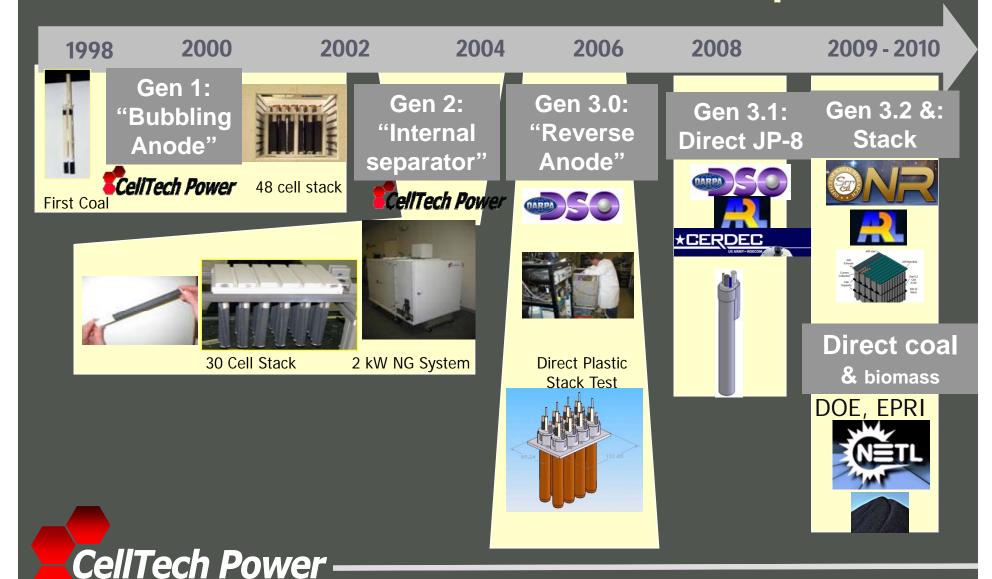


Novel Fuel Cells for Coal Based Systems

SECA Pittsburg July 27-29, 2010

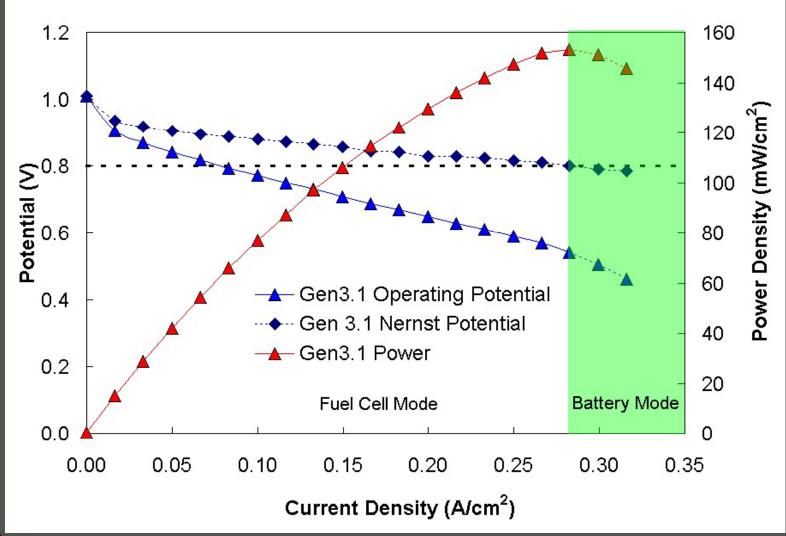
Thomas Tao, presenter, CellTech Power

3 Generations of LTA-SOFC Development



Fuel Cells for Real Fuels

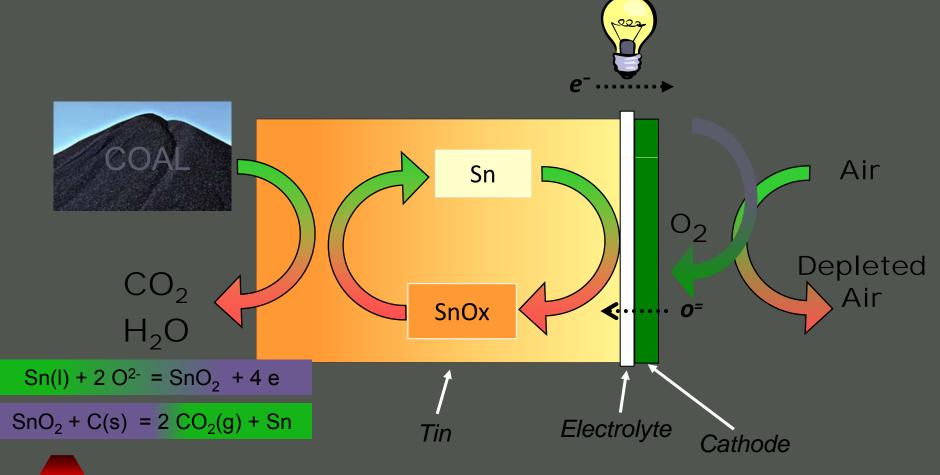
LTA-SOFC: Characteristics



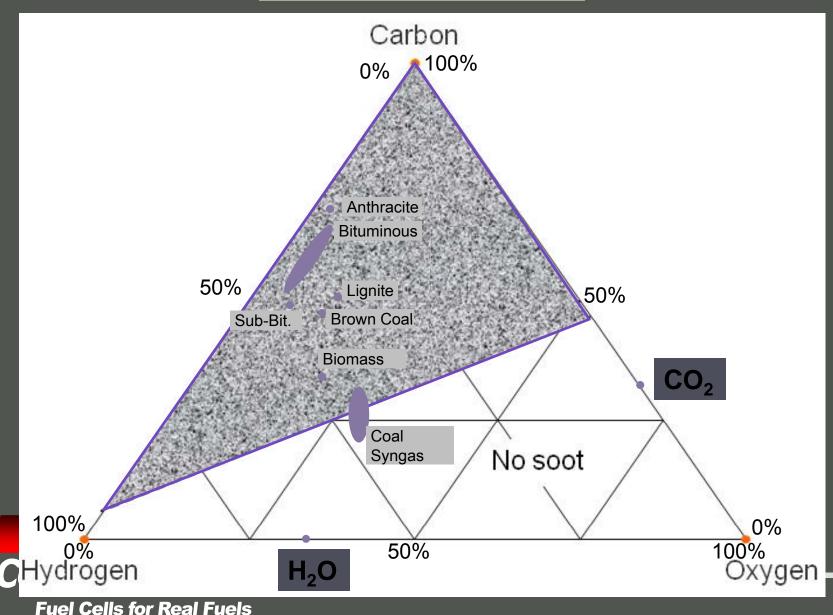
Voltage Threshold 0.78V @1,000°C, Hydrogen, Gen 3.1 LTA-SOFC



<u>Direct Coal Power Using Liquid Tin Anode</u> <u>SOFC</u>



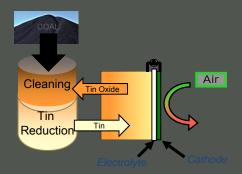
All Forms of Coal Will Make Soot – damage to Ni anode SOFC

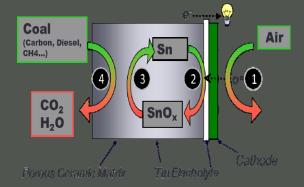


Liquid Tin Anode Fuel Cell Direct Coal – 3 Alternative Configurations

Electrochemical Looping

Based on Coal-Tin Reactor DE-NT0004111, DE-ER85006

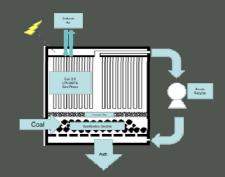


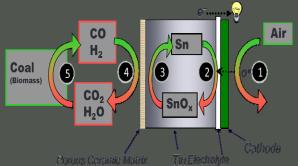


- 1 Oxygen ions extracted from air by cathode and cross the electrolyte
- 2 lons react with tin, releasing electrons and forming tin oxide
- 3 Tin oxide is independently reduced back to tin by reaction with fuel
- 4 Fuel directly contacts tin

Insitu Gasifier

Based on Portable Power Cell DE-ER95350S10



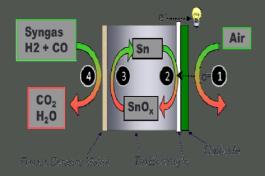


- 1 Oxygen ions extracted from air by cathode and cross the electrolyte
- 2 Ions react with tin, releasing electrons and forming tin oxide
- 3 Tin oxide is independently reduced back to tin by reaction with fuel
- 4 Tin-fuel interaction can occur inside tin or across a porous ceramic membrane
- 6 Coal or other solid fuel is gasified insitu by the cell reaction products

External Gasifier

Based on Portable Power Cell





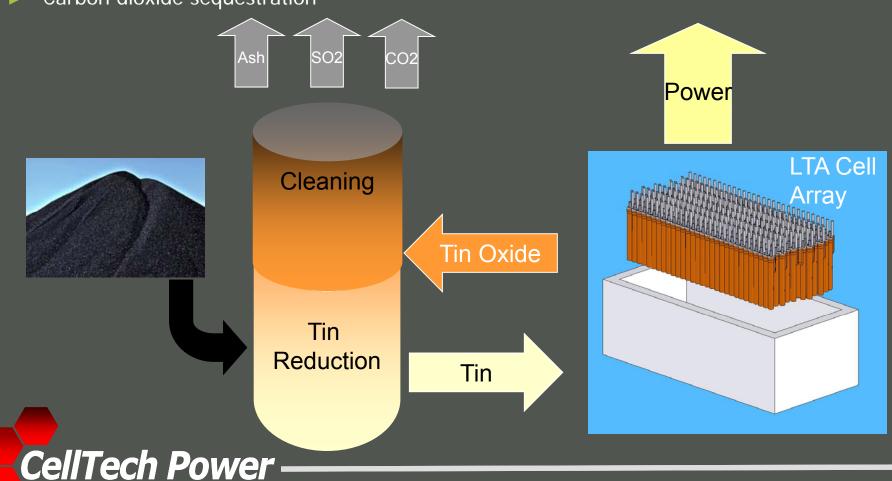
- Oxygen ions extracted from air by cathode and cross the electrolyte
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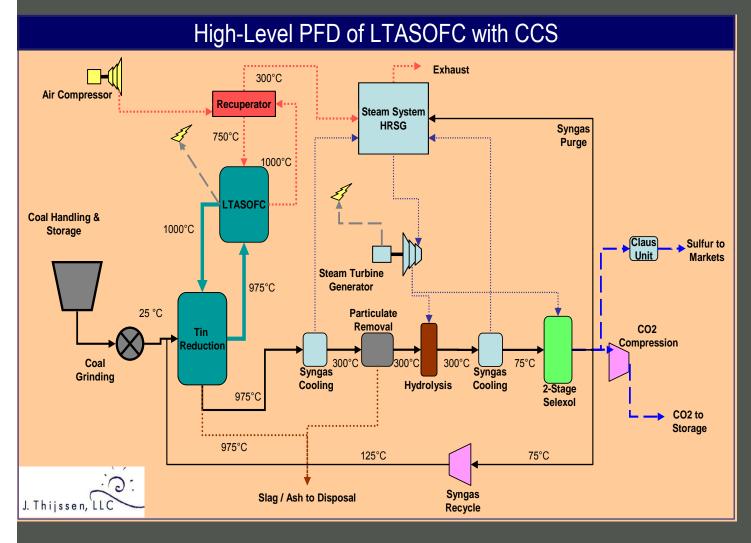
LTA- SOFC Electrochemical Looping - Tin Bath Concept for MW coal plant

- ▶ Separates fuel cleaning and reaction gases from Power Production module.
- Direct Coal-biomass feed into anode
- ► Tubular configuration without ceramic porous separator
- Carbon dioxide sequestration

Fuel Cells for Real Fuels



LTA-SOFC Coal Tin Bath Power Plant Concept



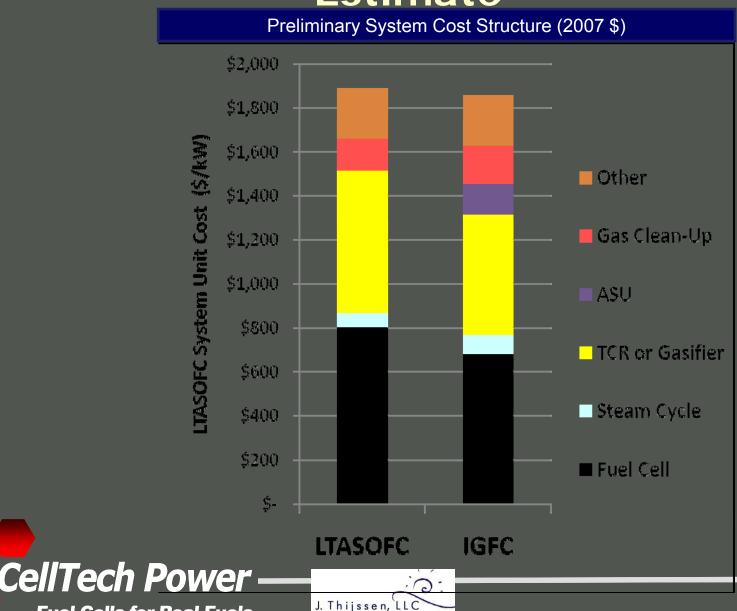
Most thoroughly analyzed concept to-date

- 63% System
 efficiency with CO2
 capture and
 compression
- System CAPEX: \$1400 – 2400/kW (similar to IGCF)
- Near 100% CO2 capture
- ► Tin provides separation of ash/impurities
- ▶ Requires development of Tin Coal Reactor similar to liquid metal gasifiers
- ► High tin recirculation rate required to meet O2 transport requirements.
- ► Tin anode requires electric current break



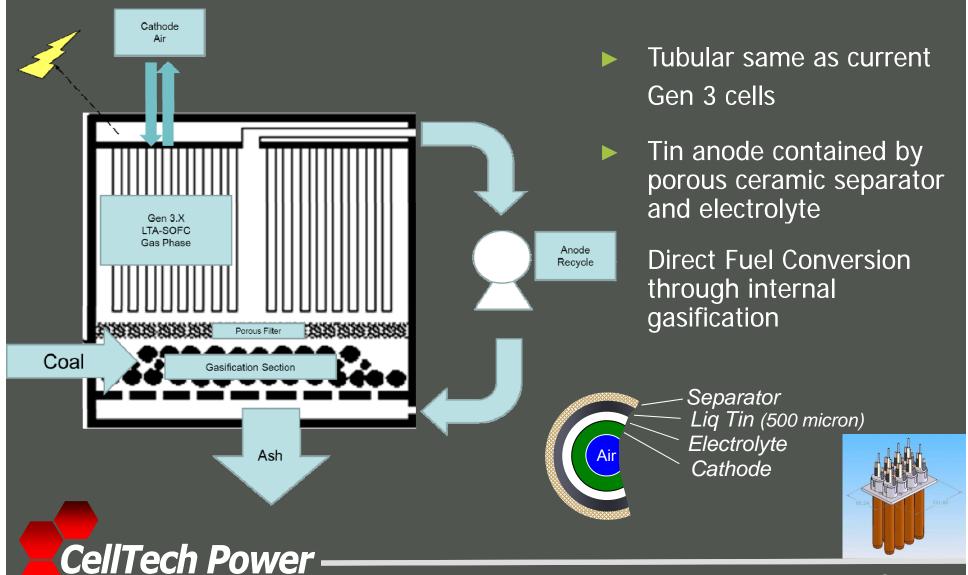
LTA-SOFC Coal Tin Bath System Cost

Estimate



Fuel Cells for Real Fuels

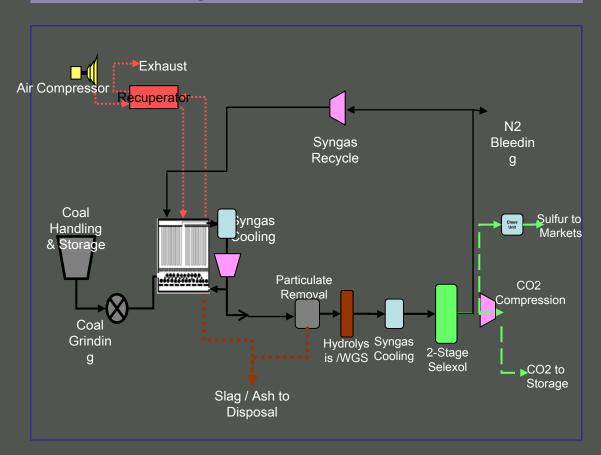
LTA-SOFC In-situ Gasification Concept



Fuel Cells for Real Fuels

LTA-SOFC In-situ Gasification Concept

High Level of PFD of Insitu Gasifier

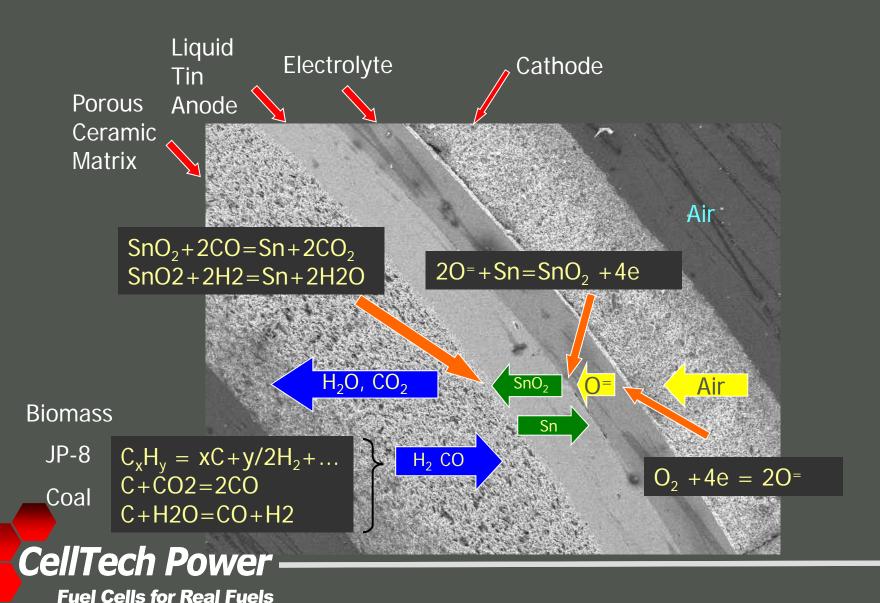


Uses cells with porous separator like existing CellTech Gen 3

- No direct contact between tin anode and solid fuel.
- Gasification is driven by CO₂ and H₂0 produced by cells (no Oxy plant required).
- Isolated anodes allow cell voltage build up.
- Ash, tar and carbon clogging of separator could be an issue.
- Volatile metal oxides in coal impact on cells unknown.
- Could test concept with Gen 3.1 cells and lab gasifier.
- Cathode air flow may increase to remove cell heat load.

LTA-SOFC Gen 3 for direct coal

Gasification cell using porous separator



LTA-SOFC External Gasification Concept



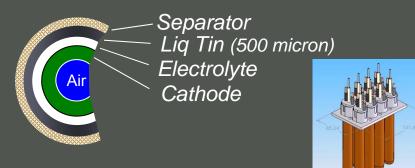
Tubular same as current Gen 3 cells

Tin anode contained by porous ceramic separator and electrolyte

Direct Fuel Conversion through internal gasification

Uses cells with porous separator like existing CellTech Gen 3

- Compatible with existing gasifiers
- •Reduced gas clean-up (Sulfur, CO)
- Lowest efficiency





Issues related to coal impurity

Impact on liquid tin anode

Impact on electrolyte

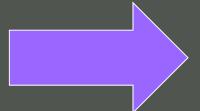
Impact on other cell components



Fuel Impurity Impact on Liquid Tin Anode

- Molten tin fluid state: Structure or surface cannot be damaged by contamination
- Gravimetric separation of ash from molten tin
- Addition of tin during plant operation is feasible and loss of tin not an issue

tin compounds of sulfur and halogens, volatile tin monoxide, volatile residual tin in ash



Evaluating fuel impurity impact on tin is a lesser issue

Coal Impurity Impact on Electrolyte

Yttria stabilized zirconia and phase destruction

Modeling for zirconia phase stability

Predictor for harmful elements and their list



Impurity Impact on Electrolyte Yttria stabilized zirconia and phase destruction

Yttria stabilized zirconia
 Tetragonal – low yttria, partially stabilized
 Cubic – high yttria, fully stabilized

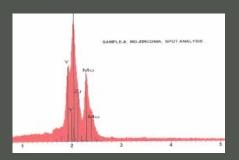
Phase destruction

Yttrium was displaced by higher CE elements and migrated to grain boundary

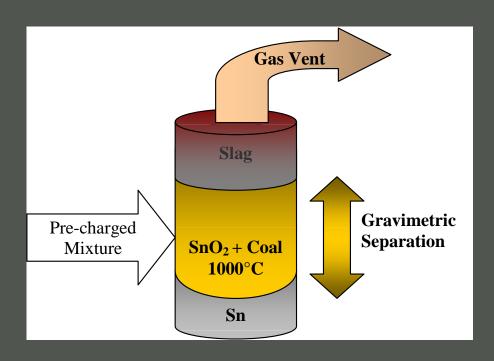


Exposed to Mo oxides, YSZ cracked

SEM/EDAX Indicating yttria migrating to grain boundary



SnO₂ reduction by coal - setup



Experimental concept for the chemical reactor that operates at 1000°C to separate the pre-charged mixture of coal and tin dioxide into tin and slag with a vented gas.

Coal contaminants with potential to harm ZrO2 based electrolyte: Arsenic, Chromium, Molybdenum, Manganese, Uranium, Niobium, Selenium, Vanadium, Tantalum, Tellurium and Tungsten



| El . | S5 Concentration | Oxide, valance at | Nernst Potential | Coulombic |
|---------|------------------|-------------------|------------------|-----------|
| Element | (ppm wt) | highest or stable | @1,000C | Energy CE |
| Ag | 1.1 | 1 | -0.24 | 0.16 |
| Se | < 0.01 | 6 | -0.2 | 2.57 |
| Rh | < 0.005 | 3 | 0.06 | 0.81 |
| As | 8.8 | 5 | 0.34 | 1.96 |
| Cu | 29 | 1 | 0.39 | 0.23 |
| Bi | 13 | 3 | 0.4 | 0.52 |
| Pb | 150 | 2 | 0.49 | 0.3 |
| Te | < 0.1 | 2 | 0.56 | |
| Ni | 2.9 | 2 | 0.65 | 0.52 |
| Sb | 400 | 3 | 0.66 | 0.71 |
| Cd | < 0.05 | 2 | 0.67 | 0.38 |
| Co | 0.28 | 2 | 0.75 | 0.55 |
| S | 23 | 4 | 0.75 | 1.95 |
| Sn | Matrix | 4 | 0.82 | 1.04 |
| Fe | 51 | 3 | 0.85 | 0.98 |
| Ge | < 0.01 | 4 | 0.87 | 1.36 |
| In | 58 | 3 | 0.89 | 0.67 |
| W | < 0.01 | 6 | 0.9 | 1.8 |
| Mo | < 0.01 | 4 | 0.93 | 1.11 |
| P | < 0.01 | 5 | 0.93 | 2.37 |
| K | < 0.01 | 1 | 1.01 | 0.13 |
| Cr | < 0.005 | 4 | 1.07 | 1.31 |
| V | < 0.001 | 5 | 1.07 | 1.67 |
| Mn | < 0.005 | 3 | 1.09 | 0.93 |
| Zn | < 0.01 | 2 | 1.1 | 0.49 |
| Ga | < 0.005 | 3 | 1.16 | 0.87 |
| Na | < 0.01 | 1 | 1.27 | 0.18 |
| Nb | < 0.005 | 5 | 1.4 | 1.41 |
| Ta | < 5 | 5 | 1.55 | 1.41 |
| U | < 0.005 | 6 | 1.55 | 1.48 |
| Si | < 0.01 | 4 | 1.77 | 1.8 |
| Ti | < 0.005 | 4 | 1.85 | 1.18 |
| Al | < 0.05 | 3 | 2.2 | 1 |
| Zr | < 0.005 | 4 | 2.22 | 1 |
| Li | < 0.005 | 1 | 2.23 | 0.24 |
| Mg | < 0.01 | 2 | 2.39 | 0.47 |
| Sr | < 0.005 | 2 | 2.4 | 0.31 |
| Be | < 0.005 | 2 | 2.51 | 0.8 |
| Ca | < 0.01 | 2 | 2.6 | 0.36 |
| Sc | < 0.001 | 3 | 2.65 | 0.72 |
| Y | < 0.005 | 3 | 2.66 | 0.6 |
| Tl | 0.04 | 3 | < 0.9 | 0.61 |

Impurities found in Sn from SnO2 reduction by coal (US Wyoming)

Ranking of soluble elements in molten tin based on their Gibbs free energy (Nernst Potential)

Only those elements in coal with Nernst Potential less than 0.9 V were found in tin (sample S5)

Potential Coal Contaminant Solubility in Tin at condition of tin-coal reactor

| | Initial | ICP-OES | Pure Sn |
|----------------|----------|----------|--------------|
| | amount | Results | GDMS results |
| Spiked Element | (ppm wt) | (ppm wt) | (ppm wt) |
| Cr | 4000 | 1098 | 2.7 |
| V | 4000 | 10 | < 0.001 |
| Мо | 4000 | 9 | < 0.01 |
| Nb | 4000 | 115 | < 0.005 |
| As | 4000 | 2535 | 1 |
| Mn | 4000 | 2405 | 0.2 |
| W | 4000 | 60 | < 0.01 |
| Та | 4000 | 8 | < 5 |
| Se | 4000 | 44.7 | < 0.01 |
| CI | 4000 | | < 0.01 |
| S | 4000 | 8 | 0.07 |
| Р | 4000 | 203 | 80.0 |
| Si | 4000 | 5 | < 0.01 |
| Br | 4000 | | < 0.05 |
| I | 4000 | | < 0.05 |

Solubility Experiment: tin spiked, 1,000C, 1% H2O in H2, 5 hours, cooled

ICP-OES analysis results: including both dissolved and entrained

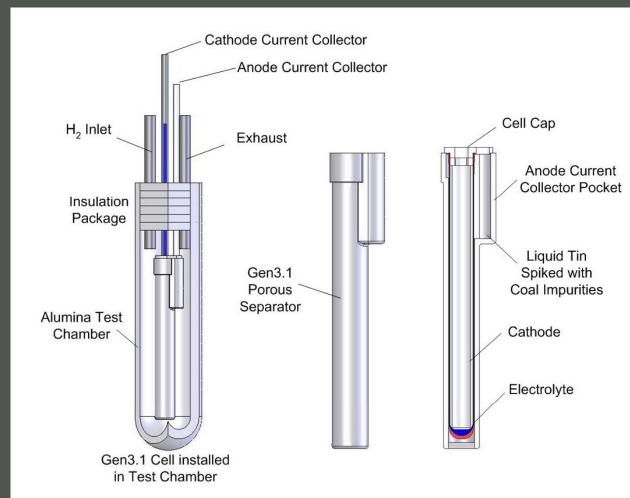
Results imply the maximum possible solubility of impurity in tin at coal-tin reactor condition



Electrochemical testing - setup

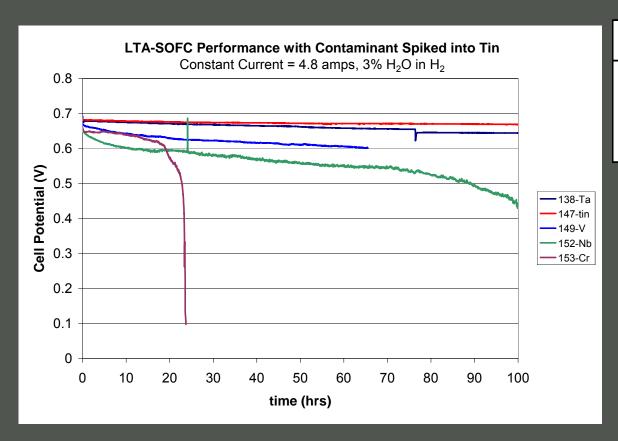
Setup: Gen 3.1 cell Hydrogen as fuel

Tin spiked with potential coal contaminants such as V, As, Ta, Ti, Mo, Nb, P, Cl, Si, Na and Cr, etc.





Potential Coal Contaminant Impact on LTA-SOFC



| Percent Voltage Drop at end of Test | | | | | | |
|-------------------------------------|------|------------|------|--|--|--|
| Element | ppm | Time (hrs) | % | | | |
| | | 100 | 2.1 | | | |
| Та | 8 | 100 | 3.2 | | | |
| V | 10 | 66 | 9.6 | | | |
| Nb | 115 | 100 | 34.4 | | | |
| Cr | 1098 | 24 | 12.9 | | | |

Testing conditions:

Gen 3.1 LTA-SOFC cells

Tin individually spiked to the maximum possible concentration

Constant current 4.8 amp @ 3% H2O in H2

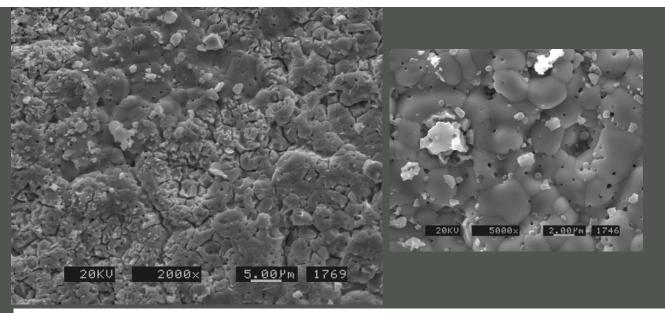


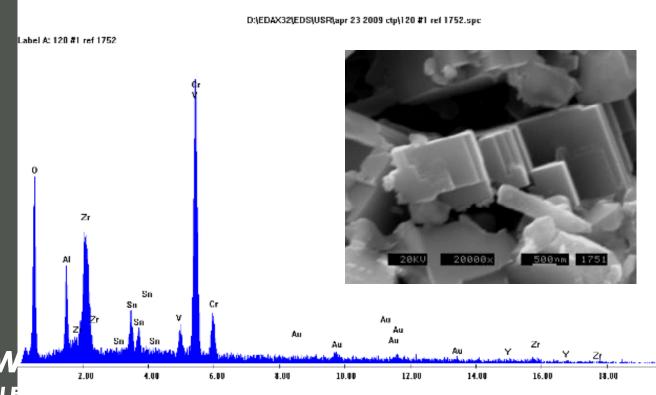
LTA-SOFC Gen 3.1 cell collectively spiked with V, As, Nb, Mo and Cr to 1,500ppm

Post Mortem analysis:

Electrolyte damage found

Oxide crystals of Cr, V found on YSZ surface







<u>Summary</u>

<u>Demonstration of Feasibility of Liquid Tin Anode SOFC as Direct</u> <u>Coal Conversion Fuel Cell</u>

- Three liquid tin anode configuration concepts for direct coal conversion
- Fuel impurities cause degradation / damage to electrochemical component
- Tin's potential as a media for removing or reducing fuel contaminants including from coal, biomass and diesel
- Ongoing projects in progress to address individual contaminant and coal ash



Acknowledgements

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DOD ONR Contract N00014-08-C-0164, Mr. Cliff Anderson

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