



Small-Scale Engineered High Flexibility Gasifier

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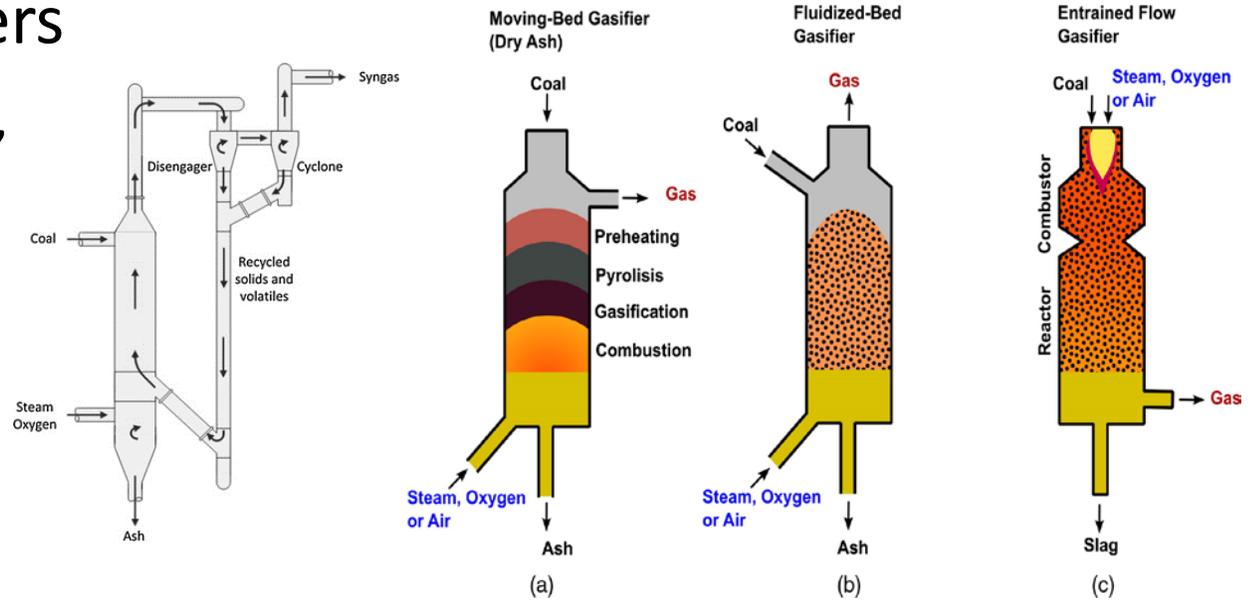
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Project Goals

- Develop a fuel flexible and modular/shop fabricated oxygen-blown small-scale coal gasifier to produce medium BTU syngas with
 - Tar < 10 ppmw
 - Ammonia < 1 ppmv
- Demonstrate gasifier performance to meet target at bench-scale (10-50 lb/h)
- Design a 1-5 MW combined heat and power (CHP) system and conduct a techno-economic evaluation (TEA)

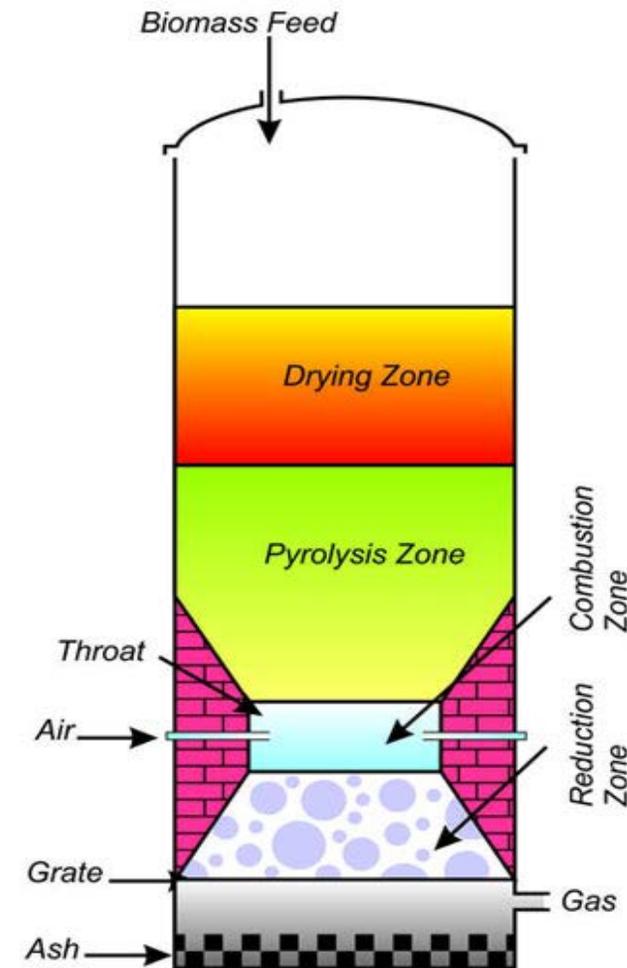
Commercial Coal Gasifiers

- Large scale commercial coal gasifiers
 - Entrained flow (GE/Texaco, E-Gas/CBI, Shell and others)
 - Updraft moving bed (Lurgi)
- Other large scale coal gasifiers
 - Fluidized bed
 - Transport
- Commercial small-scale coal gasifiers do not exist



Small-scale Wood Gasifiers are Commercial

- Downdraft moving bed
 - Many small commercial installations
 - Air blown, sub-atmospheric
 - Used mainly for producing heat
 - Very few successful power applications, mostly 40 KWe or smaller
- Reduced tar formation
 - Volatiles pass through a combustion zone
 - Tar make is typically reduced to 100 ppmw
 - Ammonia typically not reported



Downdraft Design Chosen for Project

- Develop oxygen-blown pressurized coal gasifier suitable for small scale distributed applications
 - Modular, standardized factory construction
- Construct computational model to optimize design
- Optimally designed to
 - Produce medium BTU syngas
 - Manipulate char make, quality, reactivity
 - Mitigate/reform tars, decompose NH_3
- Design for fuel flexibility – coal, biomass, MSW

Comparison to State of the Art

	State of the Art-commercial	This project
Fuel	Mostly wood	Non-caking coal
Scale	40 KW	Bench-scale; Ultimate goal--1-5 MW
Oxidant	Air	Oxygen
Steam	No	Yes
Pressure	Subatmospheric	3-5 atm
Gasification zone temp	~750-800°C	~950-1100°C
Feed flexibility	Low	High
Product flexibility	Mostly heat, char	Char, Heat, power, fuel, chemicals
Syngas	Low BTU	Medium BTU
Tar	200 ppmw	10 ppmw
Ammonia	Not reported	1 ppmv

Project Tasks

- Computational modeling to optimize gasifier design
- Laboratory testing to obtain model input parameters
 - Chars produced at relevant gasification conditions
 - Gasification reactivity measurements to develop a kinetic expression
- Design and construct gasifier based on modeling results
- Commission & test gasifier, demonstrate performance, update computational model
- Design 1-5 MW energy conversion system
- Develop Aspen-based model for integrated 1-5 MW energy conversion system, conduct TEA

Combination of High T and Char Catalysis are Keys

- Maintain 1000-1050°C + for sufficient depth in gasification zone to fully reform tar and decompose ammonia. Is this possible?
- Based on literature Information
 - It can be concluded that essentially complete tar reforming should be achieved over coal chars at ~1000°C within <1 sec [e.g. D.Fuentes-Cano et al., Chem Engg. J, 228 (2013) 1223]
 - Results from **multi-stage multi-vessel** biomass gasifier (pyrolysis-partial oxidation-char gasification) indicate that tar can be reduced to <15 ppmw [e.g. P.Brandt et al., Energy Fuels 2000, 14, 816]
- Our mass/energy balance and modeling efforts indicate that it is possible to maintain the required temperature in the gasification zone of our **simpler, single vessel** downdraft gasifier with proper management of the heat release from combustion

PRB Coal Selected for Modeling and Testing

Moisture	24.29
C	52.32
H	3.95
N	0.8
S	0.26
Ash	4.99
O by difference	13.39
Total	100

Initial Ash Fusion temperature: 1210°C

Major Ash Components (Wt%)

SiO ₂	30.2
Al ₂ O ₃	15.4
Fe ₂ O ₃	5.9
CaO	24.3
MgO	4.8
SO ₃	13

Mass Balance for Desired Wet Syngas Composition

Input (lb/h)		Output (lb/h)	
Coal	25.00	Syngas	74.75
steam	36.70	Char	1.59
Oxygen	14.65		
Total	76.34		76.34

	vol %**	Wt %
CO2	7.1	16.3
CO	20.2	29.5
H2	18.1	1.9
H2O	54.6	52
N2		0.27
H2S		0.05
Total	100	100
	** N,S free	

$$S/C = 1.47$$

$$O/C = 0.59$$

Gasification Kinetics

- Steam and CO₂ gasification measurements were made on chars produced by pyrolysis under various time and temperature conditions using TGA
- These data were used to develop a best fit rate equation
- Two kinetic equations from recent literature were used:
 - Wang, Y, D. A. Bell “Competition between H₂O and CO₂ during gasification of Powder River Basin coal” Fuel 187 (2017) 94-102.
 - Umemoto, S., Kajitani, S., Hara, S., “Modeling of coal char gasification in coexistence of CO₂ and H₂O considering sharing of active sites,” Fuel 103 (2013) 14-21.
- Best fit parameters were determined by non-linear optimization (Matlab)

Kinetic Equations

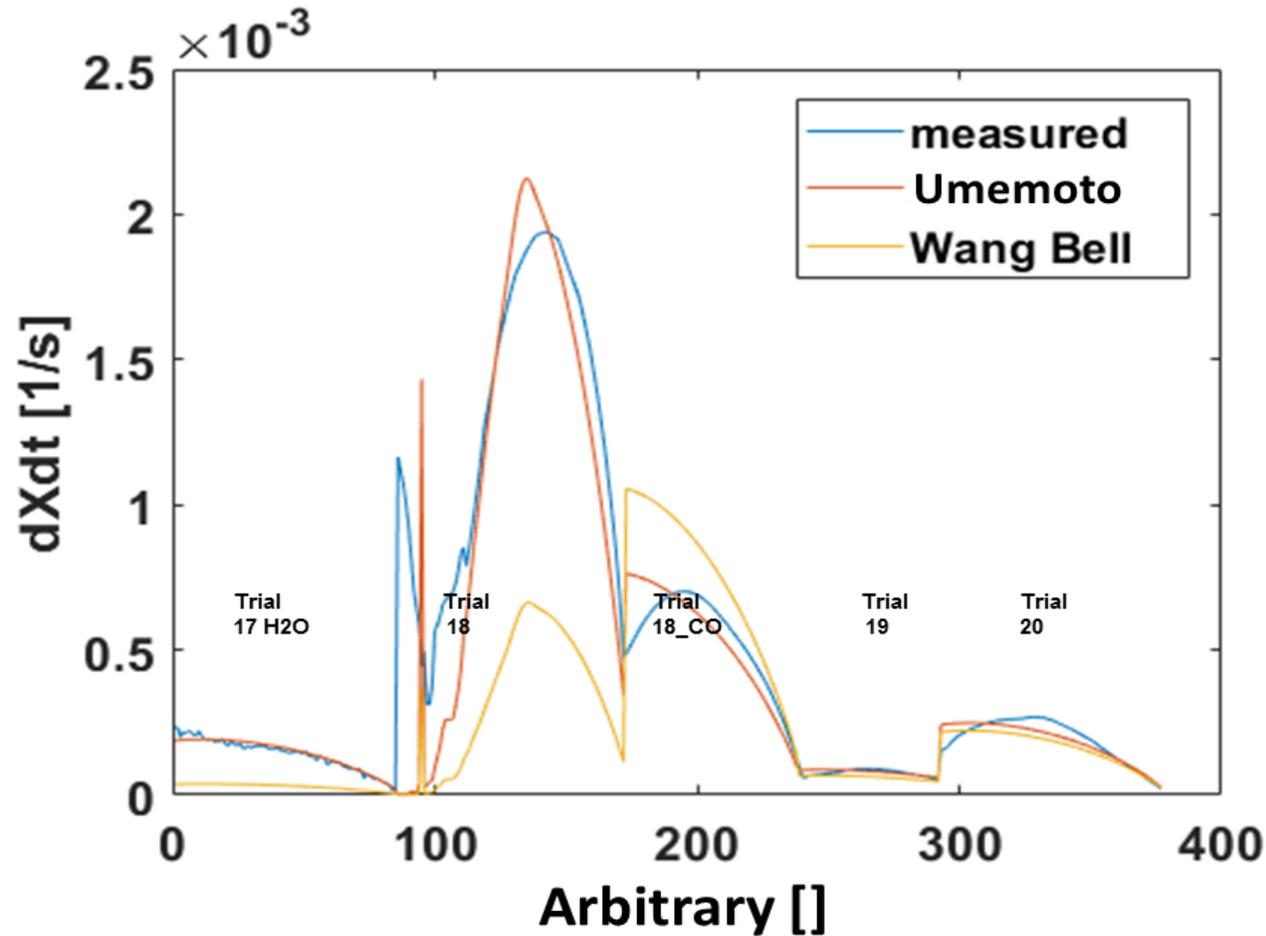
$$\frac{dX}{dt} = \left\{ \frac{K_1 p_{H_2O}}{1 + K_2 p_{H_2O}} + (1 - \theta_{H_2O}) \frac{K_4 p_{CO_2}}{1 + K_4 p_{CO_2}} \right\} (1 - X) \sqrt{1 - \Psi \ln(1 - X)}$$

Wang and Bell
Competing Sites
Model

$$\frac{dX}{dt} = \left\{ \frac{K_{21} p_{H_2O}}{1 + bcK_{12} p_{CO_2} + bcK_{13} p_{CO} + K_{22} p_{H_2O}} + \frac{K_{11} p_{CO_2}}{1 + K_{12} p_{CO_2} + K_{13} p_{CO} + \frac{a}{c} K_{22} p_{H_2O}} \right\} (1 - X) \sqrt{1 - \Psi \ln(1 - X)}$$

Umemoto Shared Active Sites
Model

Umemoto Shared Sites Equation Provided a Better Fit



Optimal kinetic model parameters for Umemoto model

A_{11}	2.65e9
A_{12}	9.451e7
A_{13}	2989
A_{21}	1.001e9
A_{22}	2.681e12
A_{23}	0.1620
E_{11}	231.3
E_{12}	129.70
E_{13}	20.521
E_{21}	206.4
E_{22}	236.6
E_{23}	280.3
a	0.999995
b	4.0645e-05
Ψ_1	4.2980

Figure 1. Kinetics model fits for Umemoto and Wang Bell for 5 trials data sets

REI Modeling Effort

- Based on prior work REI employed a two-stage approach to modeling the SR modular gasifier
 - **Stage 1** adapted an existing, one-dimensional, zonal model. The purpose of the zonal model was to help establish process parameters, rather than details of the micro processes and mixing within each zone (addressed in Stage 2).
 - **Stage 2** used a porous-media CFD approach to explore multi-dimensional mixing of injected oxygen & steam into the porous bed
- 15 cases involving variations in amounts and positions of steam and oxygen injection were investigated. Gasifier exit results are presented for cases 8 and 9. Modeling effort is complete. Models will be adjusted by REI for scale up based on bench-scale gasification results

Exit Conditions from Gasifier Model Results

	Case 8	Case 9
Temperature, °C	456	466
H ₂ , % vol wet	16.66	15.06
CO, % vol wet	20.87	18.12
CO ₂ , % vol wet	6.29	7.16
H ₂ O, % vol wet	55.79	59.40
CH ₄ , % vol wet	0.154	0.052
Gas Mass Flow, kg/s	0.00885	0.00974
Density, kg/m ³	0.957	0.954
Volume Flow, actual m ³ /s	0.009247	0.01021
Char Mass Flow, kg/s	5.99e-5	4.55e-5
Carbon Content, %	42.2	32.0

Work in Progress

- Based on the kinetic studies and modeling efforts, a design of the 25 lb/h modular gasifier has been carried out. The design is highly flexible to achieve the desired syngas composition, guided by the model.
- Discussions were initiated with experts at Unitel and TR Miles, inc, and CUNY for assistance with critical components, in particular, for gasifier start up, selection of coal feeder, char withdrawal, materials of construction, temperature measurements within gasifier. Balance of plant components have been determined, they are fairly straight forward and will be obtained from commercial vendors
- Gasifier construction task is about 4 months behind because of move of our laboratory from RTP to Birmingham, Alabama. A site has now been established at the new location.
- Aspen simulations and preliminary TEA efforts have been carried out. TEA indicates reduced cost due to standard factory components. Potential sale of char byproduct can make small distributed systems economical

Conclusions and Future Work

- Modeling efforts and flexible input capability for oxygen and steam have confirmed the ability to manipulate temperature distribution within gasifier and achieve the desired syngas composition, char composition, tar, and ammonia levels.
- Gasifier design and construction will be completed and testing should begin in late 2019.

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Thanks for Listening! Questions?



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