Microstructure of Non-fusion Joints:

Friction Stir Welding, Transient Liquid Phase Sintering and Pulsed Plasma-Assisted Diffusion Bonding

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Outline of Presentation

- Problems with fusion joints in ODS ferritic stainless steels
- Friction Stir Welding
- Transient-Liquid Phase Bonding
- Pulsed Plasma-Assisted Diffusion Bonding

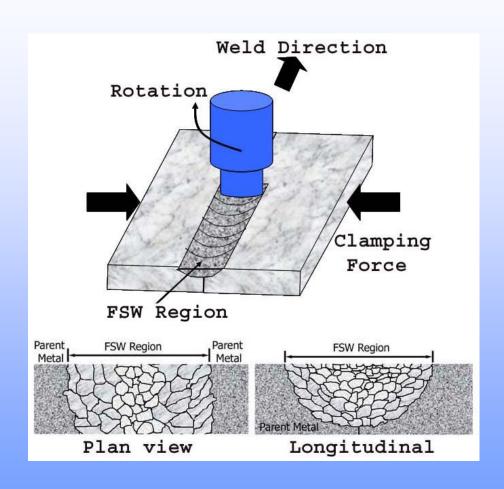


Joint Microstructure

Fusion Weld Original Interface Ideal



Friction Stir Welding



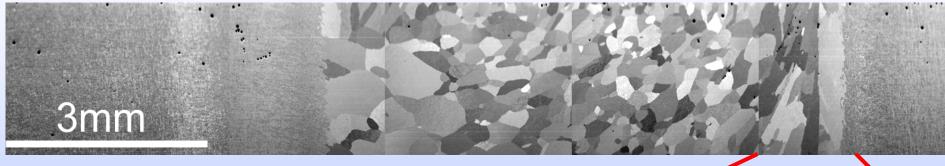
PM2000 Plan view



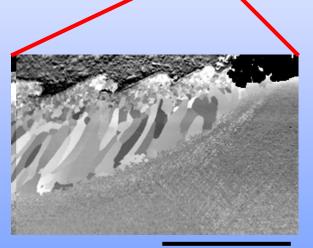
10 mm



Friction Stir Weld in PM2000



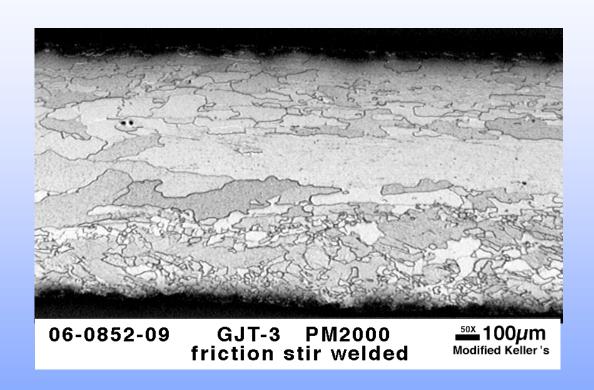
SEM plan view image of PM2000 FSW Annealed at 1380°C for 1h after removal of top layer



Cross section 1mm



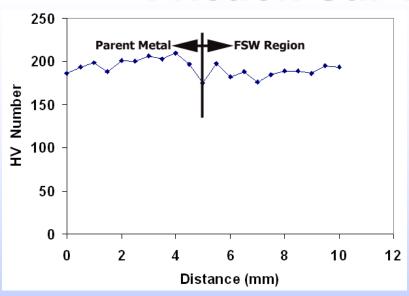
Friction Stir Weld in PM2000

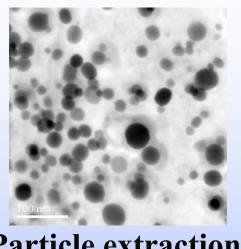


Annealed, rolled at 175°C, 40% reduction, then recrystallised at 1380°C for 1h.



Friction Stir Weld in PM2000

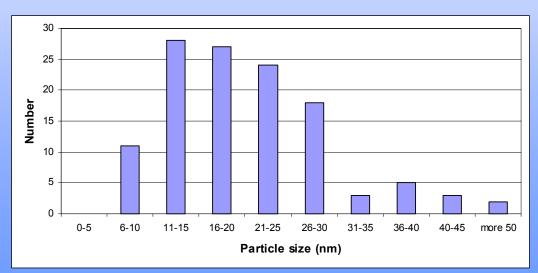




Particle extraction

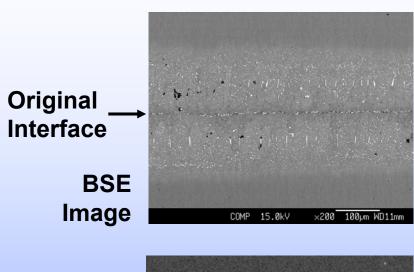
Hardness

Particle Size Distribution of Friction Stir-Welded Region in PM2000 after 1 hr heat treatment at 1380°C

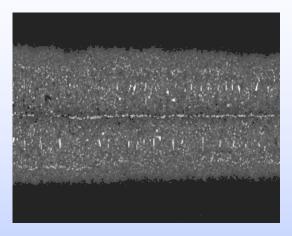




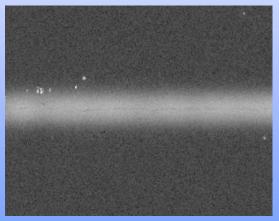
TLP Bonding of PM2000

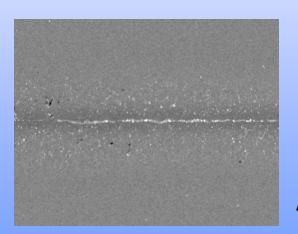


Si map



Au map



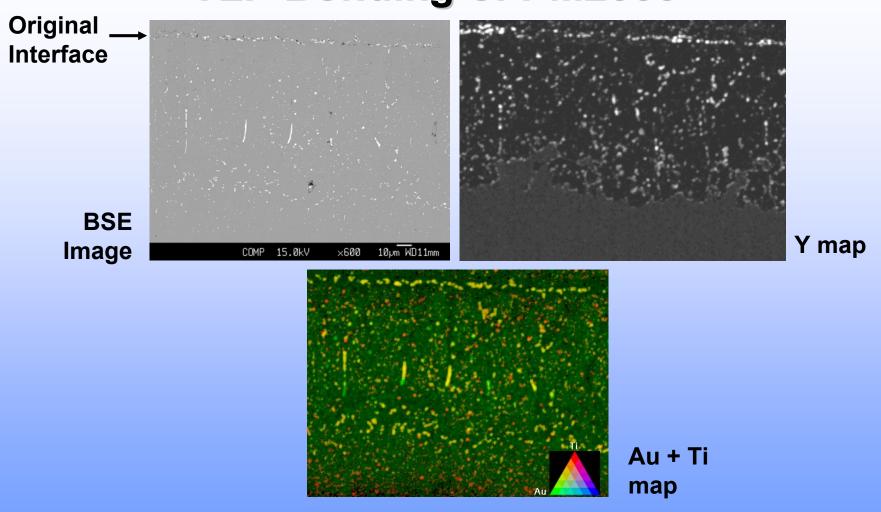


Al map

As-joined



TLP Bonding of PM2000

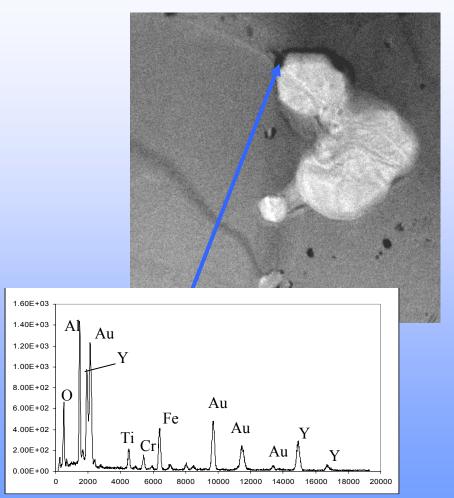


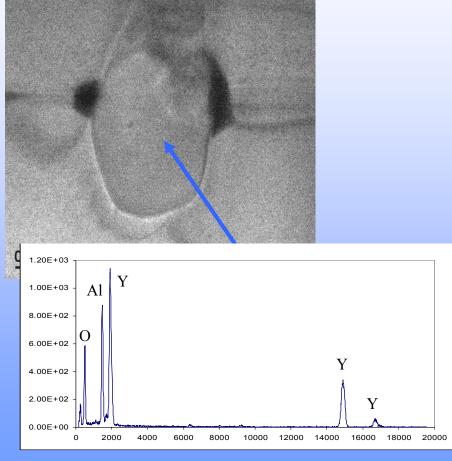
Annealed for 4h at 1000°C after joining

Bornstein, Hurley and Wright (2006)



Agglomeration of particles surrounded by Au rich phase





PM2000 annealed for 4h at 1000°C after joining



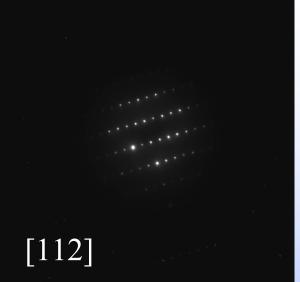
Diffraction Patterns from YAG Particles



FeCrAl matrix plus YAG (Y₃Al₅O₁₂)

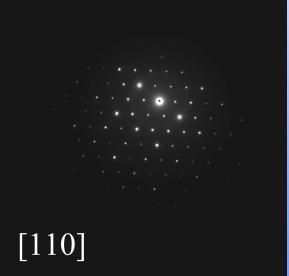
 $d_{YAG (002)} / d_{Fe (110)} = 2.94$ c.f. 2.962 from PDF files.

(Addition of 20% Cr increases lattice parameter of Fe by 0.2%)





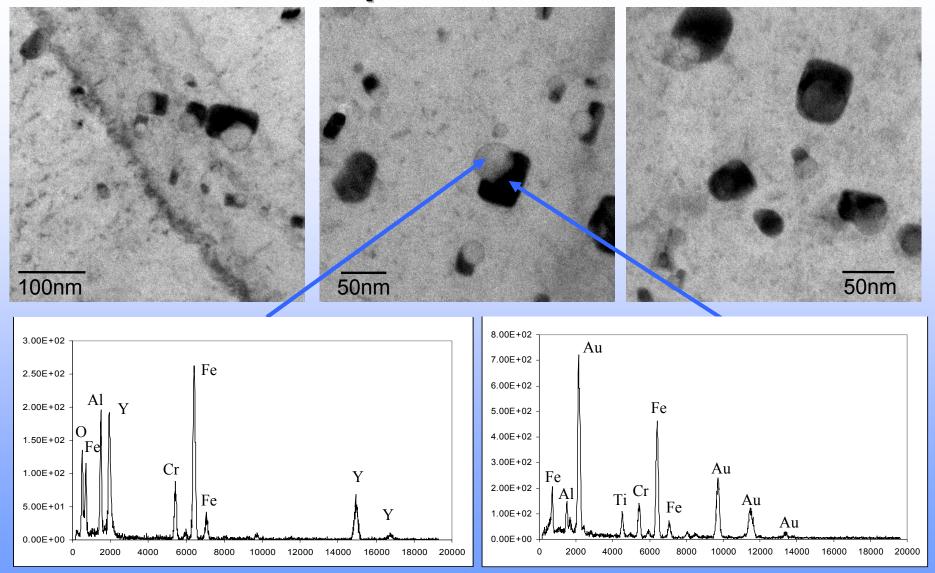






PM2000 annealed for 4h at 1000°C after joining

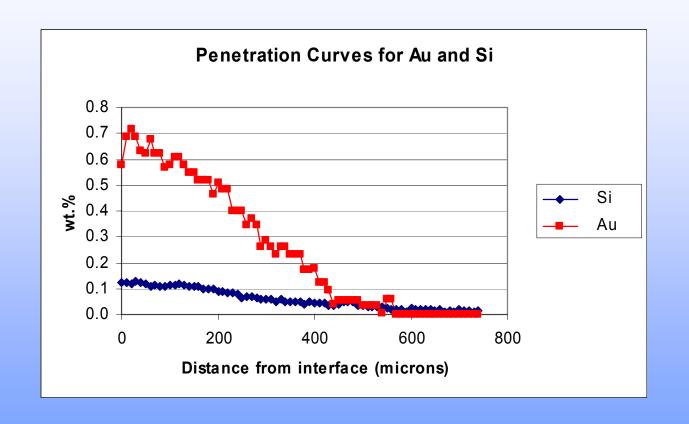
Duplex Particles



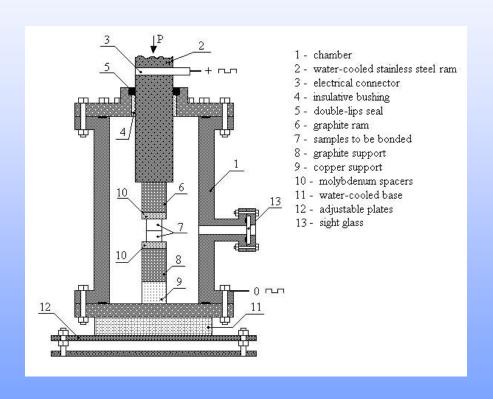
PM2000 recrystallised after joining



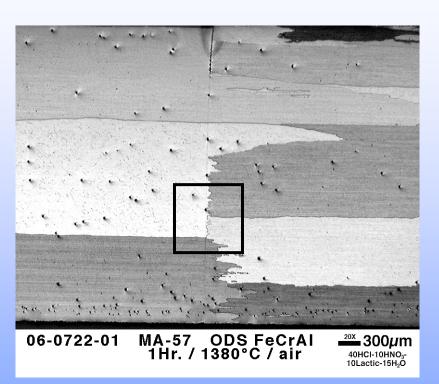
Diffusion of Au and Si away from the interface

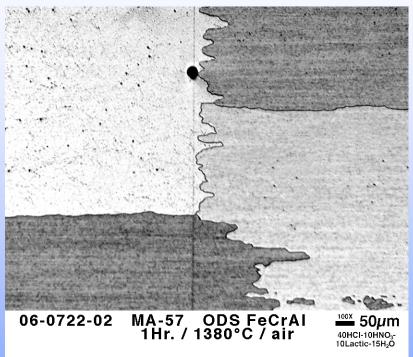






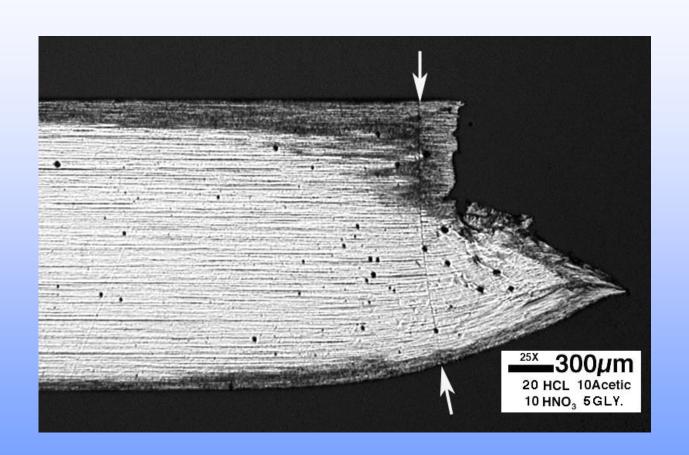
Eugene Dyadko, MER Corporation, Tucson, AZ



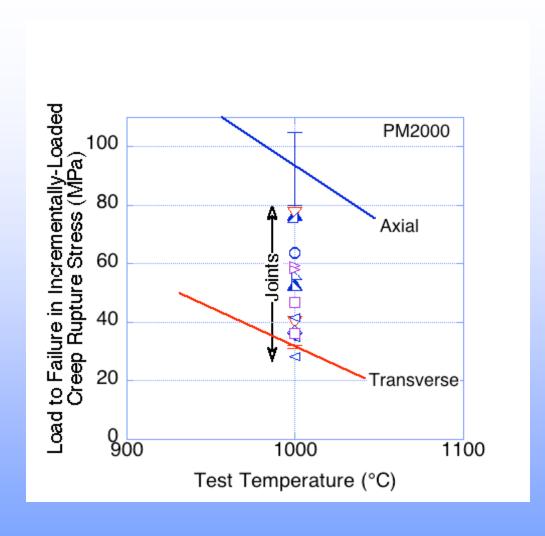


Wright and Dyadko (2006)



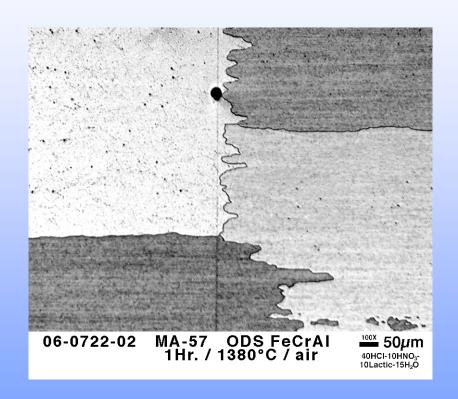




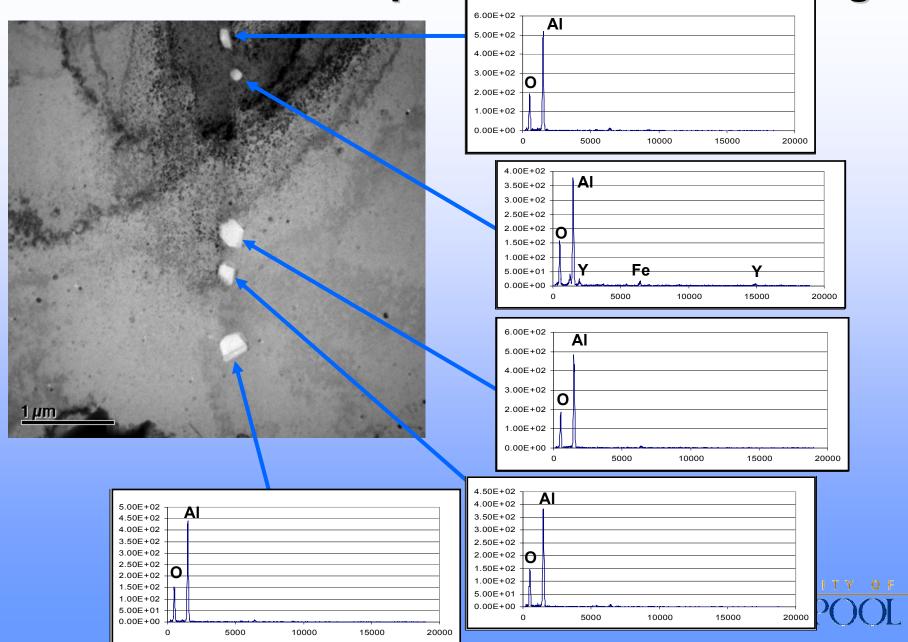


I. G. Wright ORNL









Conclusions and Future Work

- All three methods of joining ODS alloys look to hold great promise.
- The grain structure of friction stir welds can be modified by a small amount of further deformation.
 Welds in sheets, which are amenable to secondary recrystallisation, are now needed.
- The TLP process needs to be modified to reduce any agglomeration of oxide particles near the interface, but the gold and silicon appear to diffuse rapidly away from the interface without causing further disruption to the structure.



Conclusions and Future Work

- The weld interface after plasma assisted bonding is very clean and only marked by a row of remnant alumina particles, which do not pin the grain boundaries during secondary recrystallisation.
- The successful joining of ODS FeCrAl alloys, which has alluded us for so long, finally appears to have been achieved.



Acknowledgements

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