

Development of a Two-Fluid Drag Law for  
Clustered Particles using Direct Numerical  
Simulation and Validation through Experiments  
HBCU/MI Award DE-FE0007260 Review Meeting  
Program Manager: Vito Cedro

Seckin Gokaltun<sup>1</sup> , Norman Munroe<sup>2</sup> , Shankar Subramaniam<sup>3</sup>

<sup>1</sup>Applied Research Center

Florida International University, Miami, FL

<sup>2</sup>Mechanical and Materials Engineering

Florida International University, Miami, FL

<sup>3</sup>Mechanical Engineering

Iowa State University, Ames, IA

May 31, 2012

# Technical Background

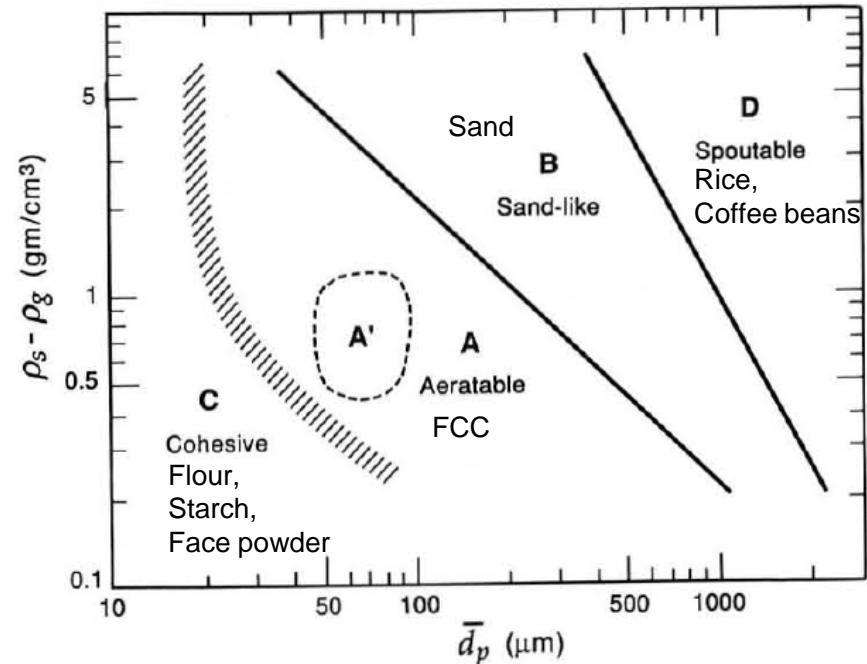
- ❑ Developers of gasifiers, combustors, chemical reactors, and owners of energy power plants are incorporating simulation in their design and evaluation processes to enhance process control and increase efficiency yield and selectivity.
- ❑ Several computational fluid dynamics (CFD) codes have been developed to simulate the hydrodynamics, heat transfer, and chemical reactions in fluidized bed reactors (MFIIX, CFDLIB, etc.).
- ❑ Closure laws are required in the CFD simulations in order to capture the interaction between the gas and the solid phases in the system. For large scale simulations, a drag law is used in order to model the average interphase momentum transfer.
- ❑ Empirical correlations based on experiments by Ergun<sup>1</sup> and Wen-Yu<sup>2</sup> have been used frequently to calculate the drag force in dense and dilute flow regimes.

(1) Ergun, Chemical Engineering Progress, vol. 48, pp. 89-94, 1952.

(2) Wen and Yu, Chemical Engineering Progress Symposium Series, vol. 62, pp. 100-111, 1966.

# Technical Background

- ❑ Particle-resolved direct numerical simulation (DNS) of flow past fixed particle assemblies<sup>3,4,5</sup> yielded a drag relation that is more accurate than the Ergun and Wen-Yu correlations.
- ❑ These drag laws are applicable to suspensions where particles do not form clusters, and they have been useful in modeling the hydrodynamics of fluidized beds for Geldart B and D particles<sup>6</sup>.
- ❑ CFD simulation of fluidized beds with Geldart A particles remains a challenge because they fail to reproduce the pressure drop and bed expansion that are observed in experiments<sup>7,8</sup>.
  - Formation of particle clusters significantly reduces the drag force.
  - The drag force is overestimated by standard drag laws.



(3) Hill et al., Journal of Fluid Mechanics, vol. 448, pp. 243-278, 2001.

(4) Beetstra et al., AIChEJ, vol. 53, pp. 489, 2007.

(5) Tenneti et al., International Journal of Multiphase Flow, 37, 1072-1092, 2011.

(6) van der Hoef et al., Annual Review of Fluid Mechanics, vol. 40, pp. 47-70, 2008.

(7) Wang et al. Chemical Engineering Science, vol. 64, no. 3, pp. 622-625, 2009.

(8) Wang, Ind. Eng. Res., vol. 48, no. 12, pp. 5567-5577, 2009.

# Technical Background

- ❑ Ad hoc approaches to account for the presence of particle clusters have been proposed (e.g., the Energy-minimizing Multi-Scale model) to modify the standard drag laws and these give improved simulation results in a limited fluidization regime.
- ❑ However, these ad hoc modifications do not have any predictive capability over the parameter range that is necessary for design optimization, nor do they provide insight into the fundamental multiphase flow physics.
- ❑ Therefore, a first-principles based approach is needed to quantify the mechanisms underlying particle clustering and their effect on the drag force.

# Technical Background

- ❑ The current research includes utilization of a combination of numerical and experimental approaches to provide detailed data necessary for validation and optimization purposes.
  - Experimental evaluation of particle clusters will be investigated using high speed imaging.
  - The drag law applicable to particle clustering in fluidized beds will be developed using direct numerical simulations.
  - Finally the developed drag law will be implemented in the MFIX software and the results will be validated against experimental data.

# Significance of the results of the work

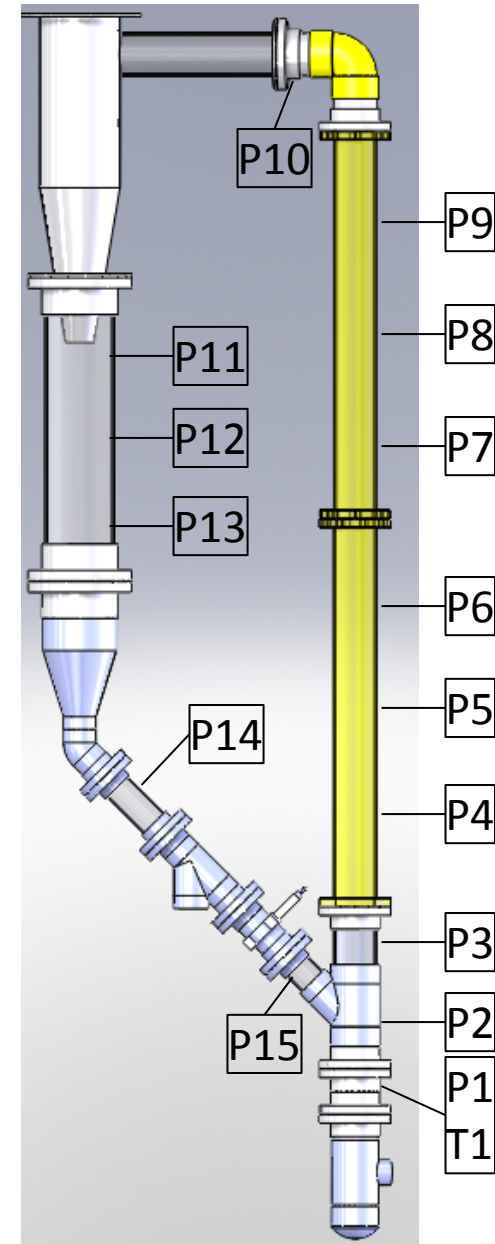
- ❑ Supports the vision of the NETL 2006 Workshop on Multiphase Flow Research<sup>9</sup>:
  - *"To ensure that by 2015 multiphase science based computer simulations play a significant role in the design, operation, and troubleshooting of multiphase flow devices in fossil fuel processing plants."*
- ❑ Will develop missing critical constitutive relations to increase the fidelity of CFD models.
- ❑ Accurate drag law will result in improved modeling of multiphase flow systems such as fluidized beds and risers.
- ❑ Computational advances will be provided to NETL's open-source CFD tool MFIX and validation cases will be provided.

(9) Report on Workshop on Multiphase Flow Research, Morgantown, WV, Ed. M. Syamlal, DOE/NETL-2007/1259, 2006.

# Statement of project objectives

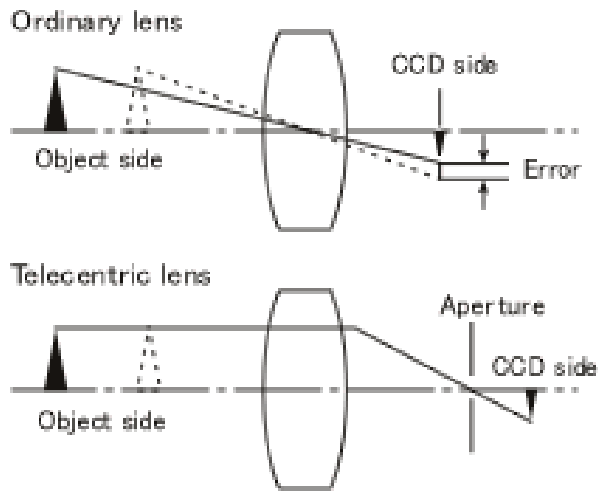
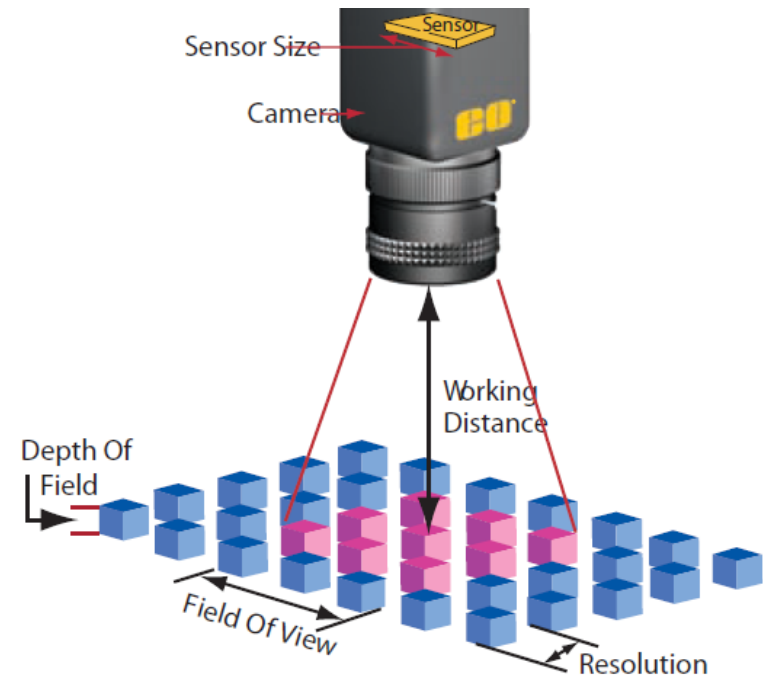
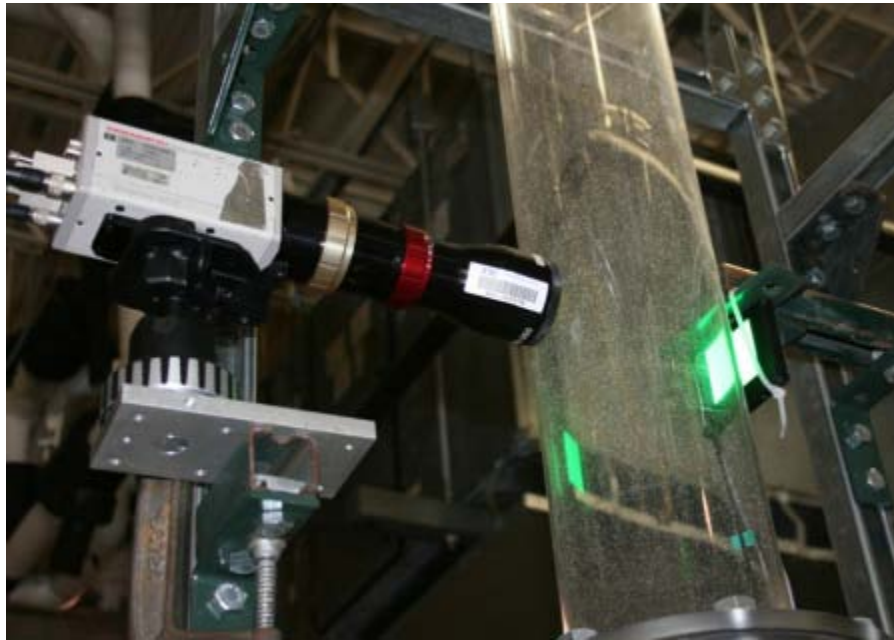
- ❑ To develop a two-fluid drag-law for clustered particles using direct numerical simulations with experimental validation.
  - Fluidization experiments at the FIU CFB facility:
    - ✓ Geldart A type particles to observe clustering of particles,
    - ✓ High speed imaging to capture the instantaneous distribution of particles,
    - ✓ Convert the images of particle clusters into particle configurations to be used in the DNS.
  - Conduct DNS simulations at ISU:
    - ✓ Use the outcome of the DNS for pressure field, velocities of the gas phase and solid particles to calculate the actual drag force on the system of particles.
  - Develop a new drag correlation in the presence of particle clustering and implement in the MFIX computer code. (ISU and FIU)
    - ✓ Integrate the new drag-law with MFIX,
    - ✓ Simulate the experimental test cases using MFIX with the new drag correlation,
    - ✓ Compare the results against the experimental data for pressure drop in the riser.
  - Raise FIU's competitiveness with other institutions in the fields of conversion and utilization of fossil energy research.

# Experimental Approach



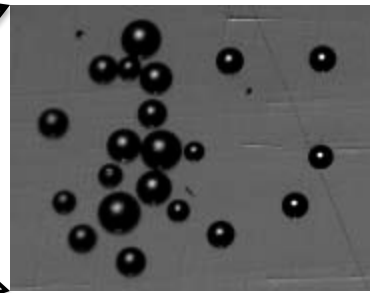
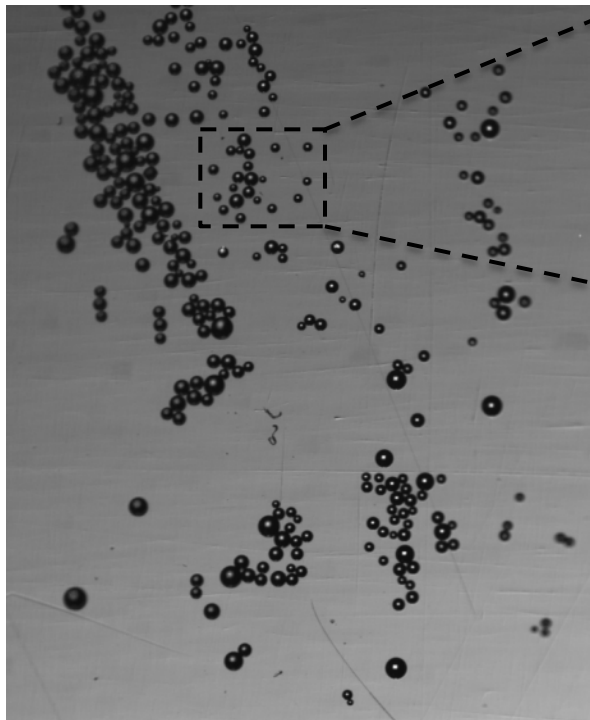


# Experimental Approach

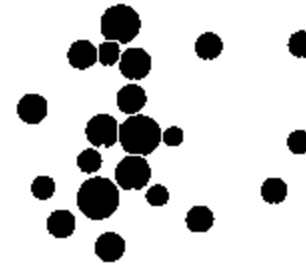


Telecentric Lens	Edmund Optics 55-350
Primary magnification	1X
Horizontal field of view	8.8 mm
Working distance	98 mm – 123 mm
Resolution (MTF Image Space @ F6)	>45% @ 40 lp/mm
Telecentricity	<.1°
Distortion	.5% Max
Depth of field (20% @ 20 lp/mm)	± 0.6mm at F12
Aperture (f/#)	F6 – F25

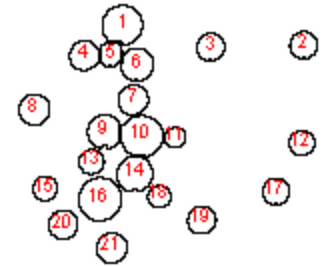
# Image processing (NI ImageJ)



Region of interest



Binary > Fill holes  
> Watershed



Particle  
analyzer

$$\varepsilon_s = \frac{\sum_i^n V_i}{Ah}$$

❑ Polystyrene particles:

➤  $d_m = 350 \mu\text{m}$ ,  $\rho_b = 650 \text{ kg/m}^3$

❑ Vision Research Phantom v5.0 (1024x1024 Sensor, 10  $\mu\text{s}$  exposure time):

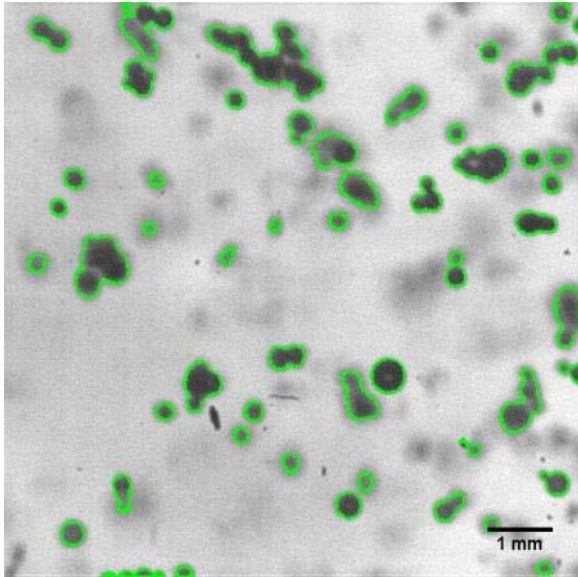
➤ 3,800 pps @ 512 × 512 pixels

➤ 60,000 pps @ 256x32 pixels

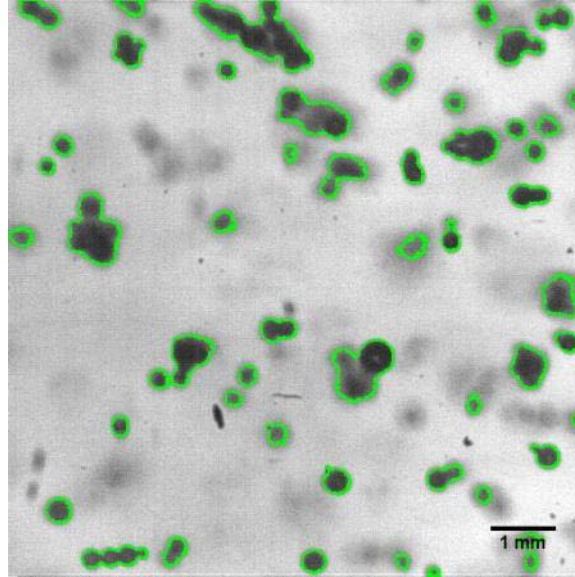
➤ 1024MB memory (1s of 1024 frames)

# Solid volume calculation

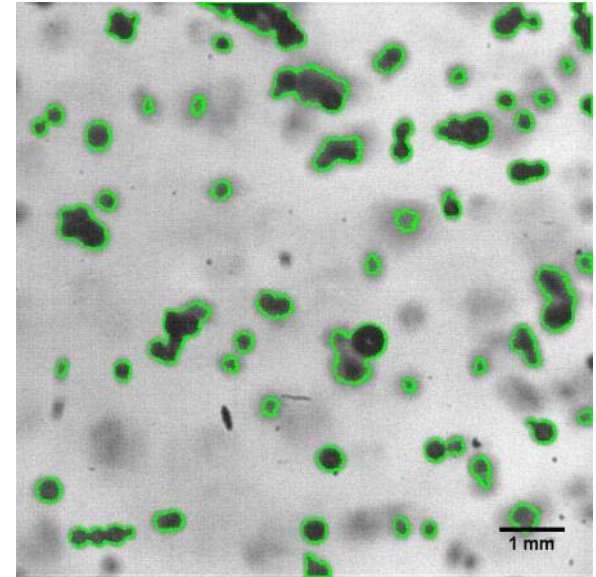
Frame 1



Frame 2



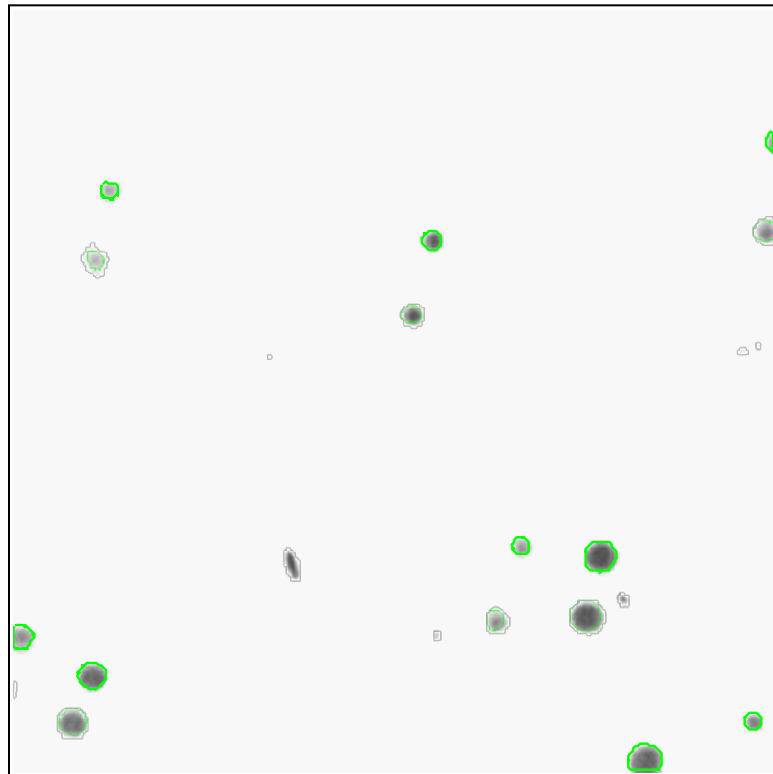
Frame 3



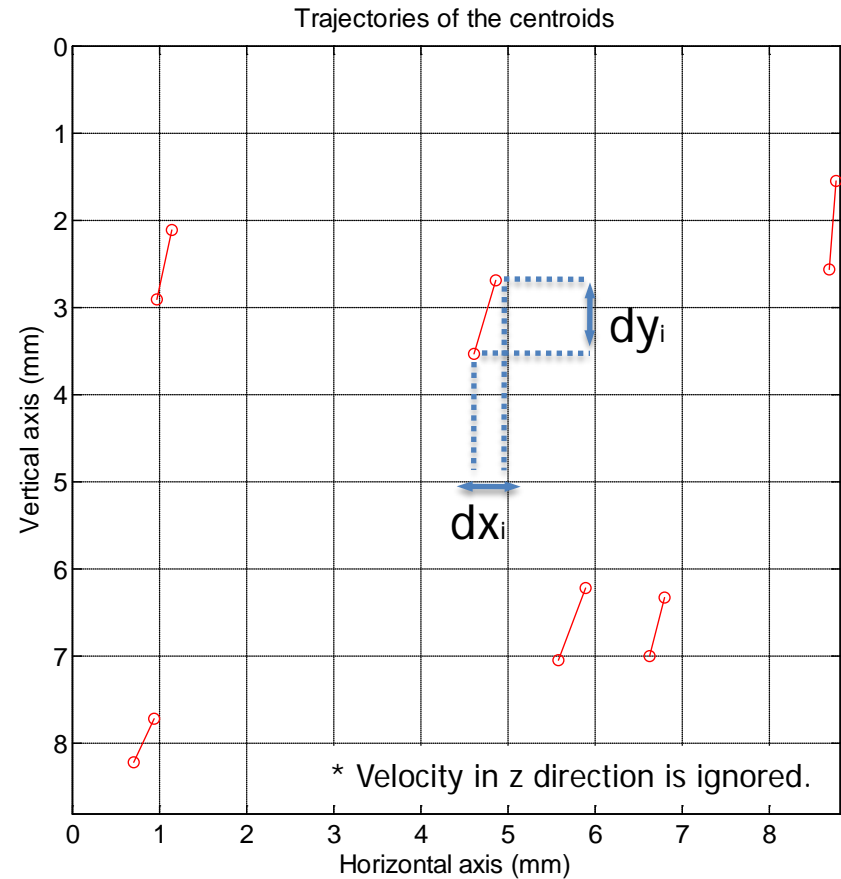
- ❑ Matlab Image Processing Toolkit used for frame by frame analysis.
- ❑ Telecentric lens (Edmund Optics Inc. 55 – 350)
  - horizontal field of view of 8.8mm
  - depth of field of 1mm

# Velocity calculation from trajectories

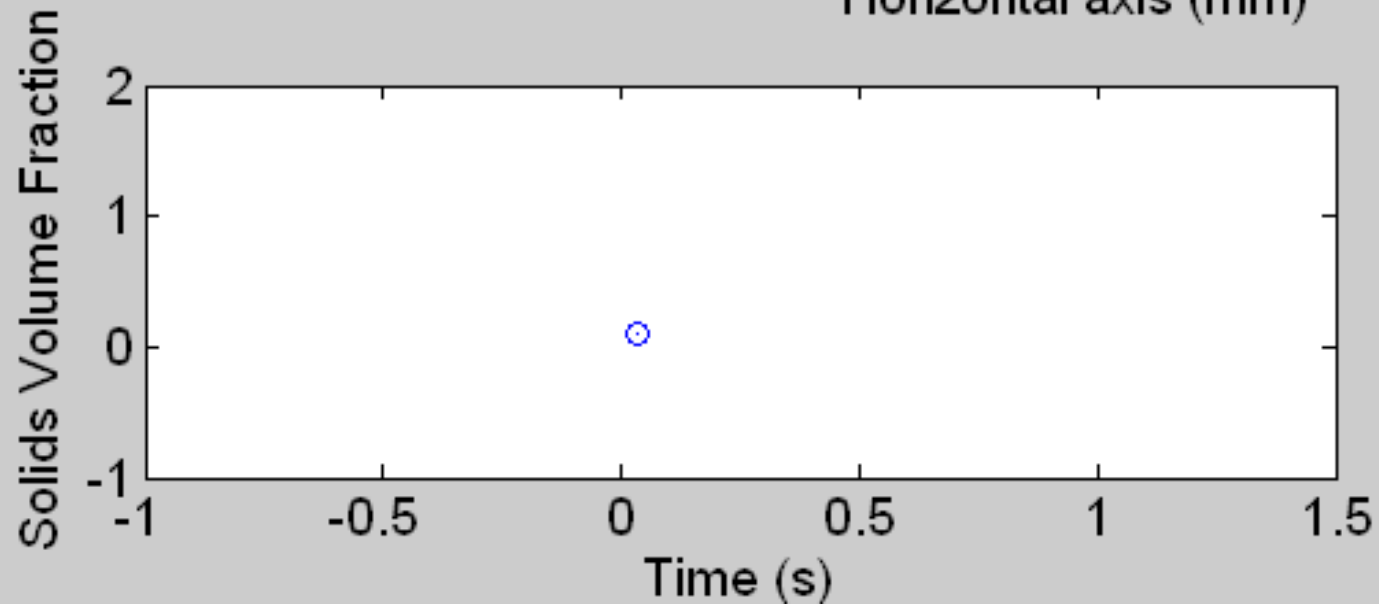
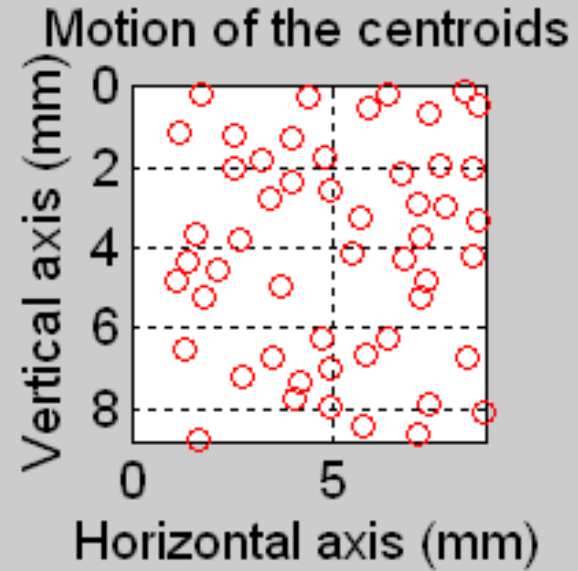
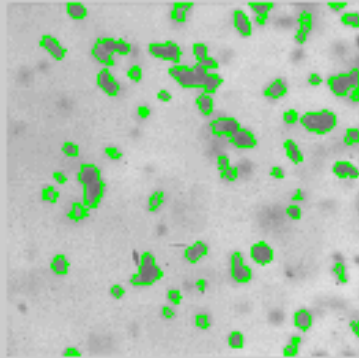
Tracking algorithm → trajectories → particle velocities<sup>12</sup>



Frame 2 imposed on Frame 1



# Particle Tracking

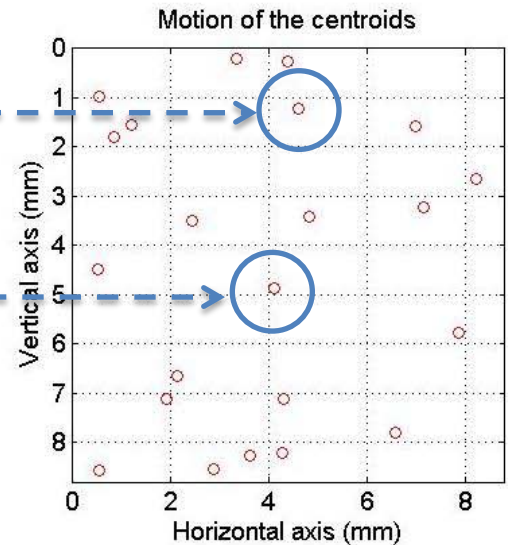
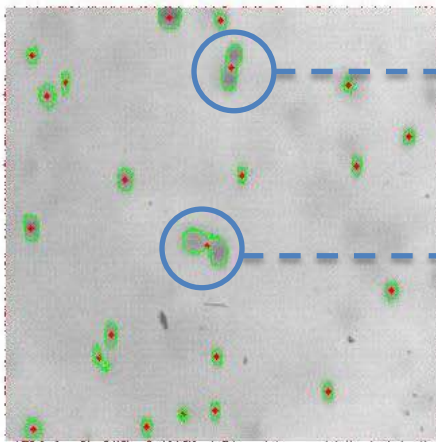
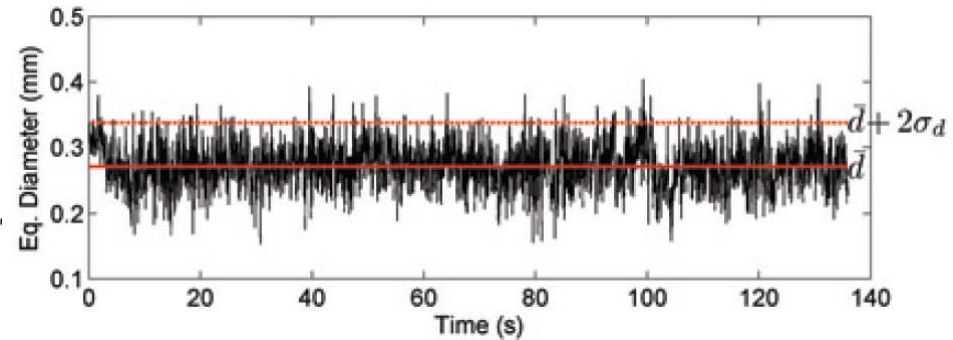
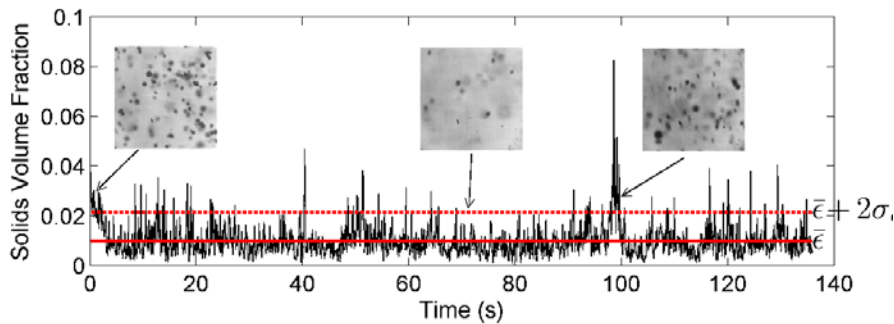


# Boundary identification issues

Mean-referenced criterion: time-mean + 2 x SD <sup>13</sup>

$$\epsilon = \sum_i^n \frac{2A_i d_i}{3hA_f}$$

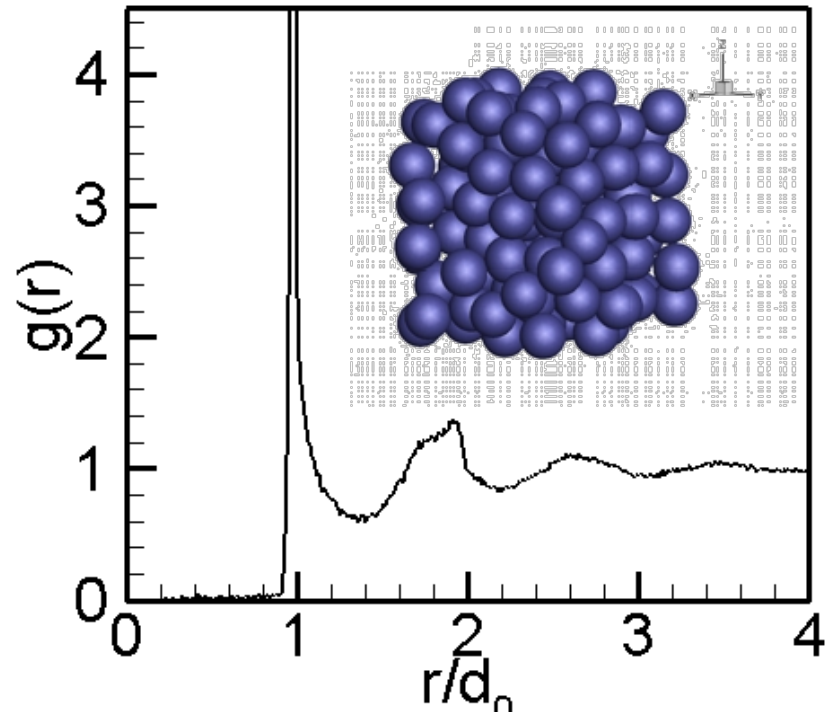
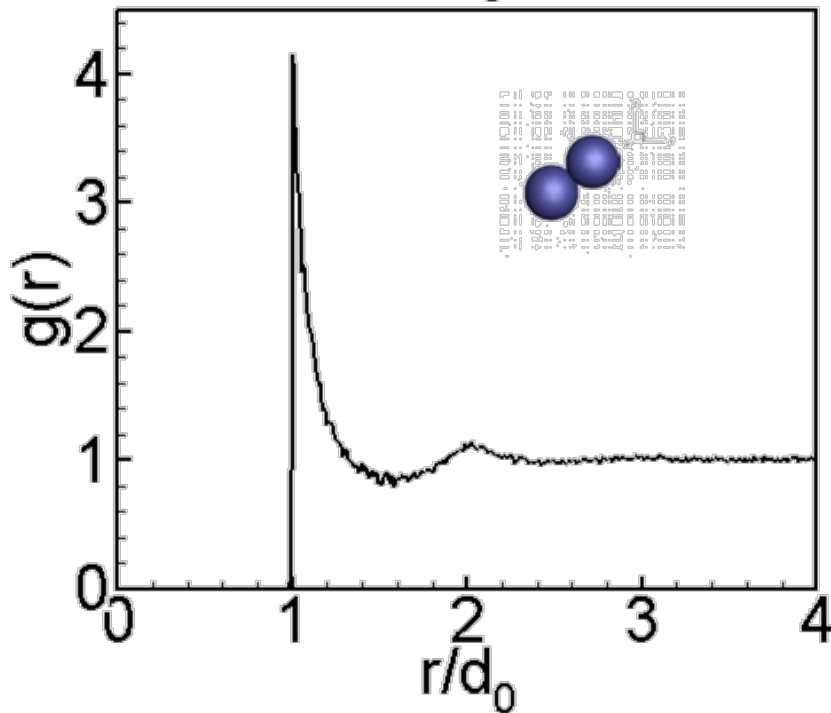
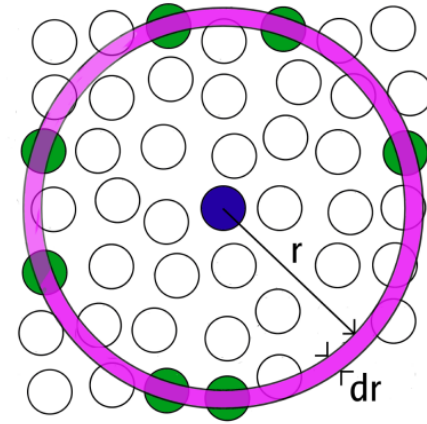
$$d_i = \sqrt{\frac{4A_i}{\pi}}$$



# Particle configurations from images

## □ Shadow sizing

- Generating 2D images of the field
- Measuring the projected area fraction
- Measuring the 2-D pair-correlation function (statistical representation of neighbor particles)

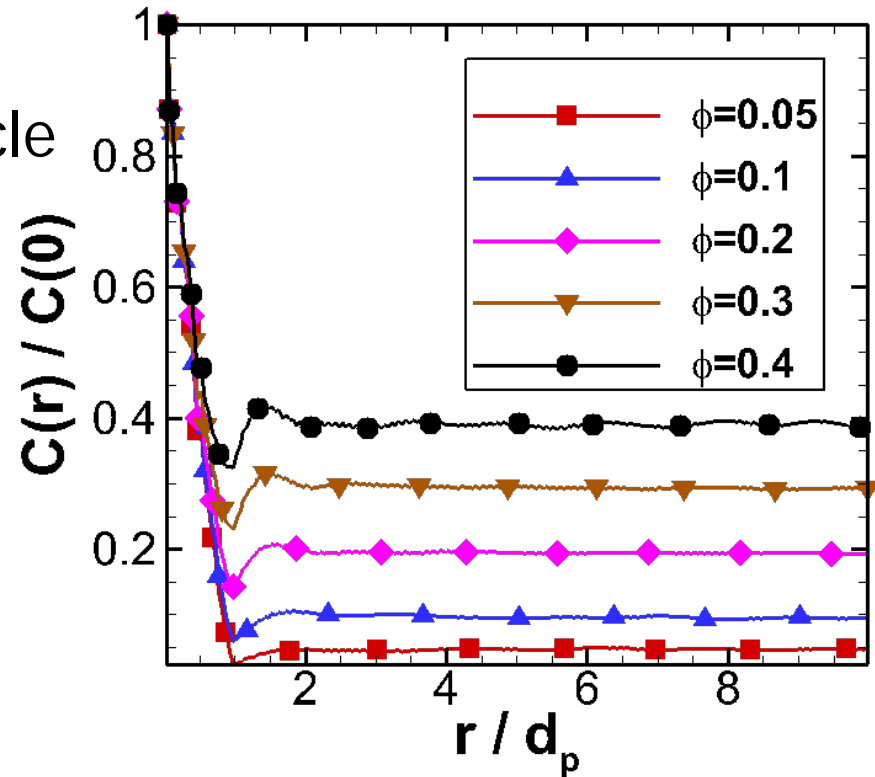
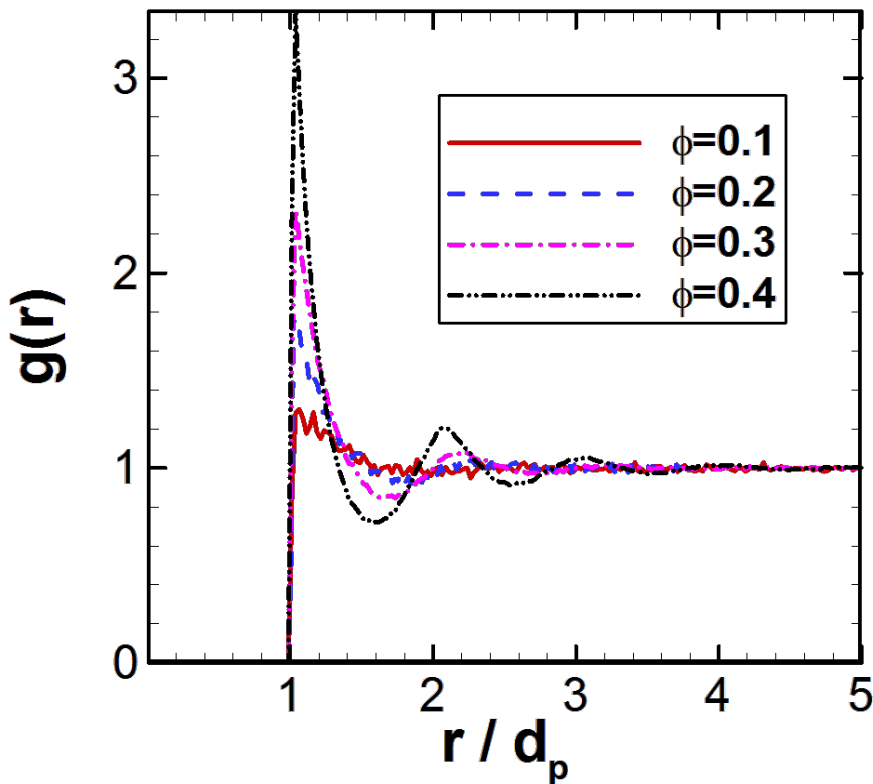


# Characteristics of Particle Configurations

## □ Radial distribution function

- Probability of finding a particle at separation

$$g(r) \equiv \frac{1}{N_p} \frac{N_r}{2 \cdot 4\pi r^2 \delta r} \frac{V}{N_p}$$



## □ Covariance of indicator field

- local solid volume fraction at separation  $r$

$$C(r) = \langle I^{(p)}(x) I^{(p)}(x+r) \rangle$$



## ❑ Experimental approach

- Shadow sizing technique
- 2D projections of 3D particle configurations at a particular plane

## ❑ Numerical approach

- Regeneration of particle configuration is non-trivial
- Consistent with experimental measurements
  - ✓ Producing 2D planar projections of numerical particle configuration
  - ✓ computing  $g_{2D}(r)$  and  $C_{2D}(r)$  for each projection
  - ✓ computing ensemble averages
  - ✓ Minimizing the difference between experimental and numerical measurements

Optimization process

□ From analogy to annealing process in metallurgy

- Heating, and then controlled cooling of a material
- Objective function

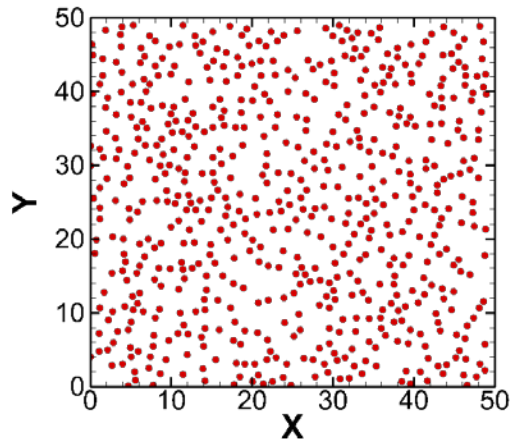
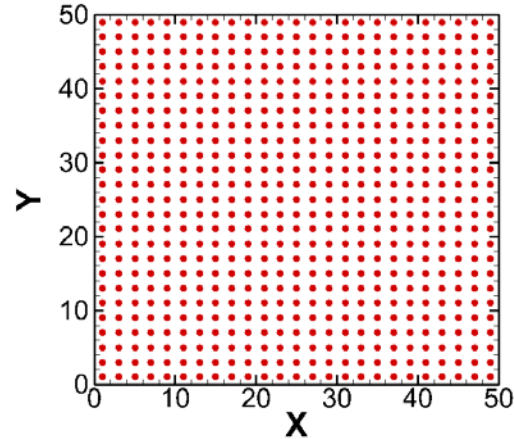
$$F(\mathbf{r}) \equiv \alpha \left\| g_{2D}^E(\mathbf{r}) - g_{2D}^N(\mathbf{r}) \right\|_2 + \beta \left\| C_{2D}^E(\mathbf{r}) - C_{2D}^N(\mathbf{r}) \right\|_2$$

- Generating a new solution by a local transformation

$$T^{n+1} = \alpha T^n \quad \mathbf{x}^{n+1} = \mathbf{x}^n + \beta d_p \mathbf{r}$$

- The probability of accepting a new solution

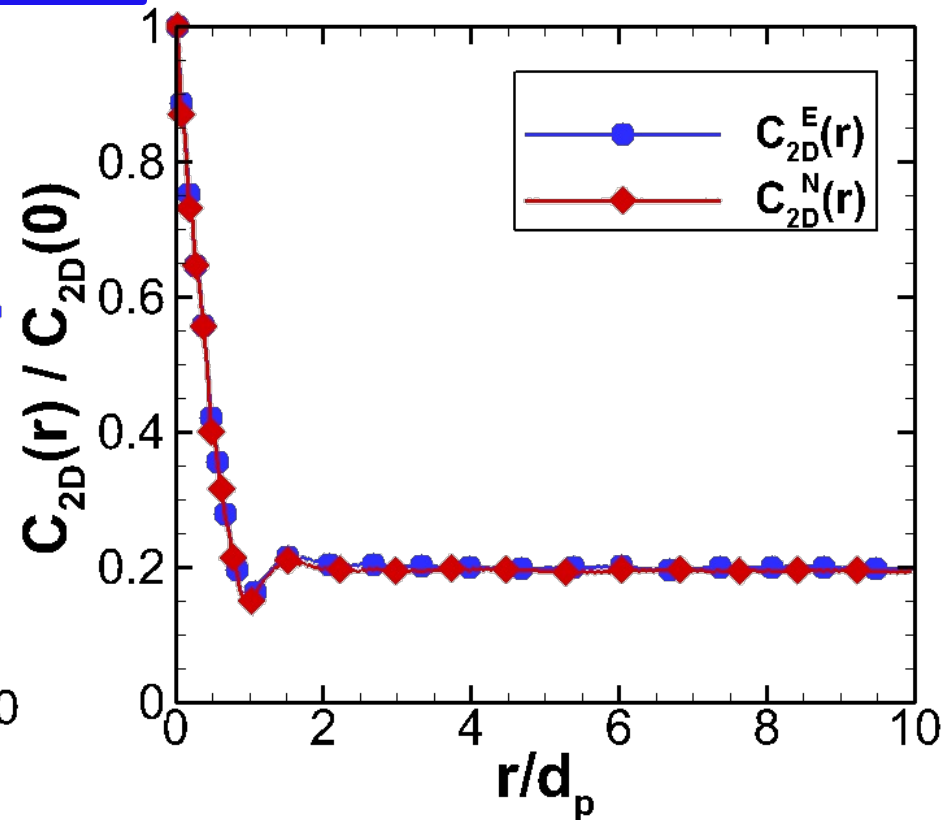
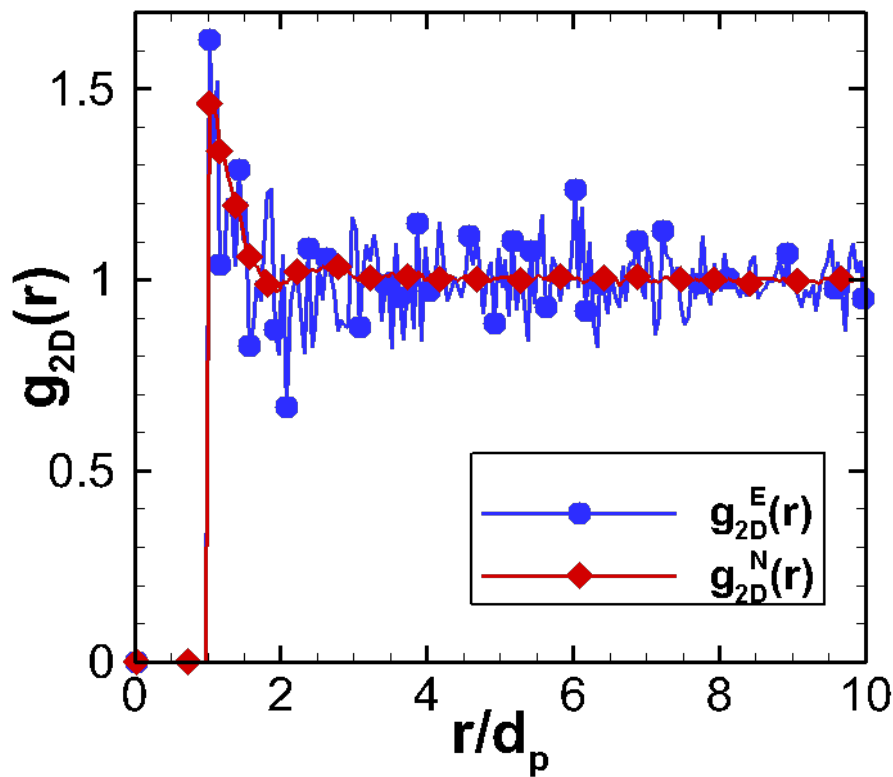
$$P = \begin{cases} 1, & \Delta F \leq 0 \\ e^{-\Delta F/T}, & \Delta F > 0 \end{cases}$$



# Simulated Annealing

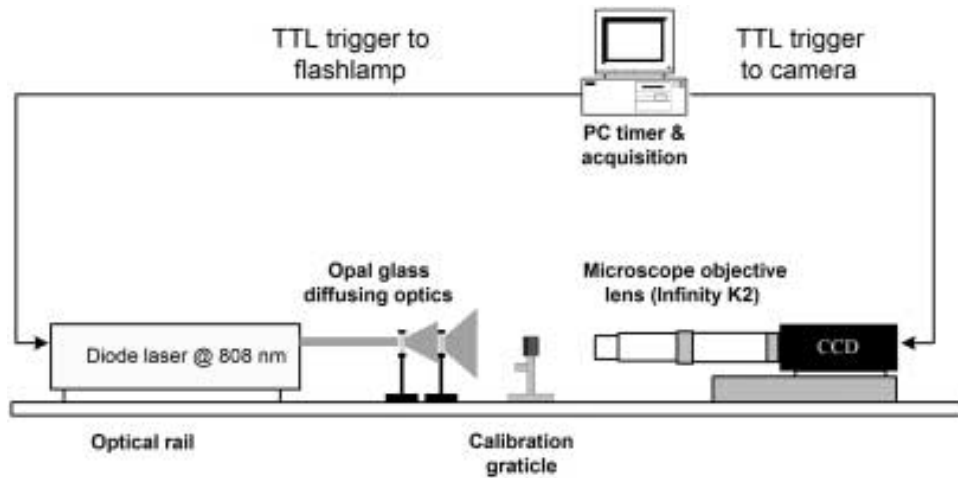
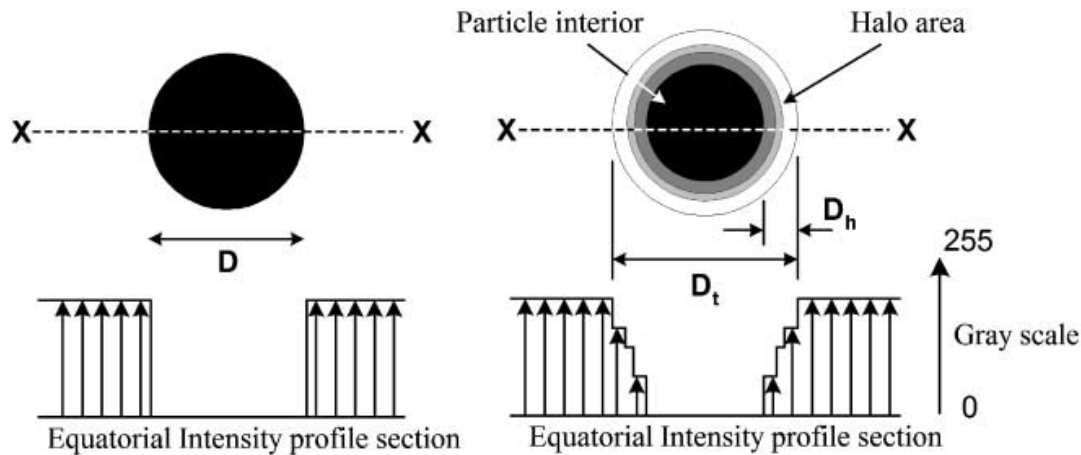
- Ensemble averages of  $g_{2D}(r)$  and  $C_{2D}(r)$  for 200 realizations used as our benchmark

$$\phi=0.2$$

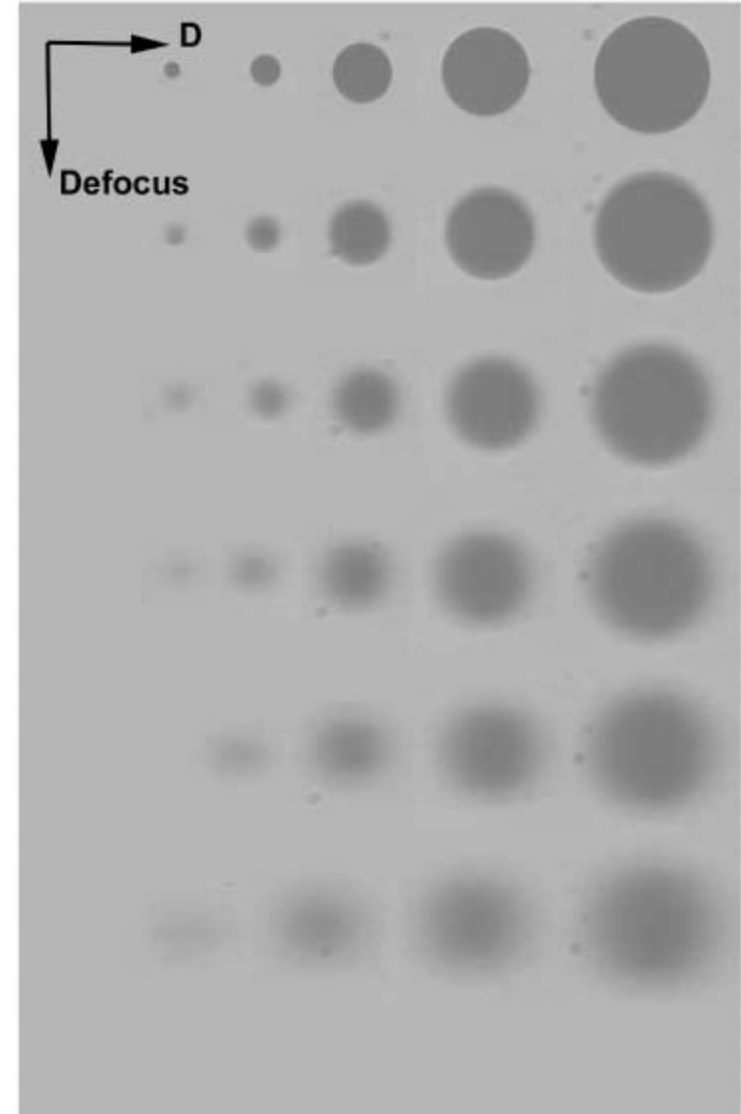


Fluctuations will be removed by generating more realizations

# Shadow Intensity profile calibration<sup>15</sup>

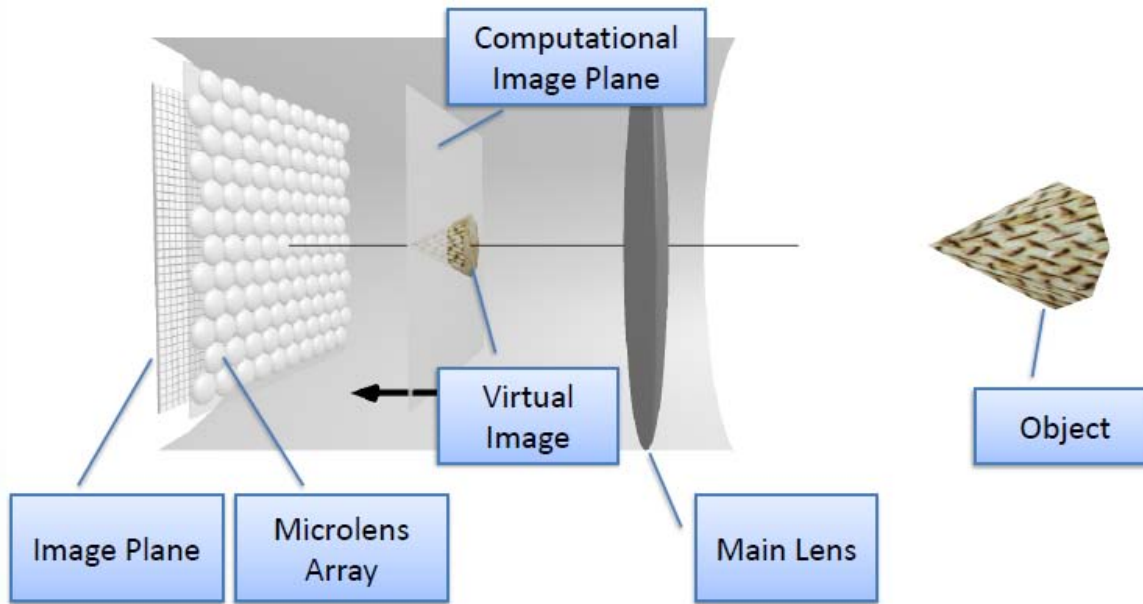


Calibration set-up<sup>15</sup>.



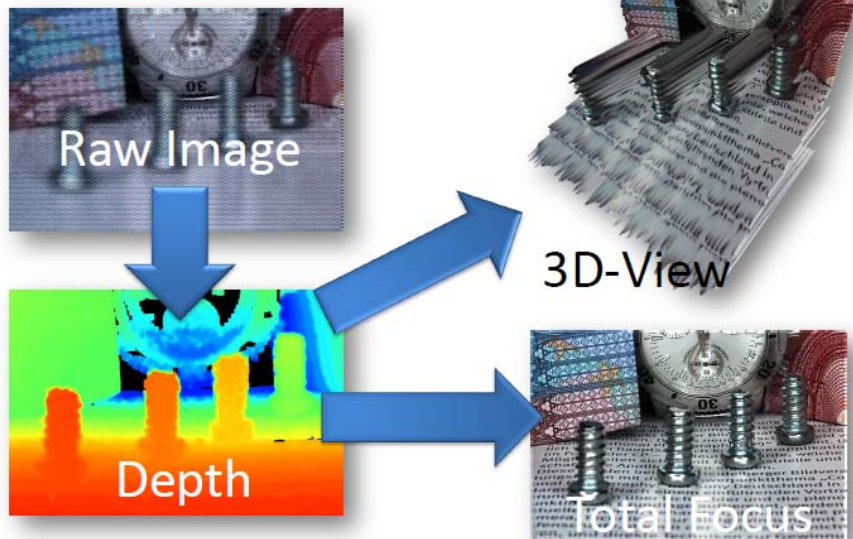
Patterson globe calibration graticle at increasing defocus distances<sup>15</sup>.

# Light field photography



Professional light-field camera (7 MP, 3D reconstruction software) [www.raytrix.de](http://www.raytrix.de)

## Calculation of 3D-Depth



Consumer level light-field camera  
Ren Ng (1.2 MP, \$400-\$500)  
[www.lytro.com](http://www.lytro.com)

# Technical Approach to Achieving the goals

## □ DNS part

- Regeneration of 3D particle configuration using the experimental images
  - ✓ Simulated annealing approach
- Quantification of drag force from simulations
- Proposing a drag law that includes the clustering effects

$$F(\phi, Re_m, \sigma_\phi)$$

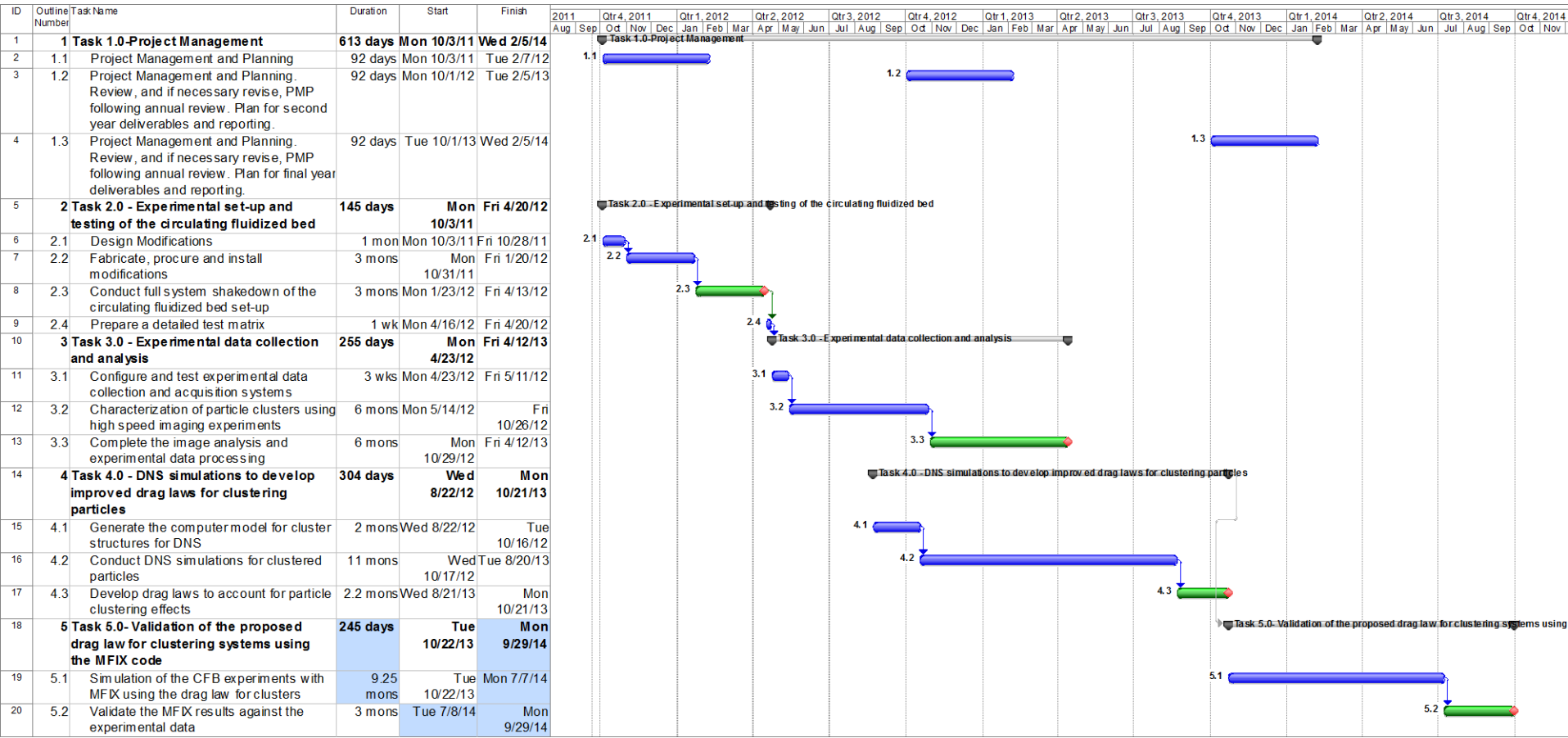
## □ Validation

- Implement the model in MFIX
- Simulating a CFB configuration (setup from NETL)
- Validating the results with experiment

# Project milestones and schedule

## Technical Milestones:

Milestone #	Description	Completion Date
1	Conduct full system shakedown of the circulating fluidized bed set-up	<del>04/13/12</del> <b>07/01/12</b>
2	Complete the image analysis and experimental data processing	04/12/13
3	Develop drag laws to account for particle clustering effects	10/21/13
4	Validate the MFIX results against the experimental data	09/29/14



## ❑ FIU:

- All CFB parts procured. FCC particles obtained. Blower identified.
- Graduate student candidates identified, Ph.D. admission process started
  - ✓ expected start date: Fall 2012.
- MFIX user account obtained. Software installation in FIU cluster in progress.

## ❑ ISU:

- Graduate student recruited (Mohammad Mehrabadi).
- Preliminary analysis of generation of particle configurations in DNS.



Distributor plate using a porous plate (Mott Corp.)



20 and 25 micron screens received from Johnson Screens



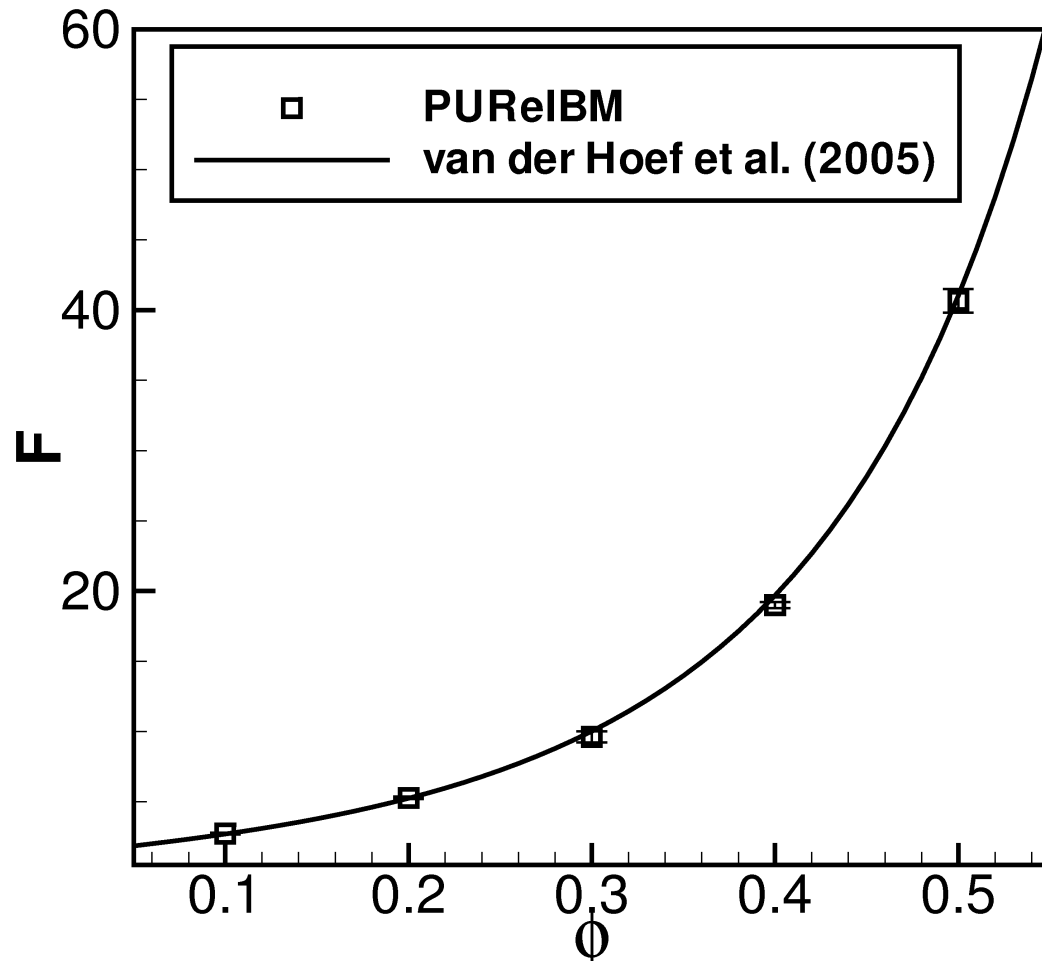
Windbox section manufactured



Questions and feedback?

Backup Slides

# Validation Tests

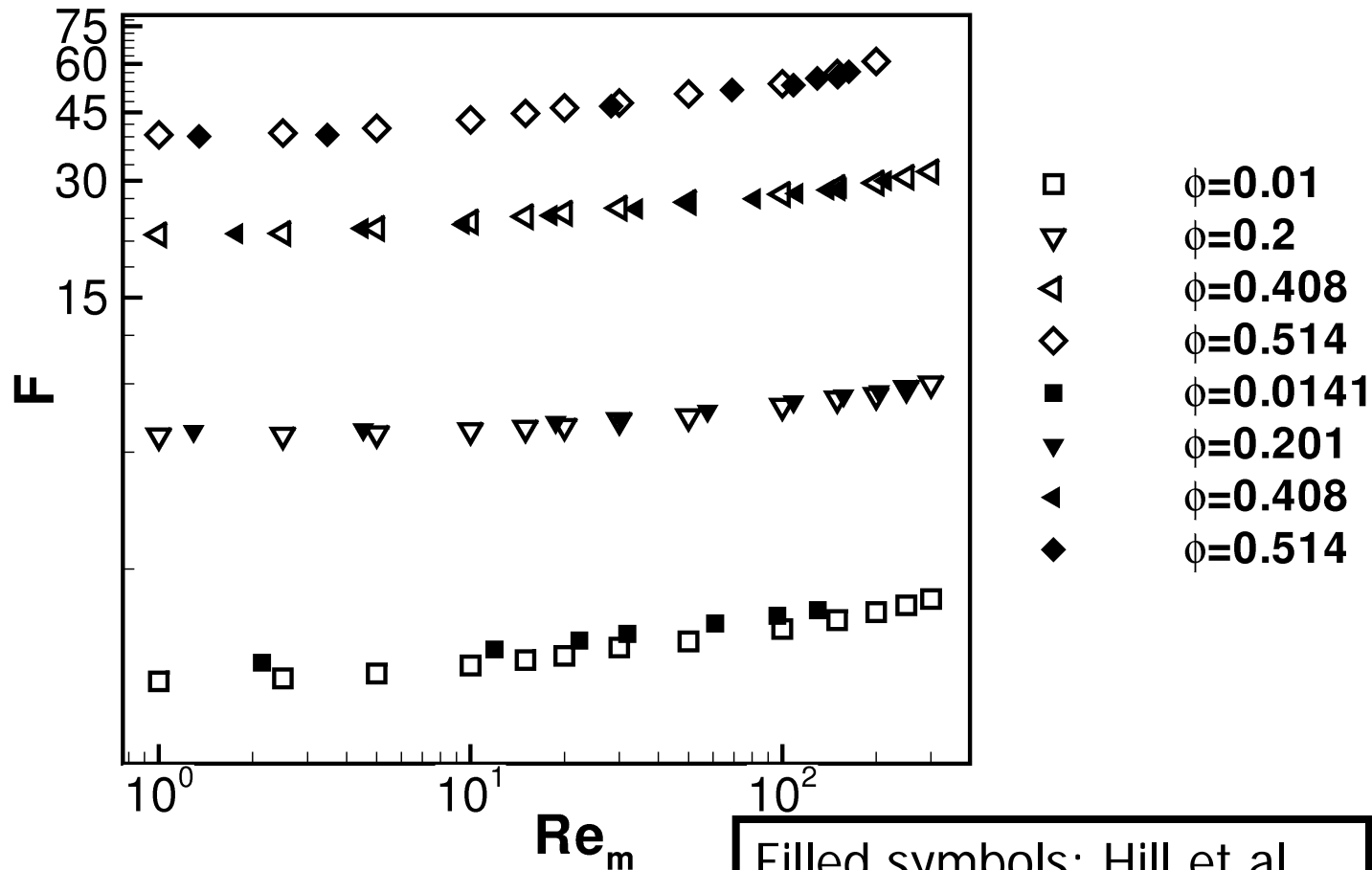


van der Hoef, M. A., Beetstra, R. & Kuipers, J. A. M. 2005 "*Lattice-Boltzmann simulations of low-Reynolds-number flow past mono- and bidisperse arrays of sphere: results for the permeability and drag force.*" JFM 528.

Stokes flow past random arrangement of monodisperse spheres

# Validation Tests

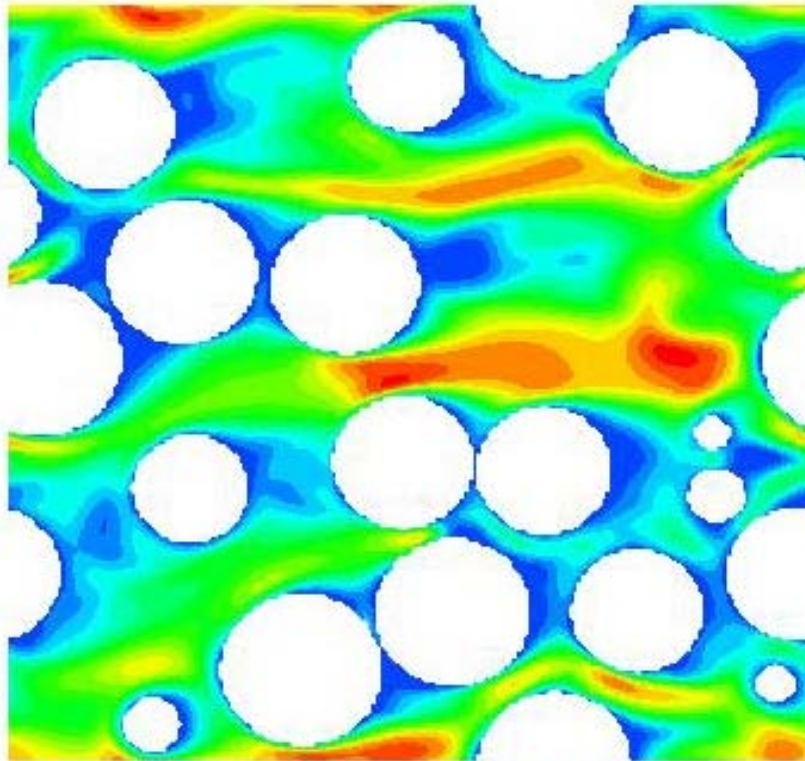
Hill, R. J., Koch,  
D. L. & Ladd, A. J.  
C. 2001 *b*  
"Moderate  
Reynolds number  
flows in ordered  
and random  
arrays of  
spheres." JFM 448



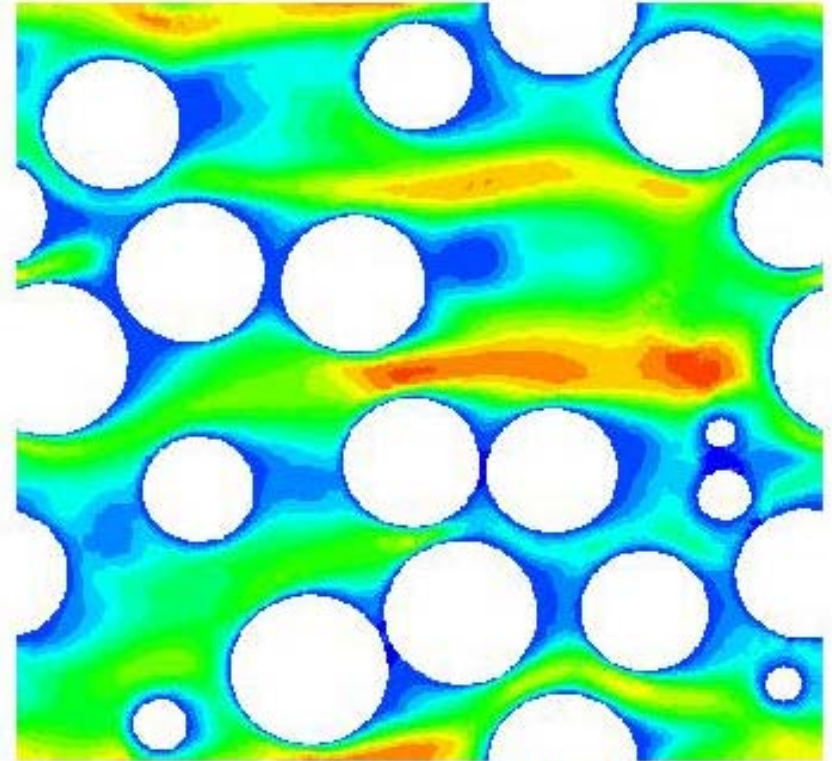
Moderate Reynolds number flow past simple cubic arrays of monodisperse spheres

# Validation Tests

PUReIBM



ANSYS-FLUENT



0 32 64 96 129 161 193 225 257 289 321 354 386 418 450

0 32 64 96 129 161 193 225 257 289 321 354 386 418 450

Volume fraction: 0.4; Reynolds number: 100

High Reynolds number flow past random arrangement of monodisperse spheres