

# **Investigation on Pyroelectric Ceramic Temperature Sensors for Energy System Applications**

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# Agenda



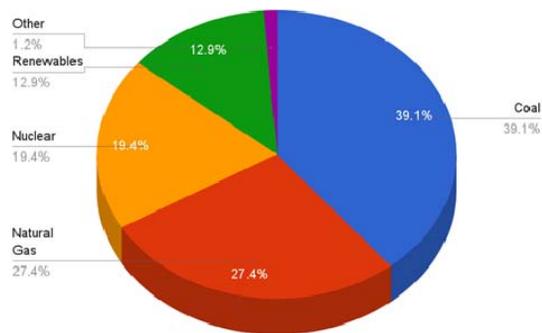
- Introduction and Background
- Objectives
- Technical Approach
- Results
- Summary
- Future Work

# Introduction

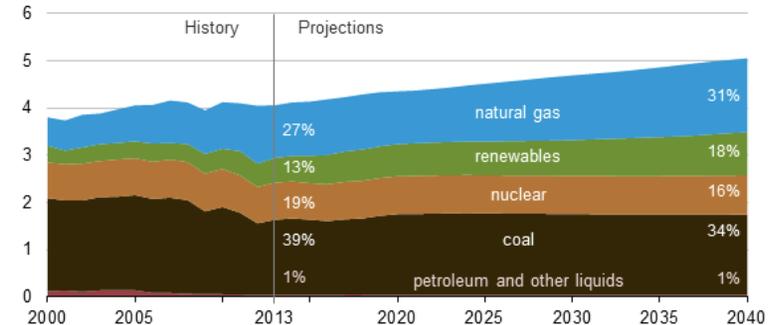


- ❑ Temperature sensing is critical in modern power plants and energy systems
  - Higher efficiencies in energy conversion
  - Lower emission for near-zero emission power plants
  - Enhanced material systems safety

U.S. 2013 Electricity Generation By Type



Electricity generation by fuel type in the AEO2015 Reference case, 2000-2040  
trillion kilowatthours



# Introduction



## ❑ Project Goal

Design, fabricate, and demonstrate a *low cost self-powered wireless* temperature sensor for energy system applications

## ❑ Expectation

Provide a complete set of documentation for sensor manufacturing, testing and characterization

## ❑ Benefit

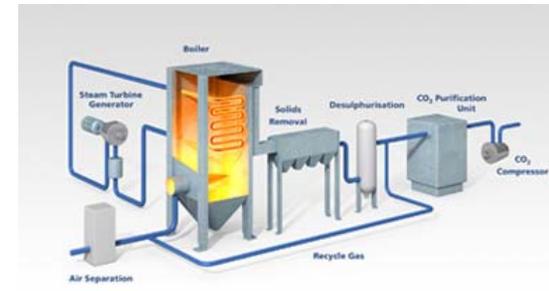
Energy conversion areas where continuous temperature monitoring required to achieve higher performance



Coal-Gasification Power Plant



Gas Turbine



Oxy Fuel Combustion

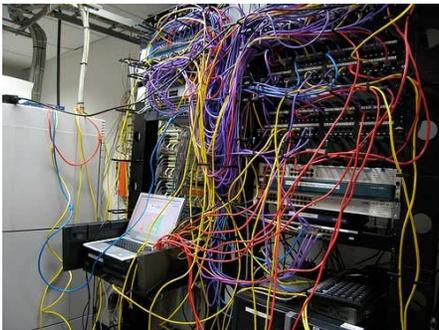
## Overview and Rationale

### ❑ Wired temperature sensors

- High cost materials required (Sapphire, laser)
- Complicated sensing systems lead to high cost and maintenance
- Typically require special coupling connection

### ❑ Wireless temperature sensors

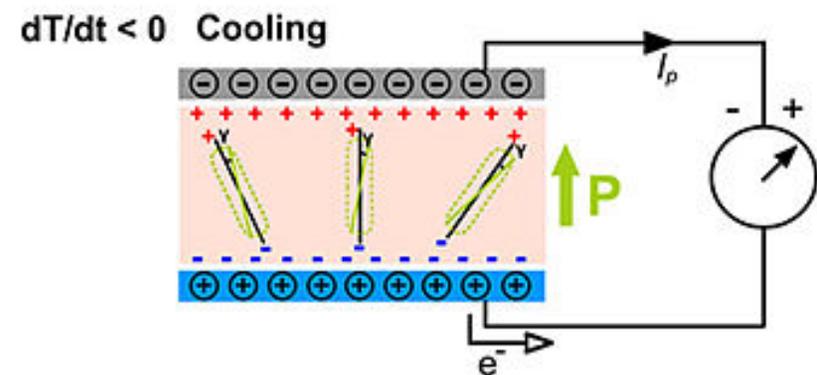
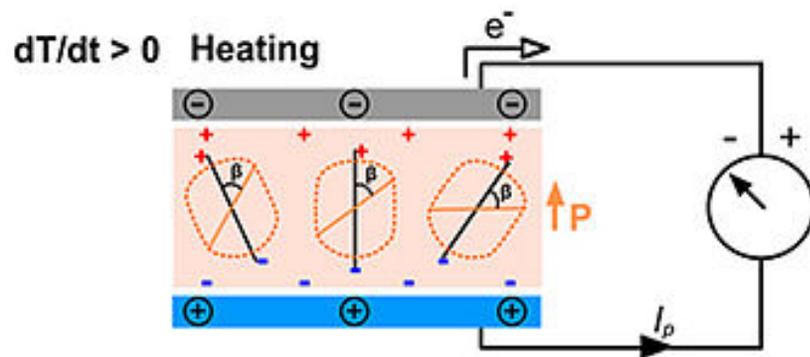
- Require built-in electronics
- High temperature limitation
- Complicated sensor design



# Background



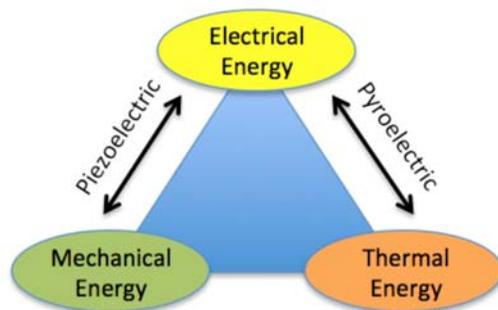
- Pyroelectric material is heated
  - Spontaneous polarization reduced through reduction of dipole moment
  - Quantity of bound charges at the electrodes decreases
  - This subsequent redistribution of charges results current flow through the external circuit
- Pyroelectric material is cooled
  - Spontaneous polarization increased
  - Current sign is reversed



# Background

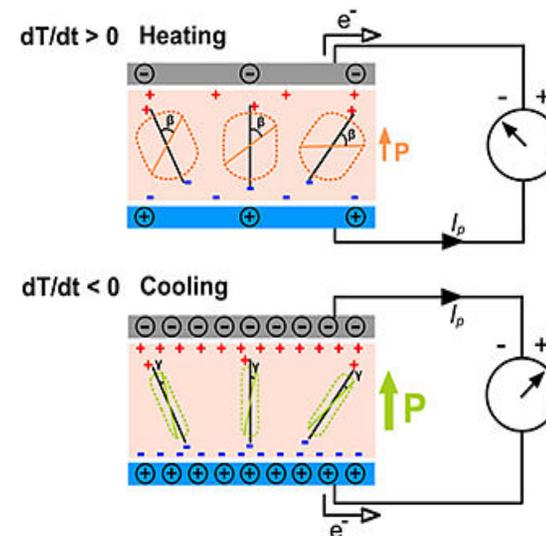
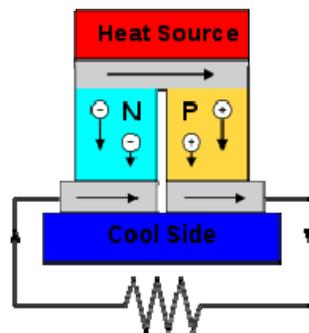


- ❑ Coupling thermal energy and electrical energy
- ❑ Different from thermoelectric, one piece
- ❑ Current proportional to temperature change



$$i_p = \frac{dQ}{dt} = Ap \frac{dT}{dt}$$

$$T_f = -\frac{1}{pA} \int_{t_i}^{t_f} I dt + T_i$$



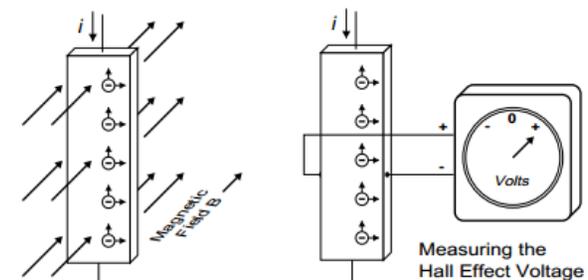
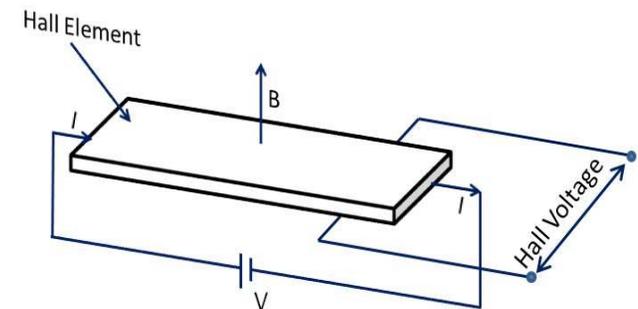
# Background



## Sensing of Magnetic Field

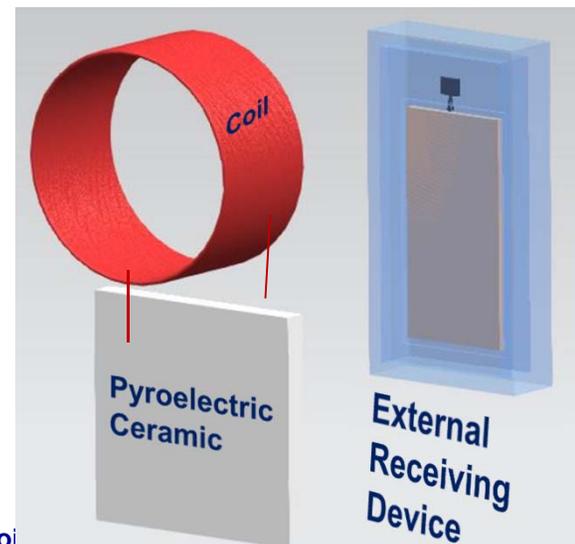
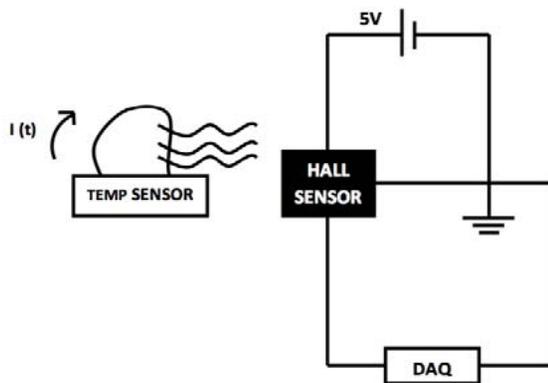
### □ Hall Sensor

- A hall effect sensor is a 3 wired sensor with reference voltage, a ground and a signal terminal
- Hall effect sensor is a transducer that varies its output voltage in presence of magnetic field
- Current flowing through a conductor in magnetic field perpendicular to the current flow would generate voltage perpendicular to both current flow and magnetic field



## Project Concept

- ❑ Low cost self-powered wireless temperature sensor
- Sensing mechanism is based on **pyroelectric ceramic**
- Pyroelectric ceramic **generates current** upon temperature changes
- Generated current will be converted into **magnetic flux** by connecting the ceramic to an inductive coil and measured wirelessly by an **external receiving device**



## Sensing Method

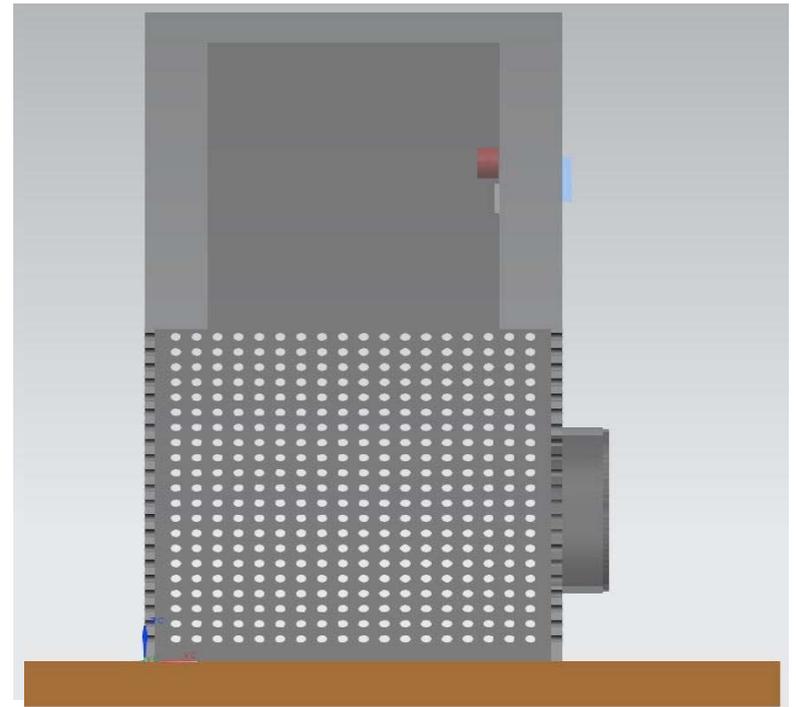
- The relation between magnetic flux and current can be described as below

$$T(f) = \frac{1}{pA} \int_{t_0}^{t_f} Idt + T(0)$$

$$\varphi = \frac{\mu_0 NIA}{w}$$

### ❑ Sensing device and processing unit

- Left side: wireless signal (Current induced magnetic flux) generated by sensor
- Right side: External receiver (Hall sensor) and Data acquisition unit





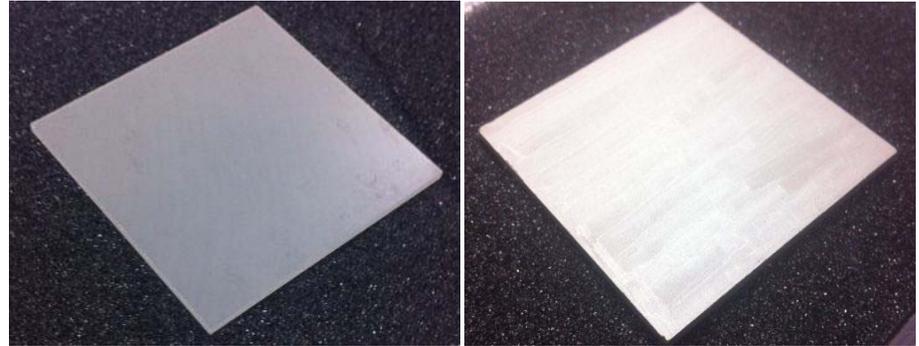
1. Determination of appropriate pyroelectric ceramics
2. Construct the wireless sensor system and demonstrate the wireless temperature sensing capability
3. Development of temperature sensor using pyroelectric properties of Lithium Niobate
  - Development of energy harvester using pyroelectric properties
4. Determine the wireless sensing performance in energy systems

# Technical Approach



## Objective 1: Determination of appropriate pyroelectric ceramic

- Pyroelectric materials include
  - Crystal (Lithium Tantalate)
  - Polymer (PVDF-Polyvinylidene Fluoride)
  - Ceramic (Lithium Niobate)
  - Biological materials
- Choice of pyroelectric materials depends on
  - Size & density
  - Availability and reliability
  - Maximum operation of temperature
  - Pyroelectric coefficient



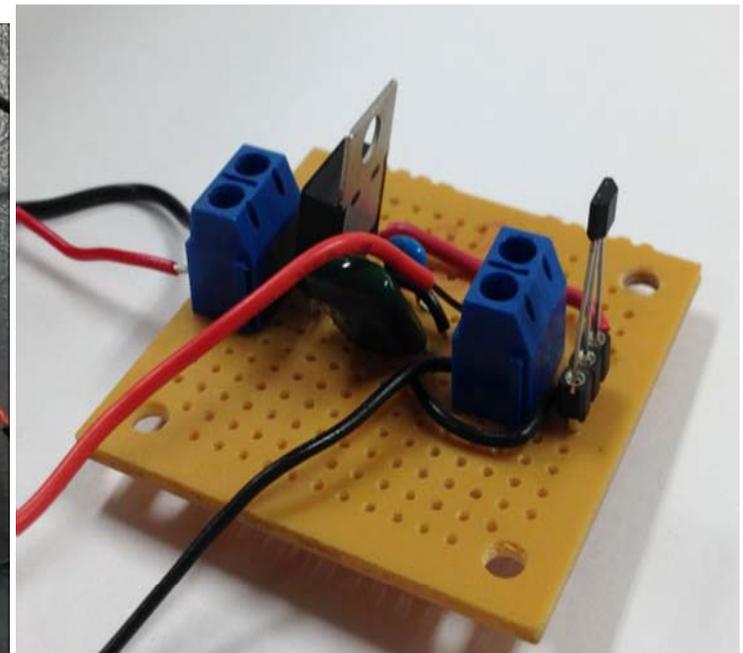
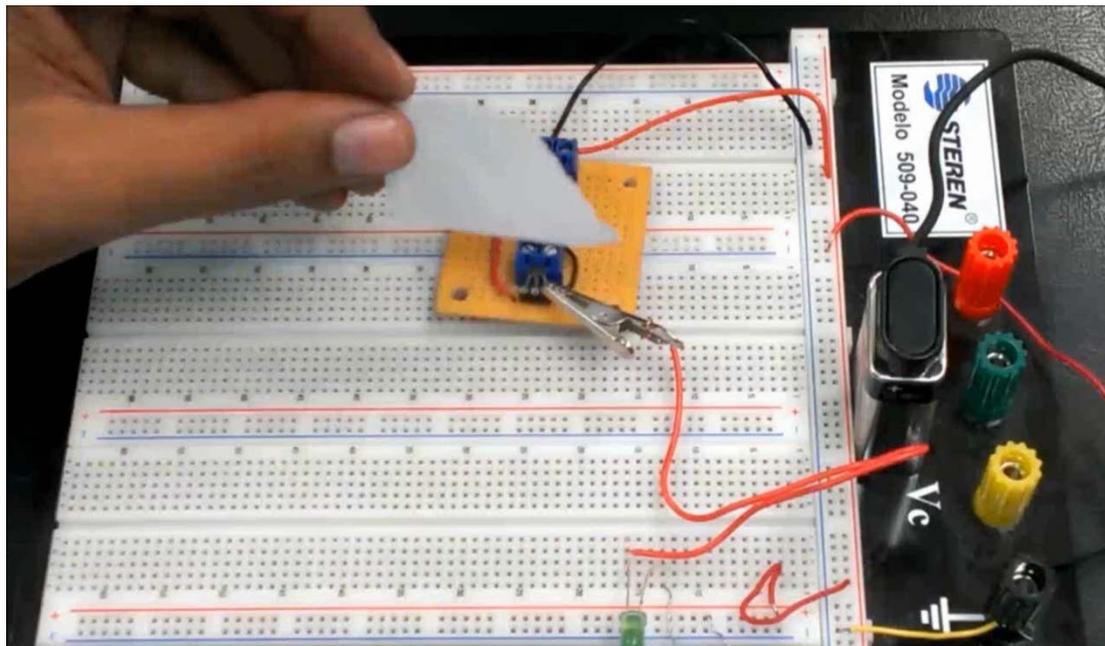
Dimension (LiNbO <sub>3</sub> )	50.8 × 50.8 cm and 2 mm in thickness
Density	4.65 g/cm <sup>3</sup>
<b>Curie Temperature</b>	<b>1142.3 ± 0.7° C</b>
Dielectric Constant (@ 25° C (unclamped <500 KHz)	$\epsilon_{11} = 85, \epsilon_{33} = 28.7$
<b>Pyroelectric Coefficient (@ 25° C)</b>	<b><math>-8.3 \times 10^{-5} \text{ C/}^\circ\text{Cm}^2</math></b>
Piezoelectric Strain Coefficients (@25°C × 10 <sup>-12</sup> C/N)	$d_{12} = 69.2$ $d_{31} = 0.85$ $d_{22} = 20.8$ $d_{33} = 6.0$
Thermal Conductivity (@ 25° C)	10 <sup>-2</sup> cal/cm.sec.°C

# Technical Approach



Objective 2: **Construct the wireless sensor system** and demonstrate the wireless temperature sensing capability

5.0 mV/Gauss ratiometric linear analog commercial Hall sensor from Allegro Micro Systems



# Technical Approach

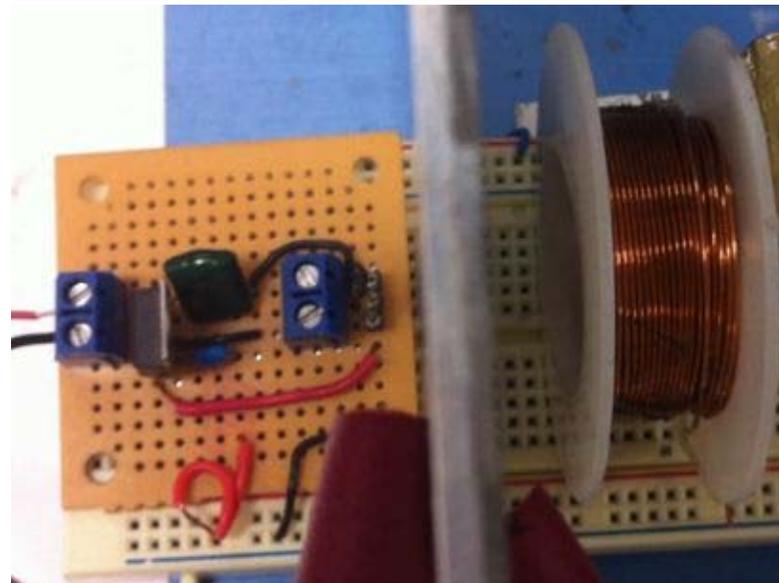
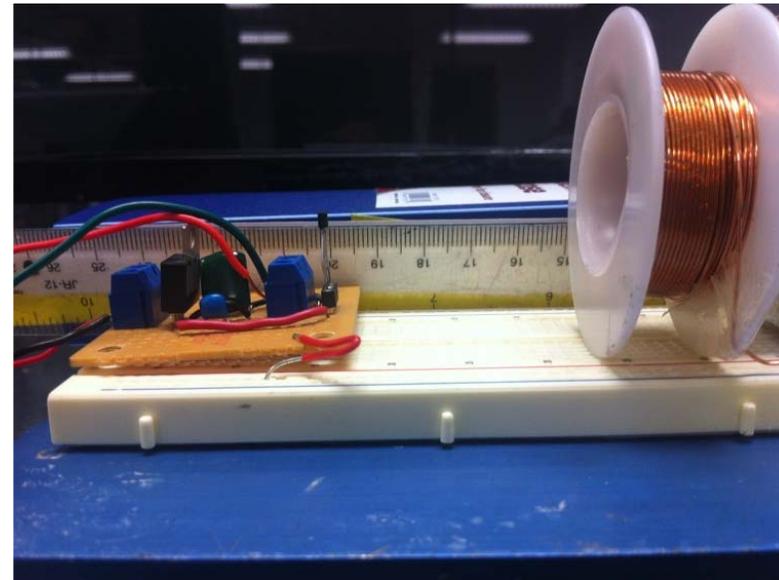


Objective 2: Construct the wireless sensor system and ***demonstrate the wireless temperature sensing capability***

□ Task

Magnetic Field Detection by Hall Effect Sensor

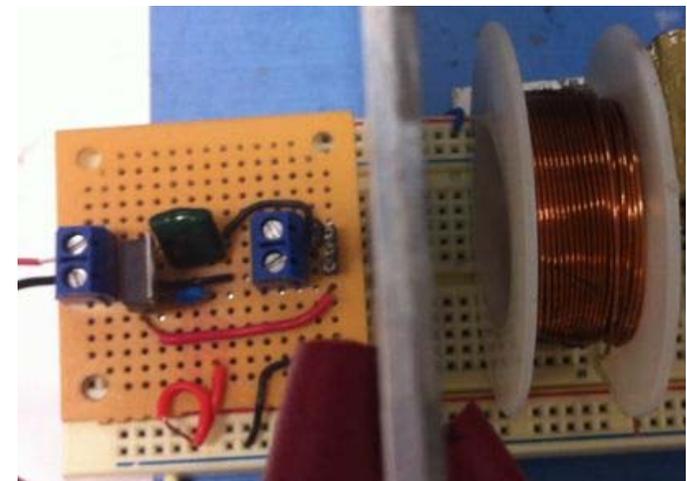
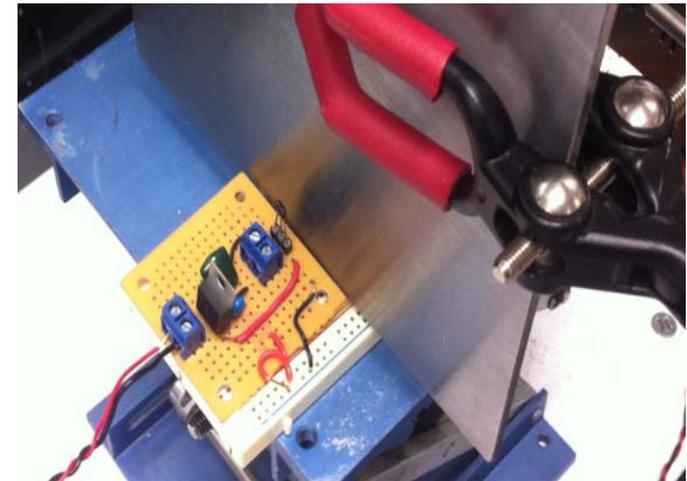
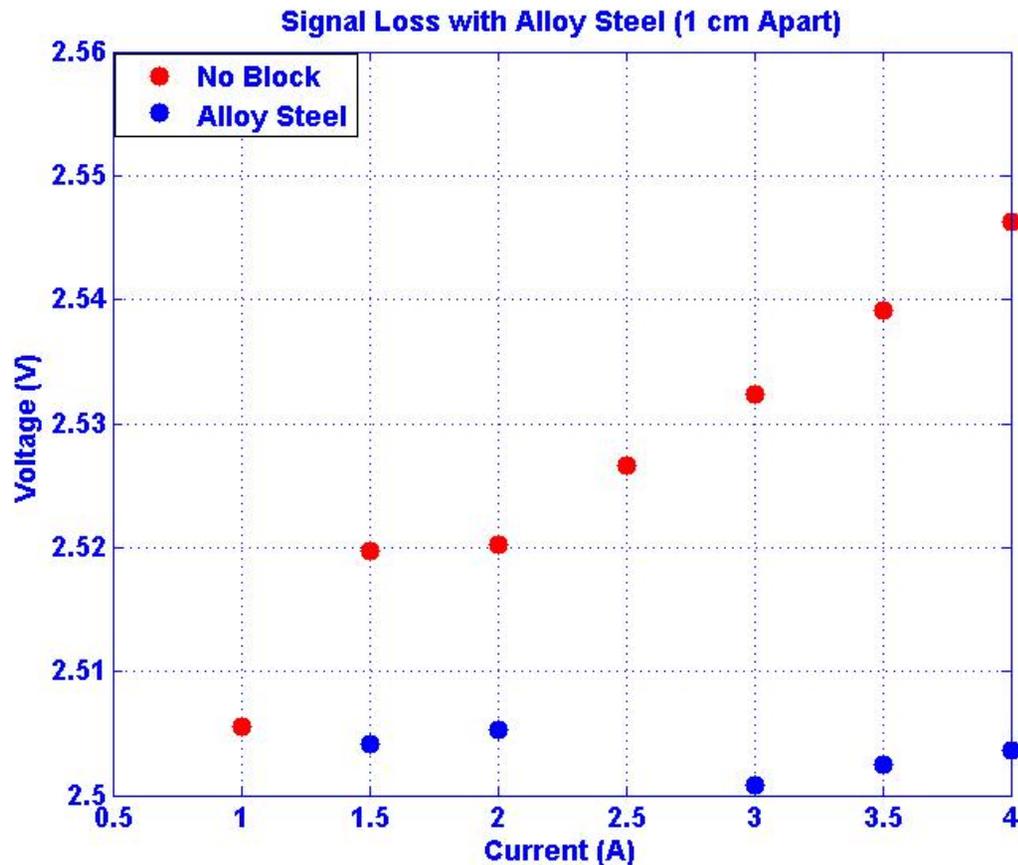
- Through Distances
- Through Material Blocks



# Results

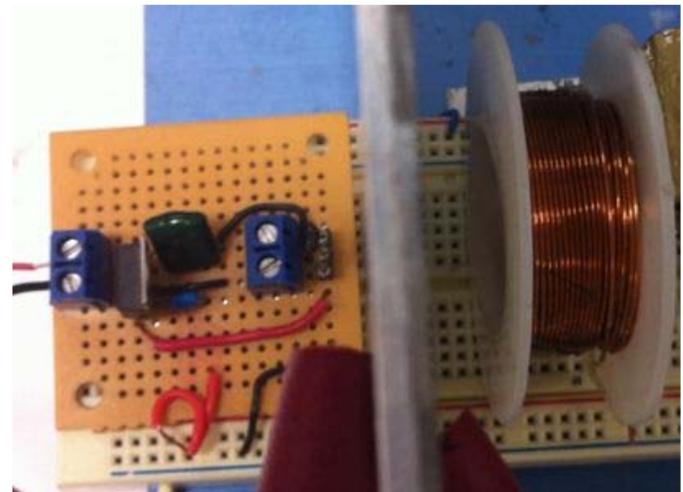
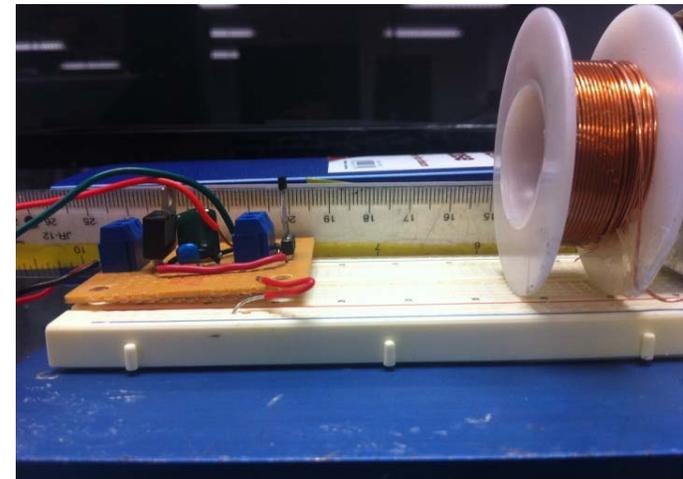
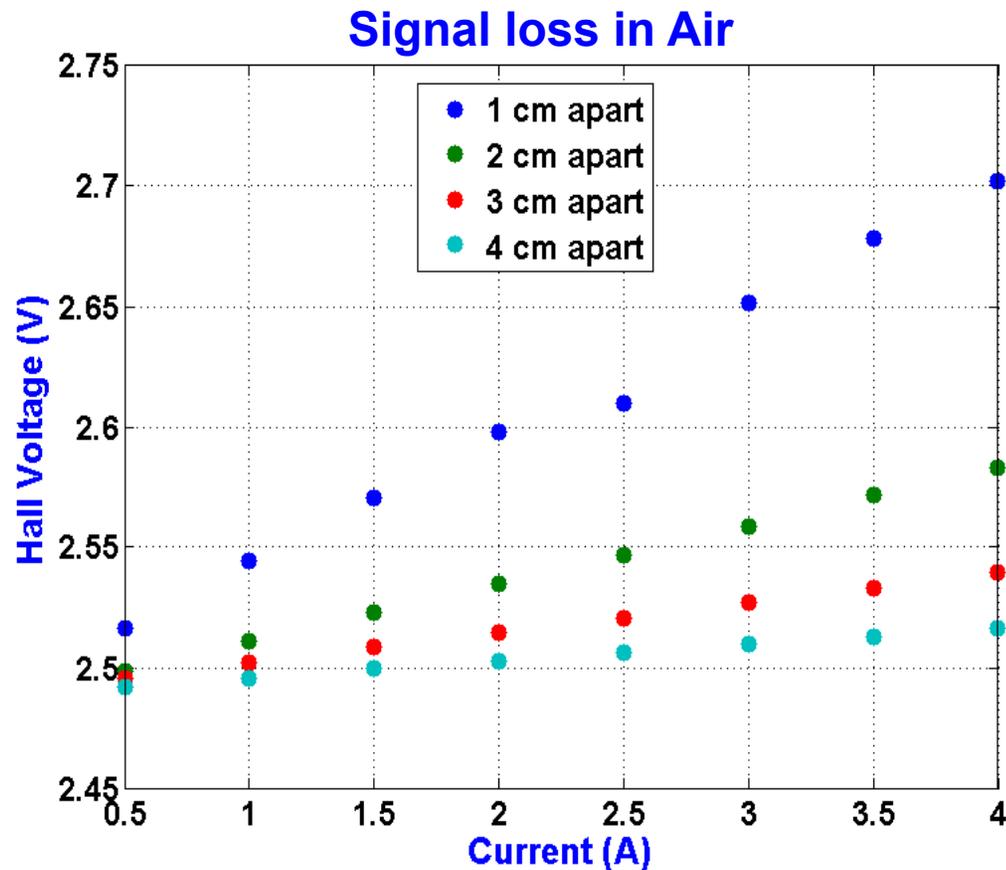


## Signal Loss with Various Materials



□ Current supplied to winded coil from external power supply

## Signal Loss for Various Distances

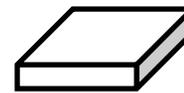
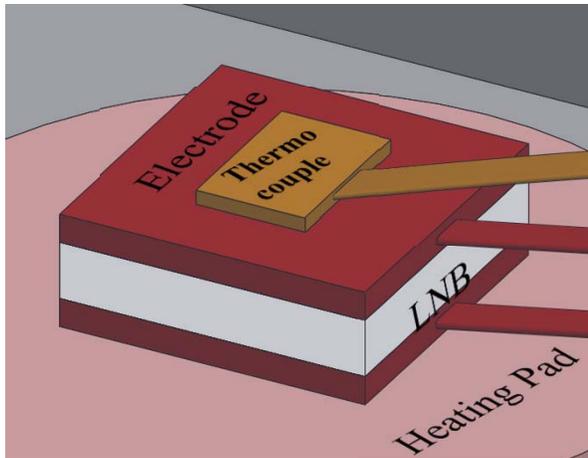


□ Current supplied to winded coil from external power supply

# Technical Approach



Objective 3: Development of temperature sensor using pyroelectric properties of Lithium Niobate

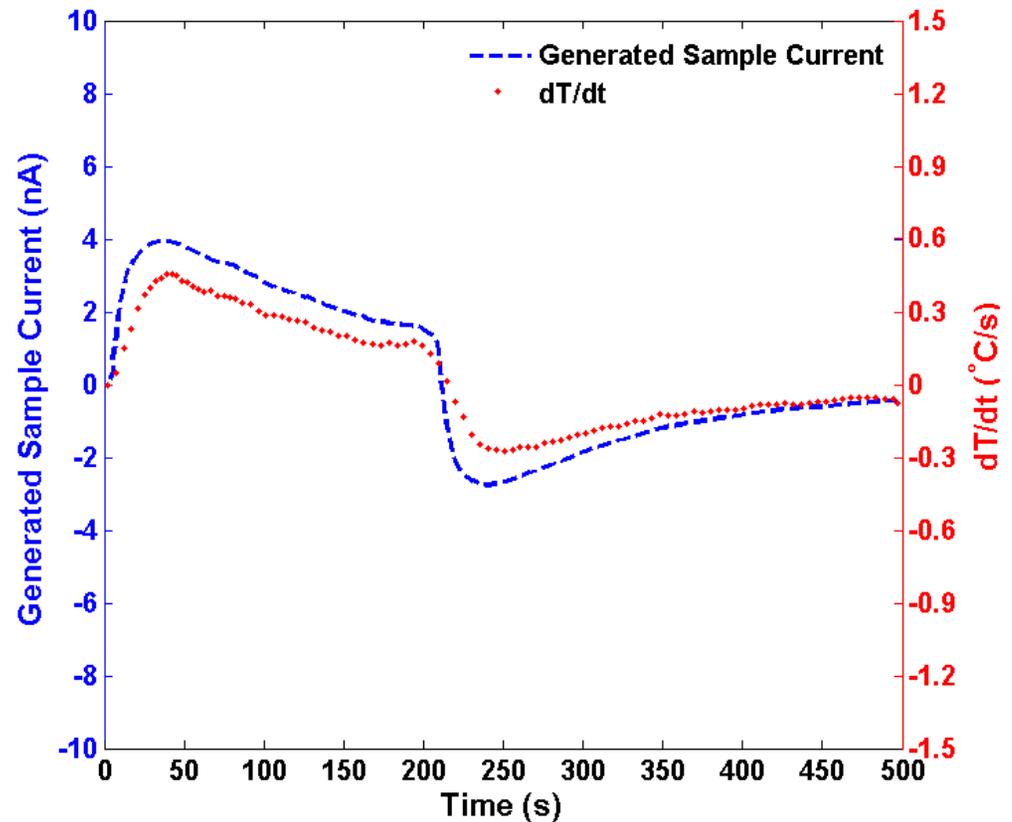
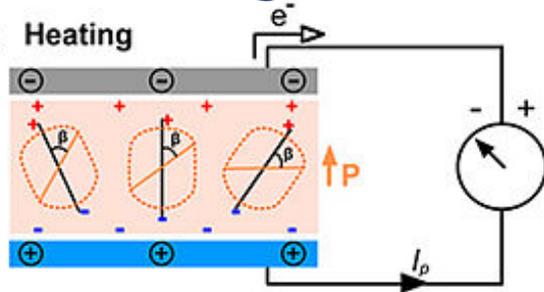


10×10×2 mm  
10×10×1 mm

## Pyroelectric Current

$$I = -pA \left( \frac{dT}{dt} \right)$$

$dT/dt > 0$  Heating

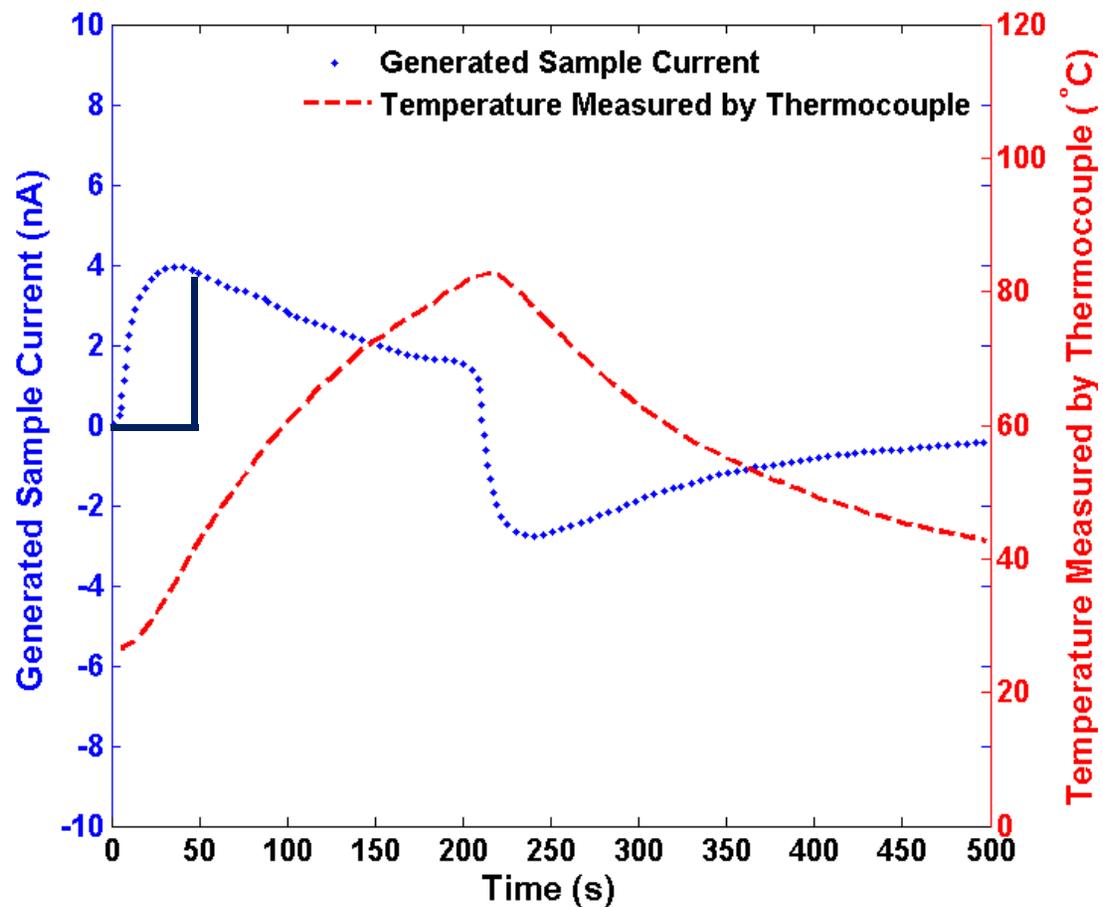


## Pyroelectric Current

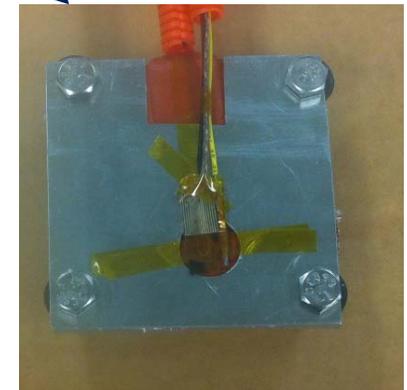
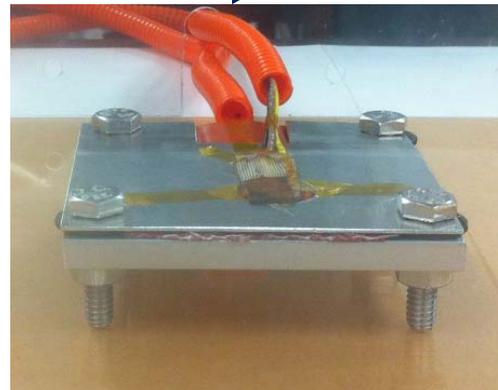
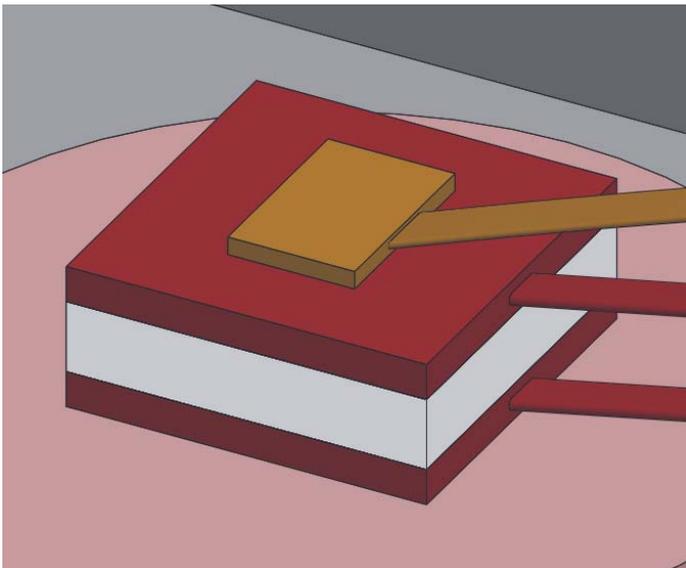
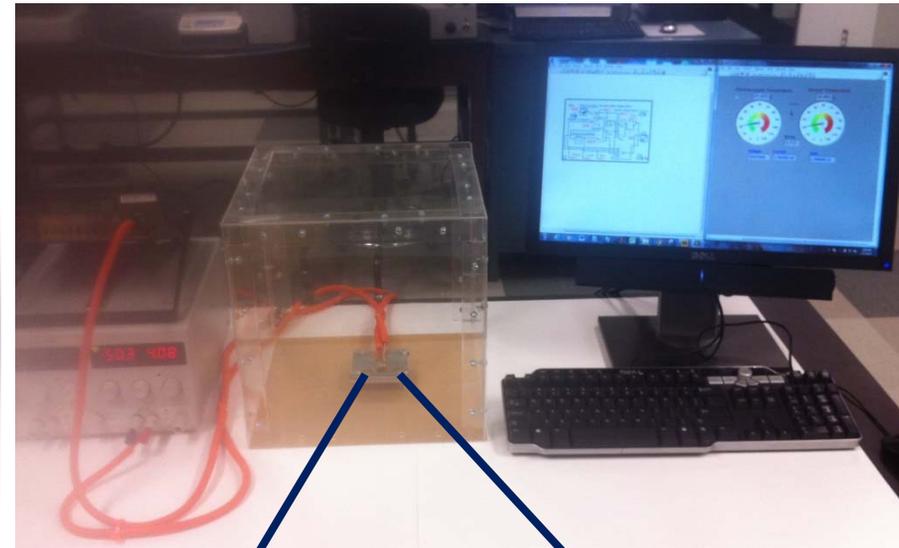
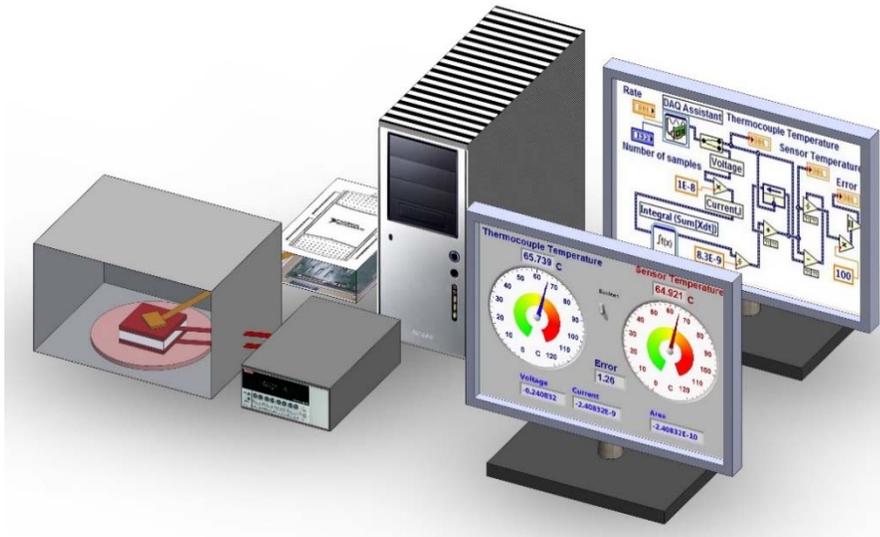
$$I = -pA \frac{dT}{dt}$$

$$T_f = -\frac{1}{pA} \int_{t_i}^{t_f} I dt + T_i$$

50s



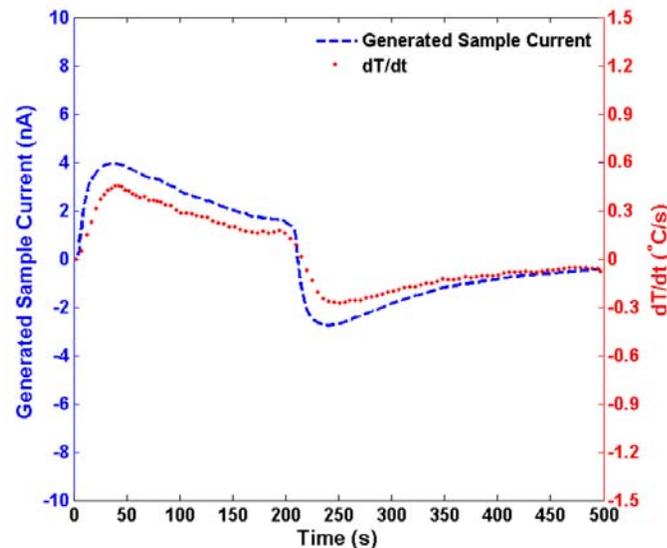
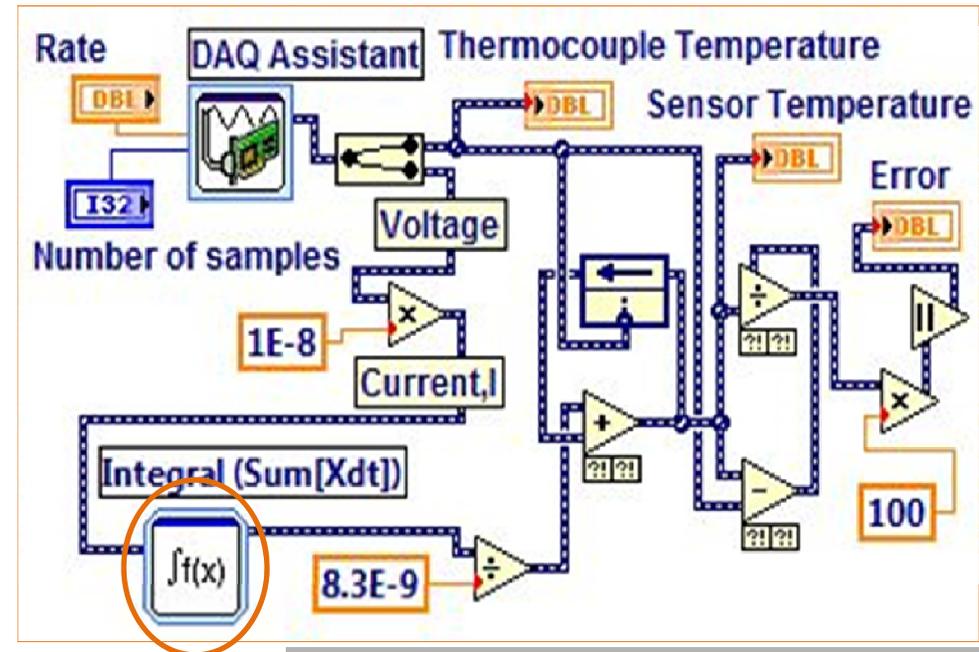
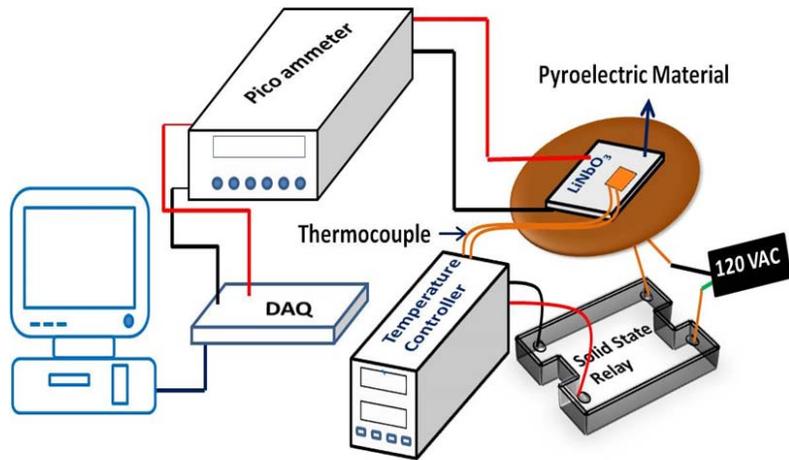
# Experimental Setup



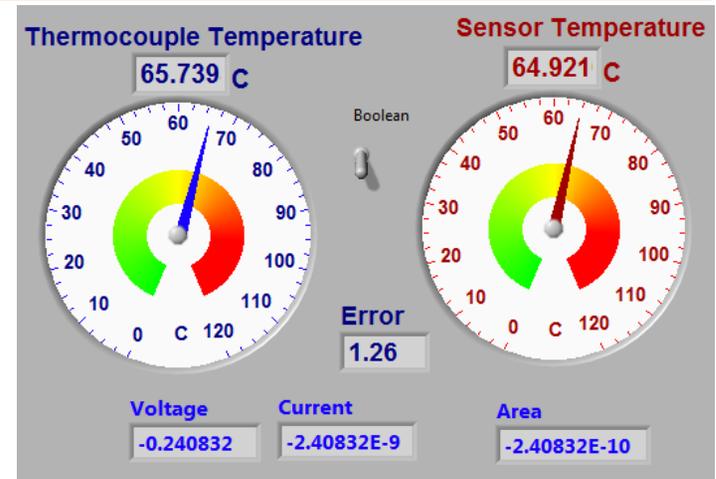
# Experimental Setup



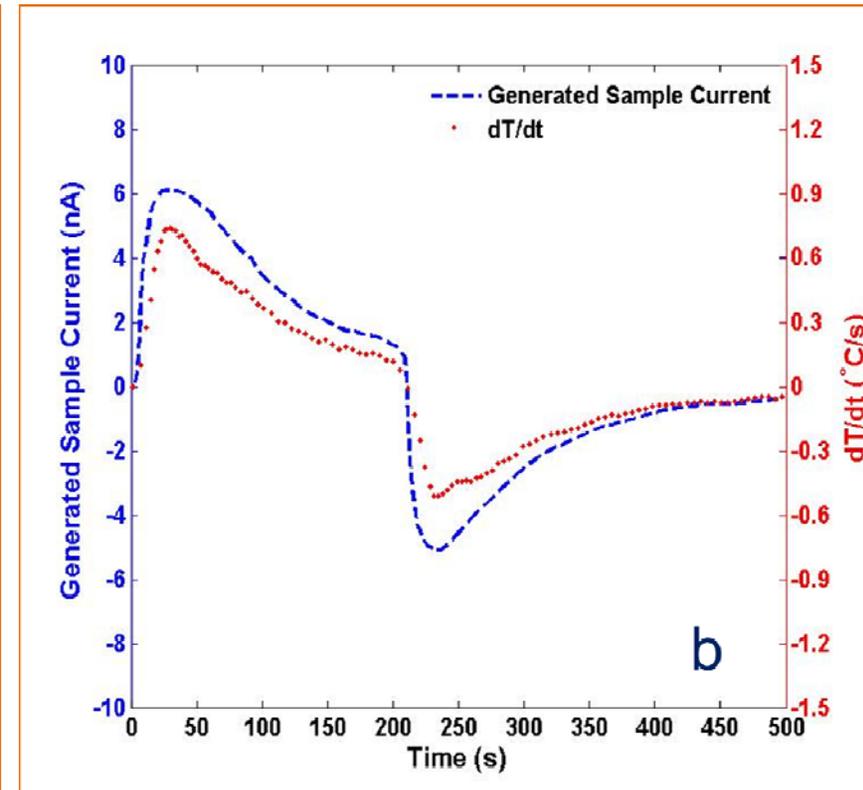
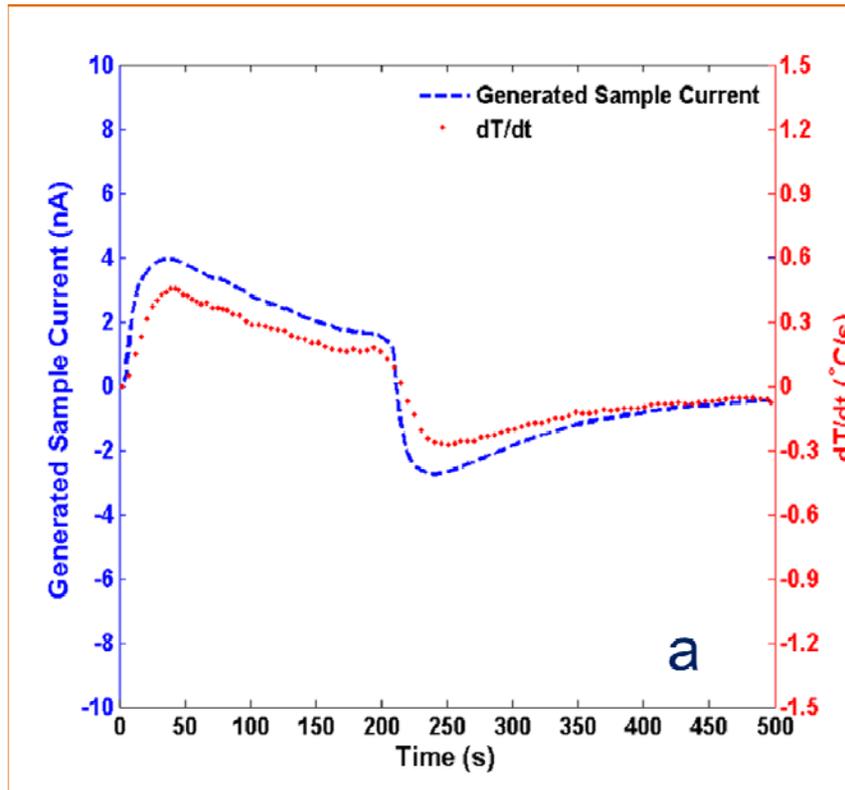
## Data Acquisition



$$T_f = -\frac{1}{pA} \int_{t_i}^{t_f} I dt + T_i$$

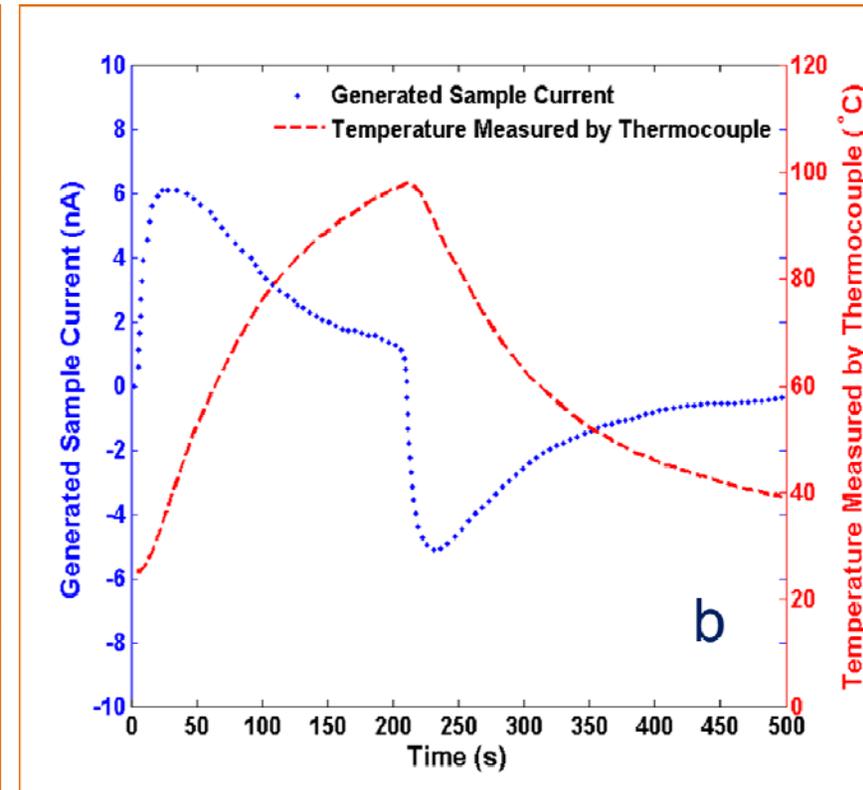
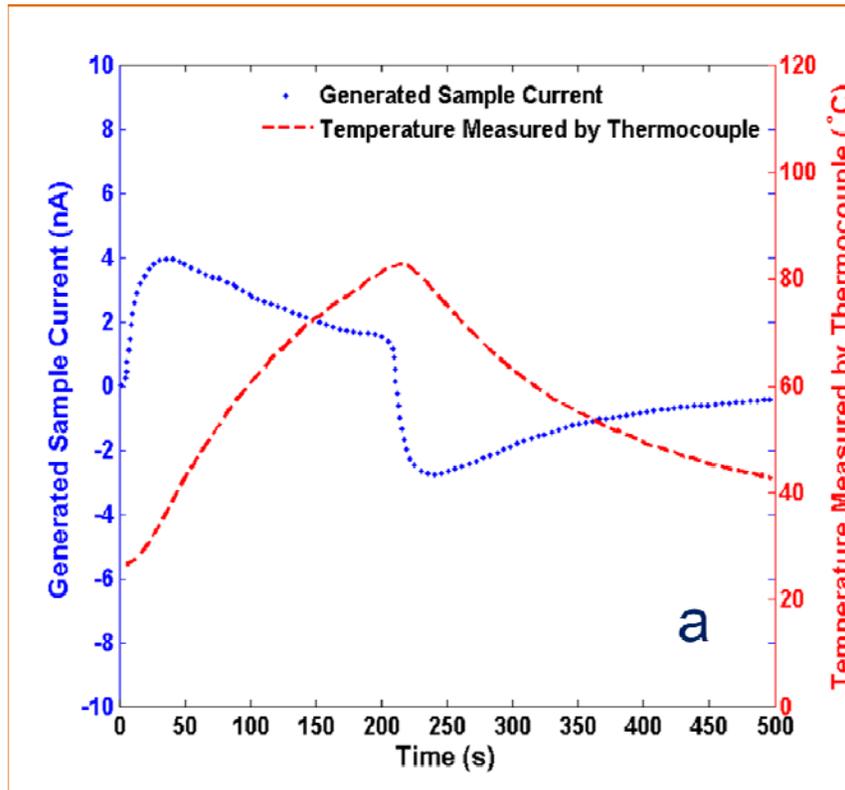


# Results



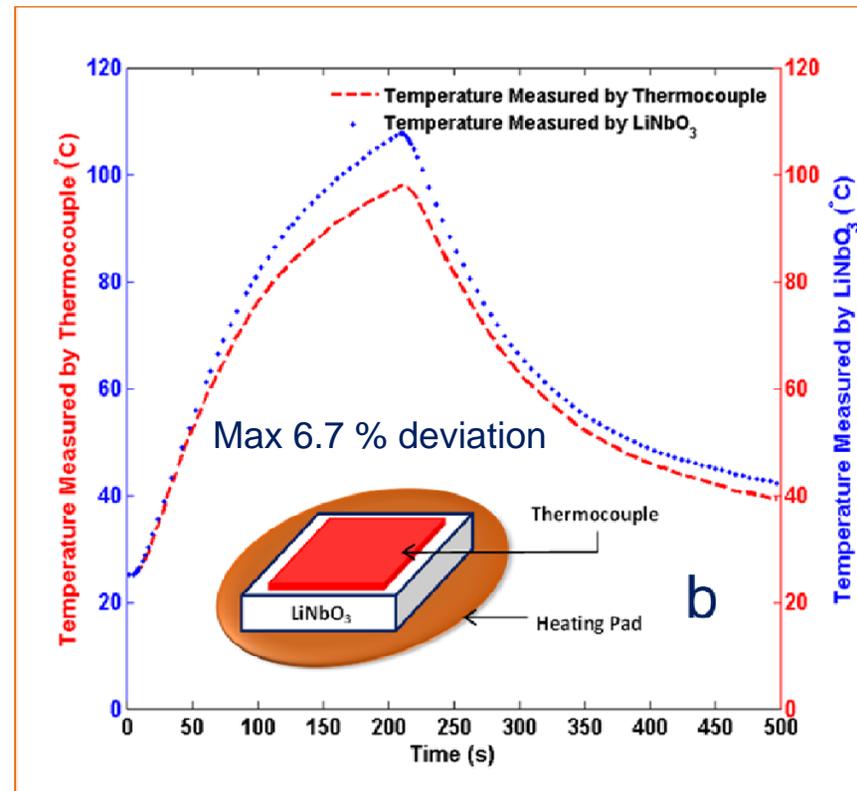
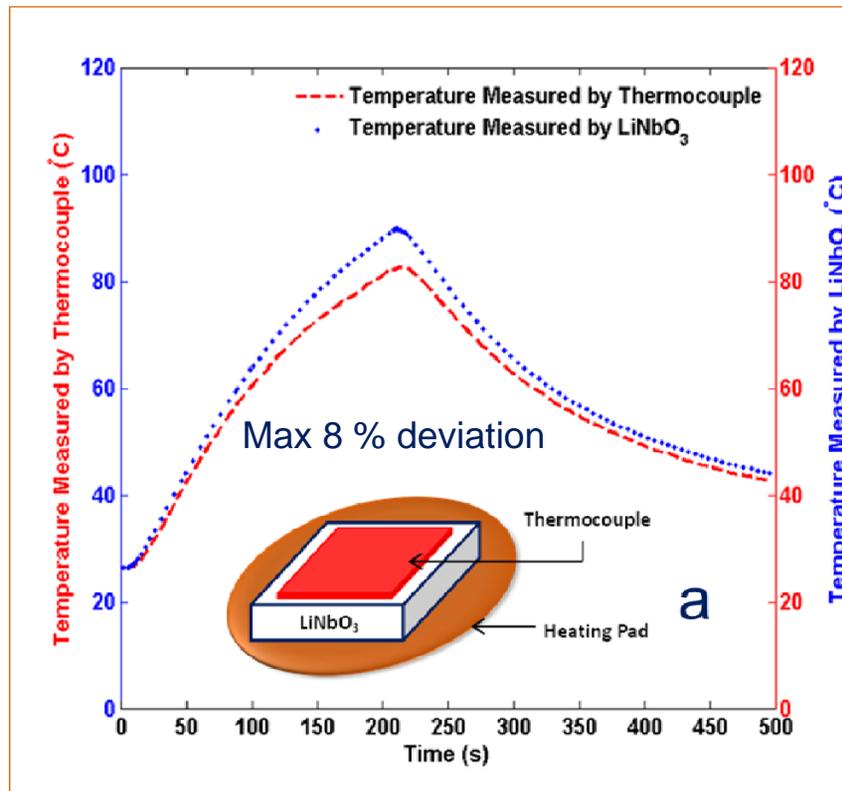
Generated current by LiNbO<sub>3</sub> and rate of temperature change of thermocouple mounted on top of (a) 2 mm and (b) 1 mm thick LiNbO<sub>3</sub>

# Results



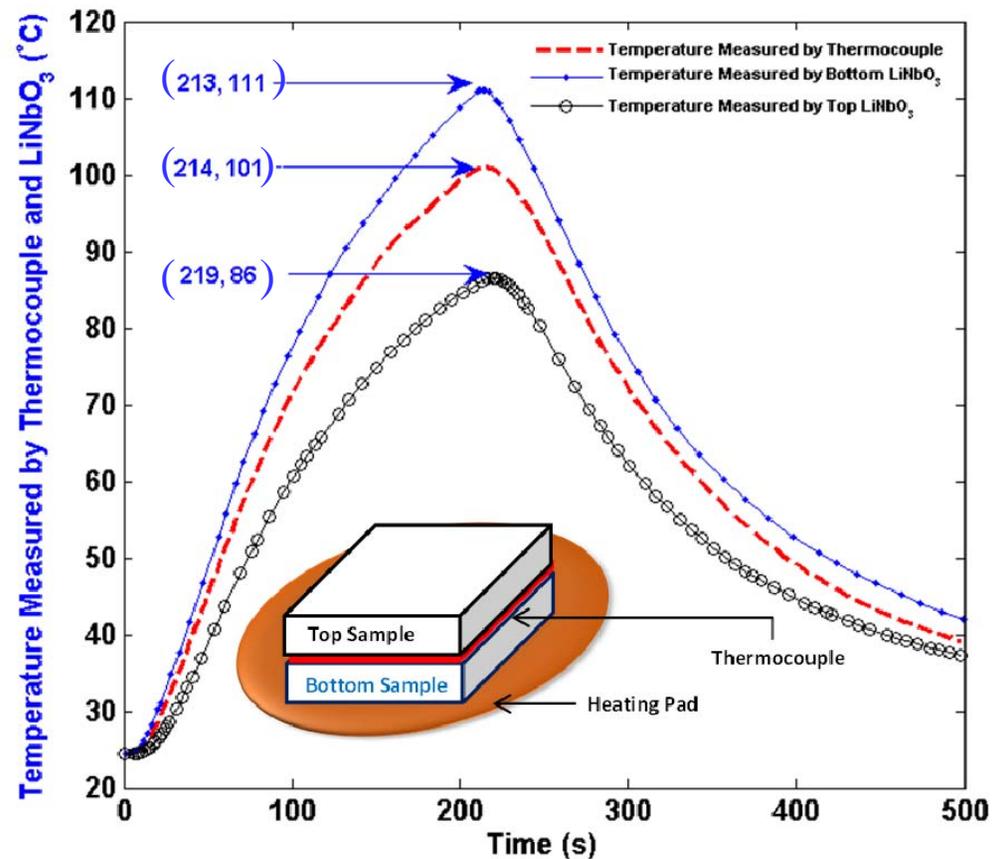
Generated current by LiNbO<sub>3</sub> and temperature of thermocouple mounted on top of (a) 2 mm thick LiNbO<sub>3</sub> and (b) 1 mm thick LiNbO<sub>3</sub>

# Results



Temperature measured by thermocouple and (a) 2 mm thick and (b) 1 mm thick LiNbO<sub>3</sub>

# Results



Temperature measured by the thermocouple and 1 mm thick sandwich structured LiNbO<sub>3</sub>

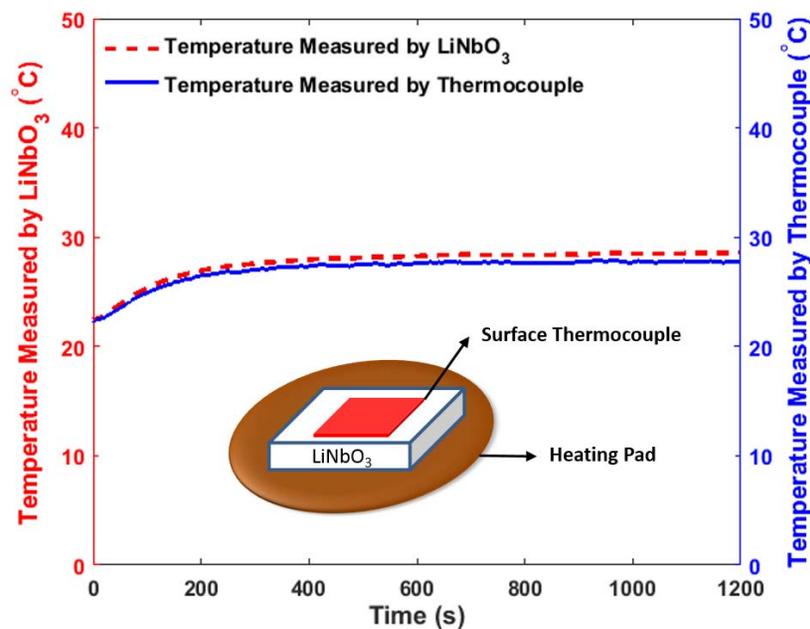
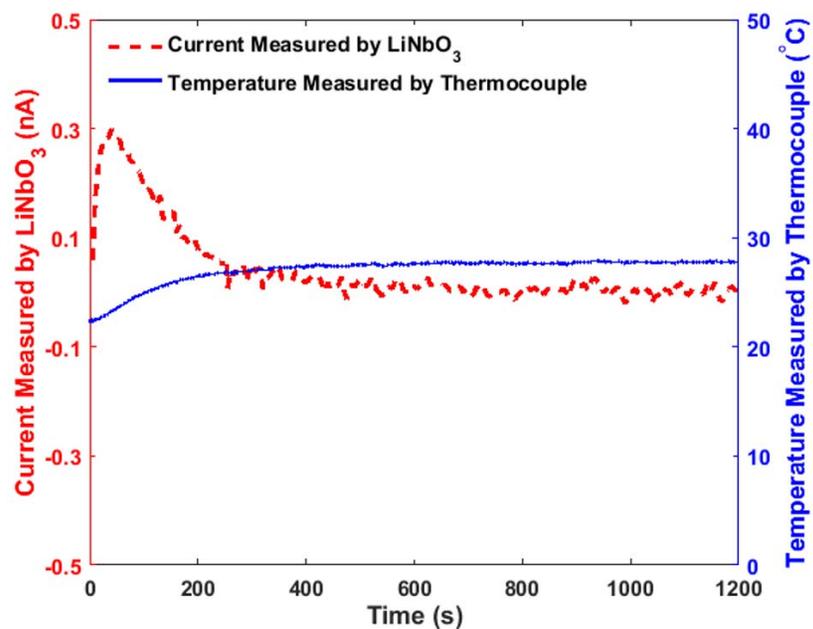
# Results



## ☐ Slow Heating Rate

22.50 °C to 27.75 °C within 650 s

Average  $dT/dt = 0.008 \text{ } ^\circ\text{C/s}$



# Results

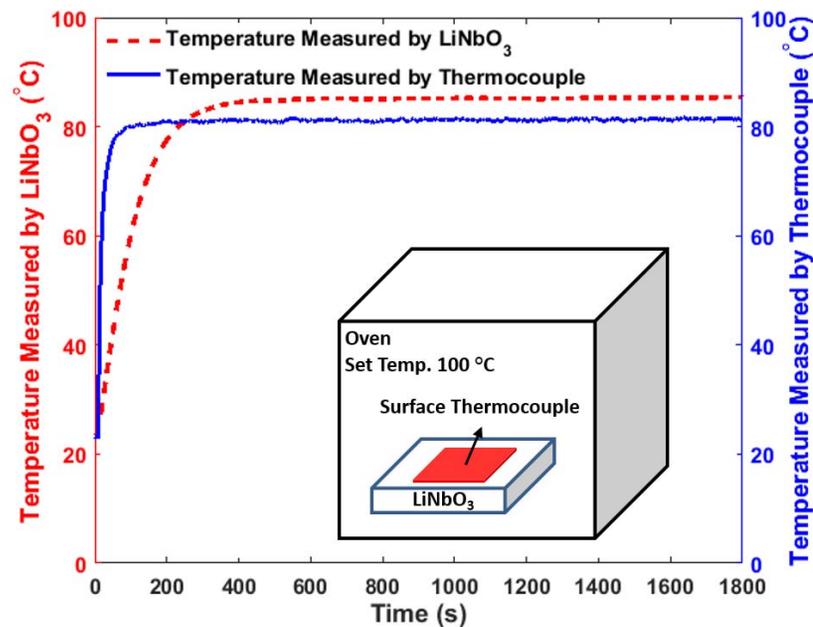
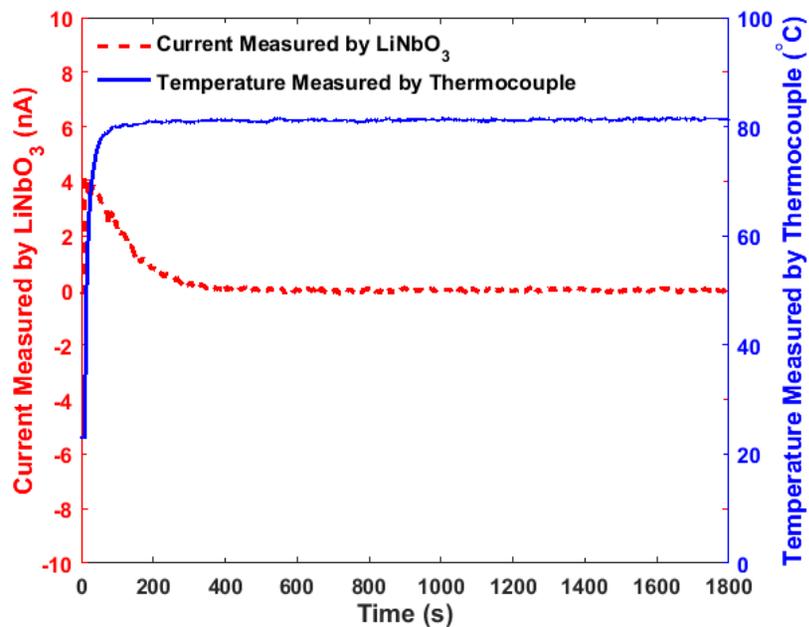


□ High Heating Rate

25 °C to 81 °C within 190 s

Average  $dT/dt = 0.3 \text{ } ^\circ\text{C/s}$

Oven Pre-heated set Temp. 100 °C

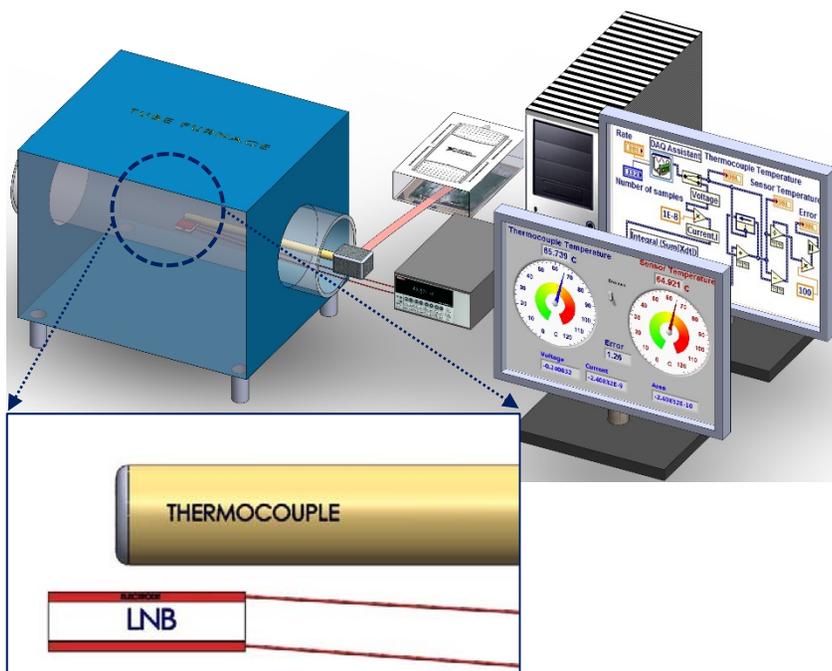


## High temperature Measurement

### Tube furnace Set Temperature

1. 25 °C to 300 °C with 0.25 °C/s
2. 25 °C to 400 °C with 0.25 °C/s
3. 25 °C to 500 °C with 0.33 °C/s

$$I = -pA \frac{dT}{dt} ; -p \text{ is a function of temperature}$$



**Tube Furnace**

04/19/16

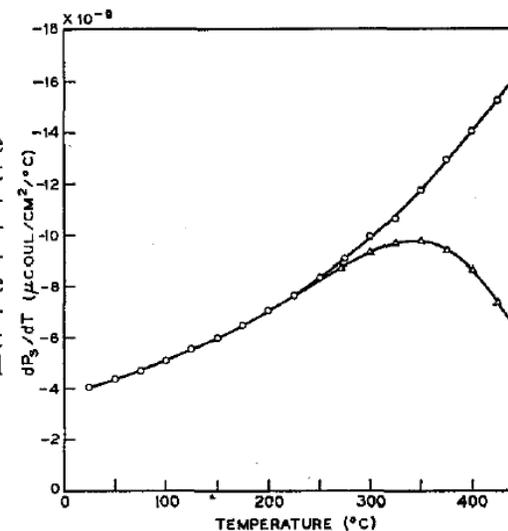
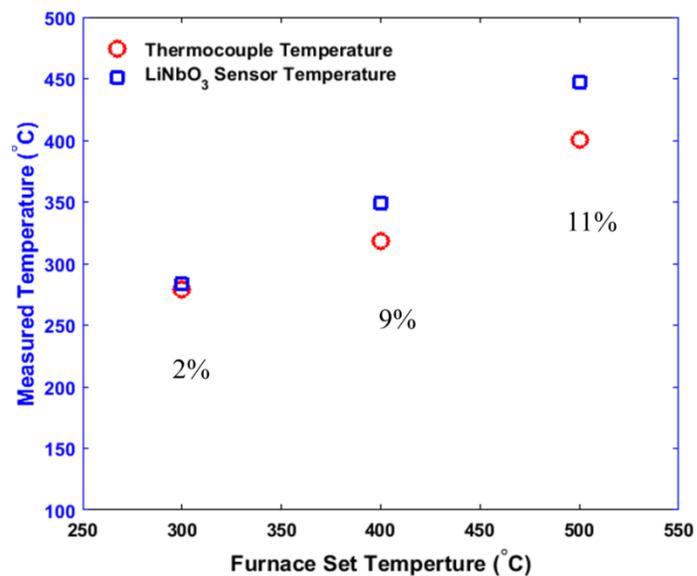
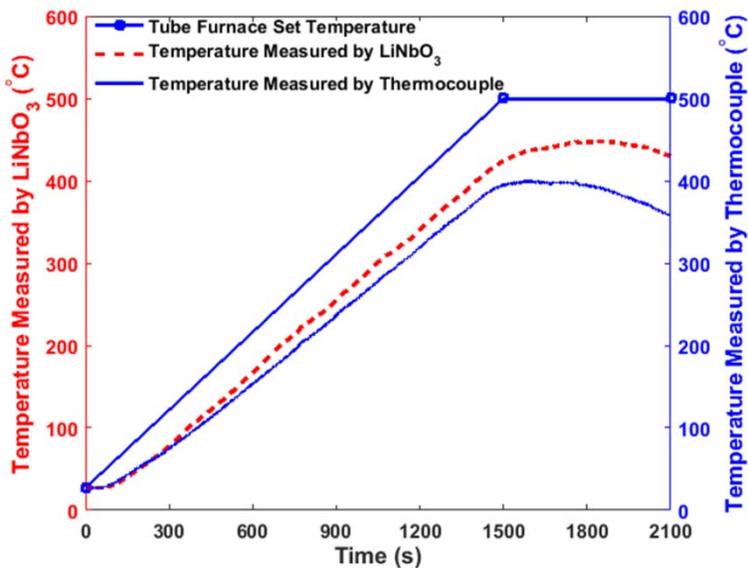
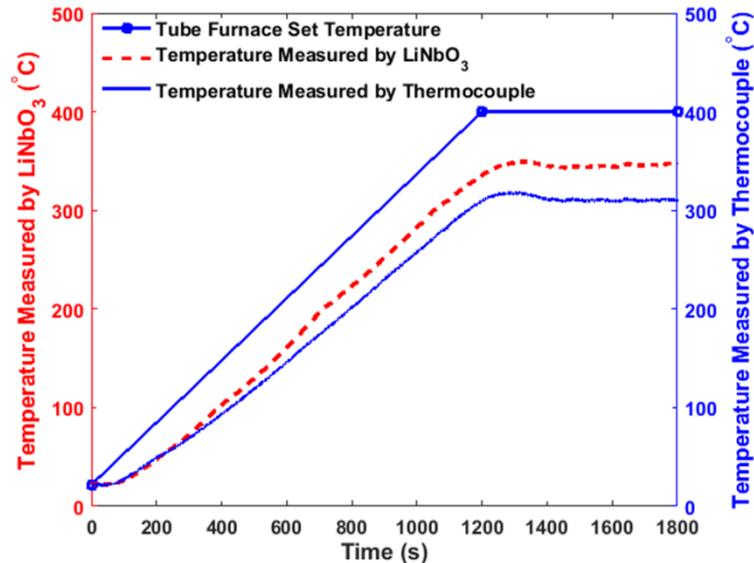
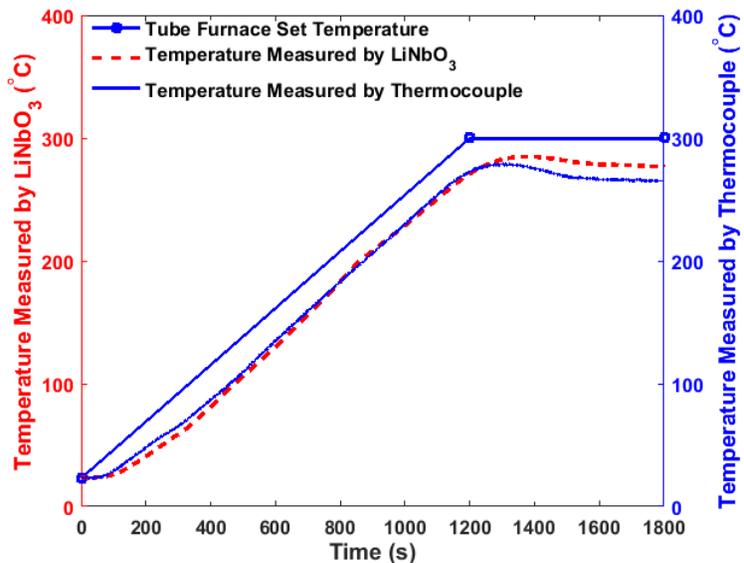


FIG. 1. Plot of the pyroelectric coefficient as a function of temperature. Triangles— $dP_s/dT$  prior to correction for the sample resistance; circles—pyroelectric coefficient after the data had been corrected.

Savage, A. "Pyroelectricity and spontaneous polarization in LiNbO<sub>3</sub>," *Journal of Applied Physics* 37, no. 8 (1966): 3071-3072.

# Results

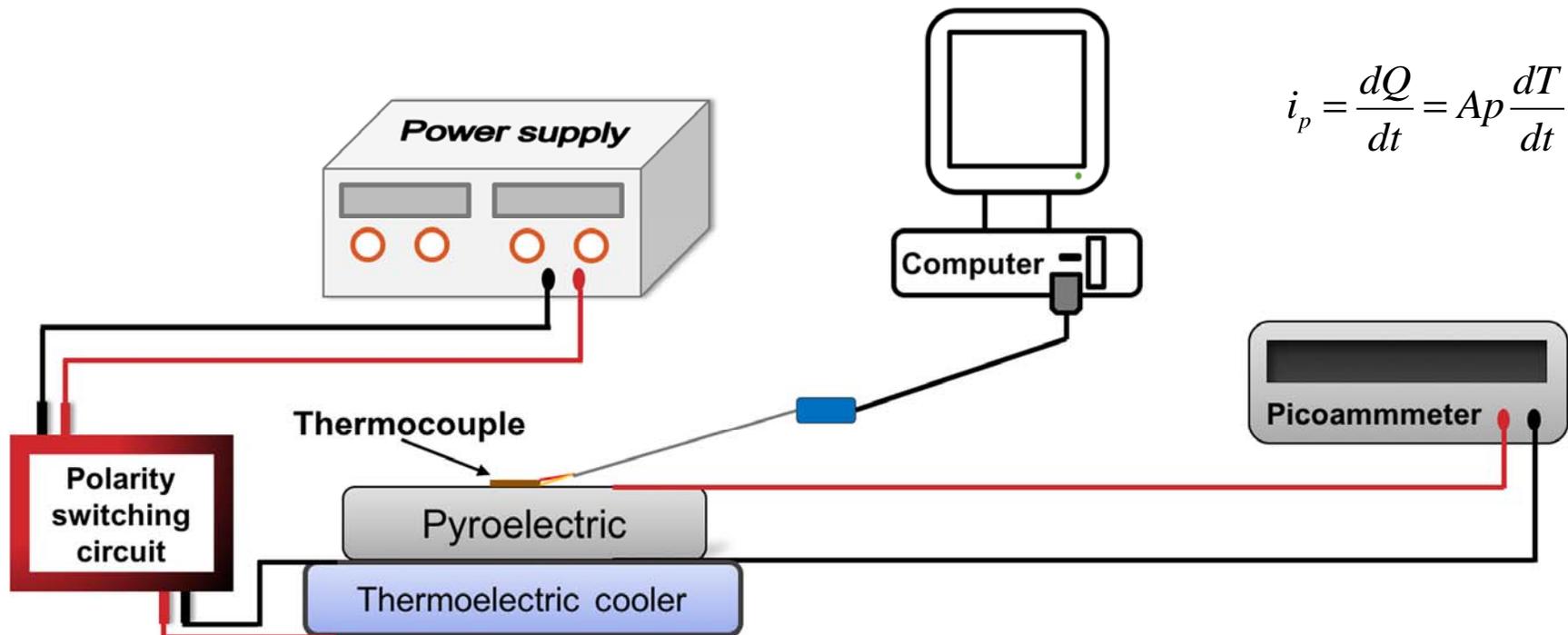
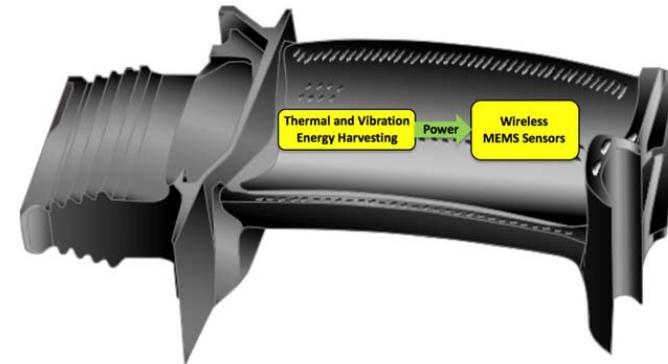


# Development of Energy Harvesting

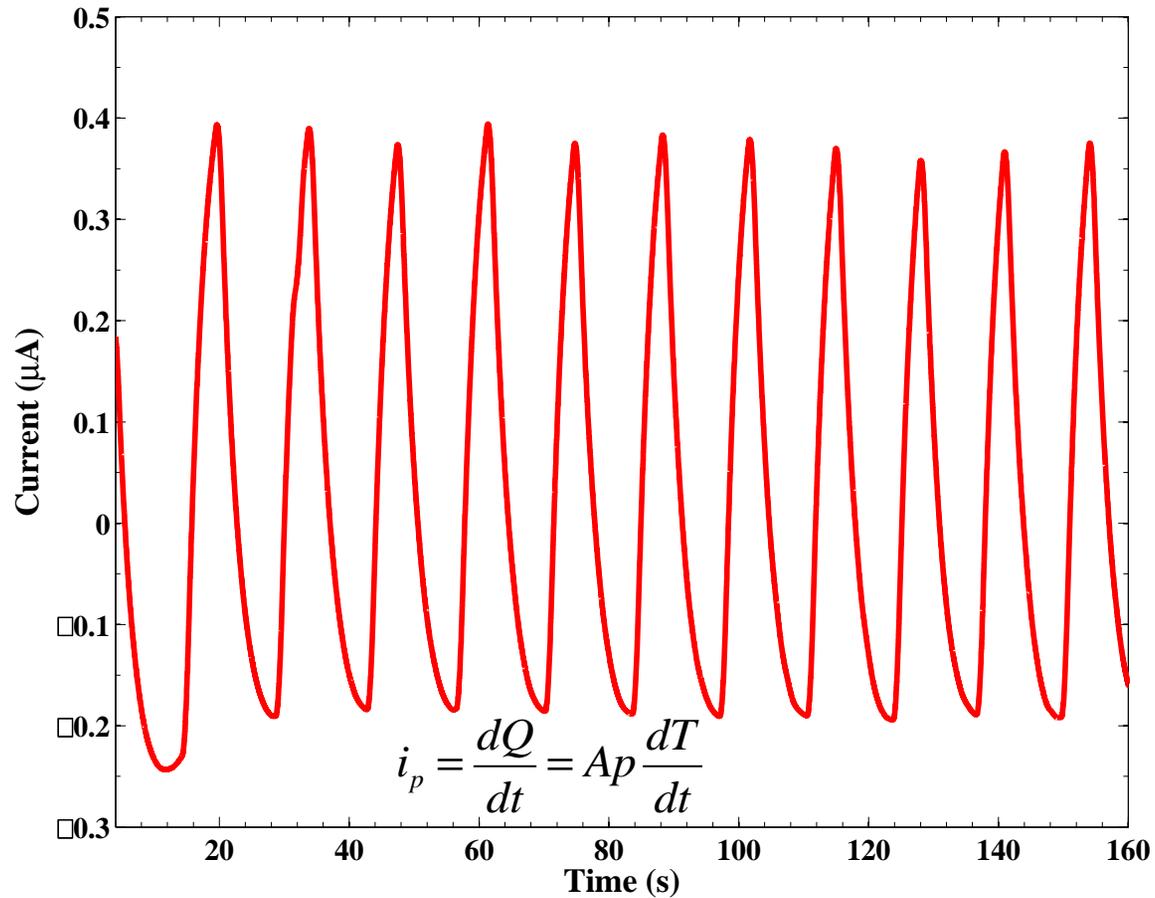


**Direct sensing:** Temperature sensing

**Indirect sensing:** Energy harvesting

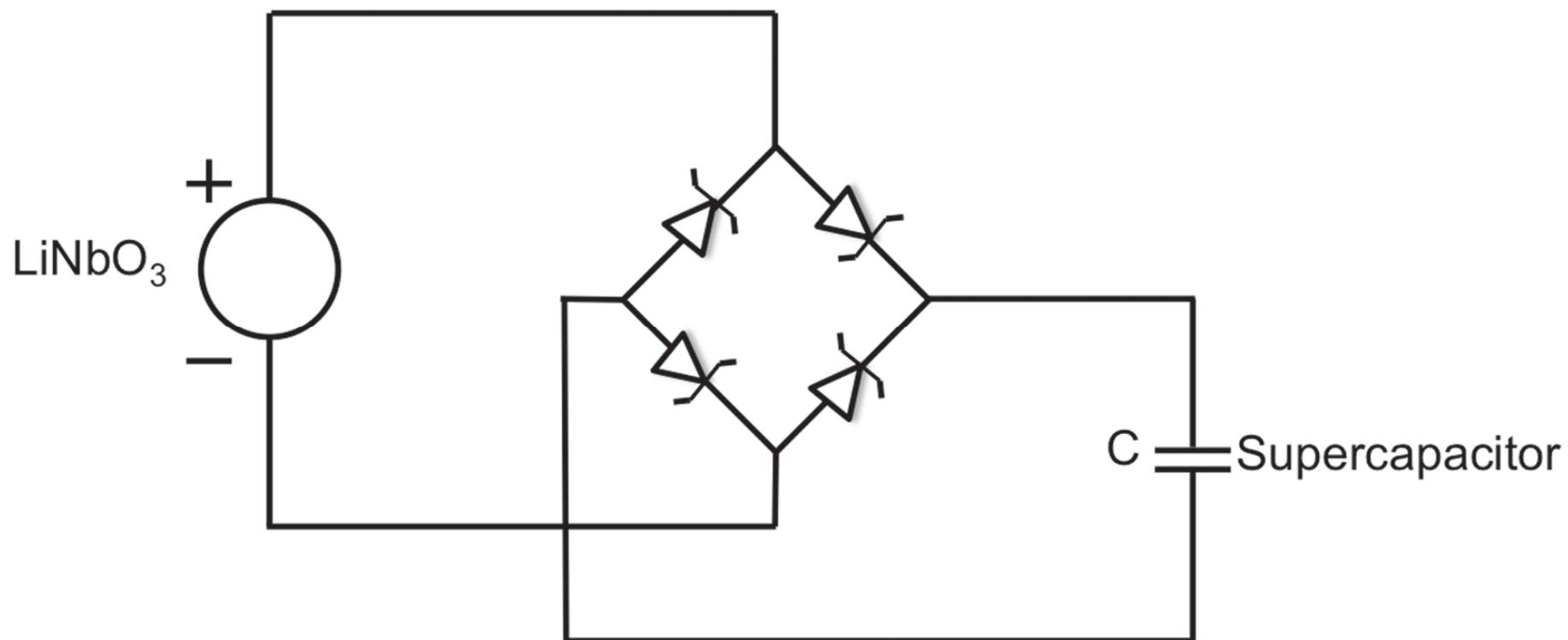


# Results - Harvesting



Current generated from  $\text{LiNbO}_3$  with continuous heating and cooling

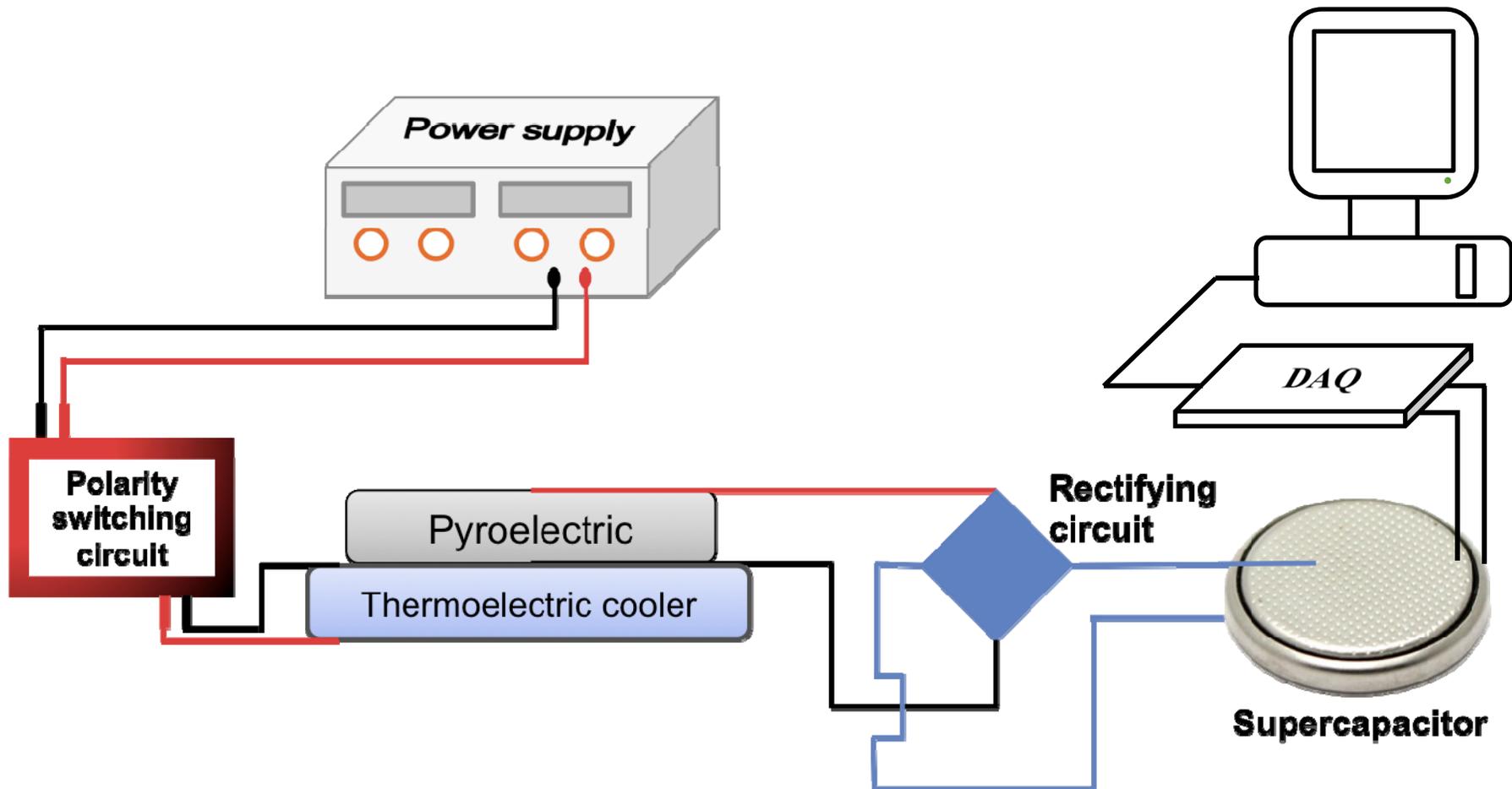
# Results – Harvesting Circuit



# Results - Harvesting



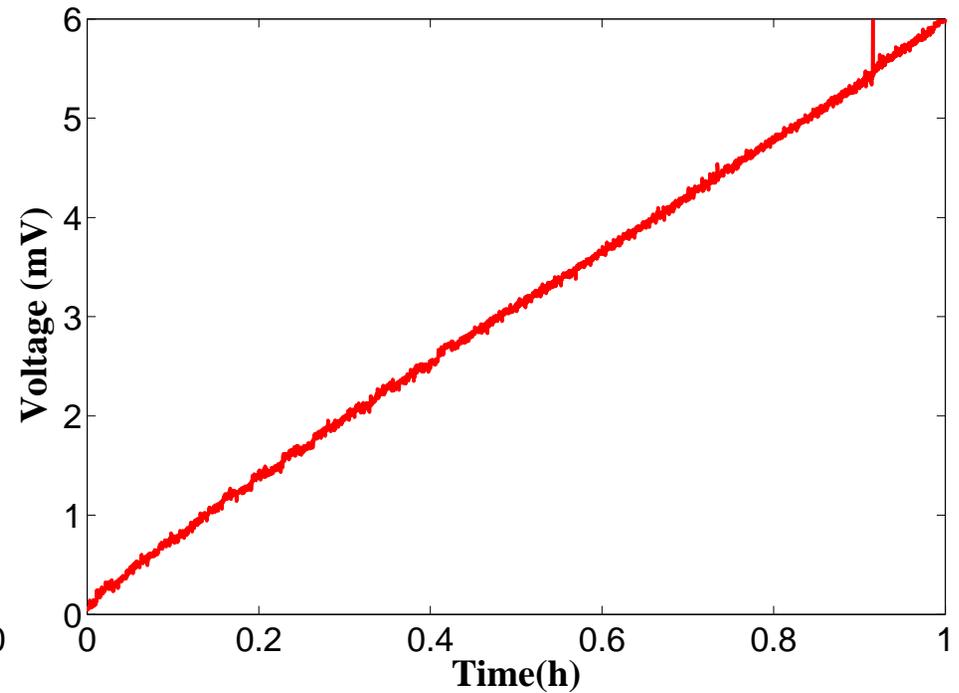
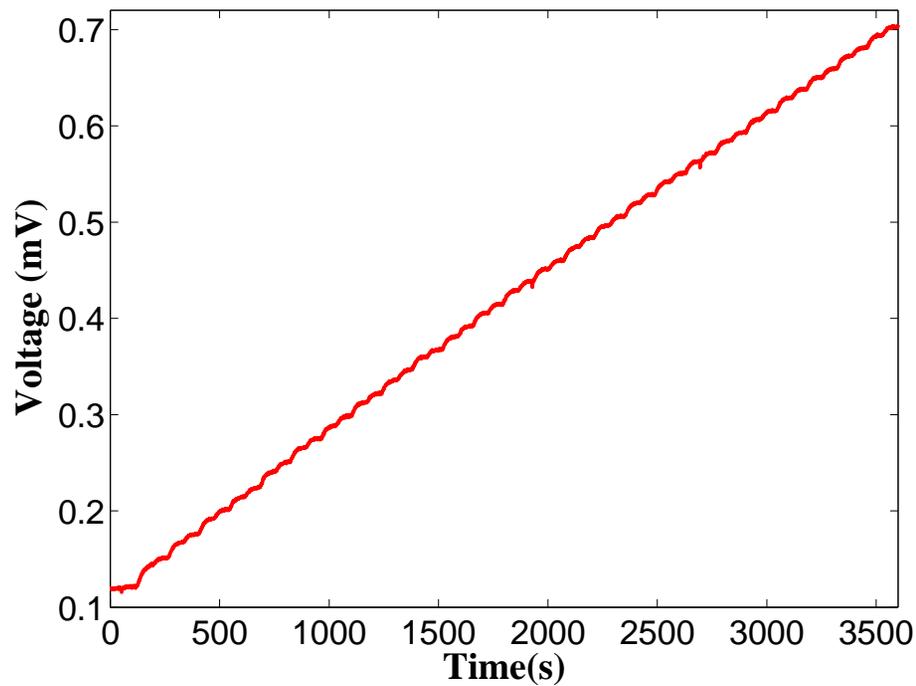
Experimental setup for Supercapacitor charging



# Results - Harvesting



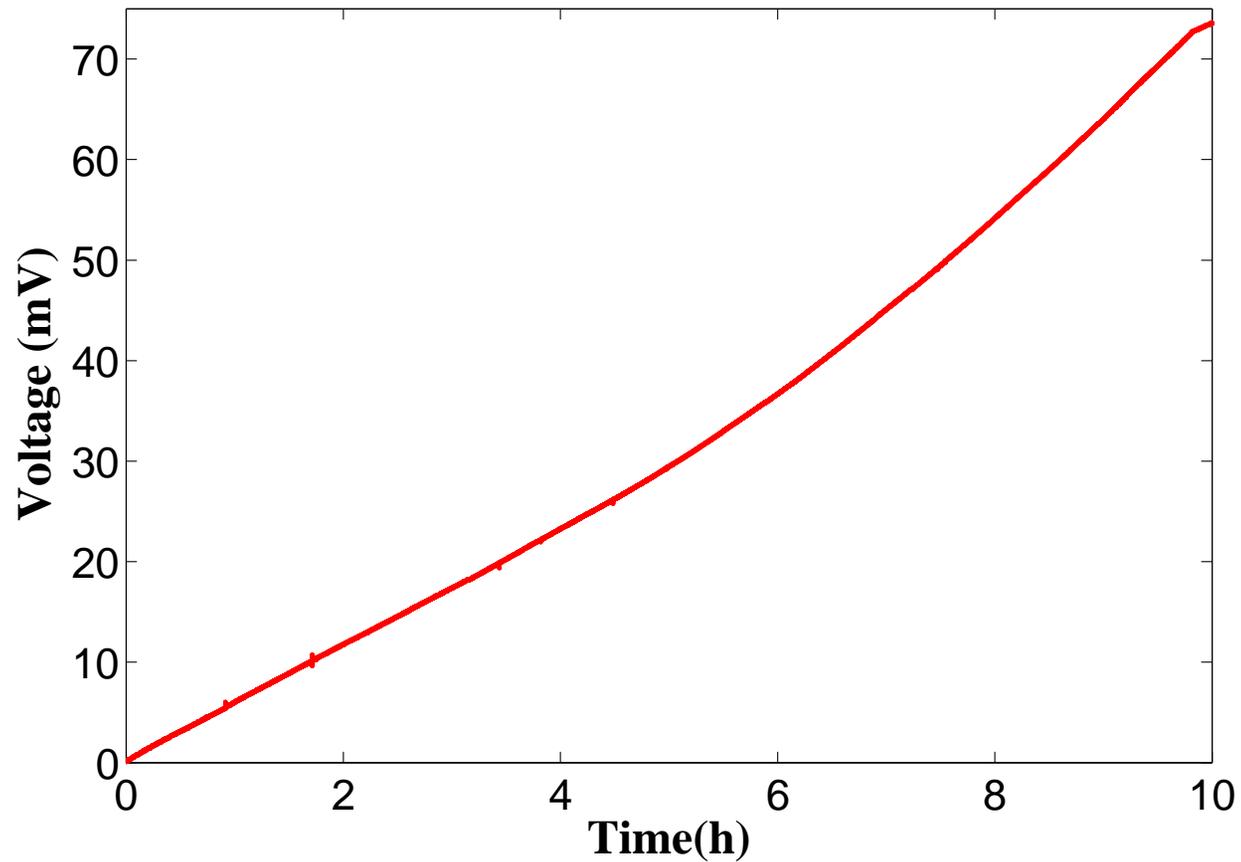
Comparison of diode NTE573 (left) vs HFA15TB60PBF (right)



# Results - Harvesting



Charging commercial supercapacitor with HFA15TB60PBF diode



# Technical Approach: Wireless Demonstration



Objective 4: Determine the wireless sensing performance in energy systems

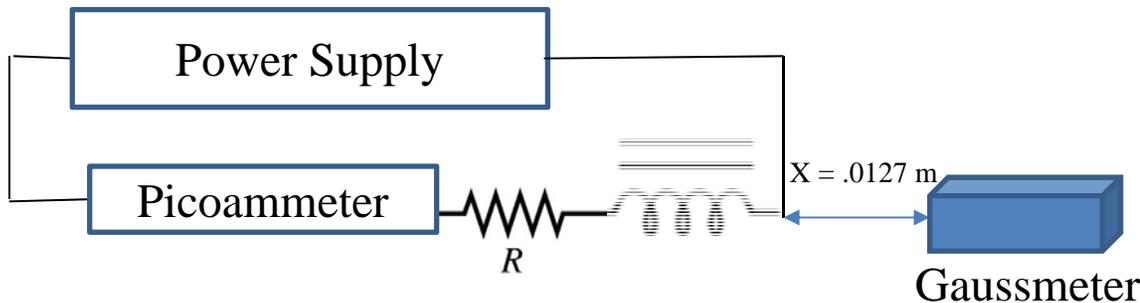
No core material Inside the electromagnet

Characterizing the Coil and Gaussmeter



Length .017 m  
 Inner radius .0127 m  
 Outer radius .02413 m  
 Number turns 6740  
 Magnetic wire resistance 1100 ohm

Applied Current.	Measured Field(milligauss)	Expected Field(milligauss)	Error %
2.50E-03	1639.2	1718.4	4.6
1.00E-03	660.5	687.36	3.91
5.00E-04	335.6	343.68	2.35
1.00E-04	77.5	68.74	12.74
5.00E-05	32.8	34.37	4.57
2.50E-05	16.7	17.18	2.79
1.00E-05	7.01	6.87	2.04
5.00E-06	3.8	3.43	10.79
1.00E-06	0.8	0.69	15.94



$$B = \frac{\mu_0 I N}{2L(R_2 - R_1)} \left[ (L + x) \ln \frac{\sqrt{R_1^2 + (L + x)^2} + R_2}{\sqrt{R_1^2 + (L + x)^2} + R_1} - x \ln \frac{\sqrt{R_2^2 + x^2} + R_2}{\sqrt{R_2^2 + x^2} + R_1} \right]$$

# Wireless Sensing Approach



## ❑ Challenges

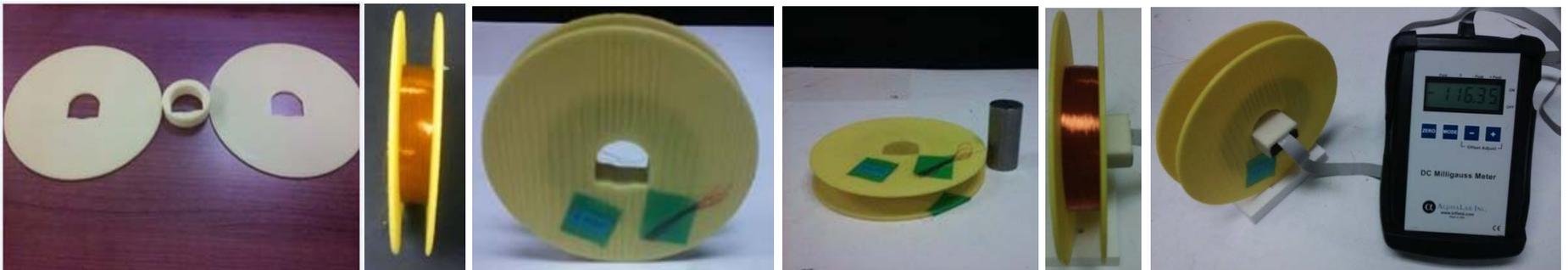
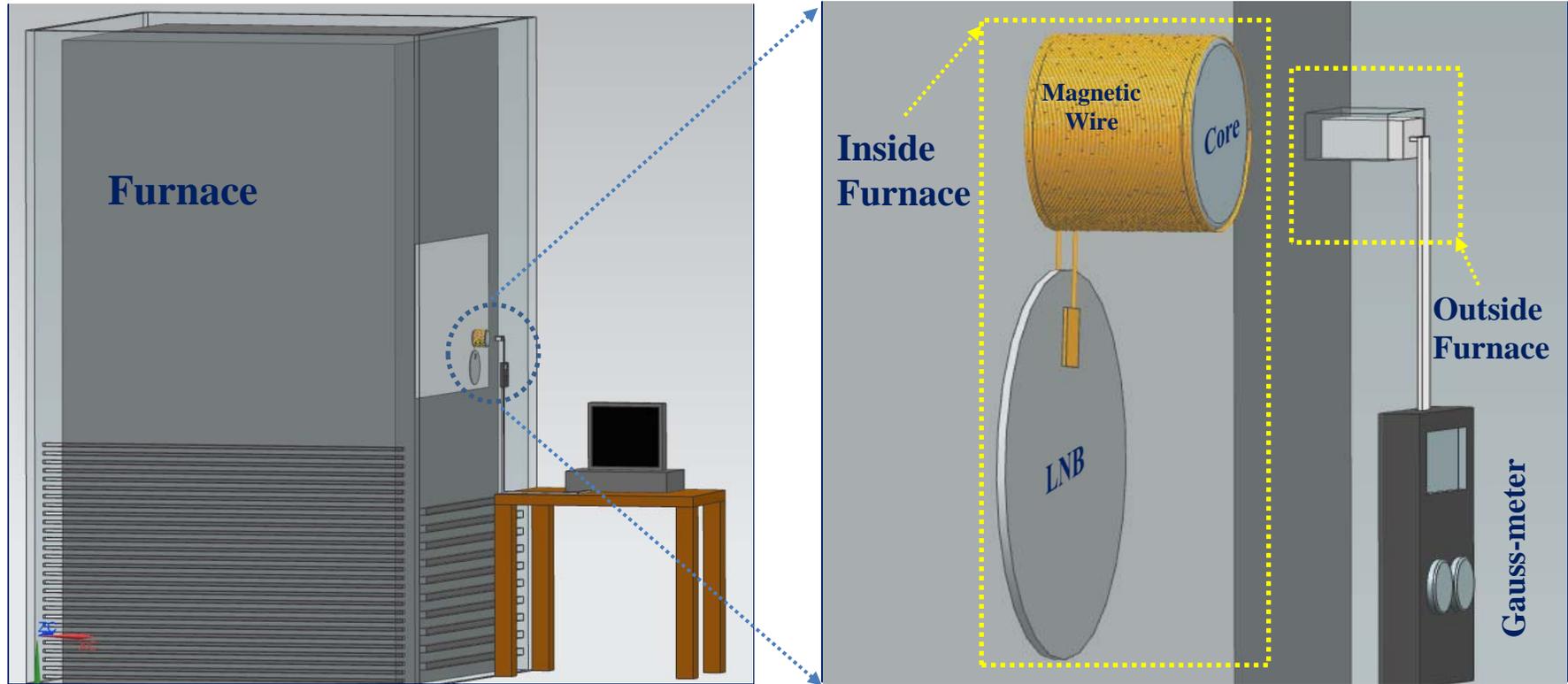
- Low Magnetic field generated in the inductor coil

## ❑ Probable solutions

- Increase the current generated by having a larger sample or stacking multiple samples together
- Proof of wireless sensing concept using PZT-5H for low temperature applications

# Future Work

- Demonstration of wireless sensing mechanism





- ❑ A simple inductance-Hall Sensor based wireless sensing mechanism
- ❑ Demonstrate effectiveness of wireless temperature sensing
- ❑ Energy harvesting at elevated temperature ( $> 500$  °C)
- ❑ Optimization of the energy harvesting circuit
- ❑ Evaluate different types of energy storage units (regular capacitors and supercapacitors) to find out more suitable options for low energy harvesting

# Conclusion



- ❑ A lithium niobate ceramic with high Curie temperature (1142 °C) material is selected
- ❑ Hall Effect sensor was constructed and tested to measure the magnetic flux remotely through various distances and through various materials
- ❑ 1 cm x 1 cm sample of lithium niobate material with two different thicknesses (1mm and 2 mm) were characterized in terms of current generation
- ❑ Measured current from lithium niobate is compared with the theoretical current. The comparison satisfies the definition of pyroelectricity
- ❑ Pyroelectric current from the lithium niobate ceramic material due its change of temperature is taken into consideration to calculate the sample temperature
- ❑ A commercial supercapacitor of 0.2F were charged using the current generated from  $\text{LiNbO}_3$
- ❑ It's possible to improve the amount of energy harvested by improving the harvesting circuit design and circuit elements

# Publications and Patent



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3. Sarker, MD, Karim, H., Martinez, R., Delfin, D., Enriquez, R., Shuvo, M., Love, N., and Lin, Y., 2015, **“Temperature measurements using a lithium niobate (LiNbO<sub>3</sub>) pyroelectric ceramic,”** Measurement, 75, 104-110.
4. US provisional patent, **“SYSTEMS AND METHODS FOR WIRELESS TEMPERATURE SENSING”**
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6. Sarker, M., Sandoval S., Love, N., and Lin, Y., 2014, **“Development of a Wireless Temperature Sensor using a Lithium Niobate Pyroelectric Ceramic”**, 4th Southwest Energy Science and Engineering Symposium, March 22nd, El Paso, TX

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- Student Involvements





**THANK YOU**