-scale (Current project, Phase III)	0.5	4 or 8-inch	1 (more than sufficient)
By 2015	2.5 MWe pilot scale	50	8-inch	17
			16-inch	5
By 2018	25 MWe demonstration	500	8-inch	170
			30-inch	14

* Calculated based on:

- CO₂ flux of 1.2 kg/m²/h
- Module area:
 - Current Ø8-inch module: 100 m²
 - Projected Ø16-inch module: 400 m²
 - Projected Ø30-inch module: 1400 m²

PoroGen has equipment capacity to produce 8-inch modules for several 25 MWe demonstration plants

Summary

- **BP1** membrane absorbers
 - Technical goal achieved: $\geq 90\%$ CO₂ removal in one stage; gas side pressure drop: 1.6 psi; mass transfer coefficient: 1.7 1/s
 - Feasibility of contactor module scale-up demonstrated
 - Economic evaluation based on membrane absorber only indicates a 56% increase in COE.
- **BP2** membrane desorbers
 - Technical goal for CO₂ purity (97%) and CO₂ stripping rate (4.1 kg/m²/h) achieved. Operation optimization is on-going to ensure “lean” solvent is lean enough for membrane absorber
 - Evaluation per membrane absorber + desorber testing so far indicates a 54% increase in COE.
- In preparation for **BP3**
 - Completed constructing bench-scale membrane skid, integration of membrane absorber/regeneration tower, membrane module and performance stable with aMDEA solvent.

Acknowledgements

- Financial support
 - DOE-NETL
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- DOE NETL José Figueroa