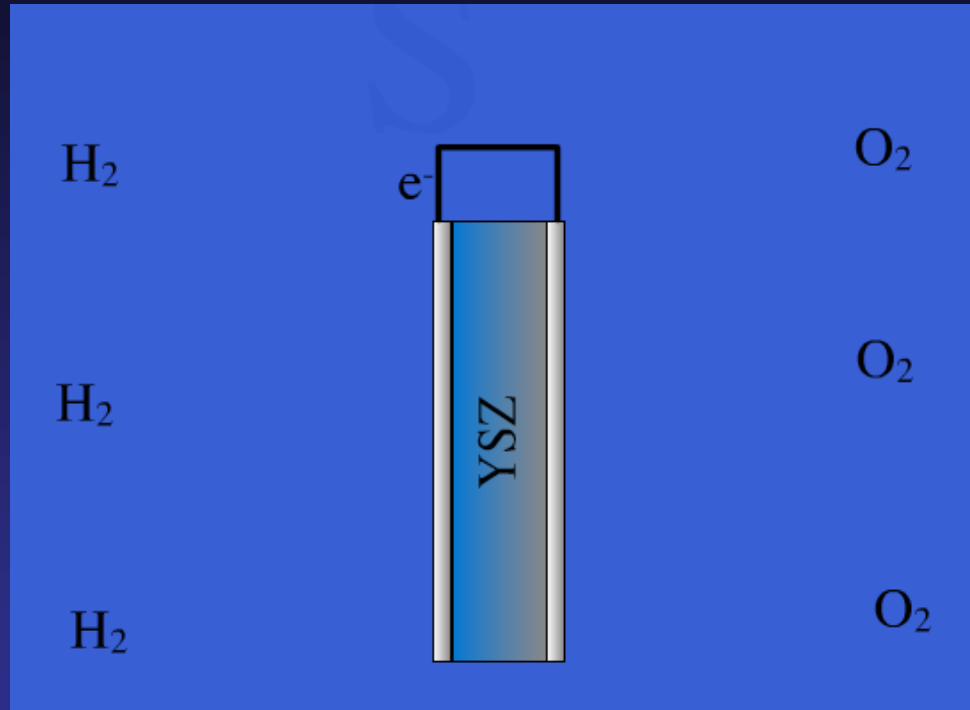
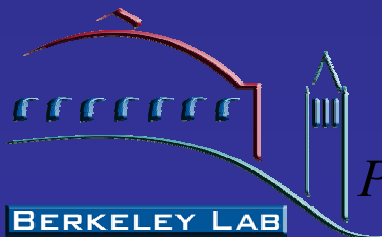


Enhancement of Electrode and Interconnect Performance

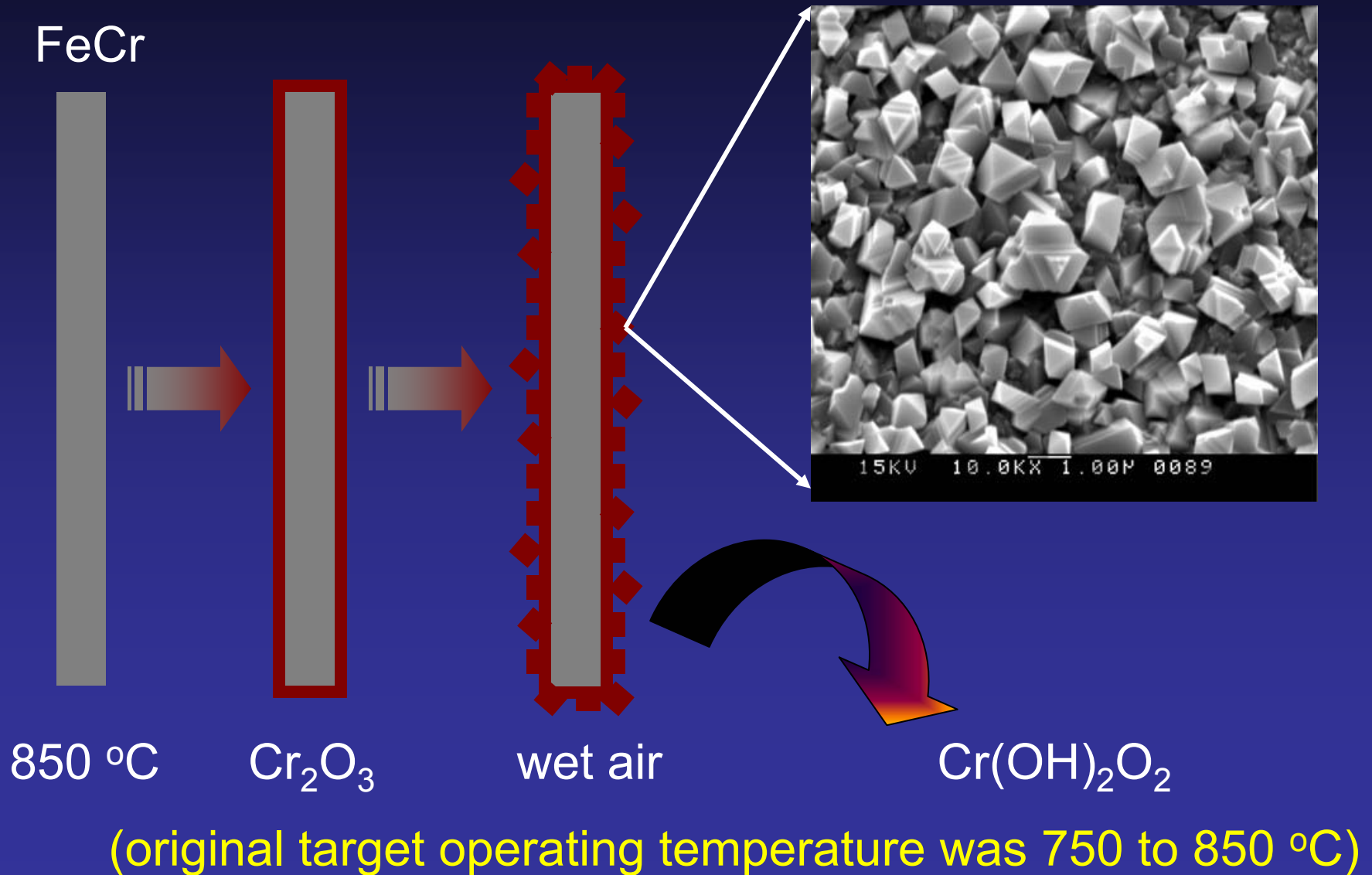


Steve Visco, Craig Jacobson, Xuan Chen, and L. C. De Jonghe
Materials Science Division
Lawrence Berkeley National Laboratory

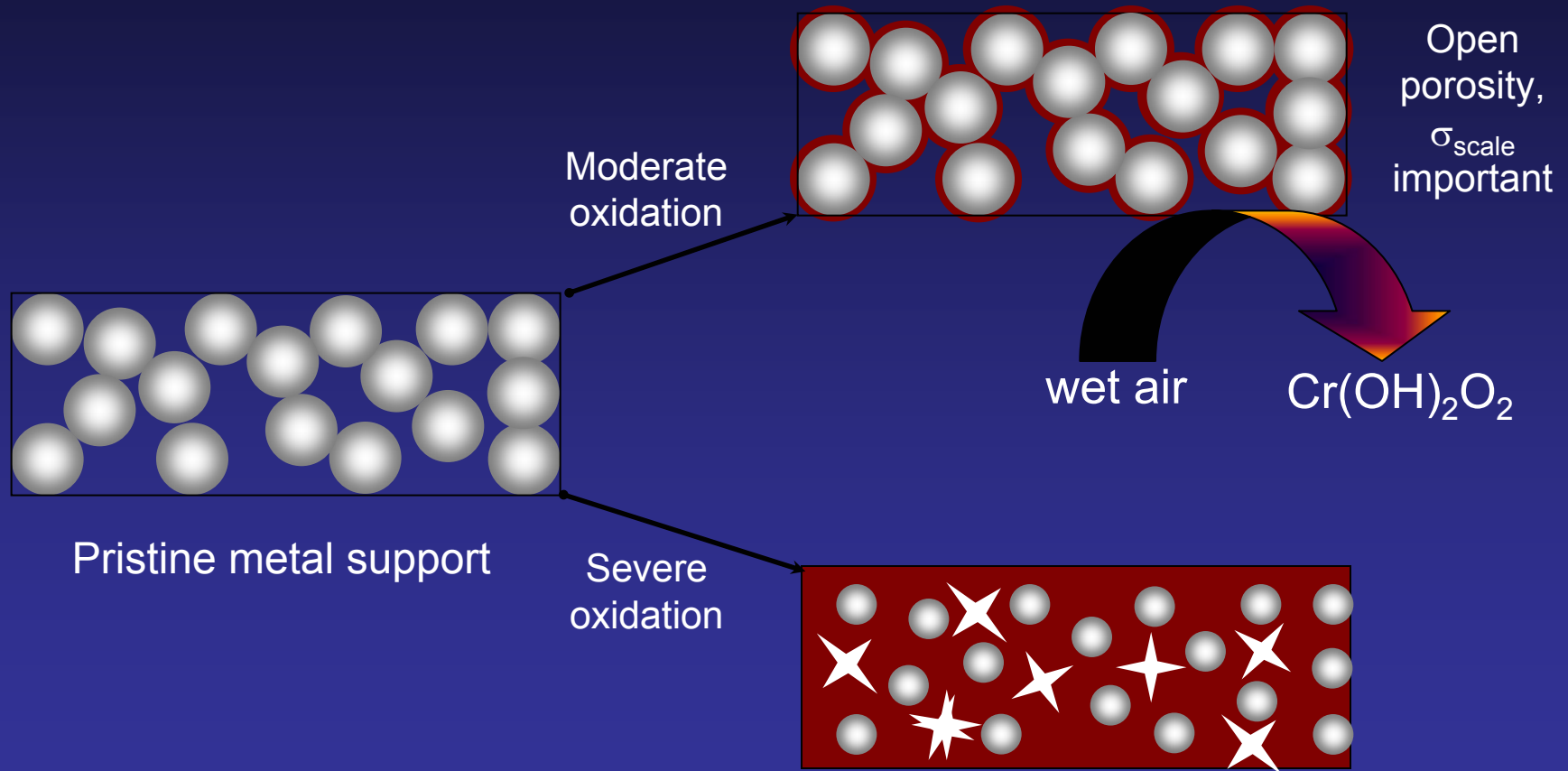


Presented at SECA core technology review, May 11-13, 2004

Oxidation of Ferritic Steels

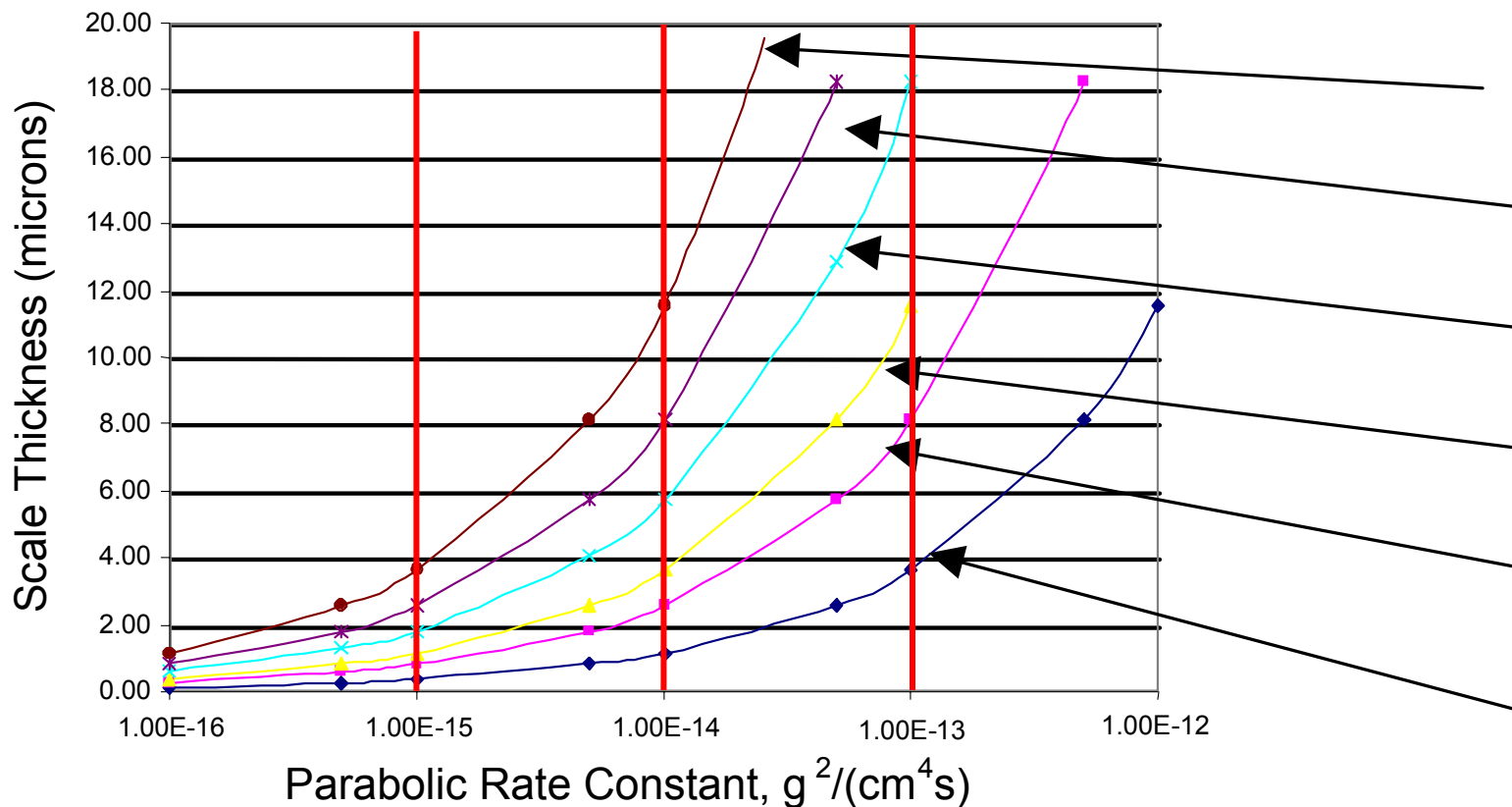


Metal Supported SOFCs



Chromia scale thickness as a function of parabolic growth rate constant and operational lifetime of the device

Dense Chromia Scale Thickness as a function of Kp



Ferritic Steel Oxidation Rate Studies

- Oxidation studies in air and in wet H₂ for a variety of ferritic steels (Cr content 12-30 wt%) have been performed for fuel cell and related applications. At 800°C the growth rates for these alloys, with or without a surface treatment of a reactive element such as yttria, **is grouped around $\sim 10^{-13}$ g²/cm⁴s**.
- Ferritic steels have scale growth rates that are acceptable for SOFC application ($< 10^{-14}$ g²/cm⁴s) at temperatures $\leq 700^\circ\text{C}$.
- However, to minimize resistive losses the conductivity of the chromia scale should be > 0.005 S/cm at 650°C in so that the contribution to cell resistance is $< 0.1 \Omega \text{ cm}^2$ after 50,000 hours.

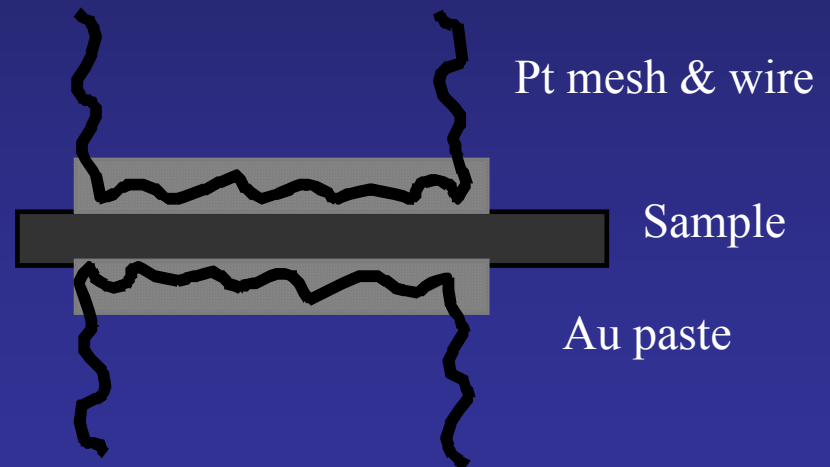
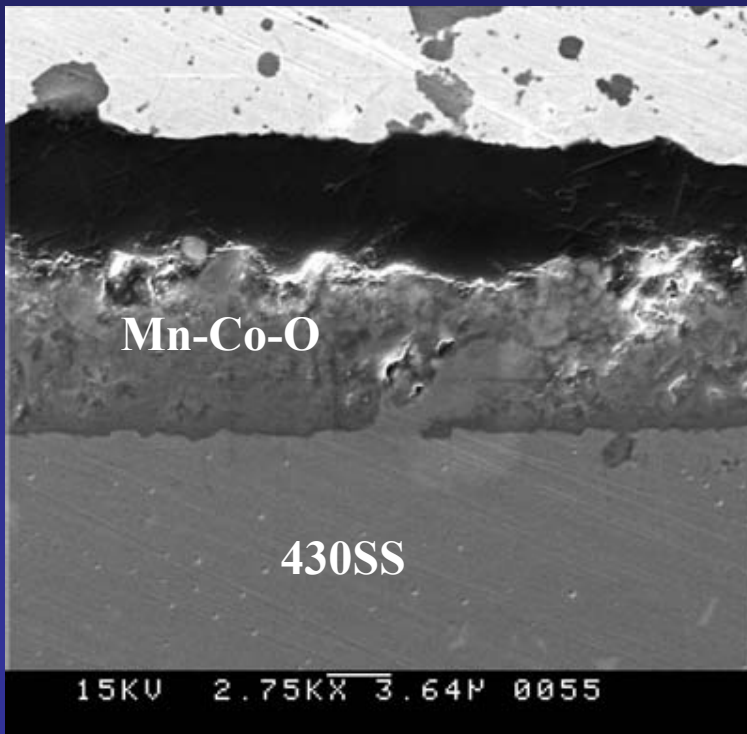
Target Parameters for Ferritic Steel

- Scale thickness limit at $<10\mu\text{m}$ for the life of the device.
- Growth rate constant, $K_p = (\text{weight gain } \text{g}/\text{cm}^2)^2/\text{sec}$, should be $<10^{-14}\text{g}^2/\text{cm}^4\text{s}$ and preferably $\sim 10^{-15}\text{g}^2/\text{cm}^4\text{s}$.
- Conductivity of the chromia scale should be $>0.005\text{ S}/\text{cm}$ at 650°C
- Cr volatilization should be below threshold for cathode poisoning and below EPA limits ($0.015\text{ mg}/\text{m}^3$)

Oxidation Studies

430 SS composition

Element	Cr	C	Ni	Mn	Si	Fe
wt%	16.3	0.04	0.2	0.45	0.40	balance

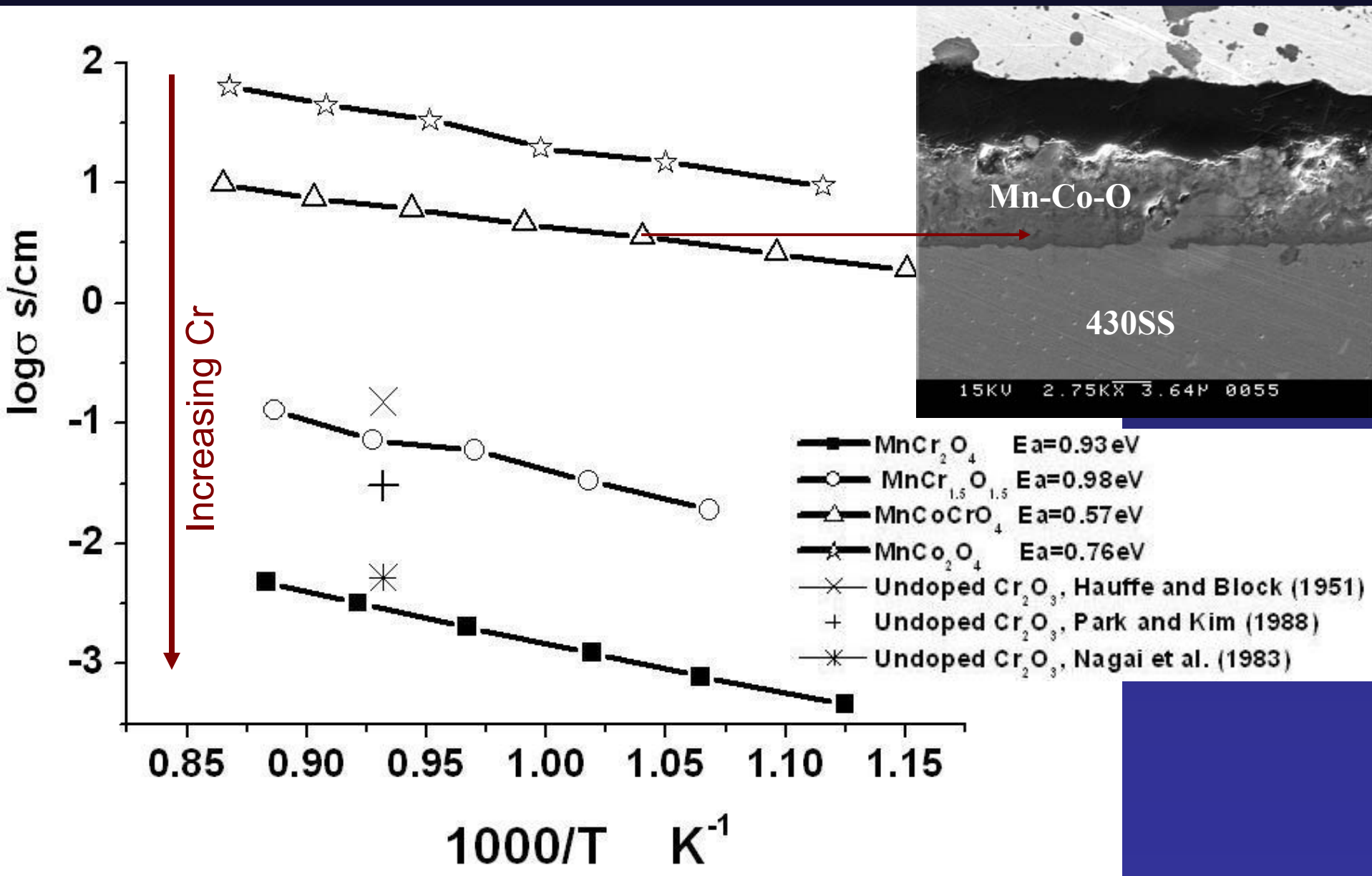


Conductivity of Oxide Films

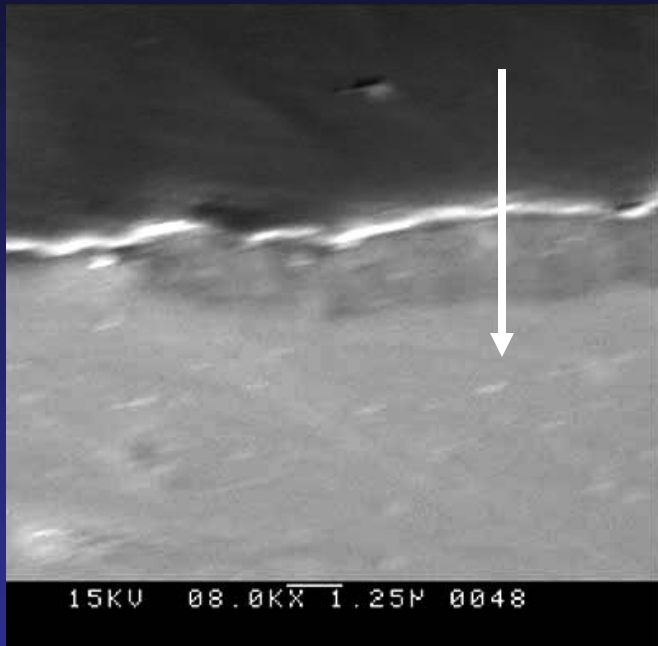
Conductivity at about 800°C (S/cm)

MnCo ₂ O ₄ , GNP, sintered at 1300°C	31.6
MnCrCoO ₄ , GNP, sintered at 1300°C	6.3
Mn _{1.5} Cr _{1.5} O ₄ , GNP, sintered at 1300°C	7.9*10 ⁻²
MnCr ₂ O ₄ , GNP, sintered at 1300°C	2.5*10 ⁻³
Undoped Cr ₂ O ₃ , Hauffe and Block (1951) [18] sintered at 1200°C	0.15
Undoped Cr ₂ O ₃ , Park and Kim (1988) [19] 99.9% sintered at 1400°C	3.02*10 ⁻²
Undoped Cr ₂ O ₃ , Nagai et al. (1983) [20] 99.9% sintered at 1200°C	5.2*10 ⁻³

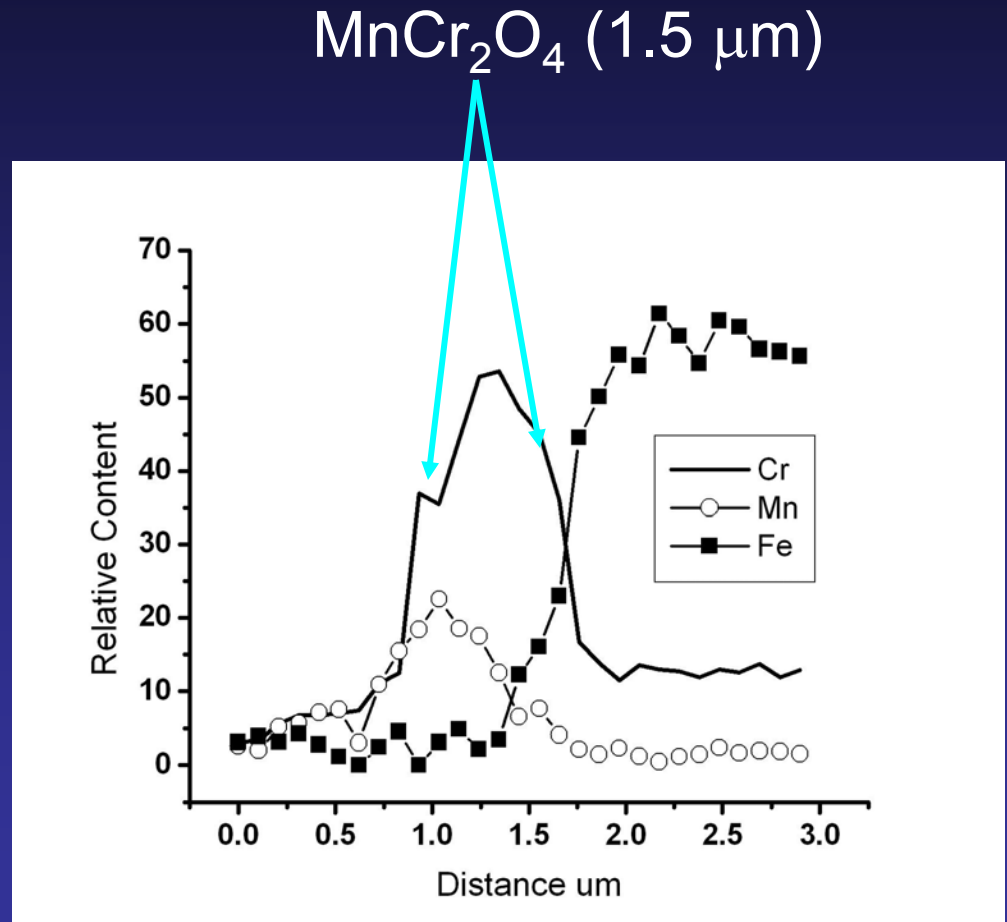
Conductivity of Potential Coatings



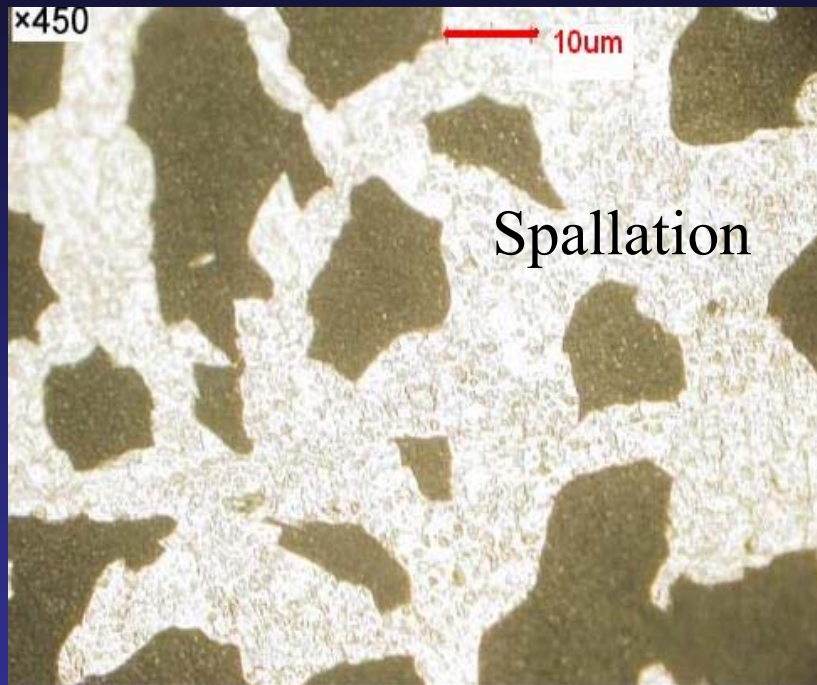
MnCr_2O_4 film is grown from alloy (low σ)



Mn already present in alloy
forms spinel, but low
conductivity will be an issue
for applications



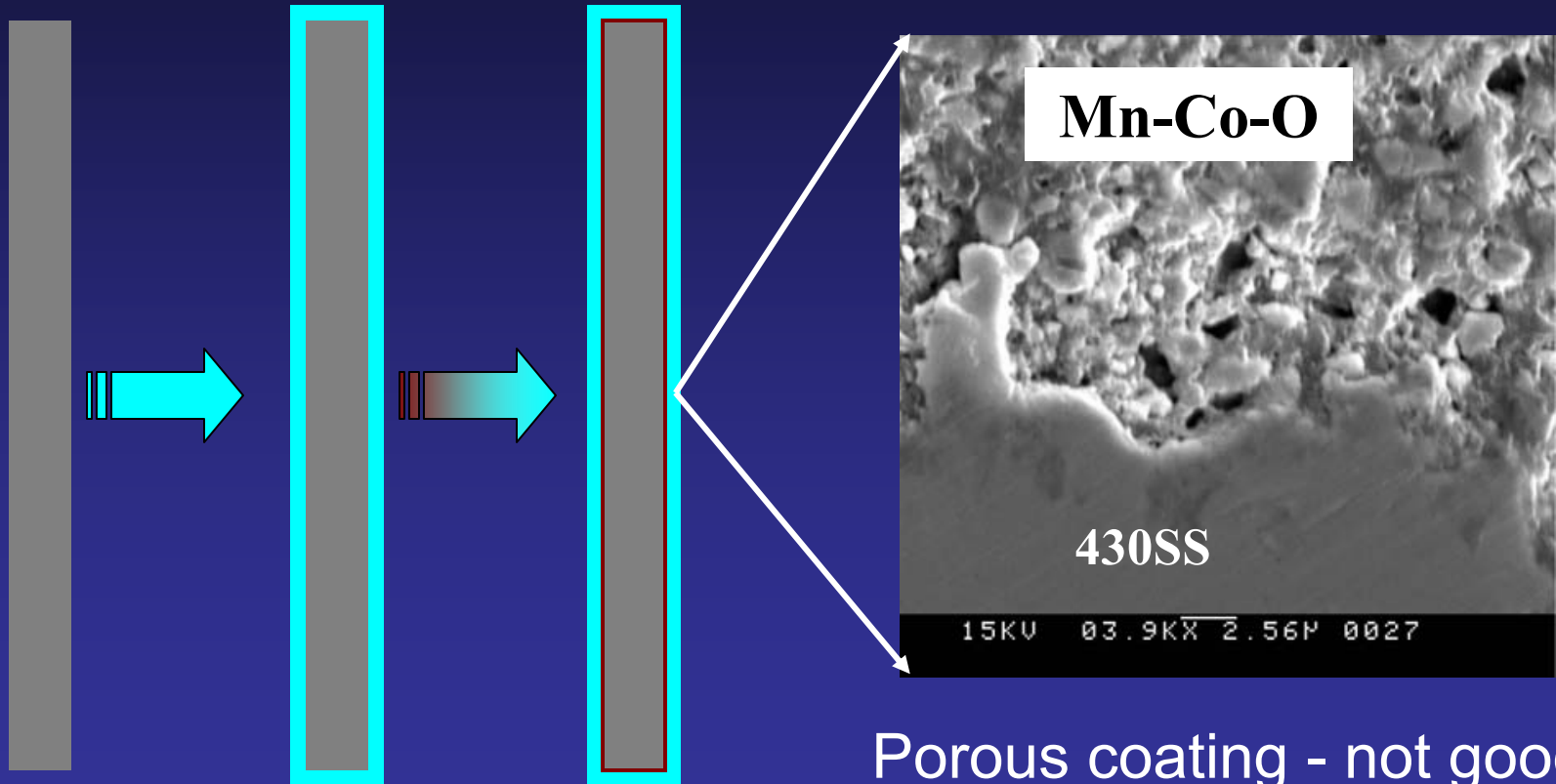
Spallation of Uncoated 430 Oxide film



After thermal cycling from 850 $^{\circ}\text{C}$ to RT (~ 50 $^{\circ}\text{C}/\text{min}$ cooling)

Preparation of Protective Coatings

400 series MnCo_2O_4 850 °C

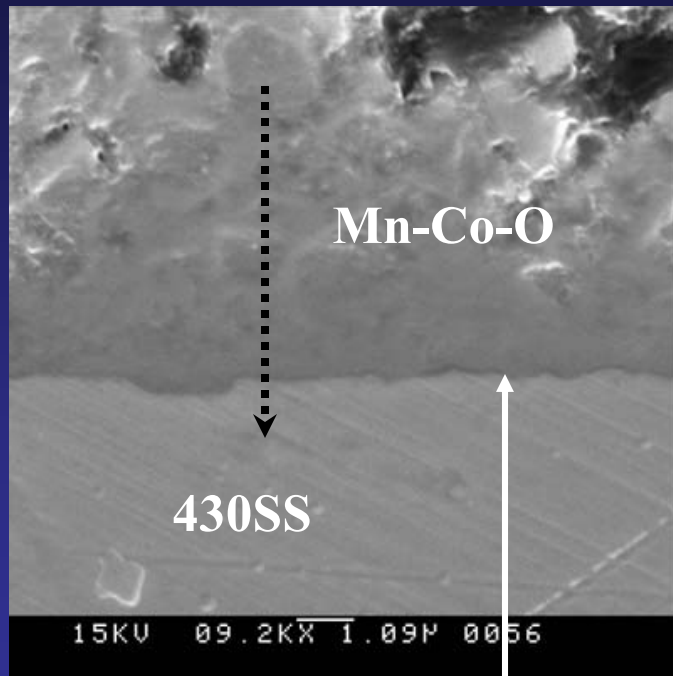


Porous coating - not good

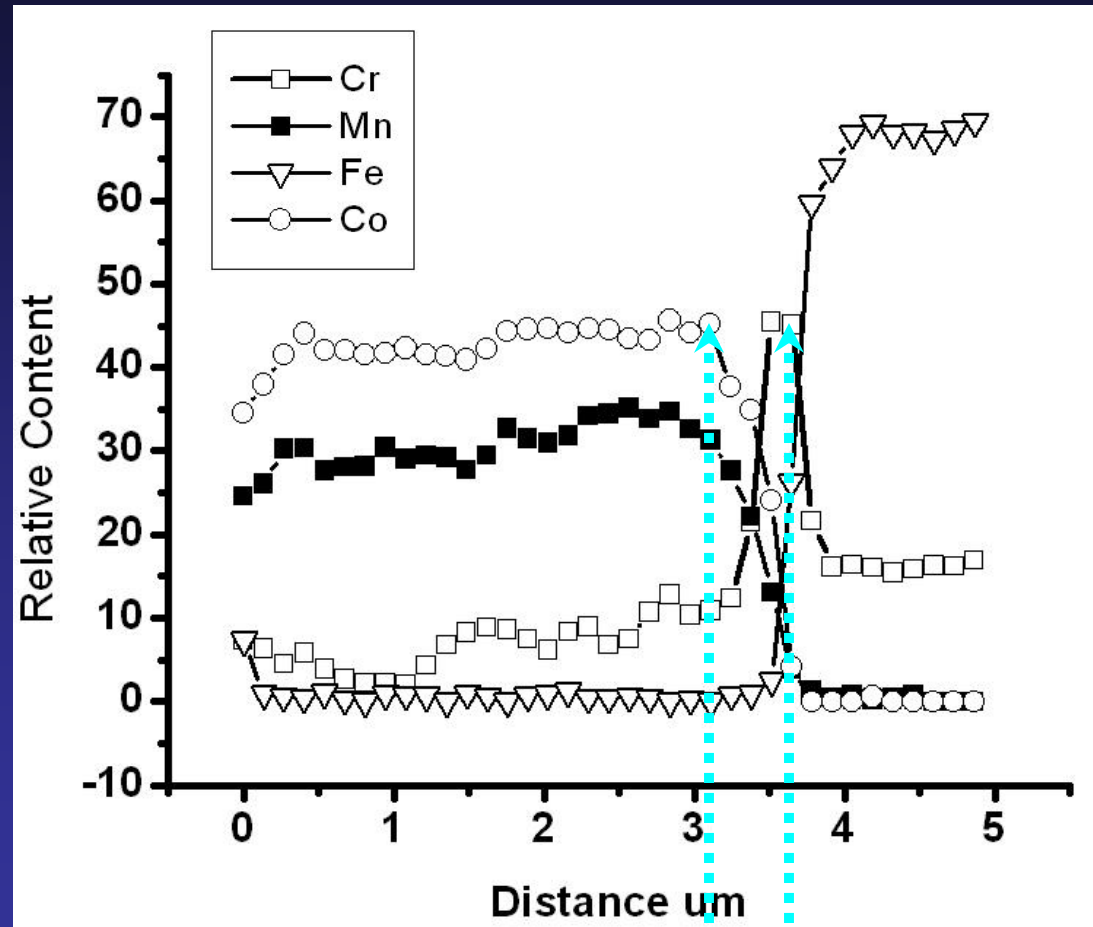
Colloidal spray coating ($\sim 10 \mu\text{m}$)

High quality LBNL coating

EDAX

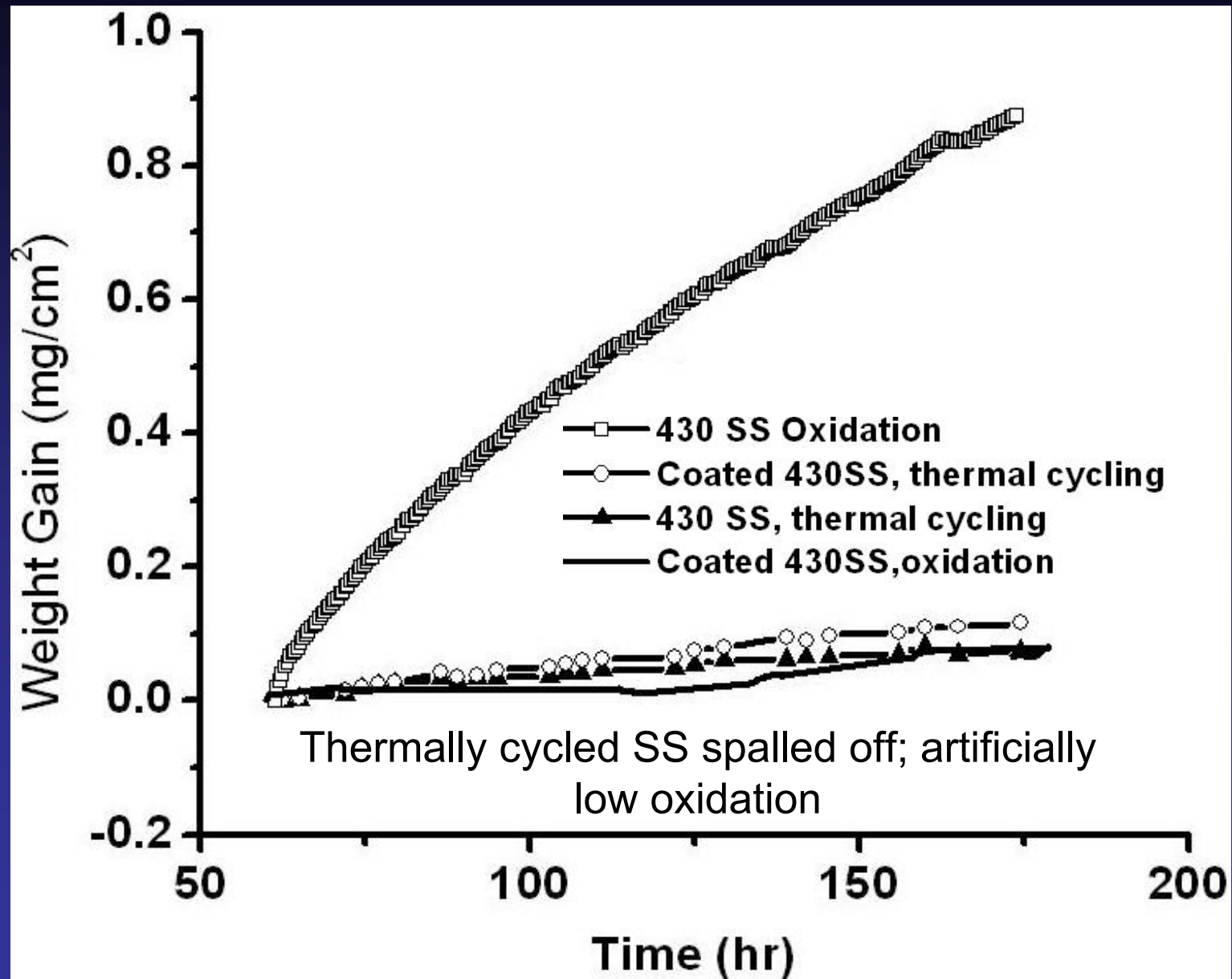


Cr₂O₃

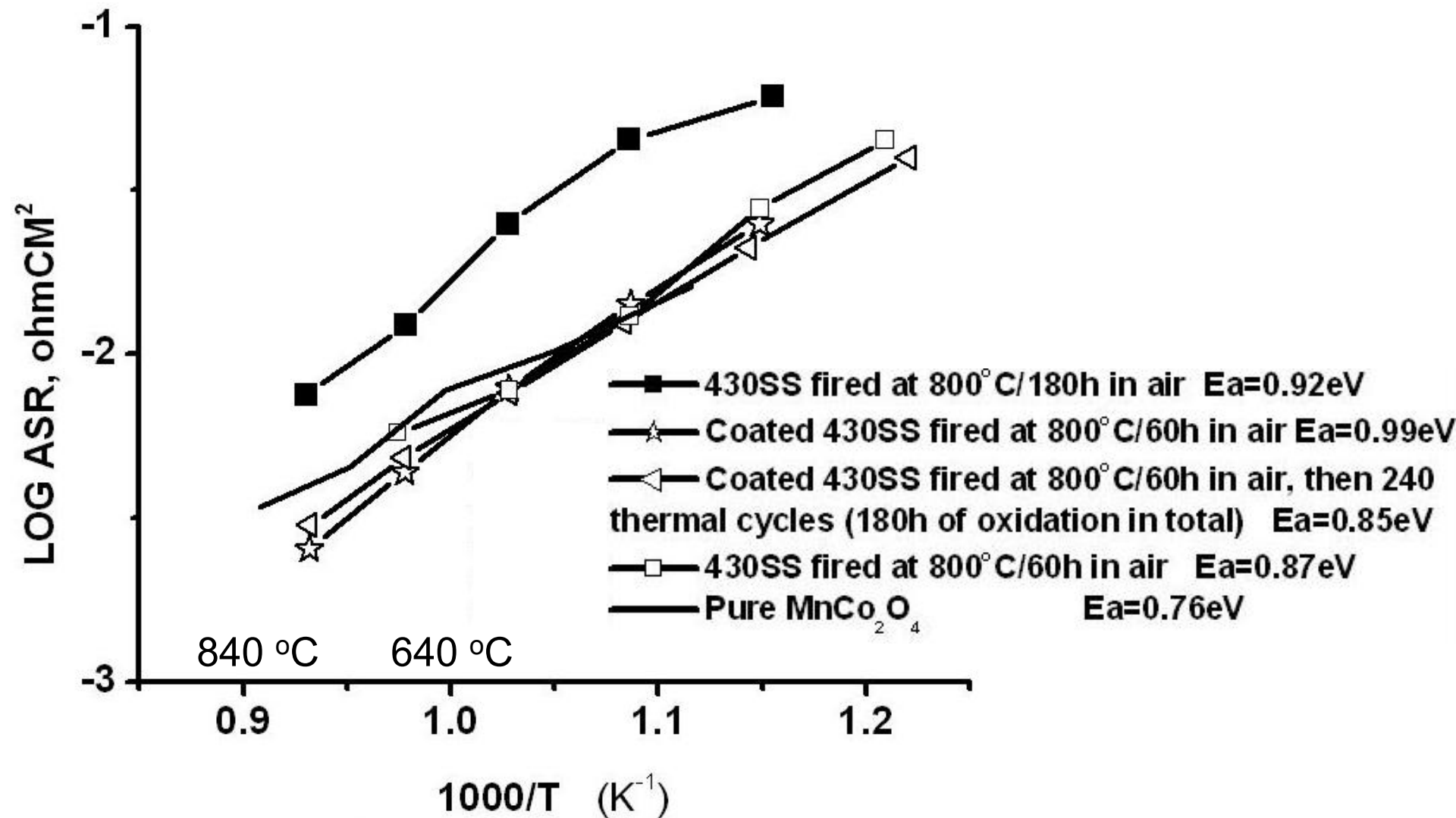


Mn-Cr-Co-O (0.3 μm)

Oxidation Behavior of LBNL Coated SS



Coated SS's 10x lower ASR - even with 240 thermal cycles



LBNL Coated Samples Exhibit 10x Lower Oxidation Rate & 10x Higher σ

	Oxidation Temp. (°C)	kg (g ² cm ⁻⁴ s ⁻¹)	kp (cm ² s ⁻¹)
Sample 3 (430)	850	3.6*10 ⁻¹²	1.3*10 ⁻¹³
Sample 2 (coated)	850	1.1*10 ⁻¹³	4.1*10 ⁻¹⁵

*the density of Cr₂O₃ is 5.21 g/cm³

Summary of FeCr corrosion studies

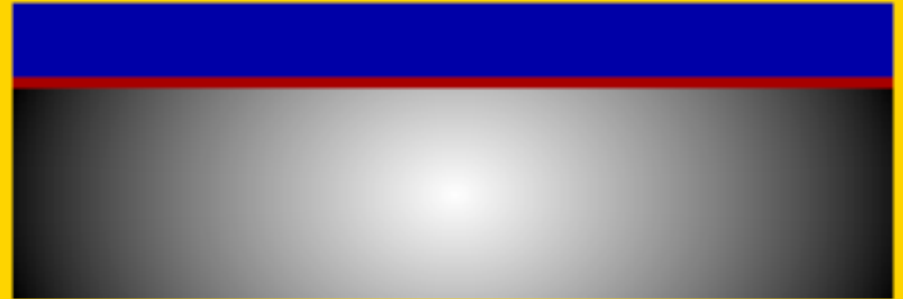
- At 850 °C, untreated 430 stainless steel exhibited spallation of scale after repeated thermal cycles
- At 850 °C, MnCo_2O_4 coated 430 SS exhibited 10x lower oxidation rate & 10x higher σ
 - Scale growth rate constant, $K_p = (\text{weight gain g/cm}^2)^2/\text{sec}$, should be $<10^{-14} \text{ g}^2/\text{cm}^4\text{s}$ and preferably $\sim 10^{-15} \text{ g}^2/\text{cm}^4\text{s}$ -
Ferritic steels have scale growth rates that are acceptable for SOFC application ($<10^{-14} \text{ g}^2/\text{cm}^4\text{s}$) at temperatures $\leq 700^\circ\text{C}$
- Cr volatilization rate has not yet been determined, but should be kept below threshold for cathode poisoning and below EPA limits (0.015 mg/m^3)

Cr Volatilization Studies



Oxidation of 430 SS

H₂O



Oxidation of coated SS

**Volatilization of Cr must be determined by
transpiration measurements**

Long Term Performance of Co-infiltrated Thin-Film SOFCs

Cell Configuration

Cathode

$\text{La}_{0.85}\text{Sr}_{0.15}\text{MnO}_3$

$(\text{Sc}_2\text{O}_3)_{0.1}(\text{Y}_2\text{O}_3)_{0.01}(\text{ZrO}_2)_{0.89}$
(10Sc1YSZ)

Post doped with $2\text{mg}/\text{cm}^2$ Co-nitrate

Electrolyte

10Sc1YSZ

Anode

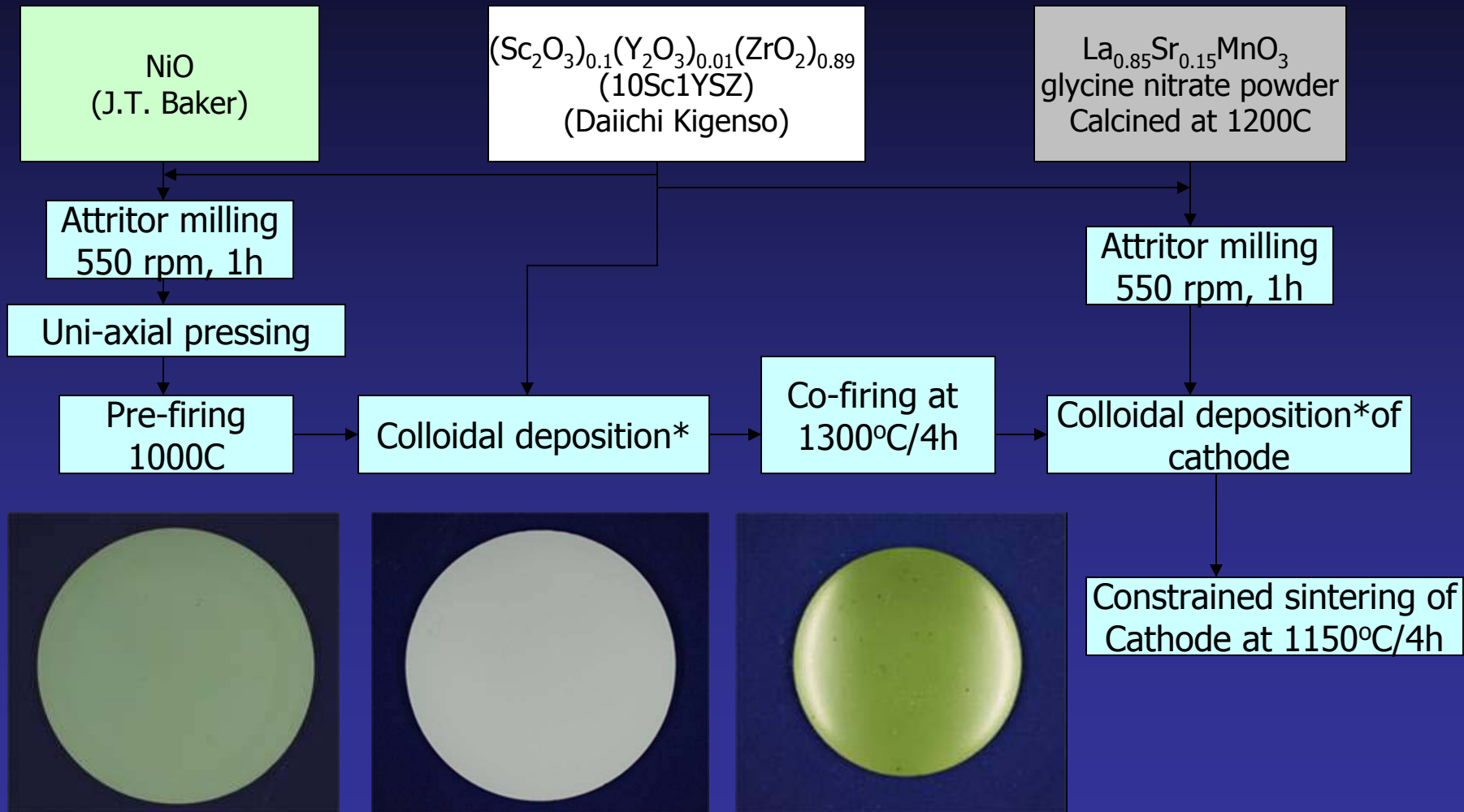
NiO

10Sc1YSZ

Motivation for Co Infiltration

- Longterm operation of SOFCs having stainless steel components will likely be operated at < 700 °C
- Performance of standard LSM electrode is poor below 700 °C
- Infiltration of appropriate catalysts (Co) into the air electrode can significantly boost performance
- Longterm stability of infiltrated electrodes is not yet known

Cell Fabrication



*S.J. Visco, C.P. Jacobson and L.C. De Jonghe, U.S. Pat. No. 6458170, October 1 (2002)

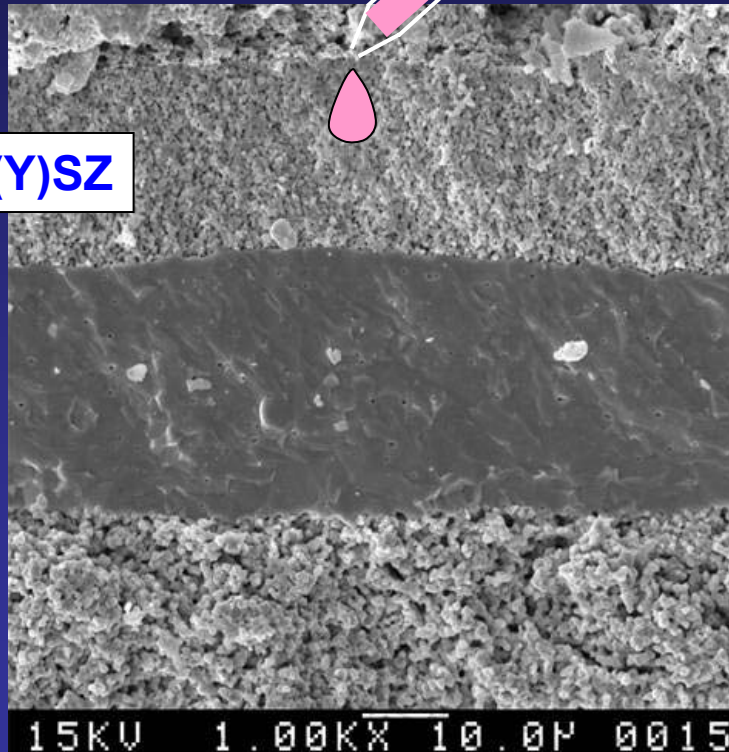
Reduction of Electrode Overpotential

Post-firing cobalt
doping of cathode

$\text{La}_{.85}\text{Sr}_{.15}\text{MnO}_3$ -10Sc(Y)SZ

10Sc(Y)SZ

Ni-10Sc(Y)SZ

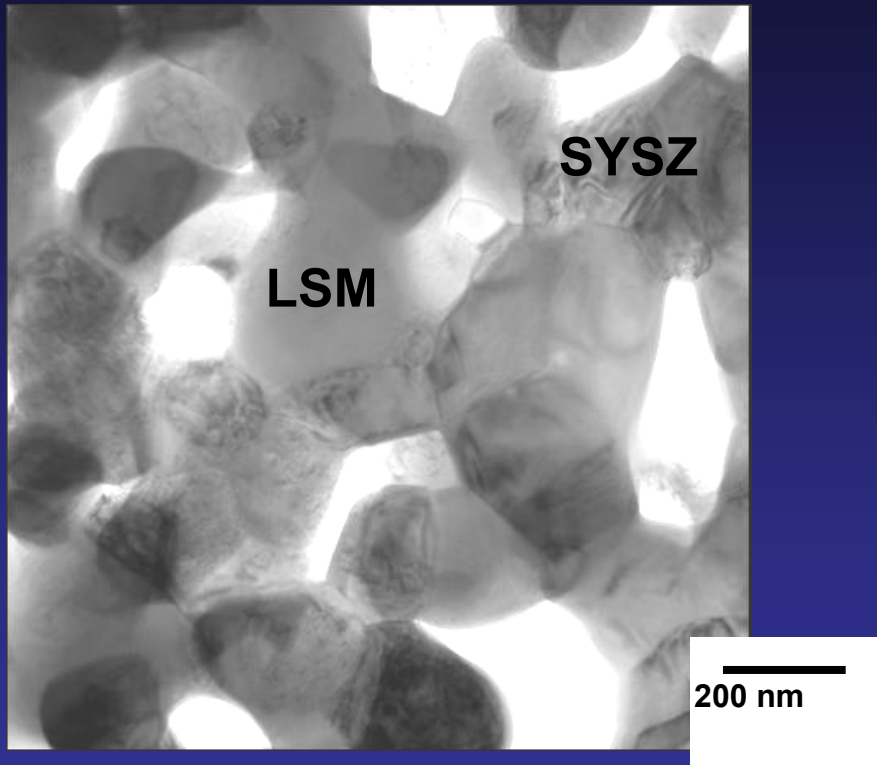


2mg/cm² cobalt
nitrate

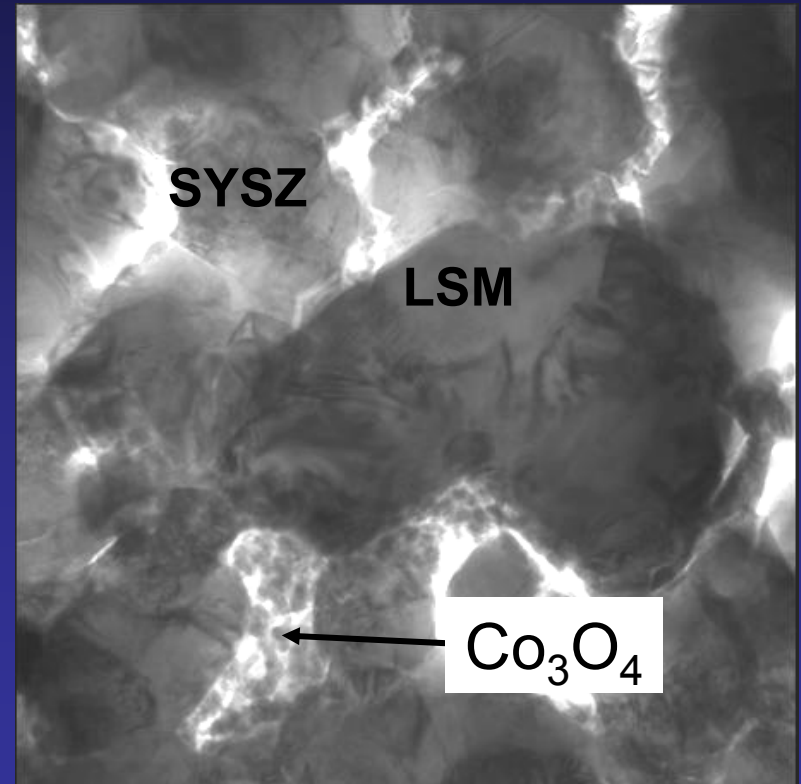
Cross-section micrograph of an
anode supported 10Sc1YSZ cell

Nano Cobalt Oxide

Co-nitrate infiltration into LSM-SYSZ

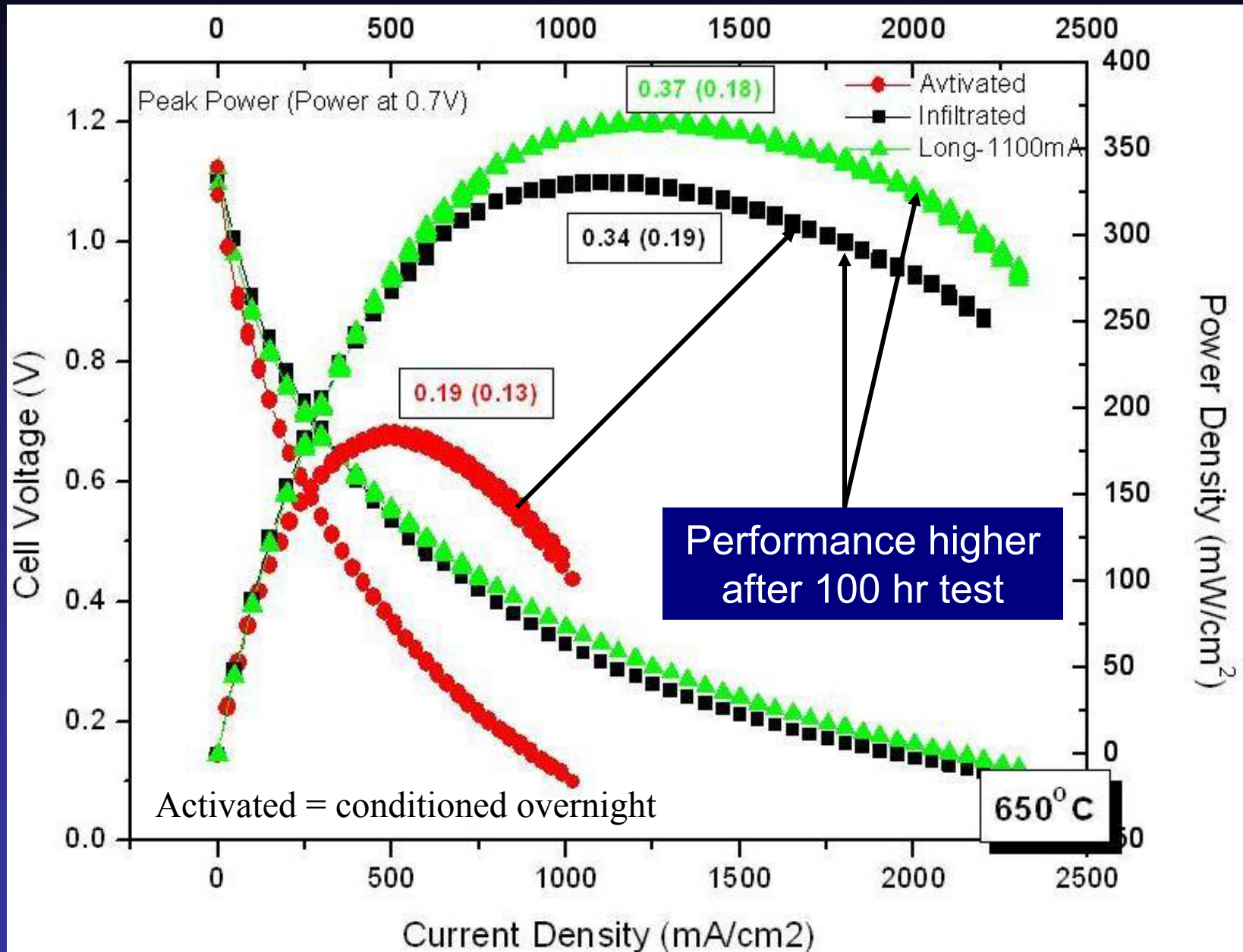


TEM image

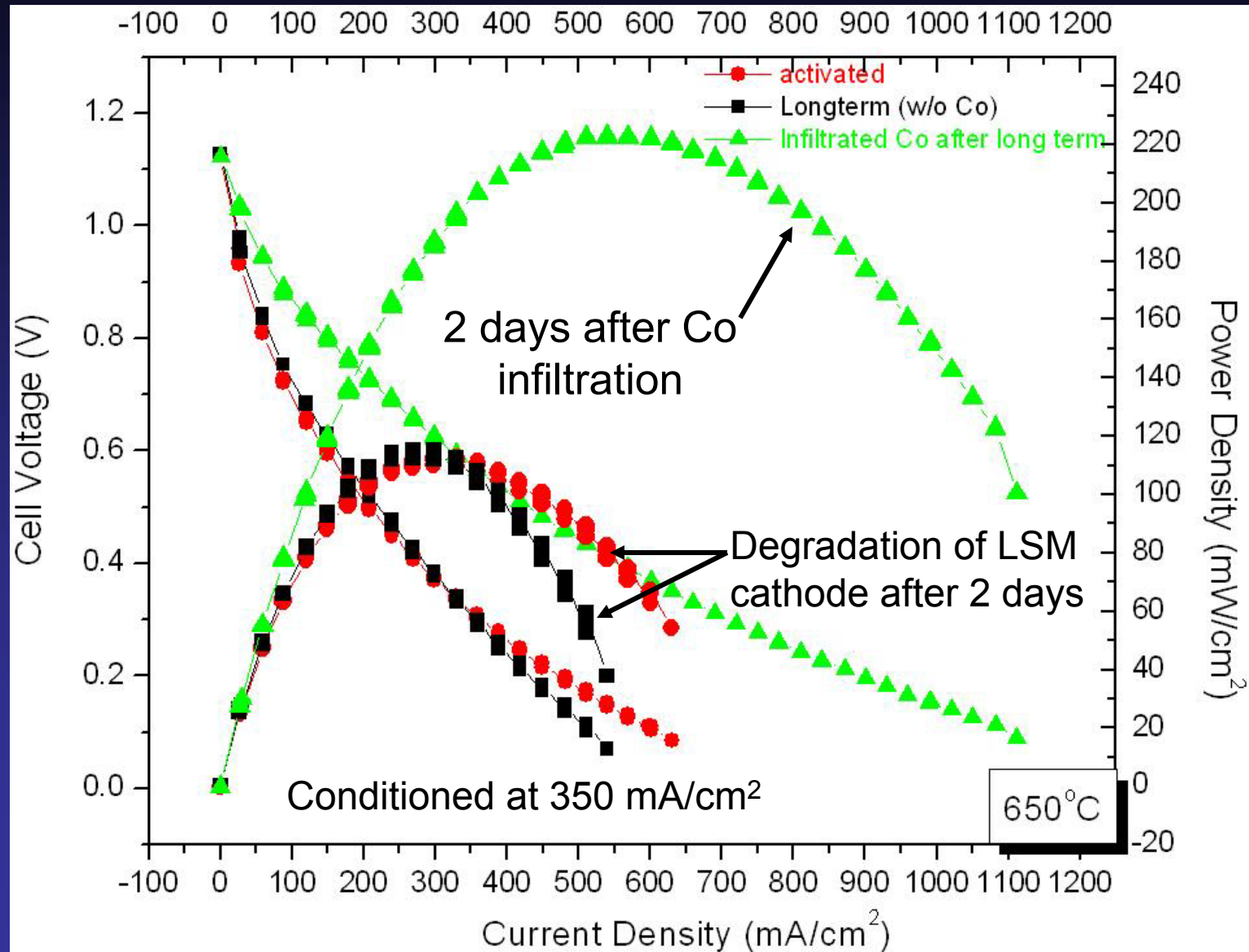


TEM image

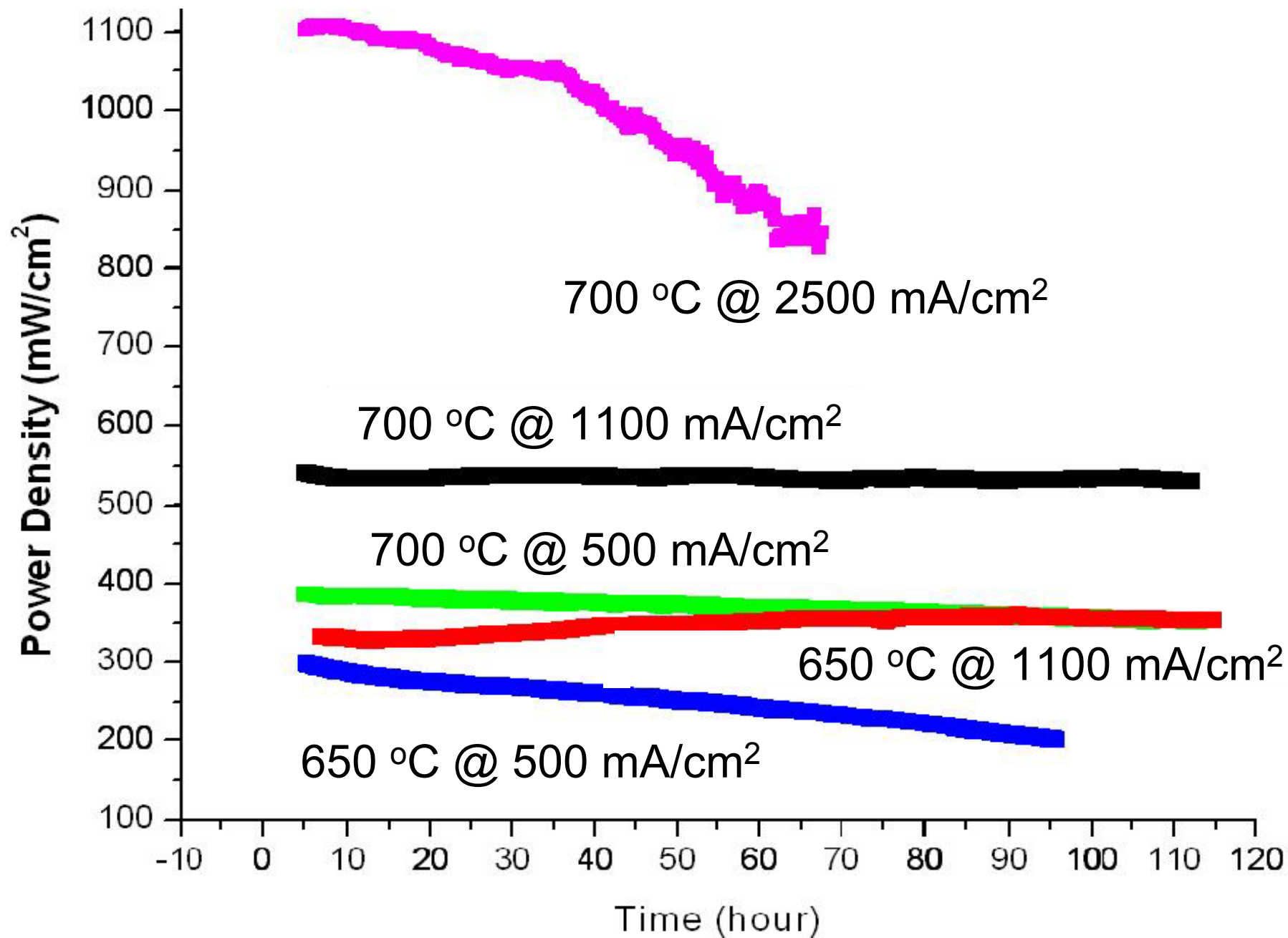
Cobalt infiltration boosts performance



Repair of Cathode After Degradation



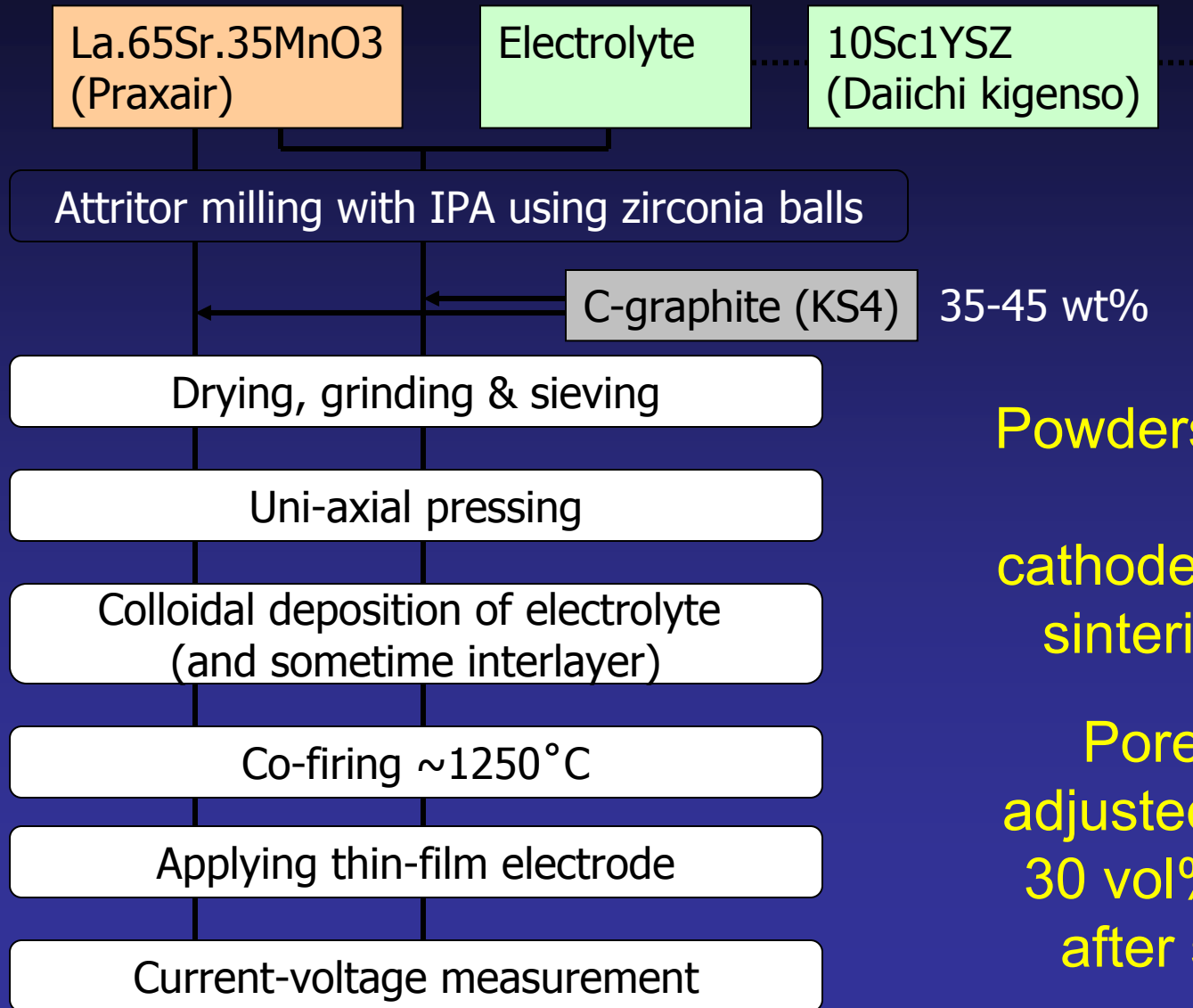
Stability of Co Infiltrated Cathodes as a fcn of i and Temp.



Motivation/Issues for Cathode Supported Cell

- Alternative anodes, such as SrTiO_3 , Cu-CeO_2 , LaCrO_3 , etc., can react or be incompatible with firing conditions for anode supported cells
- Control of porosity in cathode supported cells is more difficult than anode supported cells
- There is a potential for reaction of cathode with electrolyte if firing temperature is too high
- Cobalt infiltration into cathode dramatically improves cell performance

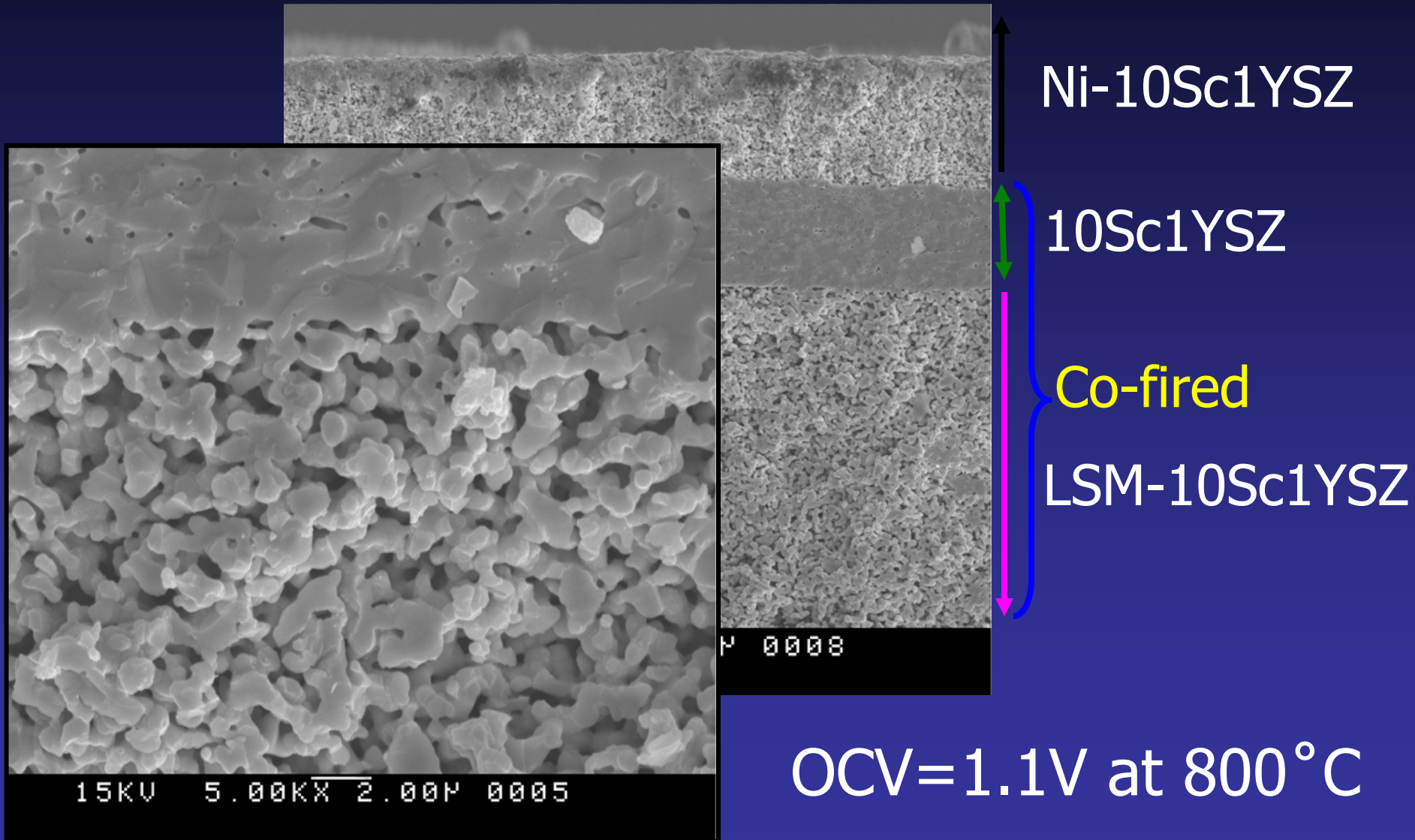
Fabrication of Cathode Supported Cells



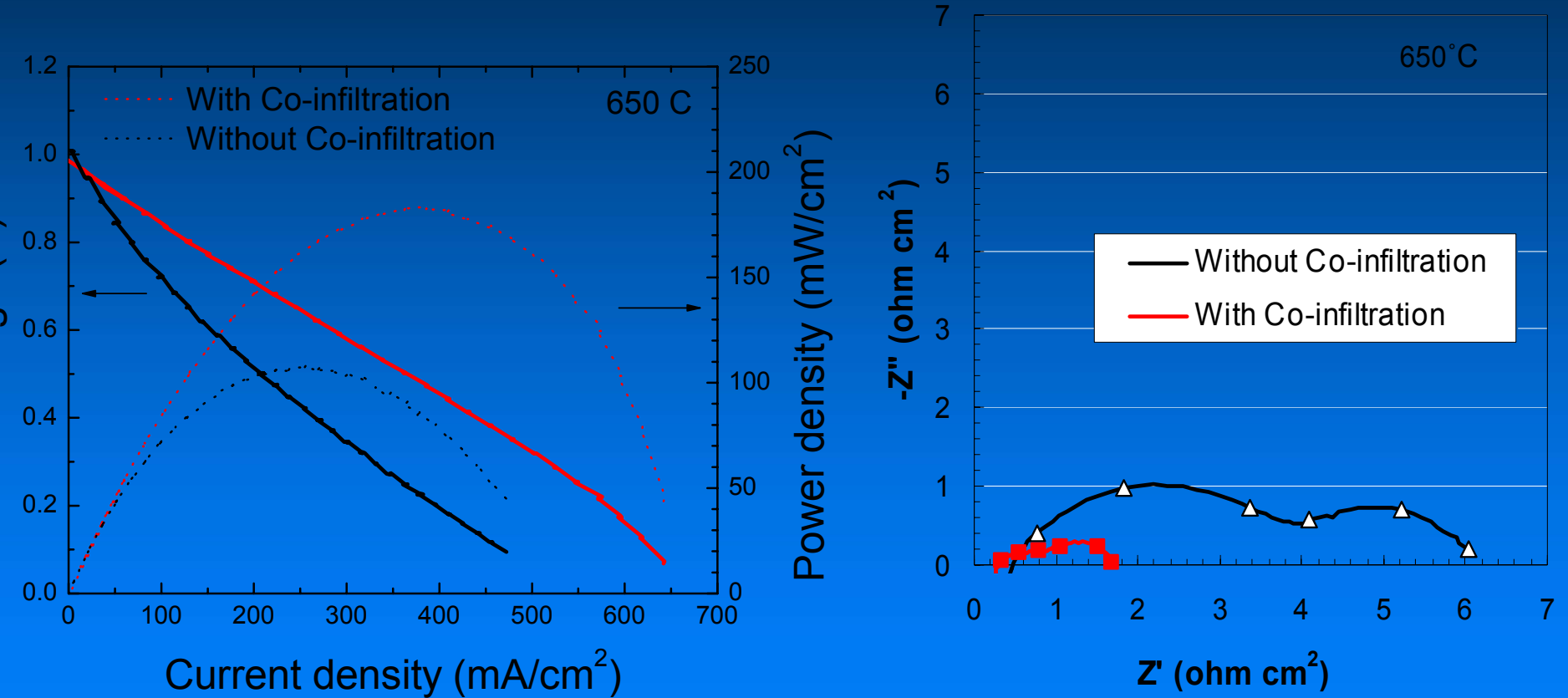
Powders optimized
for
cathode/electrolyte
sintering match

Pore former
adjusted to yield >
30 vol% porosity
after sintering

Co-Firing Bi-Layers at 1250°C

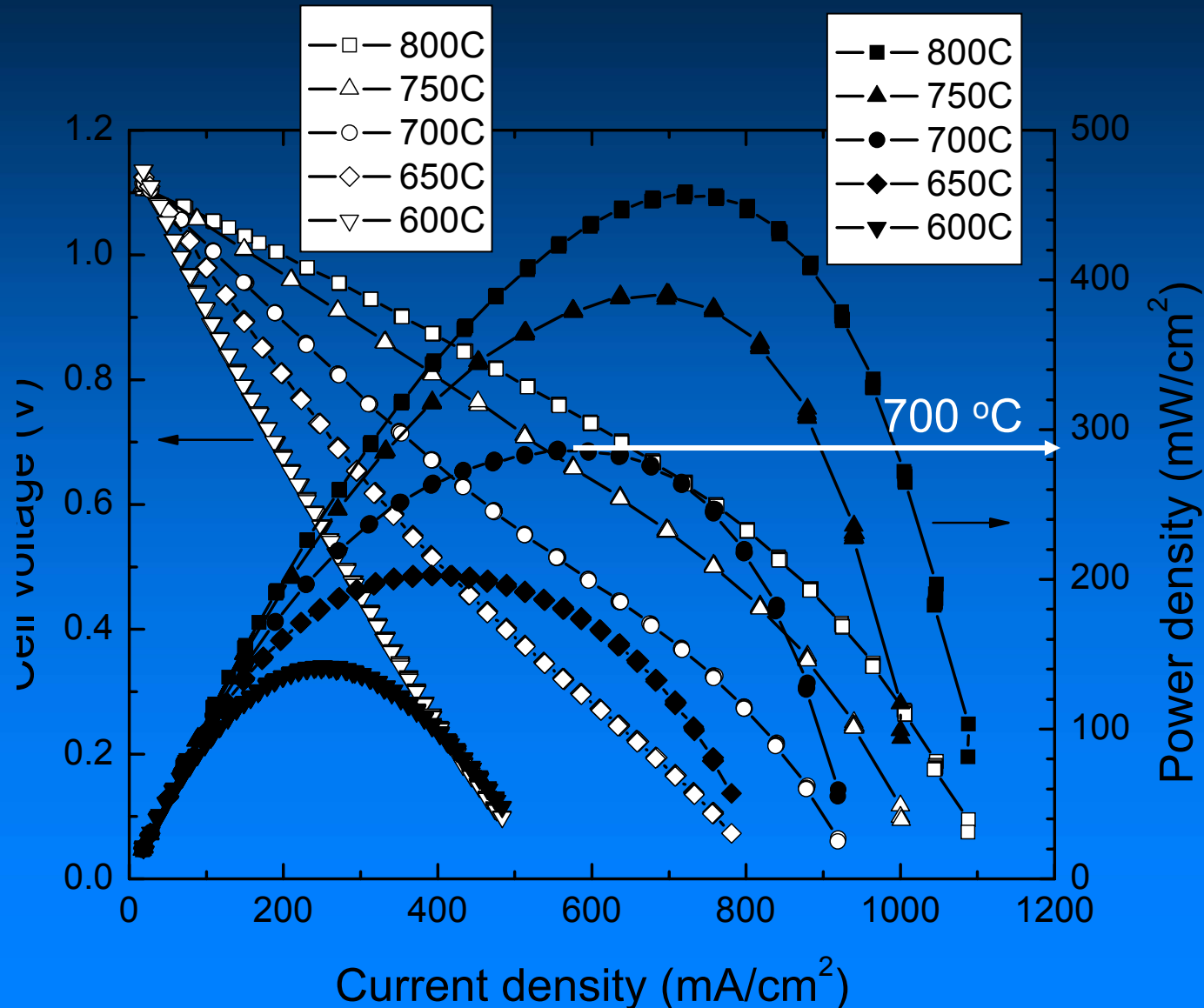


Effects of Cobalt Infiltration into the LSM-SYSZ Cathode



Dramatic improvement due to a reduction in non-ohmic resistance

Performance of Co Infiltrated Cathode Supported Cells



Alternative Anode Evaluation



Electrolyte supported cell w/ref

Define optimum firing conditions for alternative anode; determine anode overpotential



Cathode supported cell tests follow



Metal supported SOFC



Infiltrate anode & cathode

Summary

- Durability and performance of steel components should be excellent at temperatures below 700 °C
 - Growth rate constant, $K_p = (\text{weight gain g/cm}^2)^2/\text{sec}$, should be $<10^{-14} \text{g}^2/\text{cm}^4\text{s}$ and preferably $\sim 10^{-15} \text{g}^2/\text{cm}^4\text{s}$
- Protective coatings increase SS durability and improve resistivity
 - Cr volatilization may be reduced - to be determined
- Cathode performance at temperatures below 700 °C is an issue - cobalt infiltration dramatically improves performance
 - Results of 100 hr tests are promising

Summary

- LBNL has successfully developed cathode supported cells with reasonable low temperature performance
 - May enable use of alternative (C,O,S tolerant) anodes
- Alloy coating technology, low temperature cathodes, and alternative anodes can be utilized with innovative metal supported SOFCs

This R&D effort was supported by the US DOE through the NETL-Solid State Energy Conversion Alliance (SECA)