

# Pilot-Scale Silicone Process for Low-Cost CO<sub>2</sub> Capture

**GE Global Research**



**GE Global  
Research**

**DOE Award: DE-FE0026498**



**Final Report  
Dan Hancu  
October 26, 2017**

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# Agenda

- **Program Overview..** Feasibility study for 10 MW<sub>e</sub> demo
- **GE Aminosilicone..** Water lean CO<sub>2</sub> Capture Solvent
- **Solvent Manufacturing..** Wacker qualified
- **Host Evaluation..** Criteria to run water-lean solvent
- **Techno-economic Analysis..** 20 % Cost-out vs. MEA
- **Technology GAP Analysis..** Solvent management & Gen 2 Solvent



# Overview

## Large Scale Pilot Test of Aminosilicone Solvent for CO<sub>2</sub> Capture: Phase 1

### Technology Demonstration Planning

*Project Objective: Develop project definition and preliminary design for 10+MWe pilot scale testing of the Aminosilicone CO<sub>2</sub> capture solvent technology.*

2008–2010  
Lab



Design and  
Optimize Process

2010–2013  
Bench Scale



Establish Scalability  
and Commercial Value

2014–2015  
Small Pilot



0.5 MWe  
Demonstration

2015–  
Large Pilot  
10 MWe  
Demonstration



### Technical Approach

- Host site evaluation
- Solvent acquisition
- Process model & equipment design
- Environmental health and safety



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# New Solvent System.. Amino-Silicone

## Desired Solvent Properties for cost effective CO<sub>2</sub> capture:

Low/no water

Liquid carbamate salt

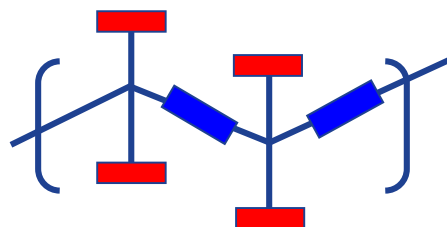
Thermal stability



High CO<sub>2</sub> loading

High desorption pressure

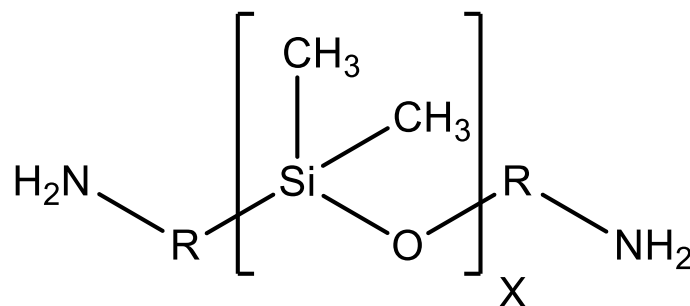
Low volatility

High reaction rates

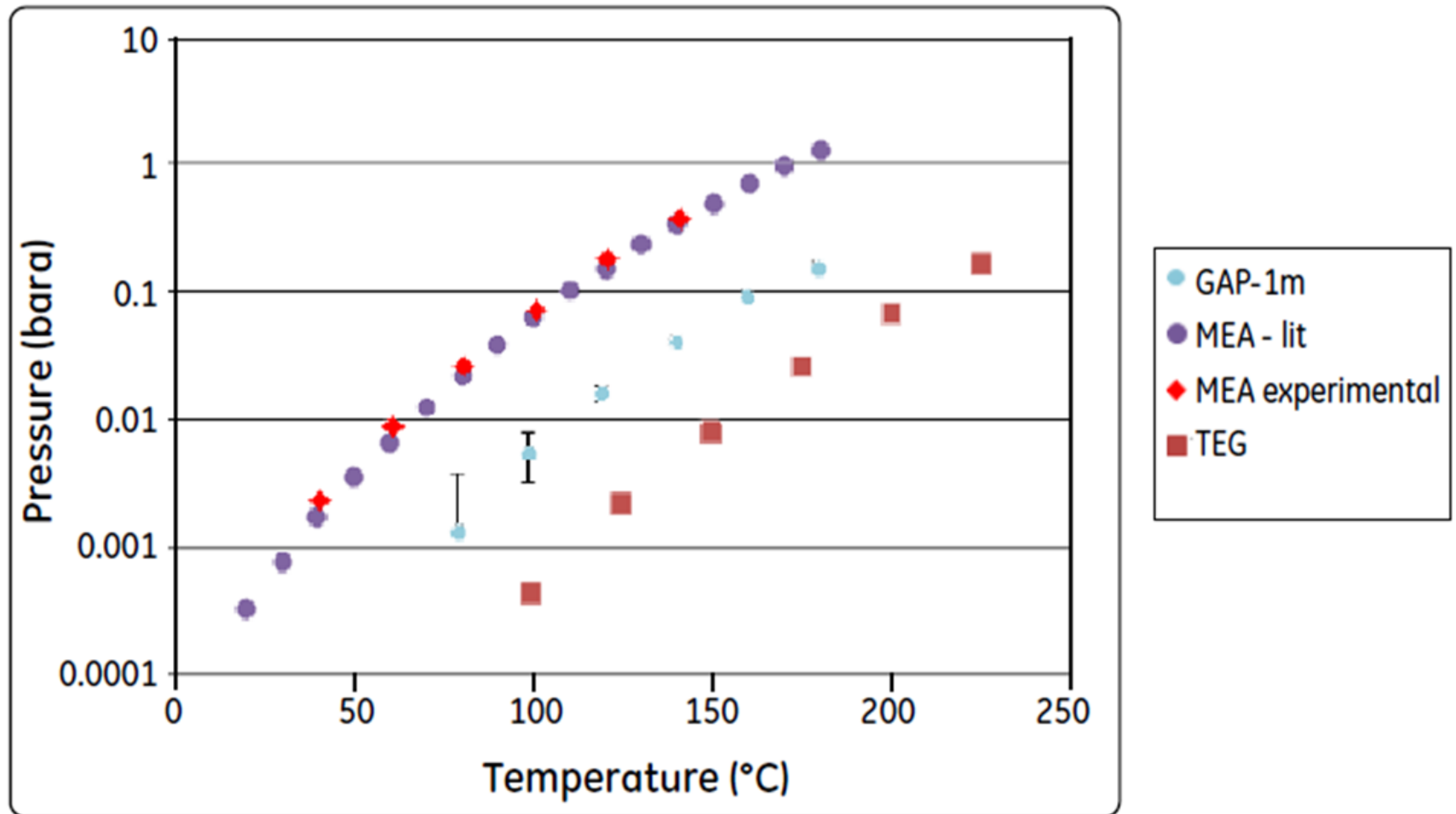


 CO<sub>2</sub>-philic backbone (physi-sorption)  
 CO<sub>2</sub>-reactive group (chemi-sorption)

## Aminosiloxanes



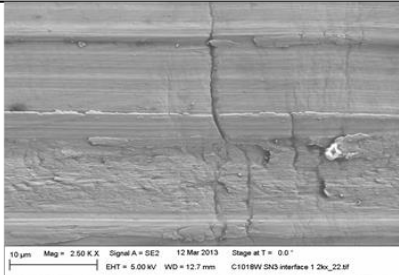
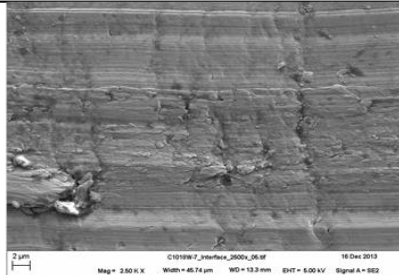
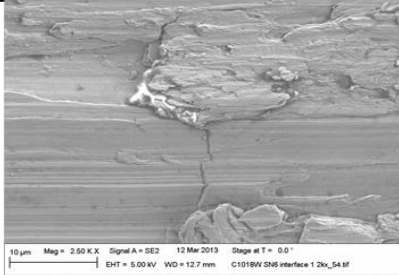
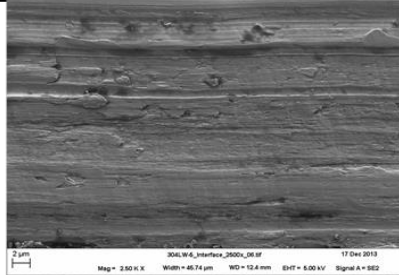
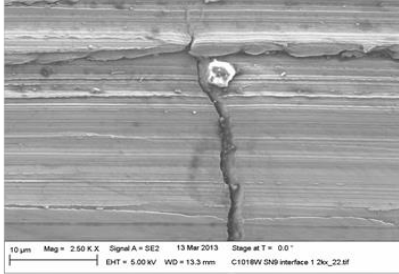
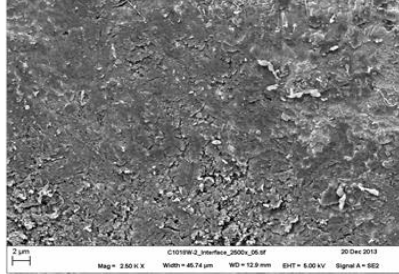
# Amino-Silicone.. Volatility



**Low Volatility..** Simplified Desorption Process  
Reduced Solvent Loss



# Amino-Silicone.. Corrosion

Location / Metal Type	Conditions	Unexposed samples (interface images)	Exposed samples (interface images)
Lean Storage / C1018	~380 hours at ~34 °C and ~6138 hours at ~25 °C		
Absorber Sump / C1018	~389 hours at ~52 °C and ~6138 hours at ~25 °C		
Desorber / C1018	~388 hours at ~145 °C and ~6138 hours at ~25 °C		

Corrosion Rate (µm/yr)

1.27

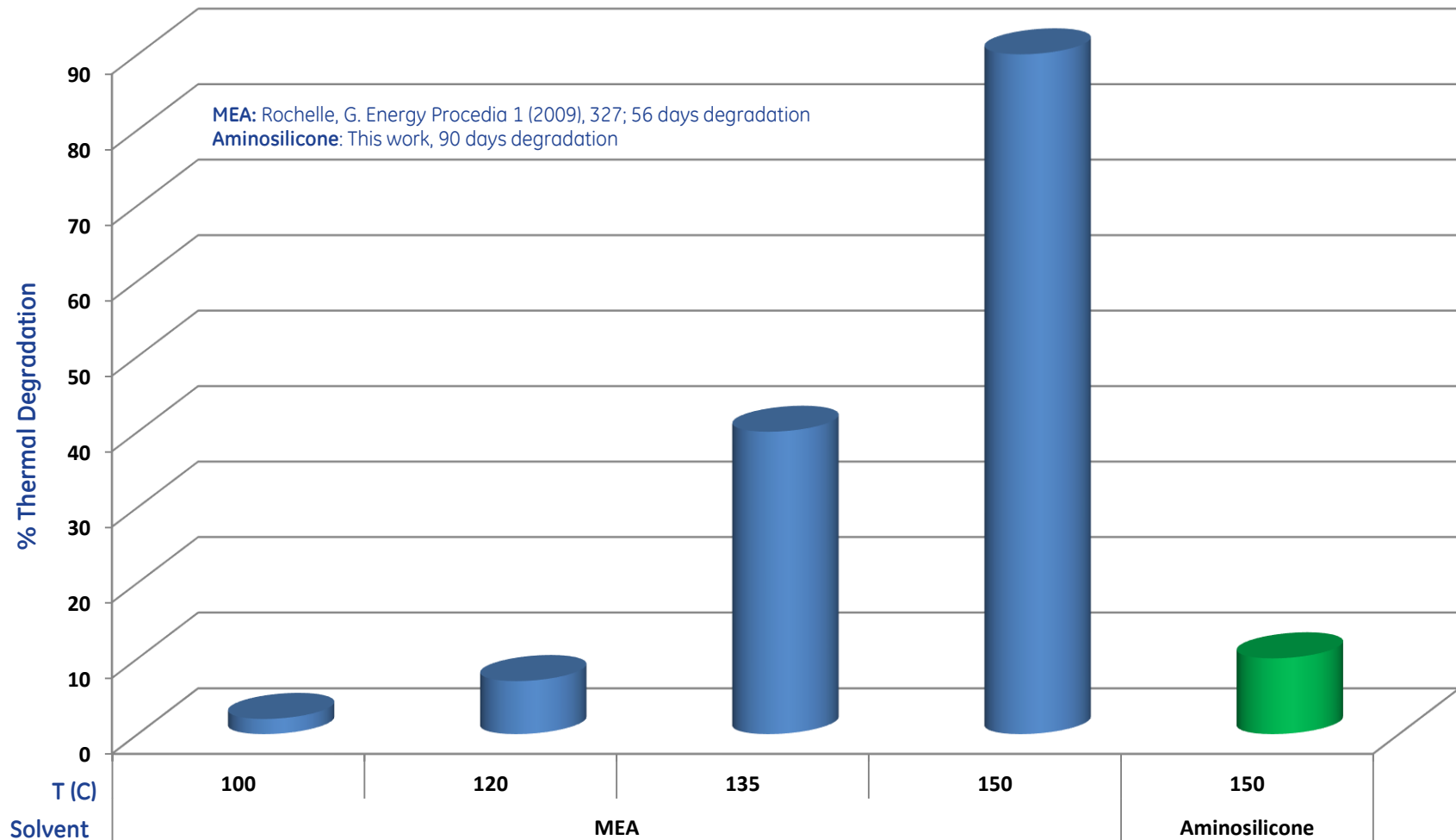
0.47

2188

**Reduced Corrosion.. Corrosion Inhibitor not Required**



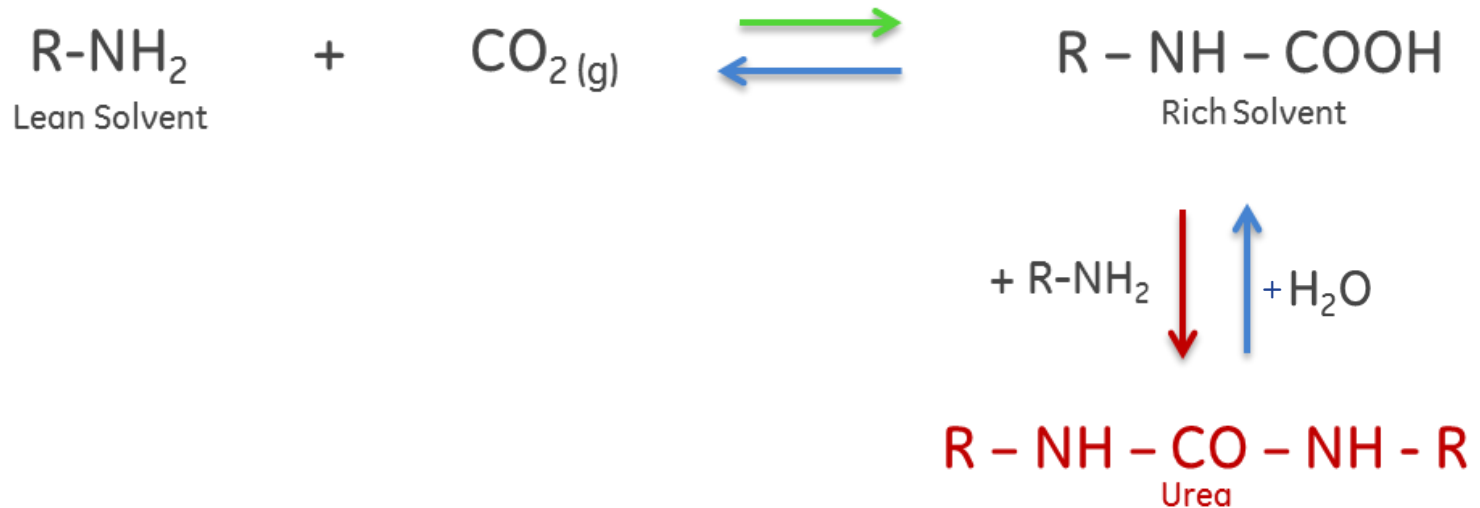
# Amino-Silicone (Lean).. Thermal Stability



Improved thermal stability for **Lean** Solvent..



# Amino-Silicone (Rich).. Thermal Stability



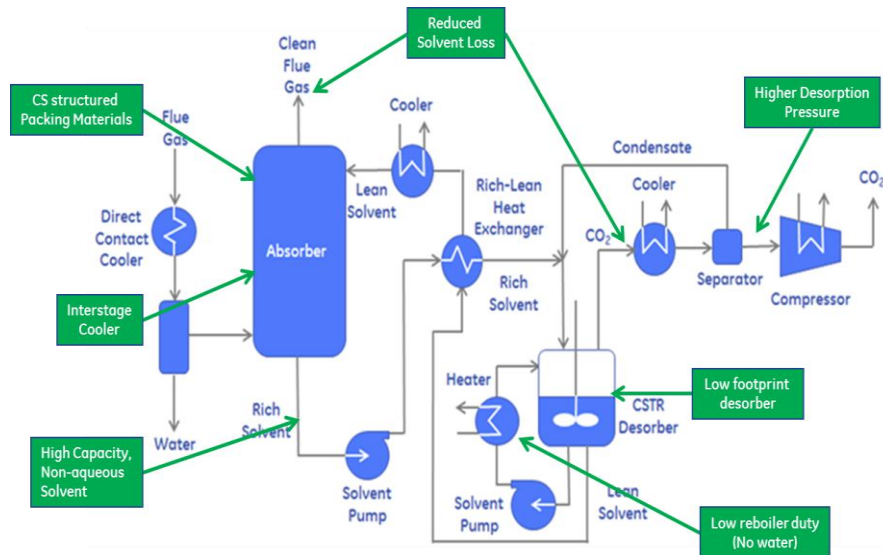
$$\text{Degradation Rate} \sim T \cdot \frac{1}{H_2O} \cdot \text{Rich}$$

Thermal stability for **Rich** Solvent ..  
Lower T & Controlled Water Addition



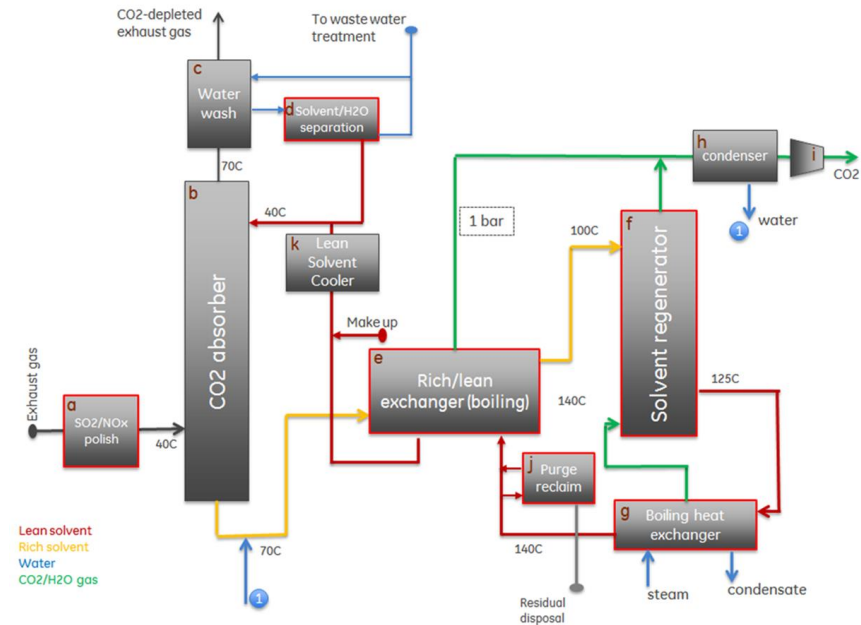
# Desorption Options.. CSTR vs. SSC

## CSTR Desorber



- ✓ Lower CAPEX and footprint
- ✓ Single Stage Desorption
- $H_2O < 5 \text{ wt.}\%$

## Steam Stripper Column (SSC)

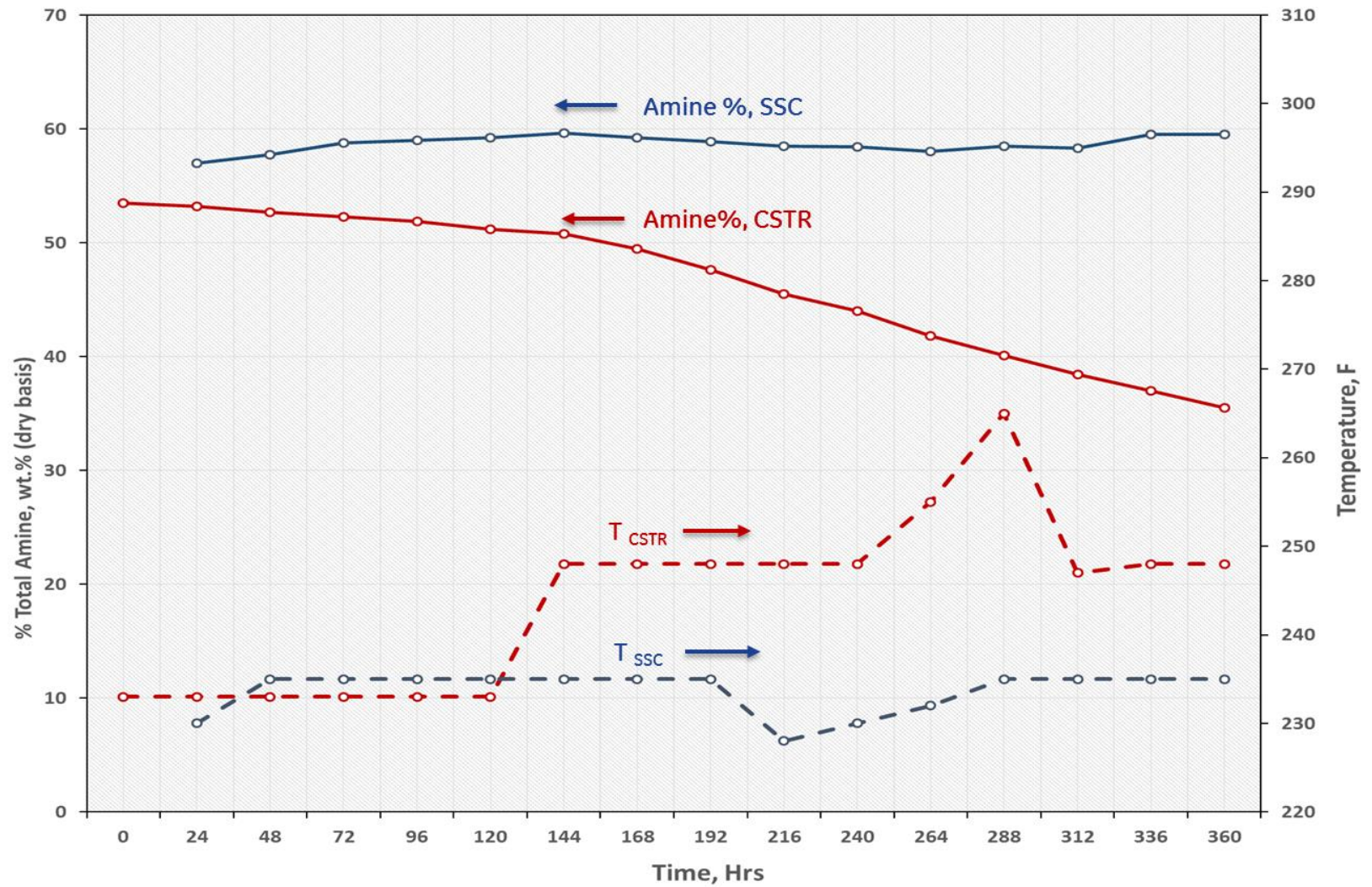


- ✓ Multi-stage desorption
- ✓ Lower desorption temperature



# Amine Degradation.. CSTR vs. Steam Stripping

NCCC (0.5 MW)

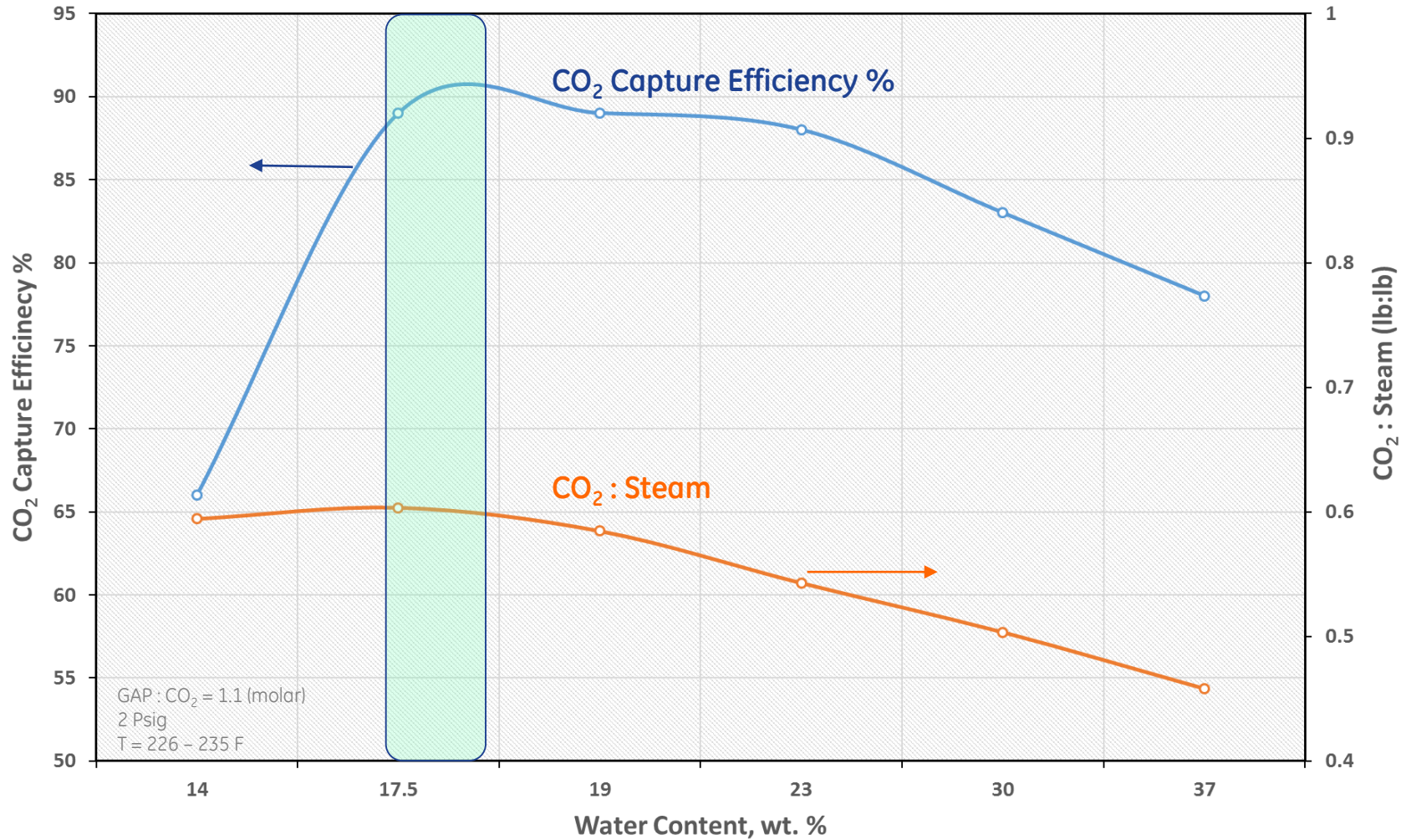


Amine degradation: SSC << CSTR



# 0.5 MW NCCC.. Steam Duty = f (H<sub>2</sub>O)

NCCC (0.5 MW)



Capture Efficiency & CO<sub>2</sub>: Steam optimum at 18 wt. % H<sub>2</sub>O



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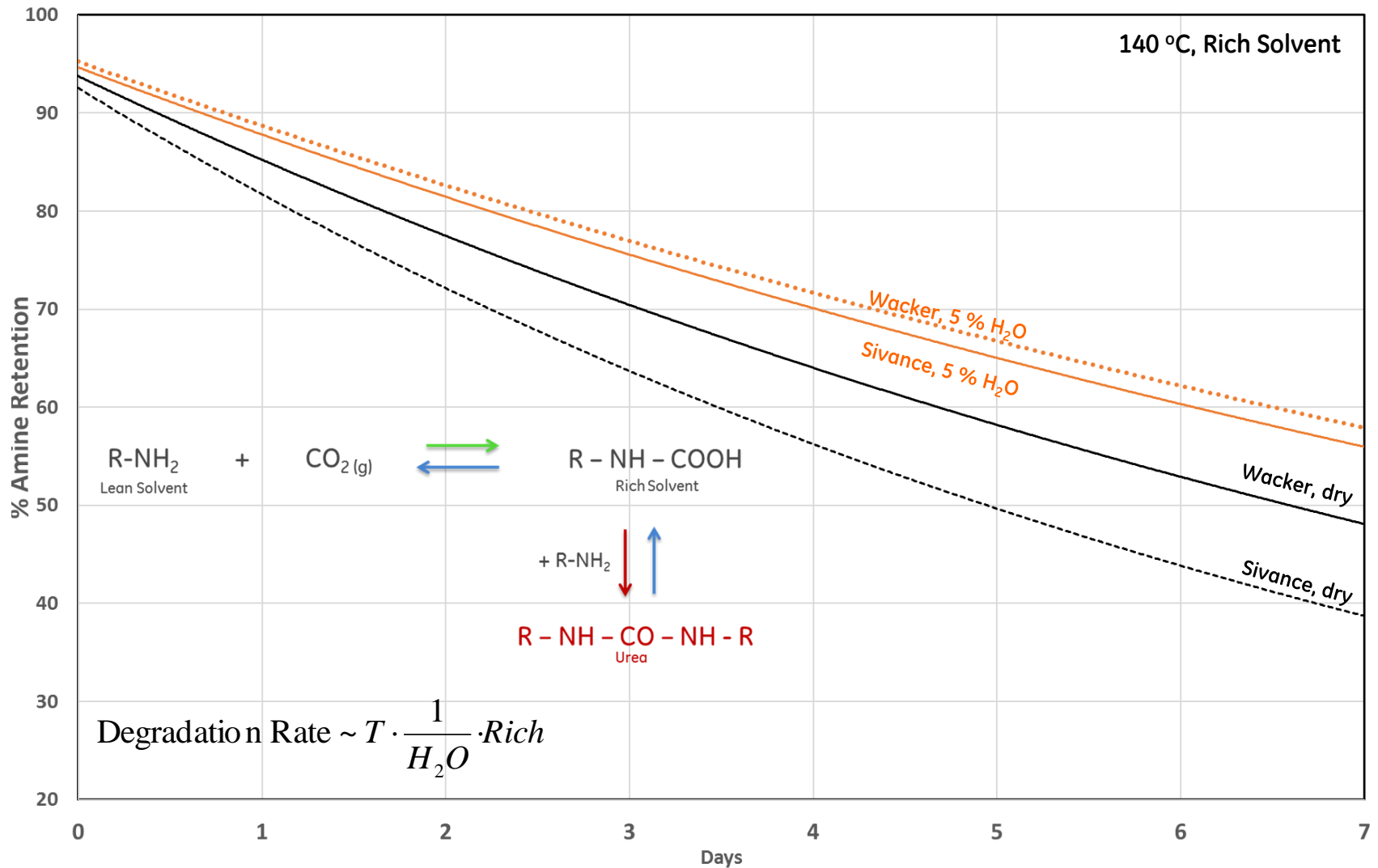
# Solvent Evaluation Protocol.. **Wacker vs. Sivance\***

- **Accelerated Thermal Degradation..** Lab evaluation
- **Oxidation stability..** Lab & 2 KW<sub>e</sub> evaluation
- **CO<sub>2</sub> Capture Efficiency..** 2KW<sub>e</sub> evaluation
- **Hydrothermal stability..** Steam stripper glass column

\*Sivance - Solvent Manufacturer for NCCC

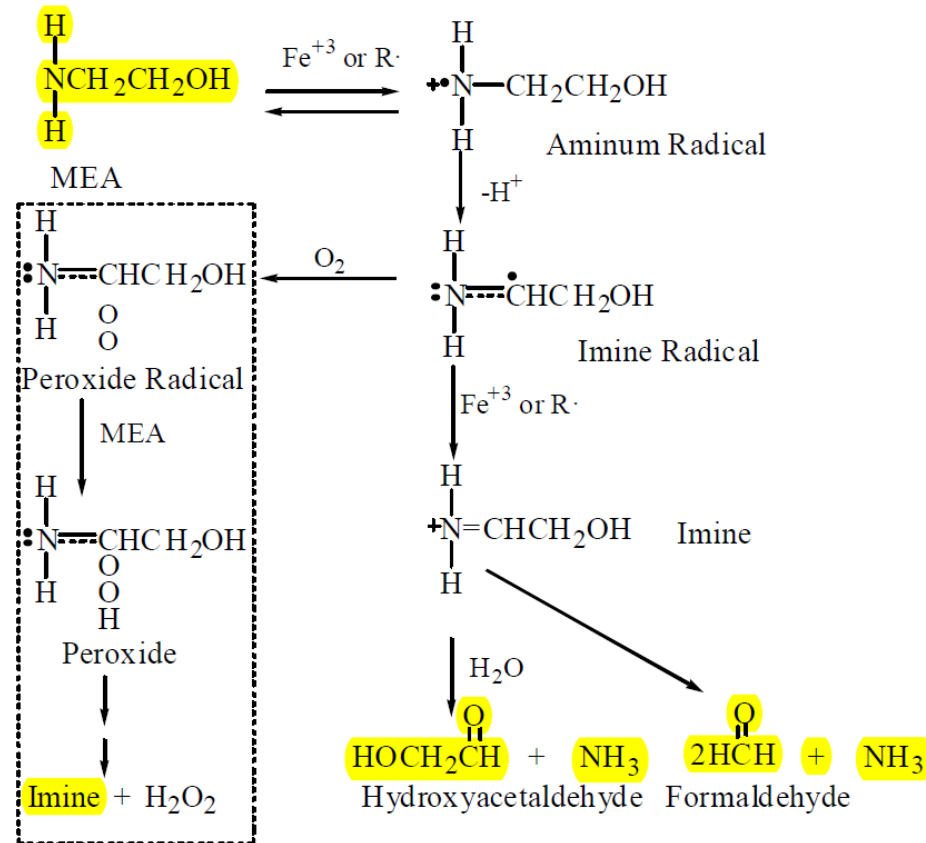


# Thermal Degradation.. Lab evaluation



✓ Accelerated Thermal Degradation: Wacker ~ Sivance

# Oxidation.. Ammonia Generation



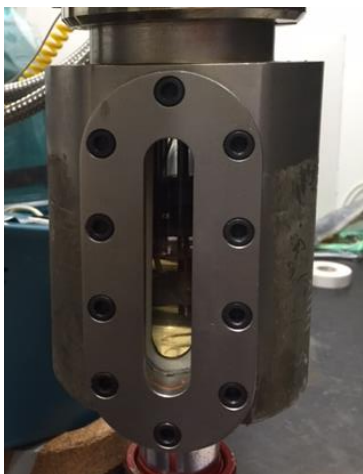
Rochelle, 2010

- Formation of ammonia is a quantifier for thermo-oxidation
- Iron is a catalyst



# Oxidation (lab).. Experimental Set-up

## Parr Reactor

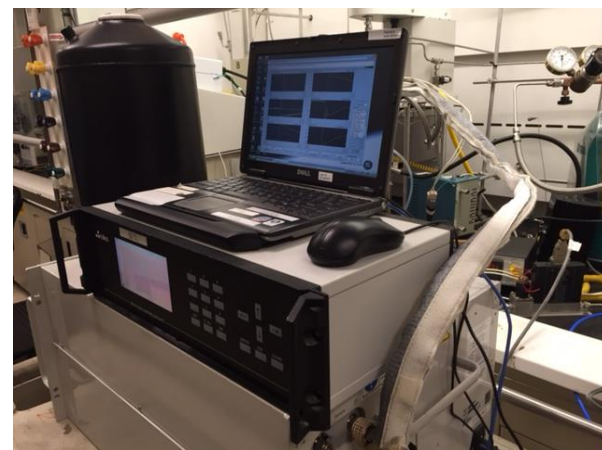


- 400 mL windowed Parr reactor
- Mechanical agitation
- 200 mL 60 wt. % GAP-1 / 40 wt. % TEG
- Gases were bubbled through the GAP-1 / TEG solution via dip-tube
- Temperature controlled via internal coil

## FTIR and Gas Delivery system

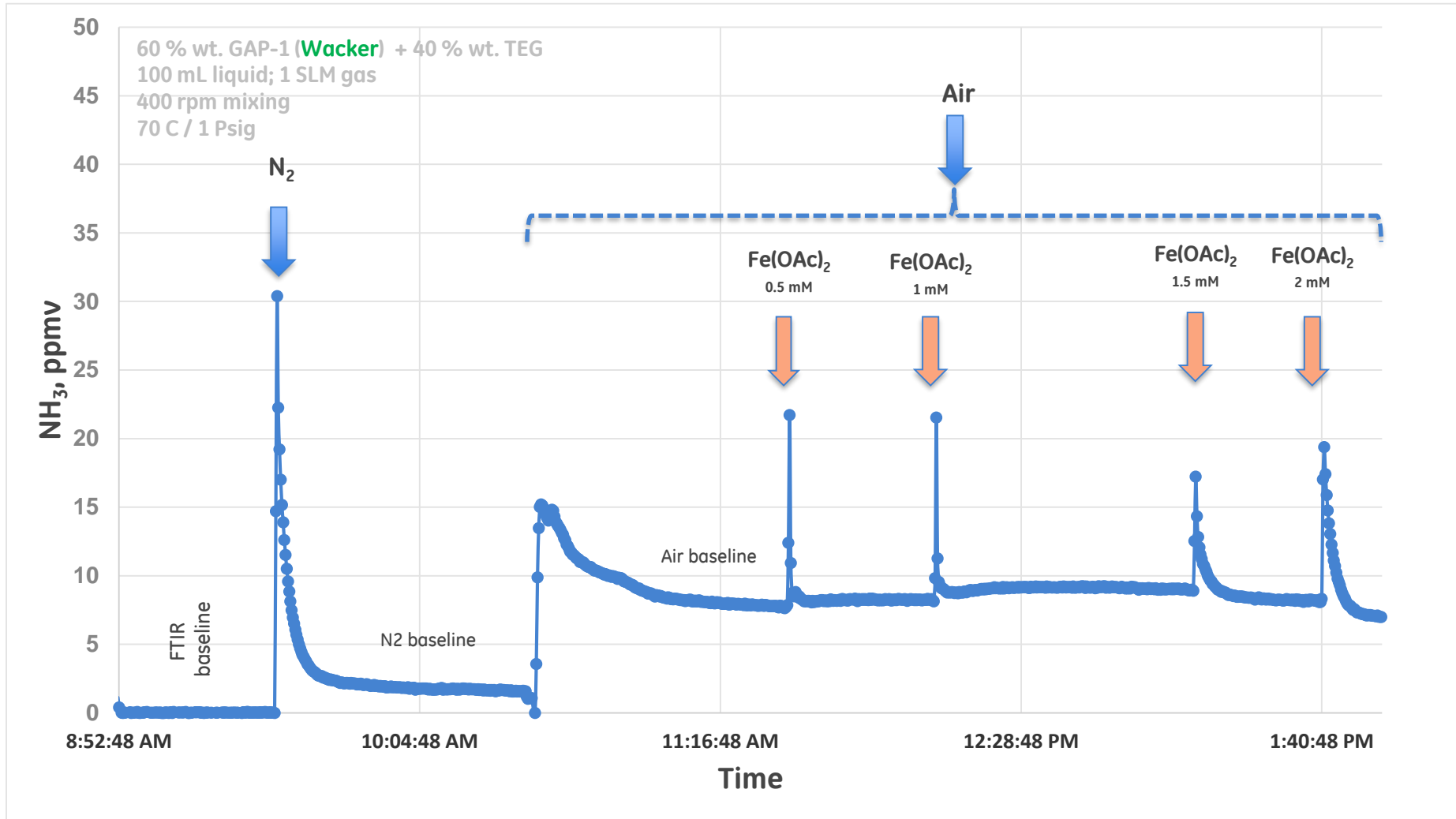


- Heated transfer line at 190 C



- FTIR (MKS): analysis of acetalddehyde, formaldehyde ammonia, propylene
- Gas Delivery System: N2 and air via MKS MFC

# Oxidation (lab).. $\text{Fe}^{2+}$ doping



# Oxidation (lab).. Sivance vs. Wacker

60 % wt. GAP-1 + 40 % wt. TEG  
100 mL liquid; 1 SLM gas  
400 rpm mixing  
70 C / 1 Psig

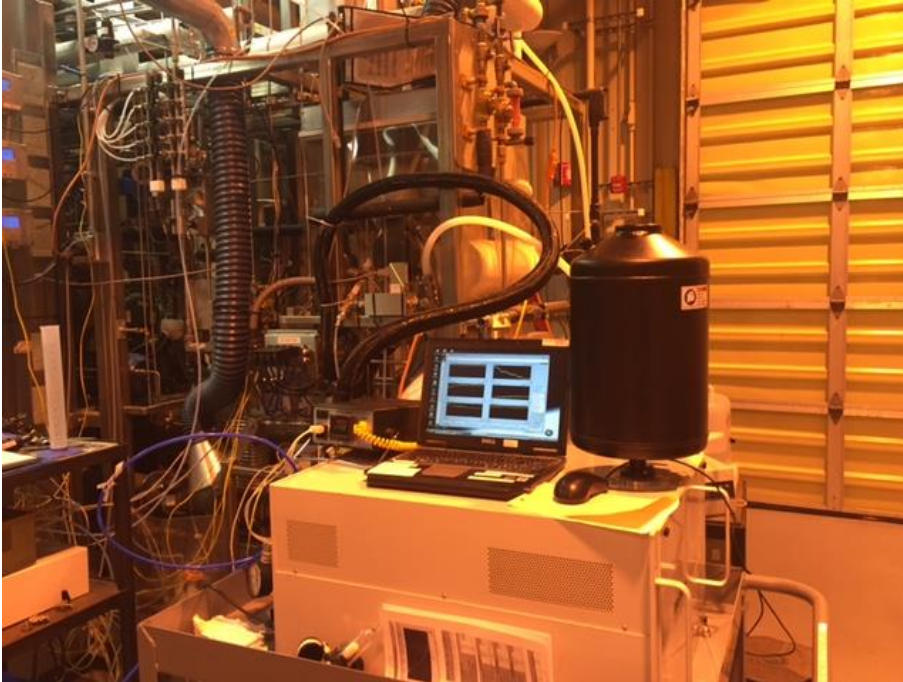
	Sivance			Wacker		
	NH3, ppmv		NH3, mol/min*10 <sup>4</sup>	NH3 ppmv		NH3 mol/min * 10 <sup>4</sup>
	Average	Max	Average	Average	Max	Average
Baseline, FTIR	0	0	0	0	0	0
N2, initial	3	1005	0.1	1	30	0.04
Air	130	212	5.8	8	15	0.4
Air & Fe <sup>2+</sup> (2.5 mM)	140	203	6.2	8	20	0.4

✓ **Rate of oxidation (lab):** Wacker = 1/10 Sivance



# Oxidation (2kW skid).. Experimental Set-up

MKS FTIR installed on the skid



- Analysis: ammonia, acetaldehyde, propylene, formaldehyde

Heated FTIR Line –  
Top of the absorber



- Heated transfer line at 190 C

# Oxidation (2kW Skid).. **Sivance vs. Wacker**

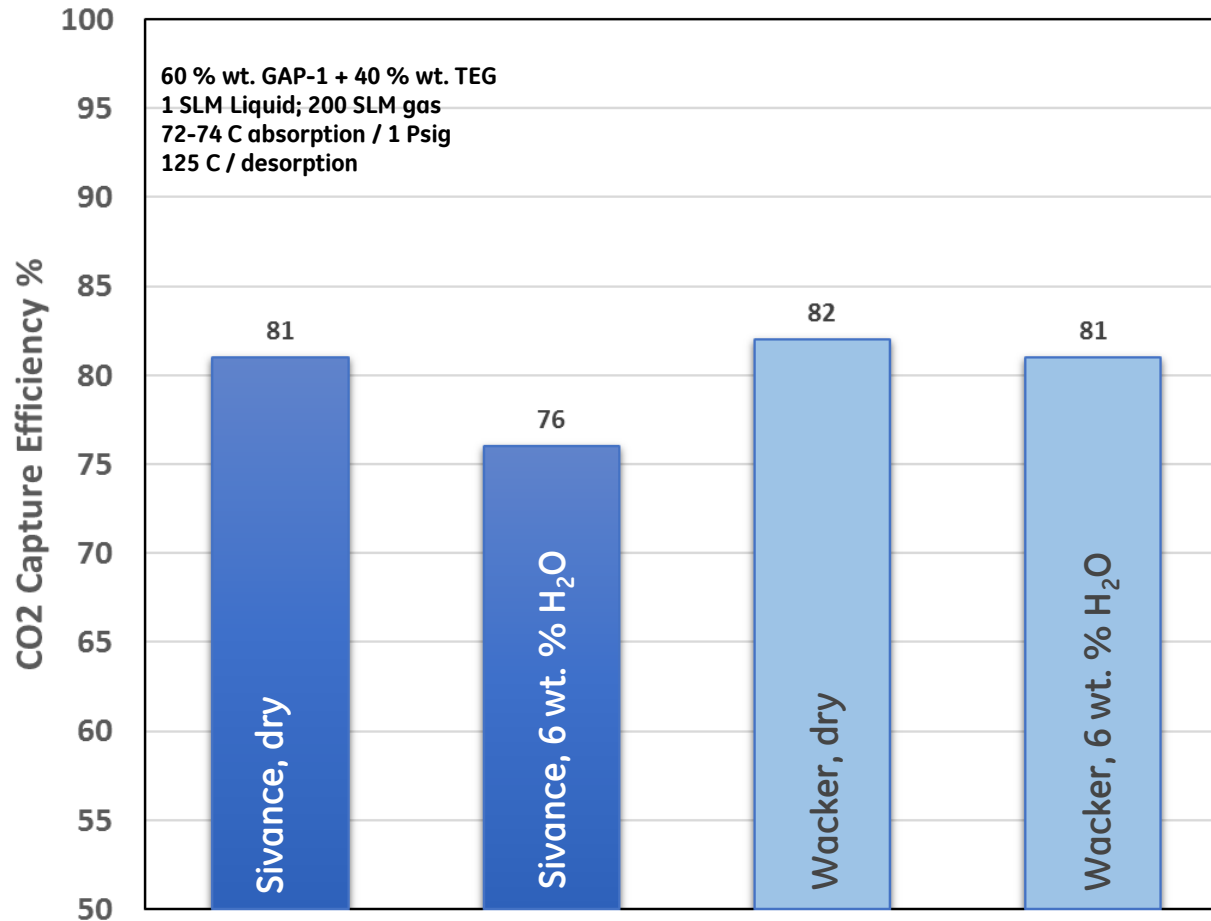
60 % wt. GAP-1 + 40 % wt. TEG  
1 SLM Liquid; 200 SLM gas  
72-74 C absorption / 1 Psig  
125 C / desorption

	<b>Sivance</b>		<b>Wacker</b>	
	NH3, ppmv		NH3 ppmv	
	Dry	Wet	Dry	Wet
<b>Baseline, FTIR</b>	0	0	0	0
<b>5 % O2, 12 % CO2</b>	60	59	7	6
<b>20 % O2, 3 % CO2</b>	NA	NA	NA	4

- ✓ **Rate of oxidation (2 kW<sub>e</sub>):** Wacker = 1/10 (Sivance)
- ✓ **Wacker GAP-1<sub>m</sub>:** not sensitive to elevated O<sub>2</sub> % (< 20%)



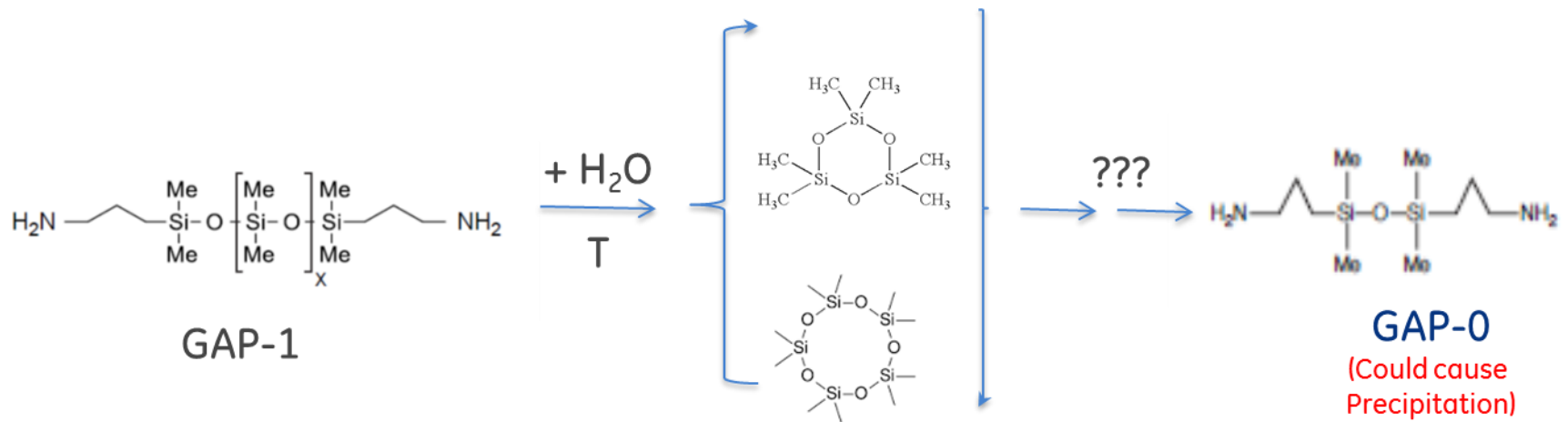
# CO<sub>2</sub> Capture (2kW Skid).. Sivance vs. Wacker



✓ CO<sub>2</sub> Capture Efficiency (2 kW<sub>e</sub> Bench): Wacker ~ Sivance



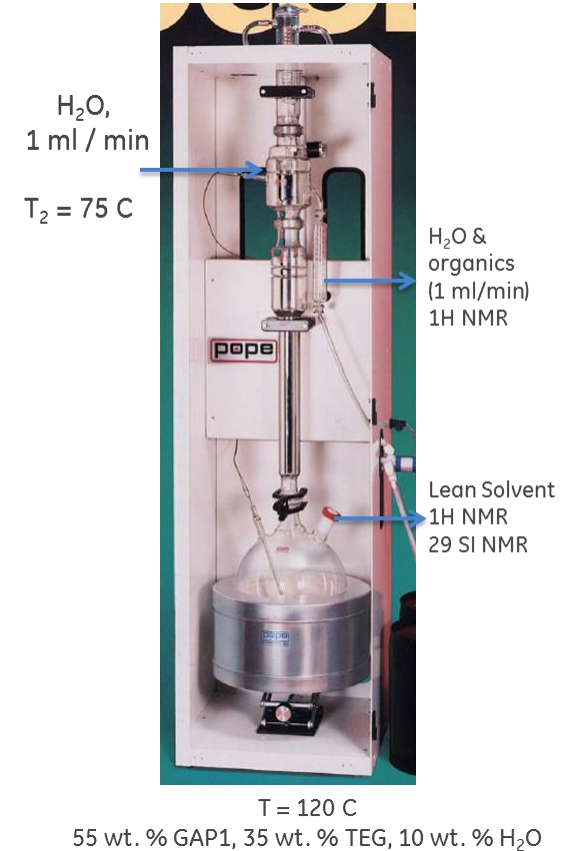
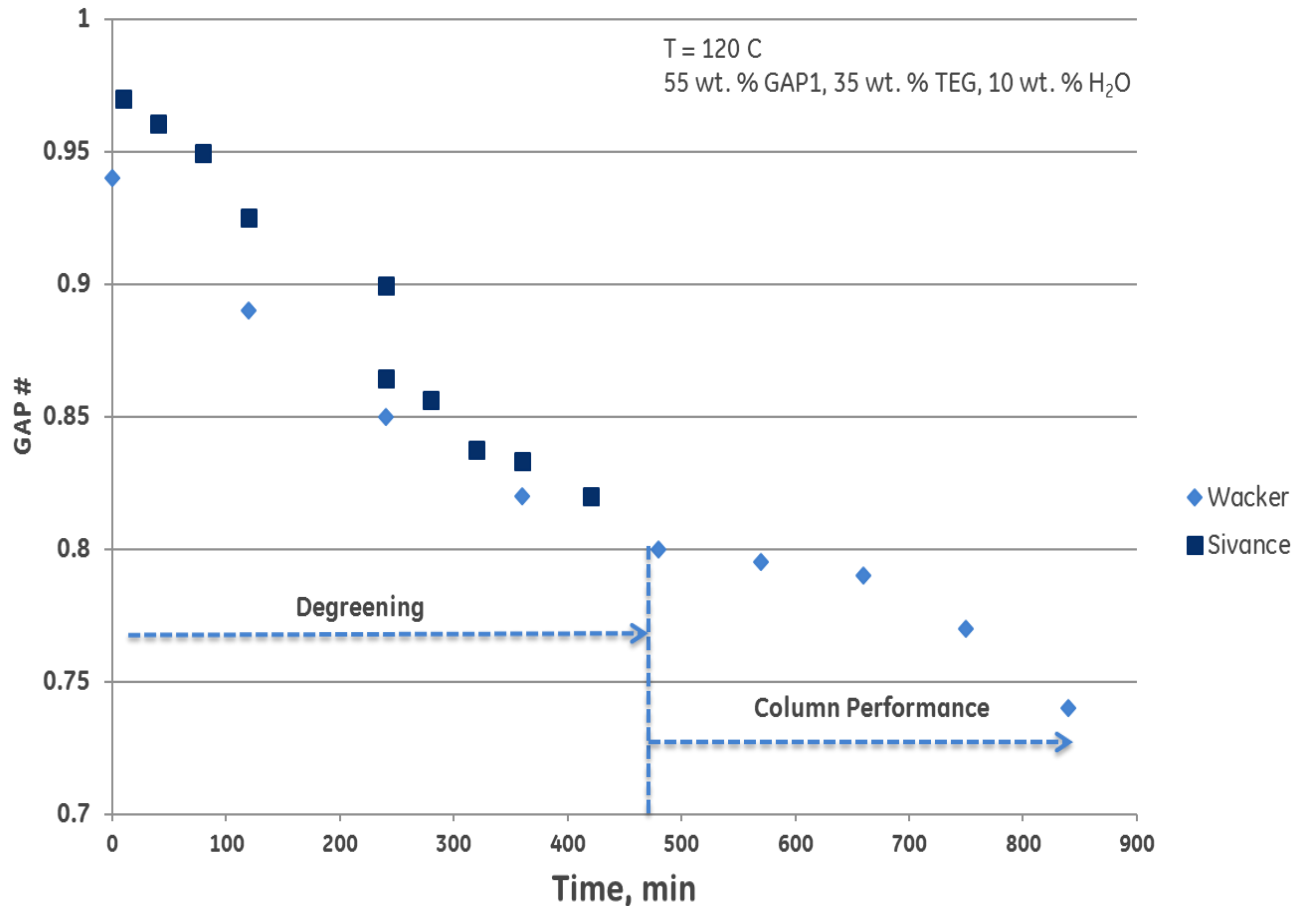
# Hydrothermal Stability.. Early equilibration



- ✓ **Early Equilibration..** Reduction in GAP# without losing  $\text{CO}_2$  Capacity



# Hydrothermal Stability (lab).. Wacker vs. Sivance



✓ Hydrothermal Equilibration.. Wacker ~ Sivance



# Wacker Qualification.. Summary

- **Thermal-degradation** <sub>(lab)</sub>.. Wacker ~ Sivance
- **Oxidation**
  - **Lab (Parr reactor, 70 °C):**  
Wacker ~ 1/10 Sivance; no influence of  $\text{Fe}^{2+}$
  - **Skid (2 kW, 1 ppm  $\text{SO}_2$ , L:G = 0.5; 125 °C desorption; 50-70 °C absorption):**  
Wacker (5 %  $\text{O}_2$ ) ~ Wacker (20 %  $\text{O}_2$ ) ~ 1/10 Sivance (5 %  $\text{O}_2$ )
- **Hydrothermal Equilibration** <sub>(lab)</sub>.. Wacker ~ Sivance
- **$\text{CO}_2$  Capture Efficiency** <sub>(2 kW skid)</sub>.. Wacker ~ Sivance (80 %)

✓ Wacker Qualified as Supplier for GAP-1



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# Host Evaluation.. Criteria to accommodate water-lean aminosilicone solvents

Unit Operation	Specifications
Absorber	Intercooling system to reject heat & maintain $T < 70\text{ }^{\circ}\text{C}$
Desorber	Steam stripping column with pre-flash system to reduce steam duty
MOC	Gaskets & seals compatible with GAP-1 <sub>m</sub> / TEG.
Water Management	Availability of water wash towers, partial and total condensers for precise water loading control. (Performance of the system is more sensitive to water content changes than the aqueous system.)
Heat Exchangers / Pumps	Designed to accommodate
Solvent Composition	% H <sub>2</sub> O = 10 – 20 wt. %
Waste Water	System to collect all waste water for disposal

Minor modifications needed to typical aqueous pilots to accommodate water-lean aminosilicone solvents



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# Techno-economical Analysis

- *Scope:*

Perform techno-economical comparison of the state-of-the art CO<sub>2</sub> capture technologies vs. aminosilicone solvent

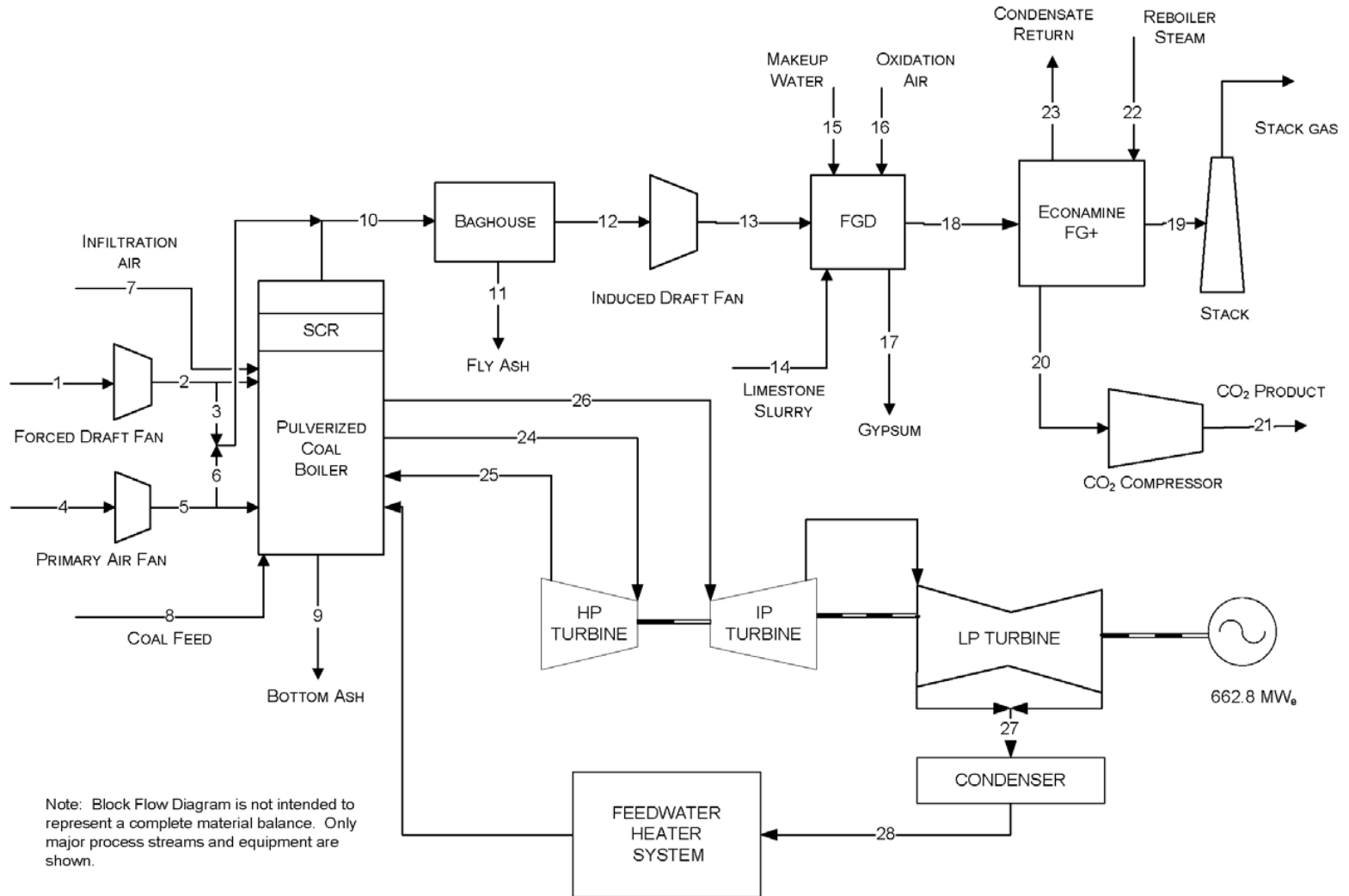
- *Methodology:*

- Technologies Included: Enhanced Fluor Econoamine, KS-1 (MHI), MTR Membrane, TDA Adsorbent
- Steam Conditions: Supercritical
- Data for competitive technologies published by DOE/NETL

(R. Stevens, 2012 NETL CO<sub>2</sub> Capture Technology Meeting)



# Pulverized Coal Power Plant.. PFD Supercritical



## Analysis Performed for Supercritical Coal Plant



# Pulverized Coal Power Plant.. Evaluation Basis

	Case 11 w/o CO <sub>2</sub> Capture	Case 12 w/CO <sub>2</sub> Capture
Steam Cycle, MPa/°C/°C (psig/°F/°F)	24.1/593/593 (3500/1100/1100)	24.1/593/593 (3500/1100/1100)
Coal	Illinois No. 6	Illinois No. 6
Condenser pressure, mm Hg (in Hg)	50.8 (2)	50.8 (2)
Boiler Efficiency, %	88	88
Cooling water to condenser, °C (°F)	16 (60)	16 (60)
Cooling water from condenser, °C (°F)	27 (80)	27 (80)
Stack temperature, °C (°F)	57 (135)	32 (89)
SO <sub>2</sub> Control	Wet Limestone Forced Oxidation	Wet Limestone Forced Oxidation
FGD Efficiency, % (A)	98	98 (B, C)
NO <sub>x</sub> Control	LNB w/OFA and SCR	LNB w/OFA and SCR
SCR Efficiency, % (A)	86	86
Ammonia Slip (end of catalyst life), ppmv	2	2
Particulate Control	Fabric Filter	Fabric Filter
Fabric Filter efficiency, % (A)	99.8	99.8
Ash Distribution, Fly/Bottom	80% / 20%	80% / 20%
Mercury Control	Co-benefit Capture	Co-benefit Capture
Mercury removal efficiency, % (A)	90	90
CO <sub>2</sub> Control	N/A	Econamine
Overall CO <sub>2</sub> Capture (A)	N/A	90.2%
CO <sub>2</sub> Sequestration	N/A	Off-site Saline Formation

DOE/NETL-2010/1397

Design basis according to DOE/NETL methodology



# Pulverized Coal Power Plant.. Cost Estimation

- 2011 \$
- CO<sub>2</sub> transport, storage and monitoring included
- Financial Assumptions: High risk / investor own utilities (IOU)
- Financial outputs:

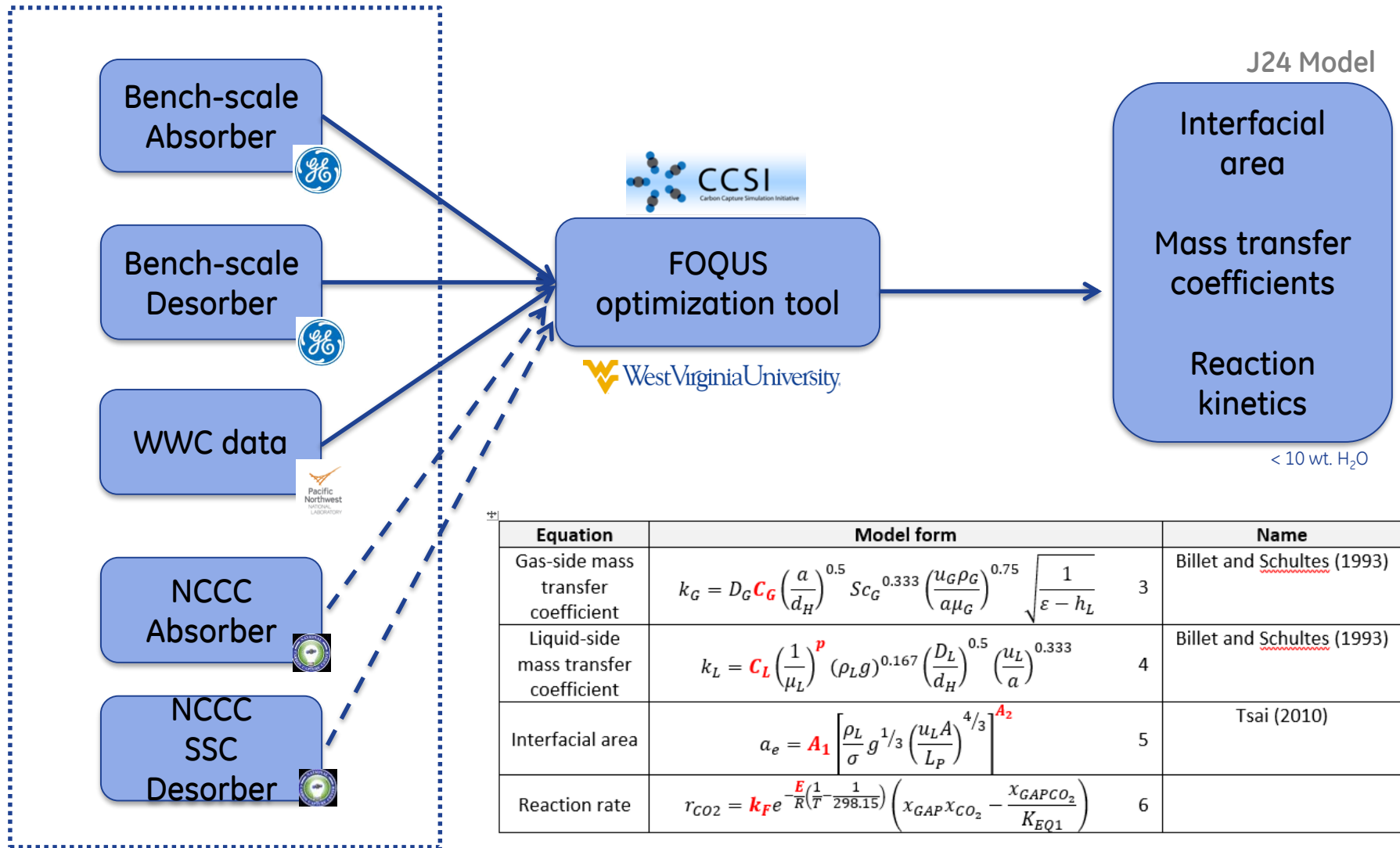
$$COE = \frac{\frac{\text{first year capital charge}}{\text{annual net megawatt hours of power generated}} + \frac{\text{first year fixed operating costs}}{\text{annual net megawatt hours of power generated}} + \frac{\text{first year variable operating costs}}{\text{annual net megawatt hours of power generated}}}{1}$$

$$Removal\ Cost = \frac{\{ COE_{with\ removal} - COE_{w/o\ removal} \} \$ / MWh}{\{CO_2\ removed\} tons / MWh}$$

Cost Estimation according to DOE/NETL methodology

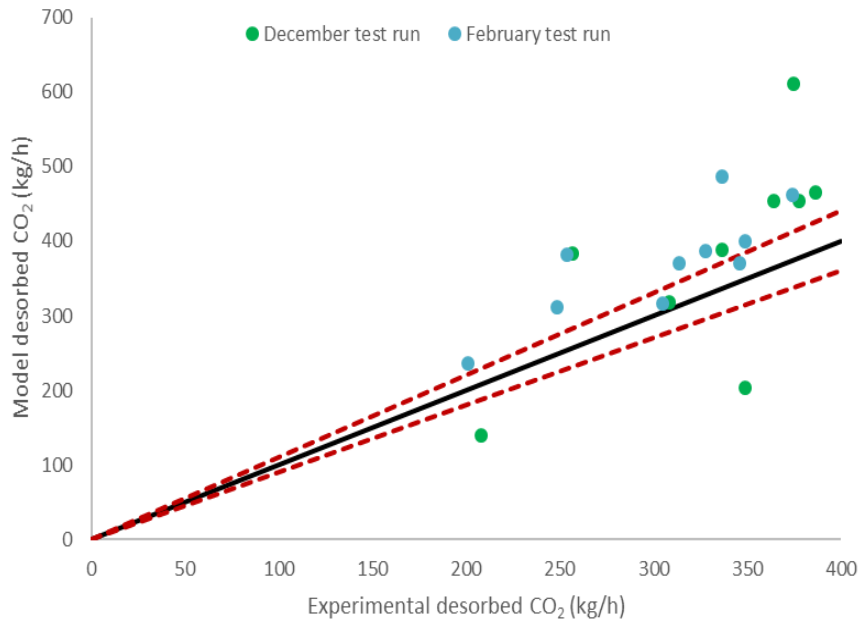


# Process Modeling.. FOQUS Optimization

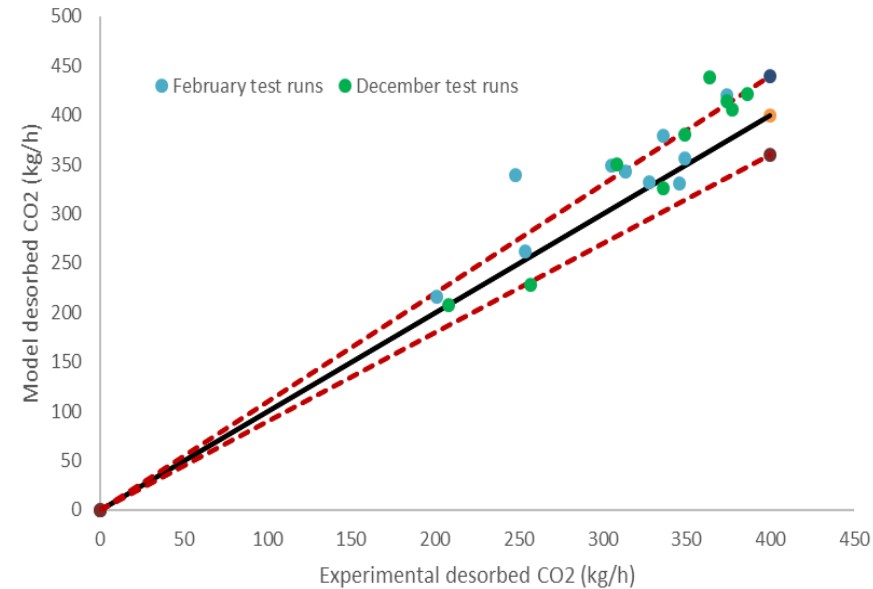


# Process Modeling.. J24 Model tuning to 0.5 MW Data

## J23



## J24



### J24 Model:

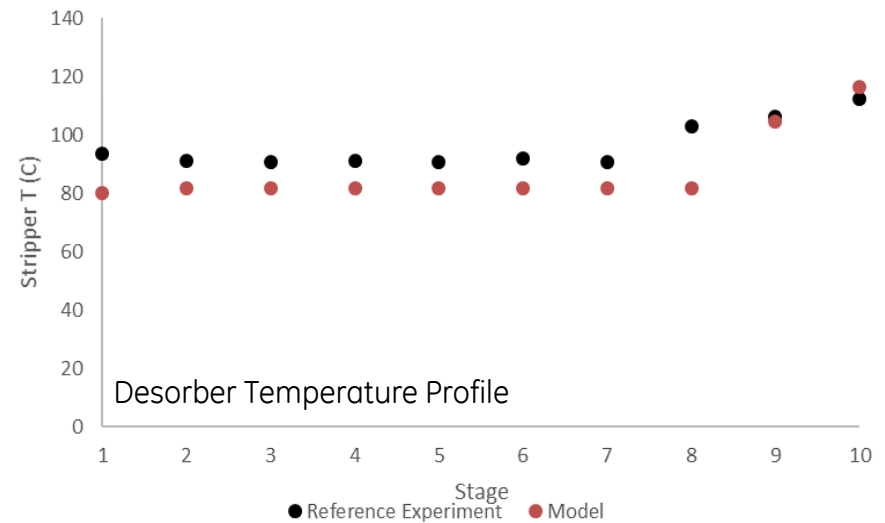
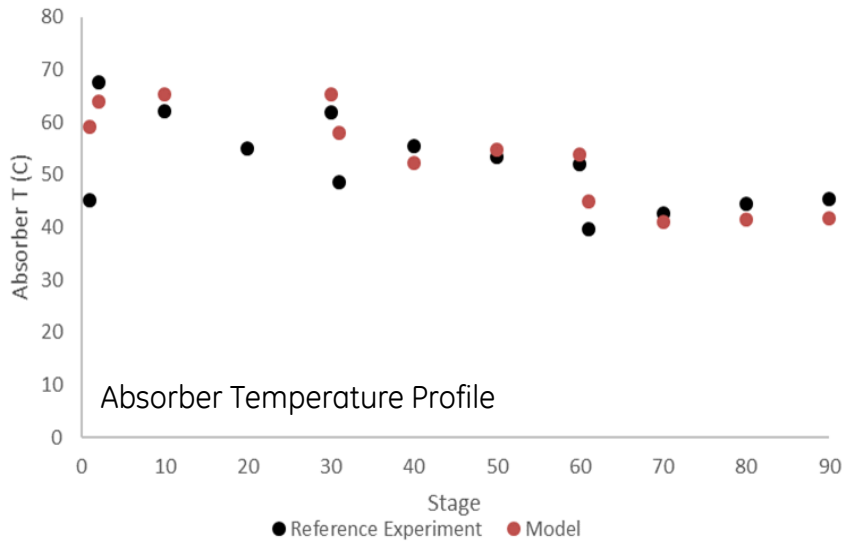
- **Steam Stripper..** 40 stages with an upgraded reboiler
- **Absorber..** Intercoolers implementation
- **Solvent Properties..** Updated to accommodate higher water content



J24 Model captures well system behavior at 0.5 MW Pilot



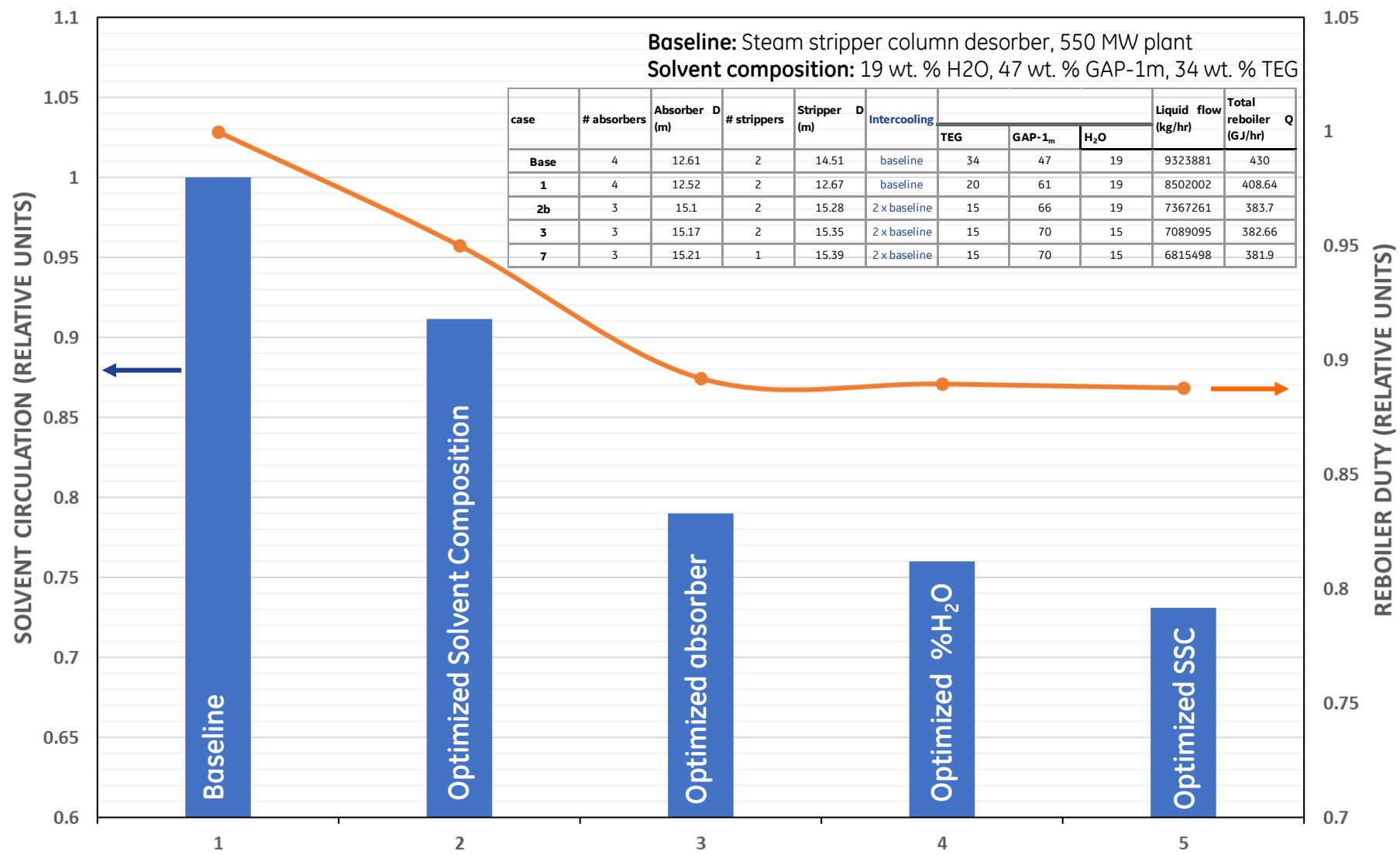
# Process Modeling.. J24 Model tuning to 0.5 MW Data



J24 Model captures well system behavior at 0.5 MW Pilot



# Process Optimization.. Composition & Absorber



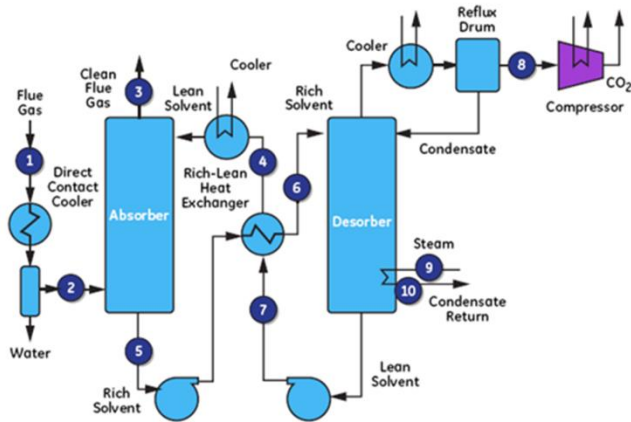
Process Optimization = f (absorber, SSC, solvent composition, intercooling)



## Technical Approach.. Process & Plant Modeling

## ASPEN PLUS: CO<sub>2</sub> Capture Island

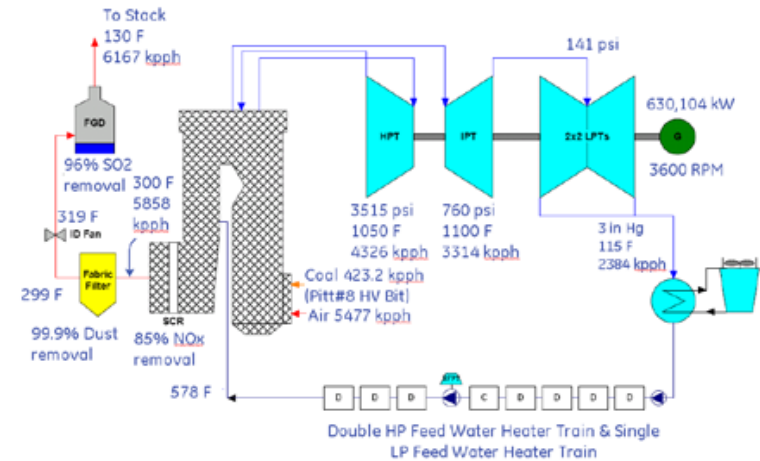
GE Global Research



- ✓ **Absorber...** Packing, intercooling, MOC
- ✓ **Desorber...** SSC, temperature, MOC
- **Solvent ...** Reclaiming, cost

## ThermoFlow: SC Power Plant

GE Power & Water

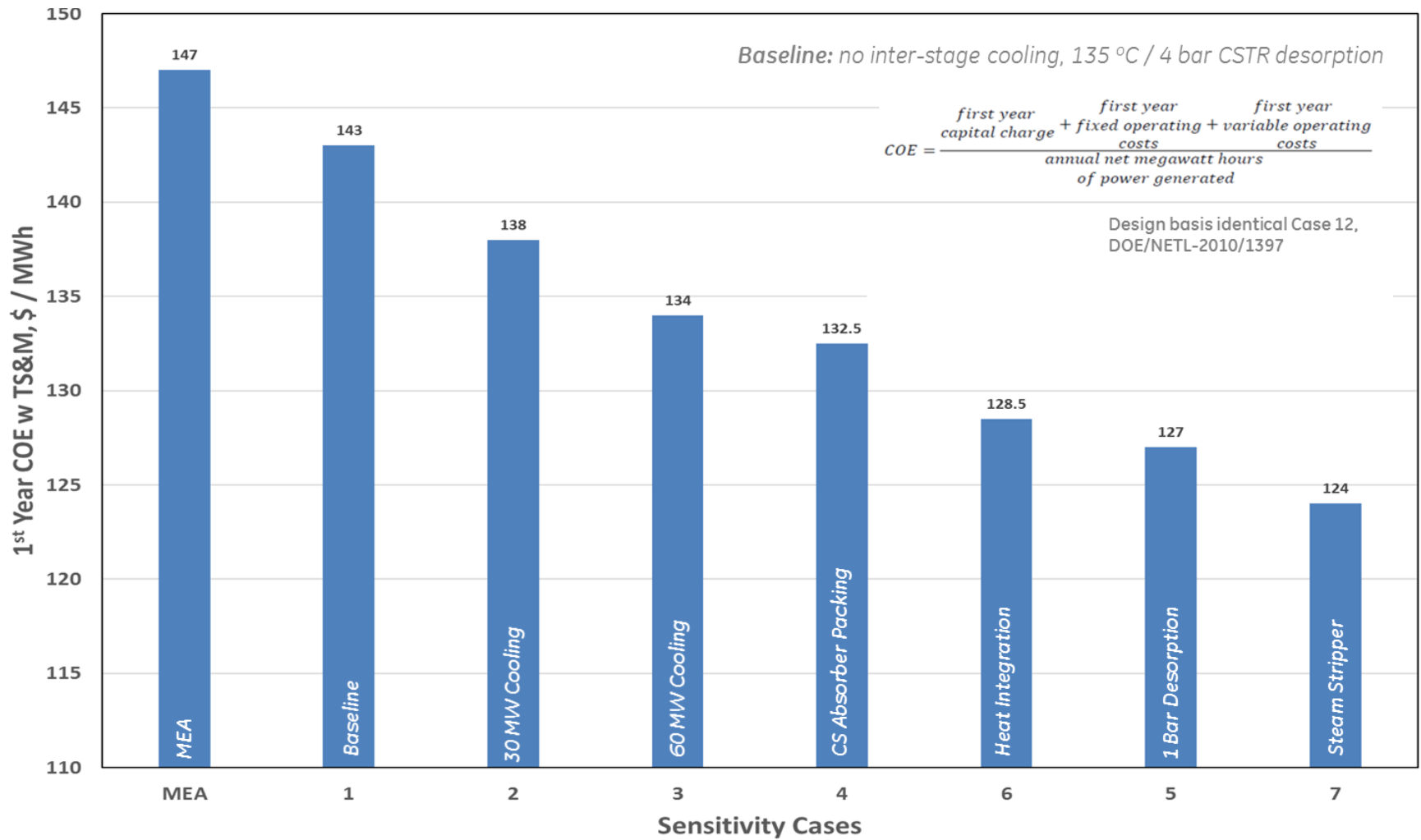


- ✓ **Tune model to DOE/NETL-2010/1397**
- ✓ **Steam extraction...** Location, T
- ✓ **FGD...** Efficiency, CAPEX
- **Heat Integration..** Cooling water, steam

## Dynamic interplay between the CO<sub>2</sub> Capture Island and Power Plant



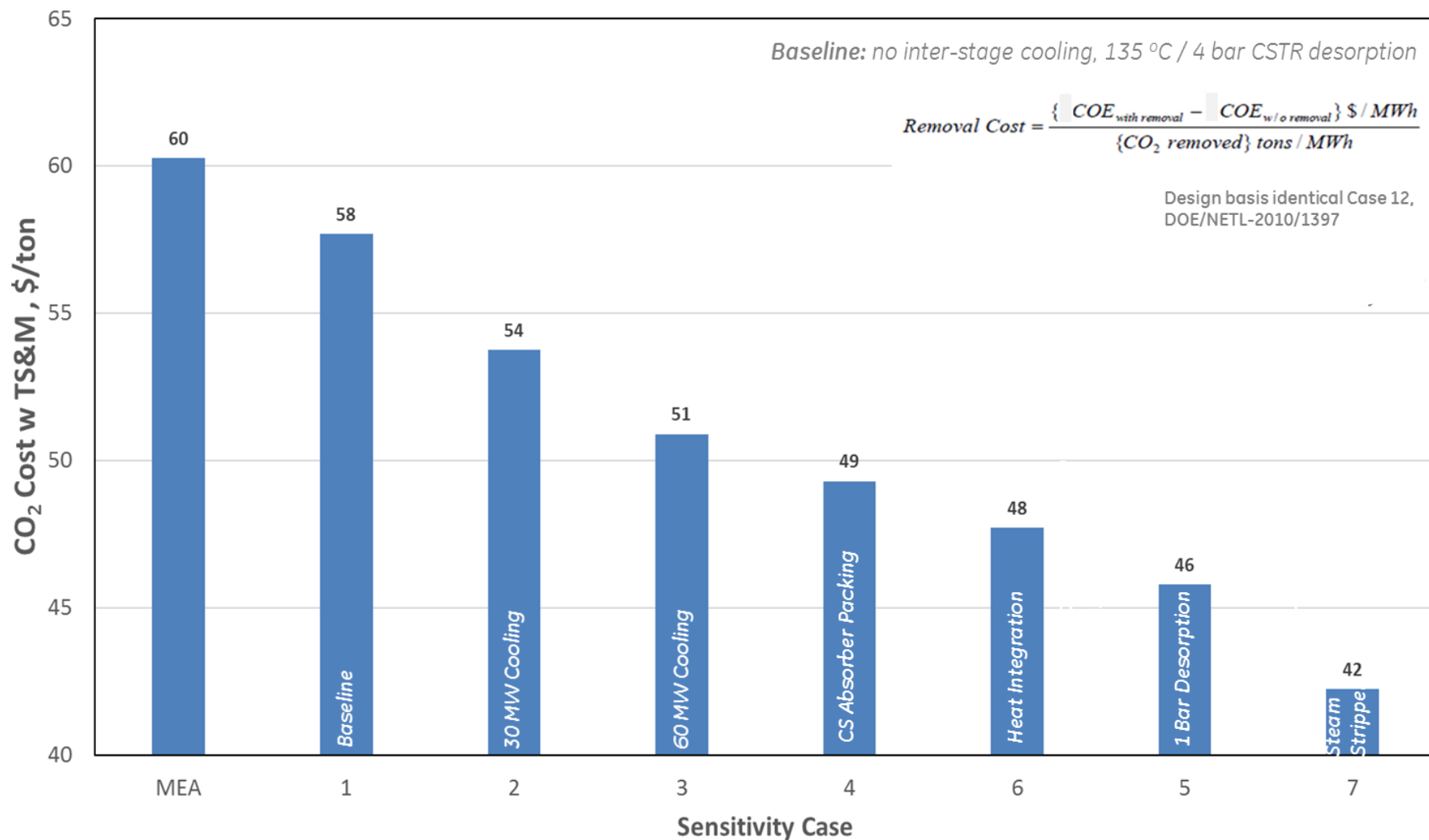
# Sensitivity Analysis.. 1<sup>st</sup> Year COE entitlement



Over 20 % Improvements in Entitlement COE over MEA Fluor



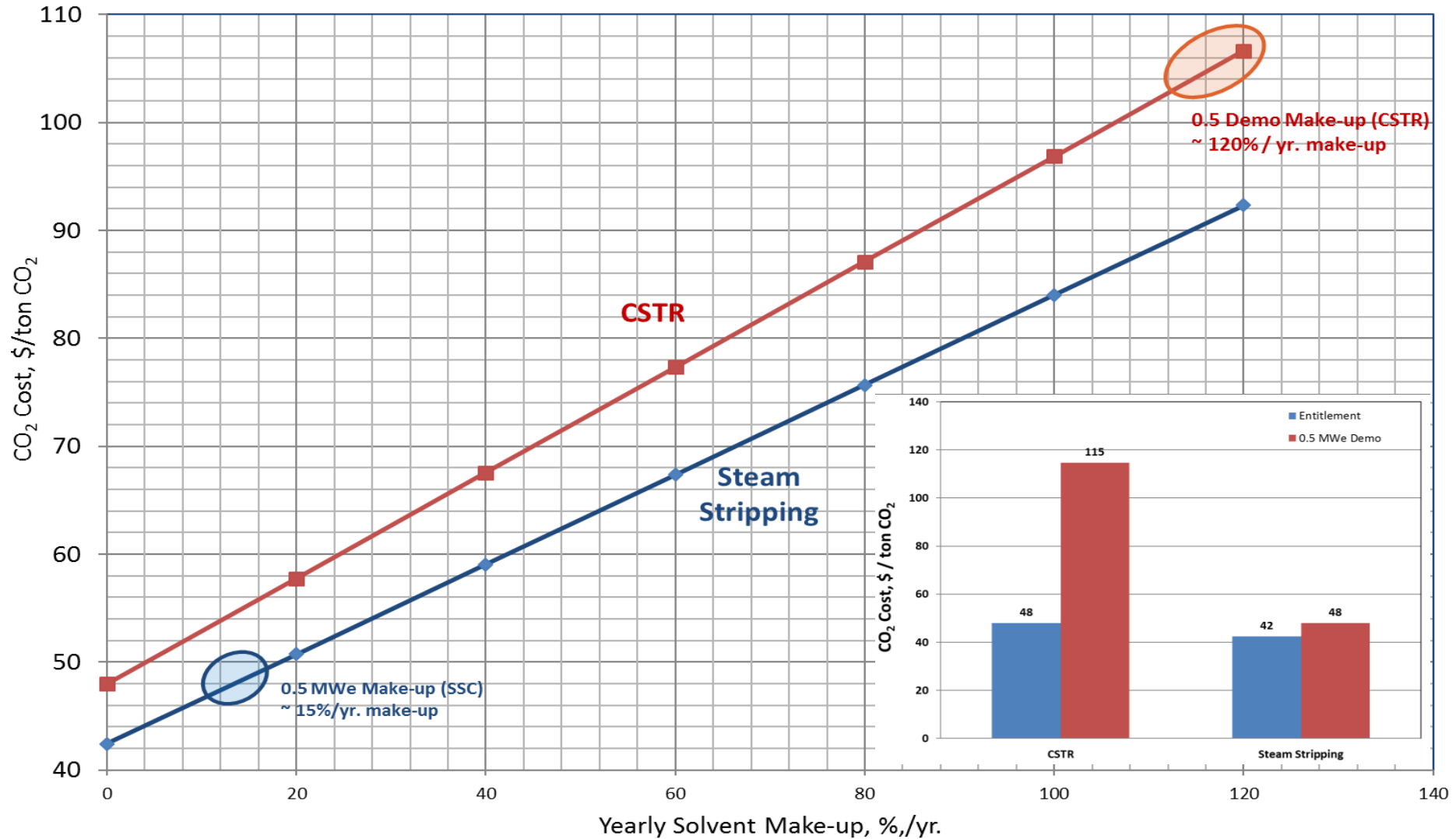
# Sensitivity Analysis.. CO<sub>2</sub> Removal Cost entitlement



30% reduction in Entitlement CO<sub>2</sub> Cost vs. MEA



# CO<sub>2</sub> Removal Cost.. CSTR vs. Steam Stripping



CSTR CO<sub>2</sub> cost.. dominated by solvent make-up

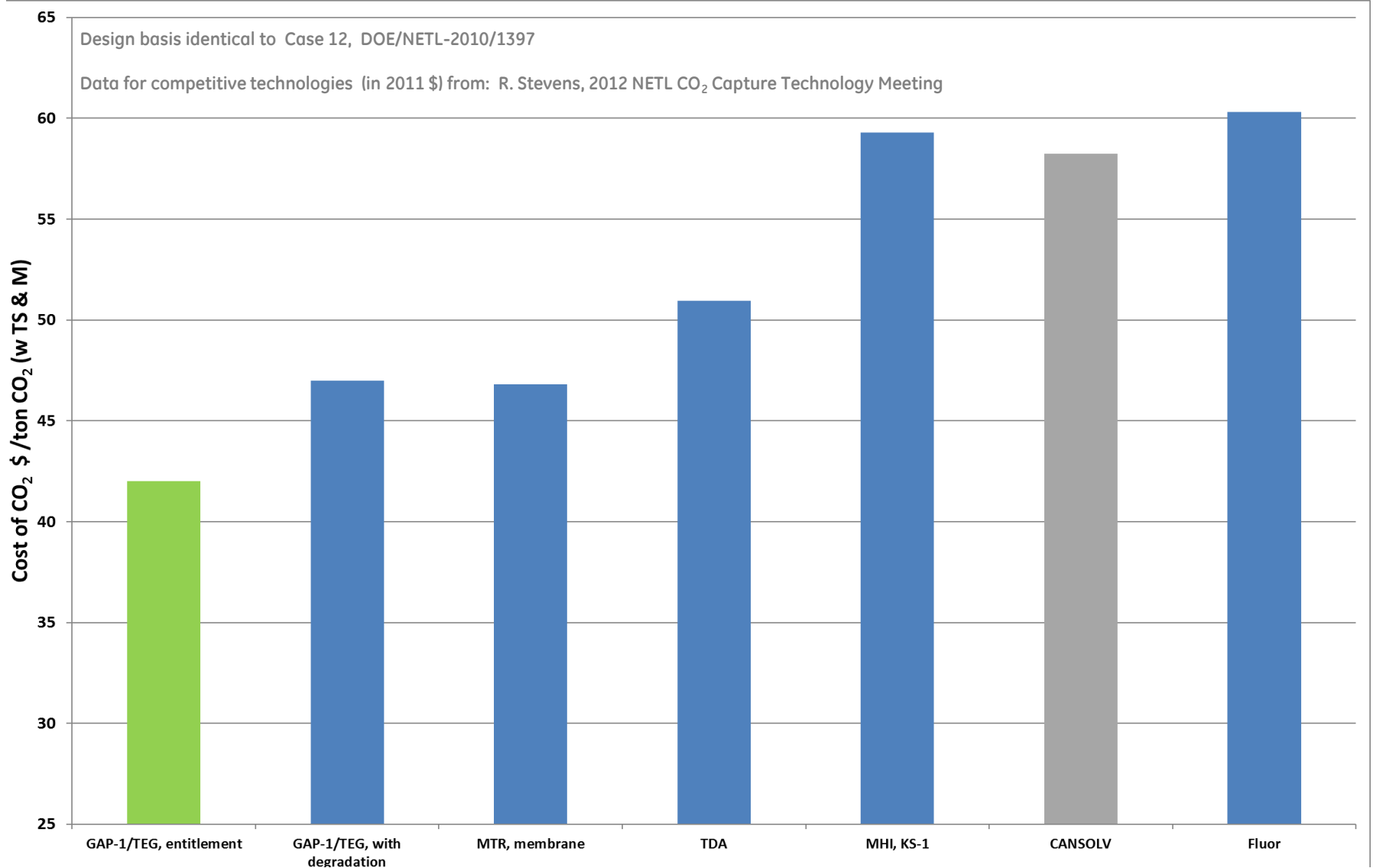
Steam Stripping CO<sub>2</sub> Cost..

\$42 / tCO<sub>2</sub> (entitlement)

\$48 / tCO<sub>2</sub> (with degradation)



# Competitive Assessment.. CO<sub>2</sub> Cost Removal

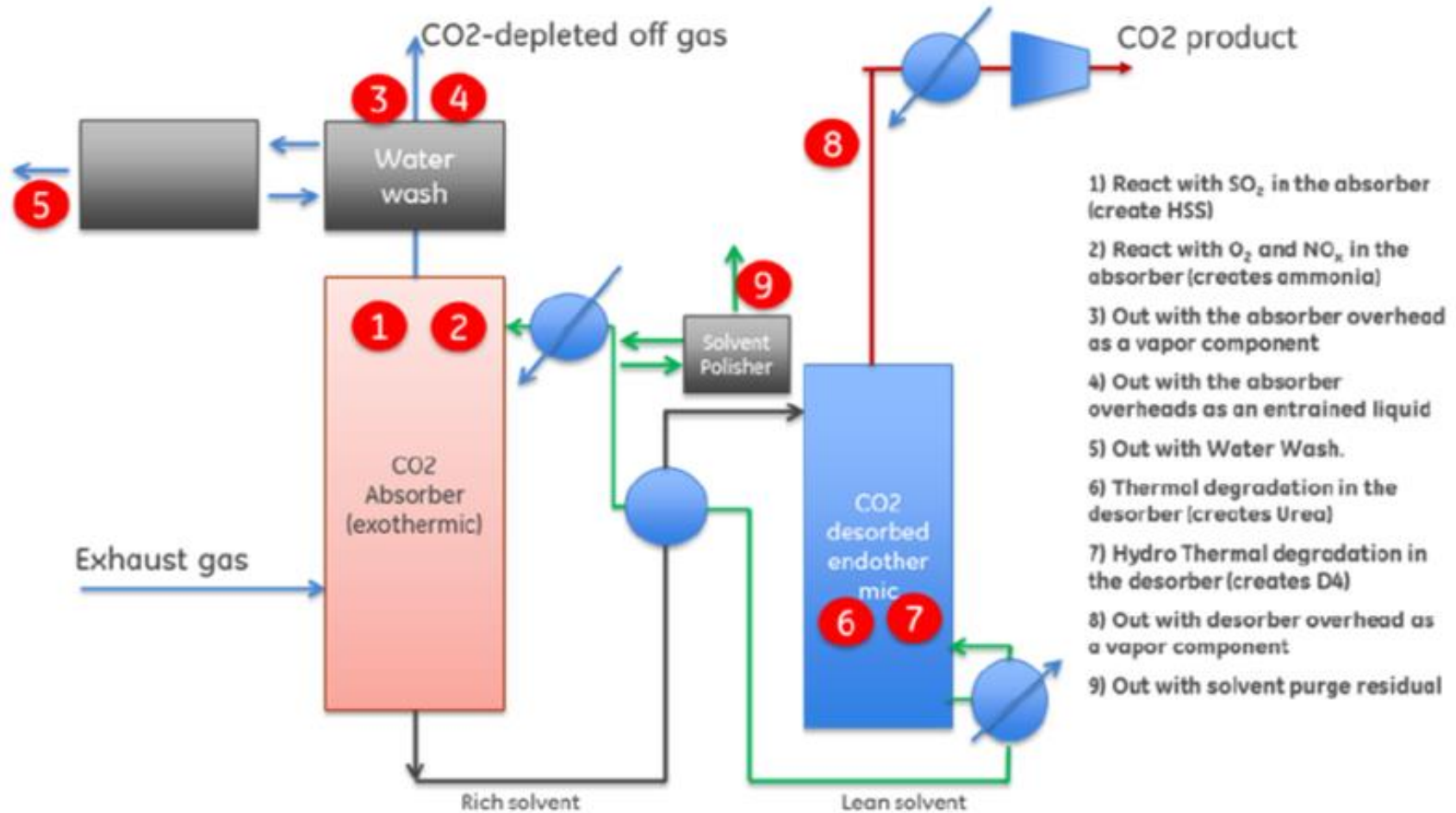


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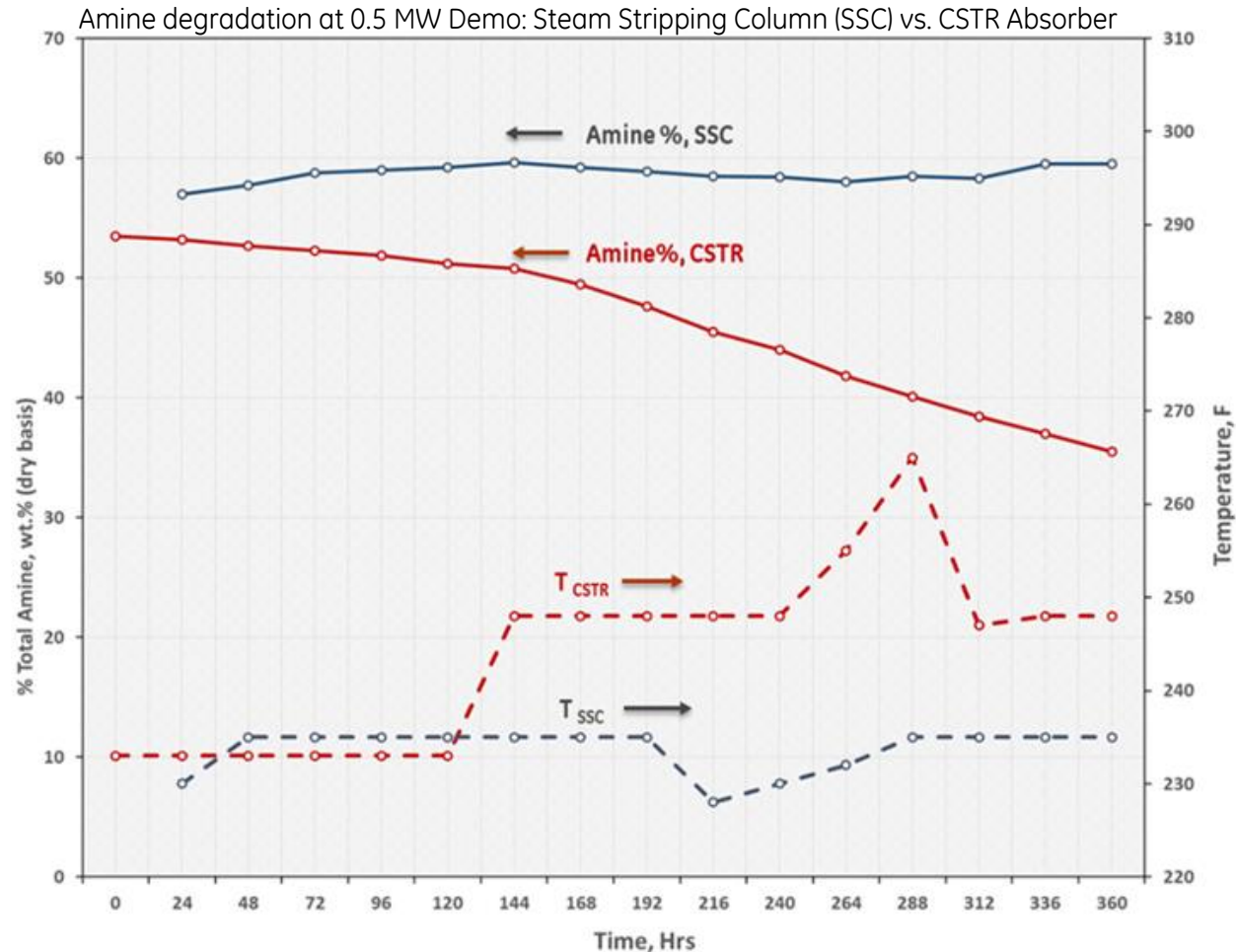
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# Technology GAP Analysis.. Solvent Management



# Technology GAP.. Solvent thermal stability

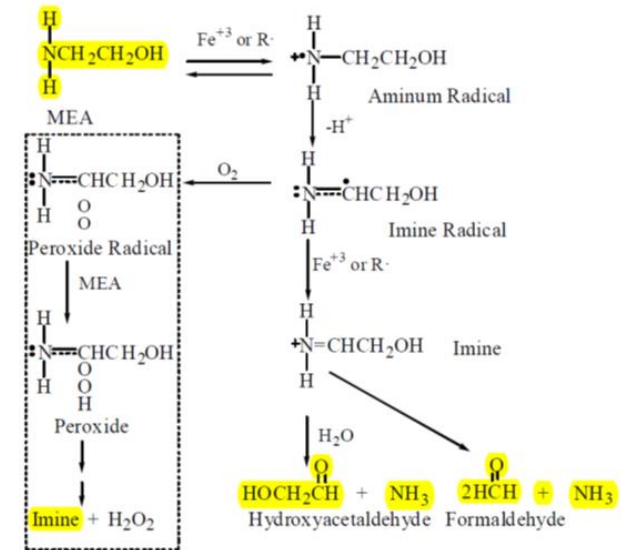
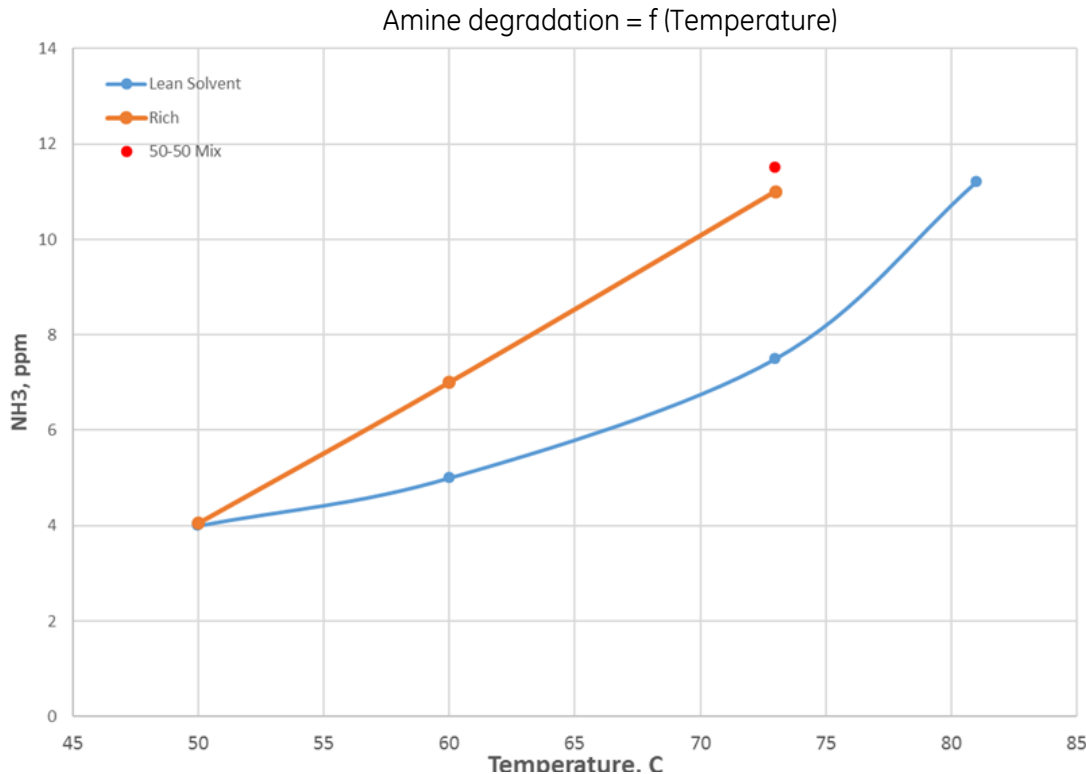


## ✓ Recommendations:

- Implement controlled water addition with SSC (TRL 5)
- Optimize water content to reduce steam duty / corrosivity of working solution



# Solvent Management.. Oxidative Stability

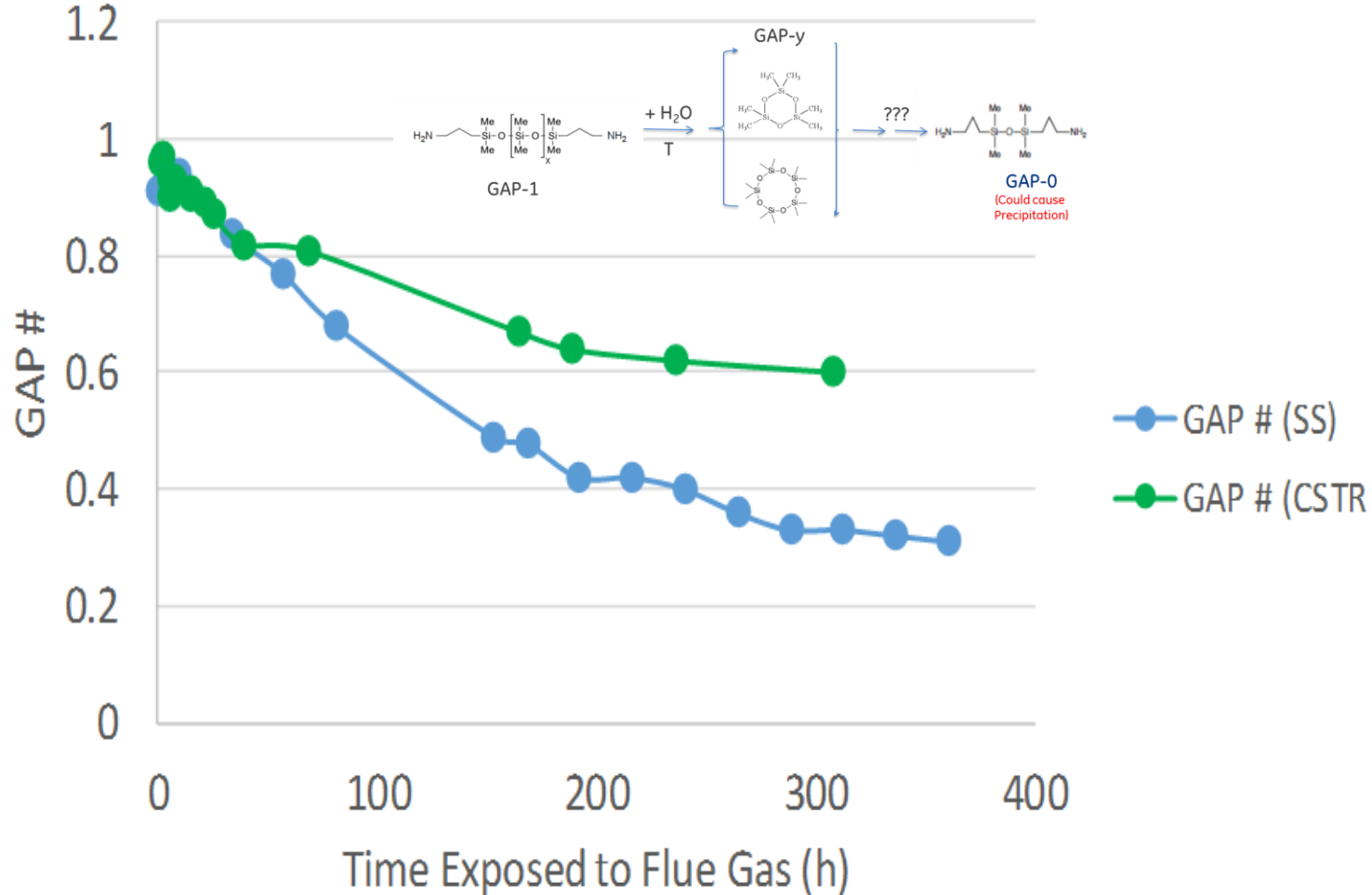


## ✓ Recommendations:

- Optimized absorber inter-stage cooling (TRL 6)
- Controlled water addition.. Reduced absorber temperature through evaporative cooling
- Development of oxidation inhibitors (TRL 2)



# Solvent Management.. Hydrothermal Stability



## ✓ Recommendations:

- GAP number of starting material ~ 0.3 (equilibration value) (TRL 4)

# Technology GAP.. Future R&D Directions

Solvent Attribute	Baseline <sup>(1)</sup>	GAP-1 / TEG (Gen 1)	Adv. Aminosilicone (Gen 2)	Process Impact <sup>(2)</sup> (Gen 2 vs. Gen 1)
CO <sub>2</sub> Working Capacity (wt.%)	4	5	10	-30 % CAPEX; -11% OPEX
Solvent Make-up (% / yr)	100	75	20	-40% OPEX
Viscosity (CO <sub>2</sub> loaded, cP)	1	576	100	-40% absorber; -30% RLHX <sup>(3)</sup>
Heat of Reaction (KJ/Kg)	1825	2263	1900	-12 % reboiler duty
CO <sub>2</sub> Cost (\$/tCO <sub>2</sub> ) COE (cents / kWh)	72 (13.7)	48 (11.6)	40 (10.6)	

## Gen 2 Solvent..

- ✓ Improved Working capacity..
- ✓ Solvent Management..
- ✓ Viscosity reduction..

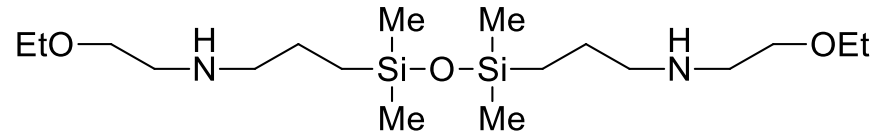
No co-solvent

No equilibration & reduced thermal degradation

4 X

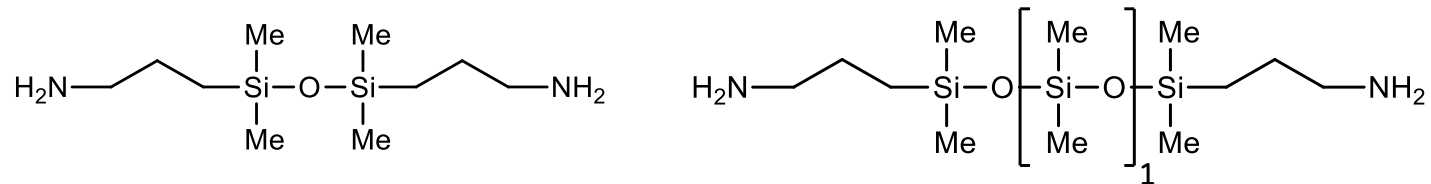


# Technology GAP.. Future R&D Directions



GEN 2 : **EEAP** (EthoxyEthylAminoPropyl GAP)

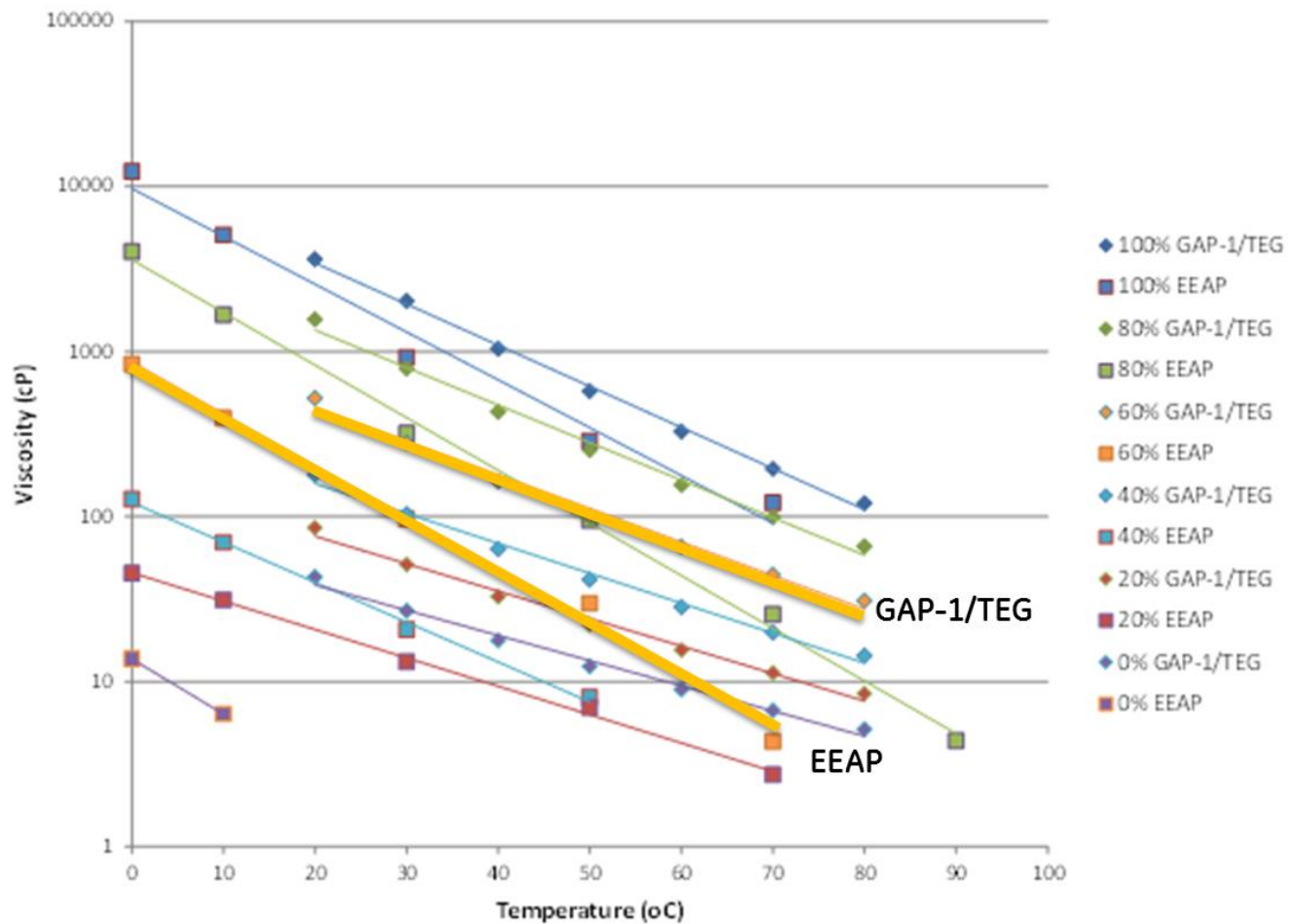
Same family of aminosilicones as GAP-0 and GAP-1



- Single component like GAP-0, not a mixture of homologs like GAP-1
- However, fully reacted EEAP remains as a flowable liquid
- No need for co-solvent



# Gen 2 Solvents.. Viscosity

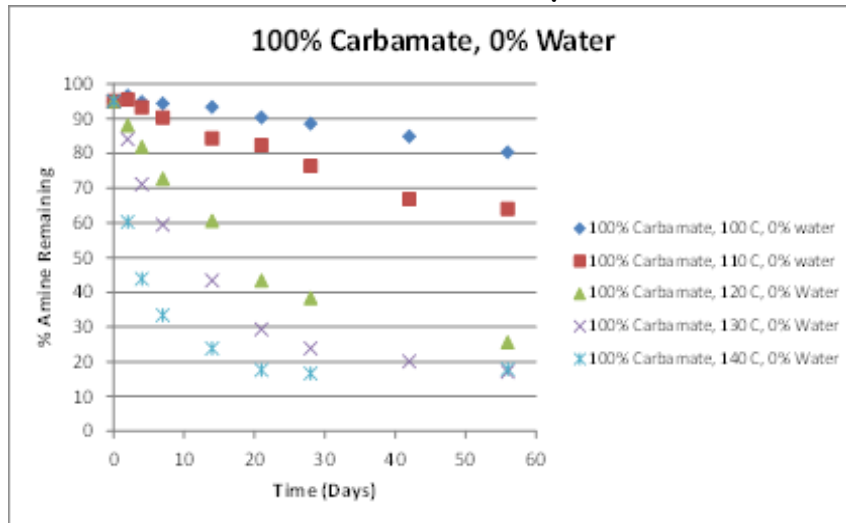


✓ **Gen 2 Solvents:** 2-3 X reduction in viscosity of the rich solvent

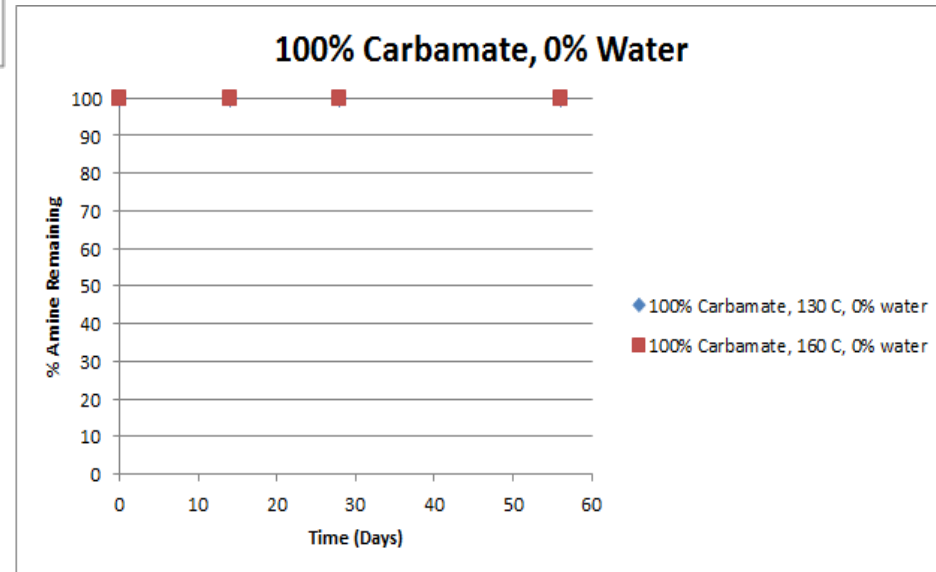


# Gen 2 Solvents.. Thermal Stability

## Gen 1: GAP-1 / TEG



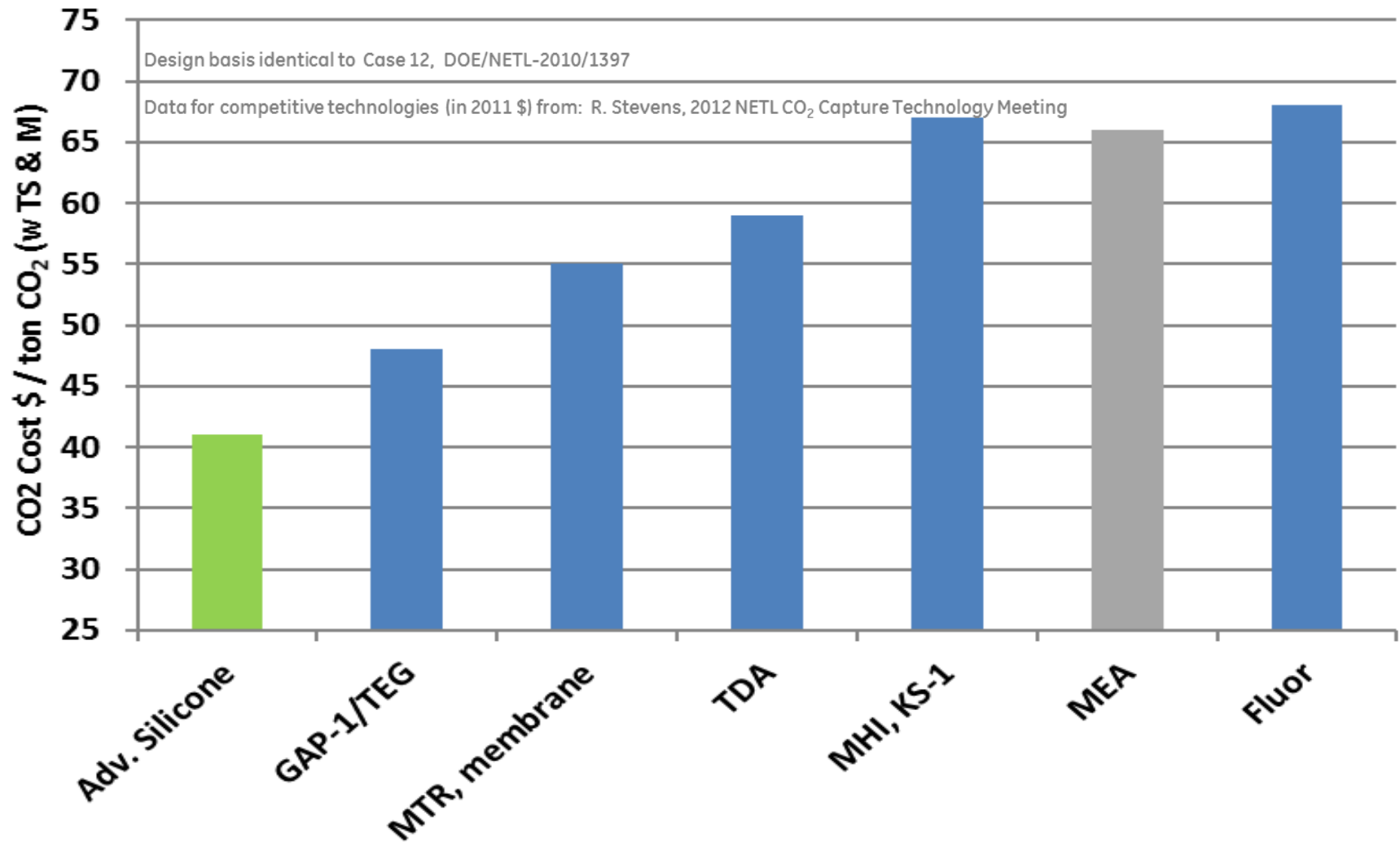
## Gen 2: EEAP



✓ **Gen 2 Solvents:** No thermal degradation of the rich solvent @ 160 °C



# Gen 2 Solvents.. Preliminary TEA



- ✓ **Gen 2 Solvents** – 20% potential CO<sub>2</sub> cost reduction vs. GAP-1 / TEG technology through increased working capacity, and reduced solvent make-up & viscosity



# Executive Summary

- Performed feasibility evaluation of the of the aminosilicone solvent technology for scale-up at 10 MW

## • Aminosilicone Solvent

- ✓ **Non-aqueous solvent..** Improved CO<sub>2</sub> working capacity, Low volatility, low corrosivity
- **Solvent degradation...** Thermal oxidative & hydrolysis

Suggested Actions: Improve solvent management through low T absorption / desorption, solvent mfg cost-out

## • Supplier Qualification

- ✓ **Qualification Process..** Solvent management (thermal, oxidation, equilibration) & CO<sub>2</sub> Capture Efficiency
- ✓ **Performance..** Wacker ~ Baseline (Sivance); Wacker solvent showed improved oxidation stability

Suggested Actions: Wacker quailed as supplier for GAP/TEG-1

## • Techno-economical Analysis

- ✓ **Process modelling..** Updated ASPEN model for process optimization of the SSC (WVU)
- ✓ **TEA..** \$42/tCO<sub>2</sub> (entitlement with SSC); \$ 48/tCO<sub>2</sub> (SSC & solvent degradation)  
CO<sub>2</sub> cost for CSTR dominated by solvent degradation

Suggested Actions: Develop Gen 2 solvent as path to \$40/tonne CO<sub>2</sub>

## • GAP Analysis

- ✓ **Technology Gaps..** Solvent management
- ✓ **Recommendations..** Controlled water addition with SSC for improved thermal & oxidation stability; adjust GAP# for starting material, oxidation inhibitors, solvent reclamation
- ✓ **Future R&D..** Develop & scale-up co-solvent free water lean aminosilicone solvent (Gen 2)

Suggested Actions: Improve specific steam duty through water loading optimization & advanced flow scheme; demonstrate solvent management & reclamation at TRL 6 before proceeding with the next scale pilot.

