

# **Low Thermal Conductivity, High Durability Thermal Barrier Coatings for IGCC Engines 10/1/11**

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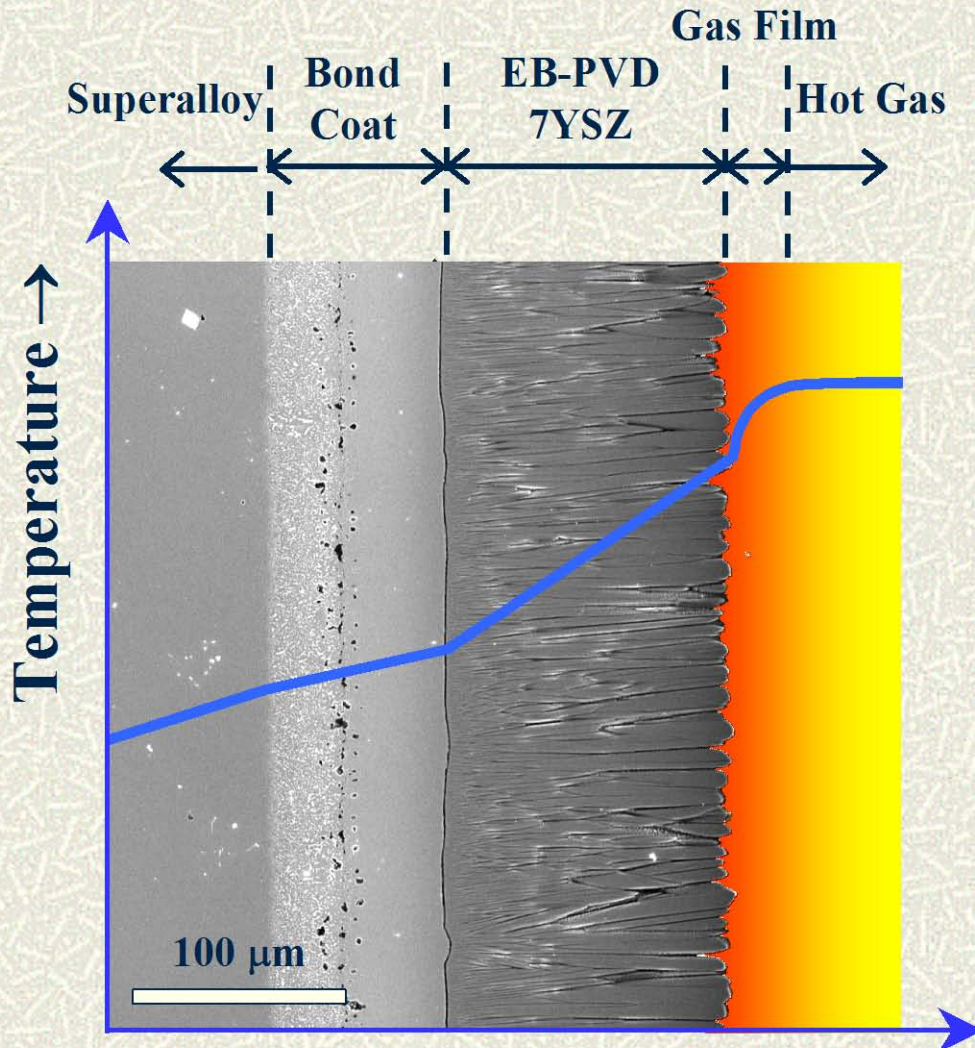
**University of Connecticut**

**Dr. Briggs White DOE Program Manager DE-SC0006814**

# Critical Industrial Participation

- Pratt Whitney and Siemens will supply bond coated superalloy substrates.
- Pratt Whitney will make CMAS glass for use in CMAS exposure testing. (and advise on composition of the glass)
- Pratt Whitney is supplying on Ph D employee student to work on the project

# Microstructure & Requirements For TBCs



## TBC Requirements

- Low Thermal Conductivity
- High Durability
  - Toughness
  - Strain Tolerance

# Goals

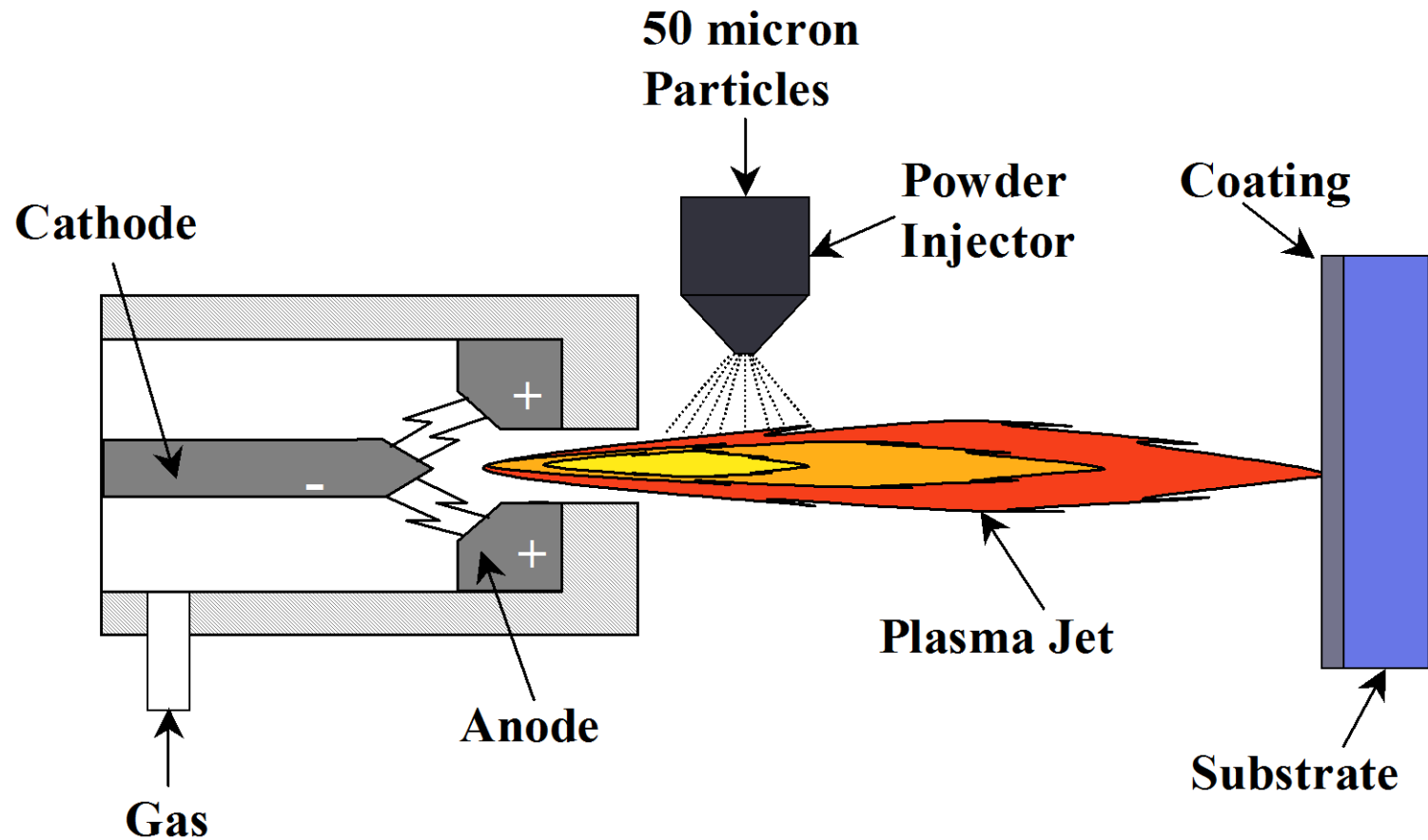
- Reduce thermal conductivity of YSZ TBCs to 0.5 watt/m<sup>°K</sup> by use of inter-pass boundaries (IPBs).
- Increase the allowable surface temperature of the YSZ TBCs by 100°C by use of thin, high temp. surface corrosion barriers layers (CBLs).
- Improve TBC durability in CMAS environment by use of CBLs + other methods.
- Reduce the use of rare earth elements compared to other low K TBCs

# Key Program Processes/Tests

- UConn Thermal Spray Facility
- Solution Precursor Plasma Spray Process (SPPS)
- TBC Cyclic Furnace Testing Facility
- Moist Environment Testing (being build for this program)

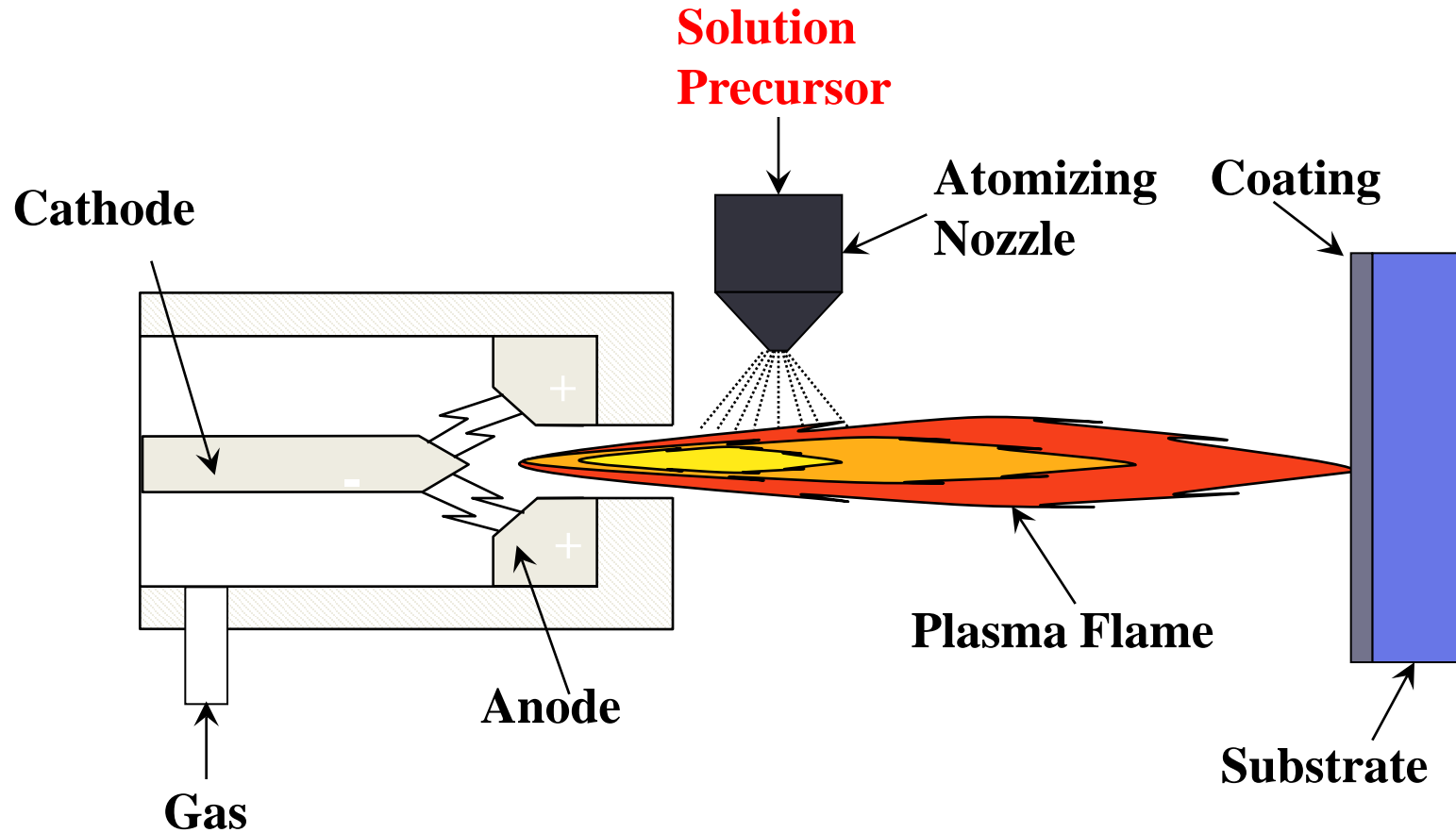


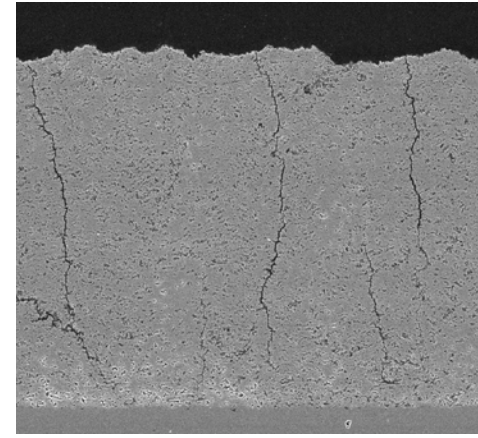
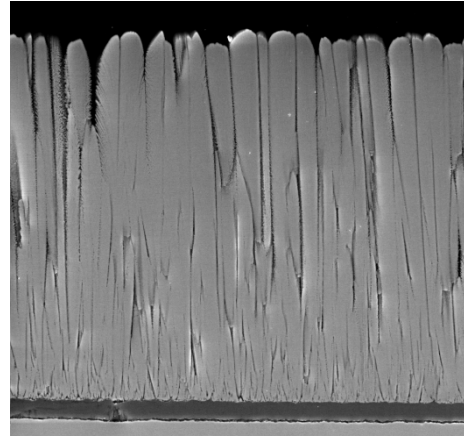
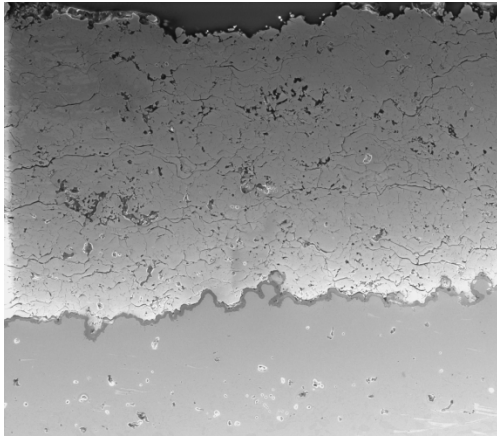
# Air Plasma Spray (SPPS)



- **Particles Melt and Build Splat Structure=> 7YSZ**

# Solution Precursor Plasma Spray Process





## APS

Lower Thermal Cond.

(✓)

Shorter Spallation Life

(✗)

Maxim thickness 1

mm (✓)

## EB-PVD

Higher Thermal Cond.

(✗)

Longer Spallation Life

(✓)

Maxim thickness 0.25

mm (✗)

## SPPS

Lower Thermal Cond.

(✓)

Longer Spallation Life

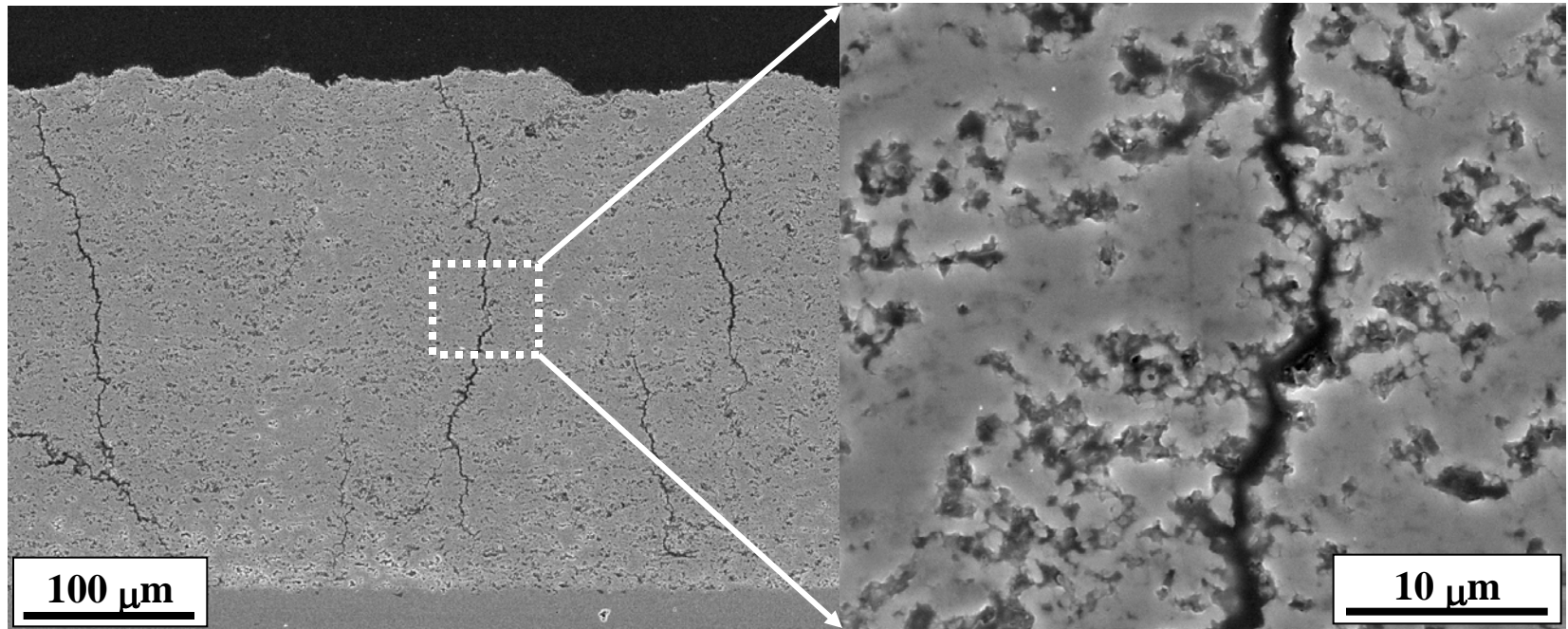
(✓)

Maxim thickness 2.5

mm (✓)



# Microstructure Of SPPS TBCs



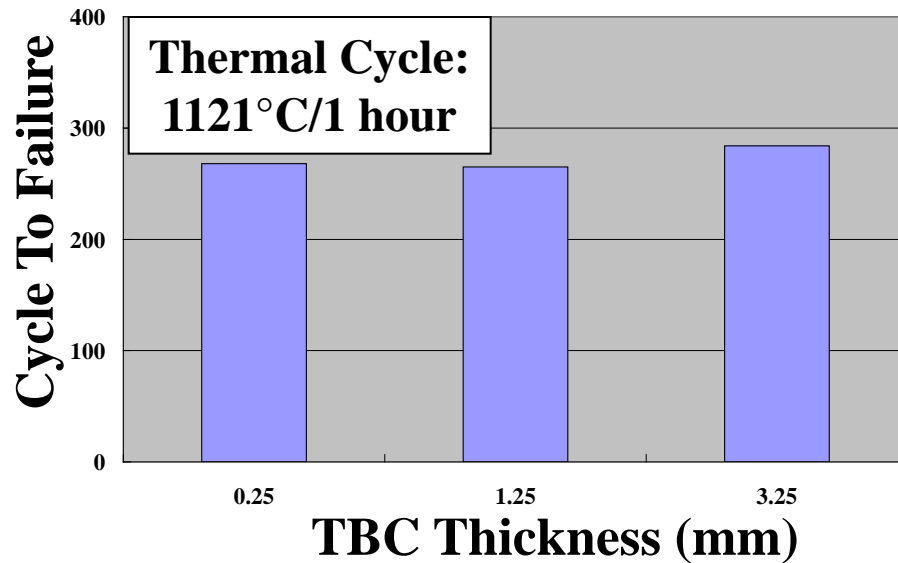
## Unique Features

- 3D Nano & Micrometer Porosity
- Through-Thickness Cracks
- Ultra-Fine Splats

# Advantages of Solution Spray

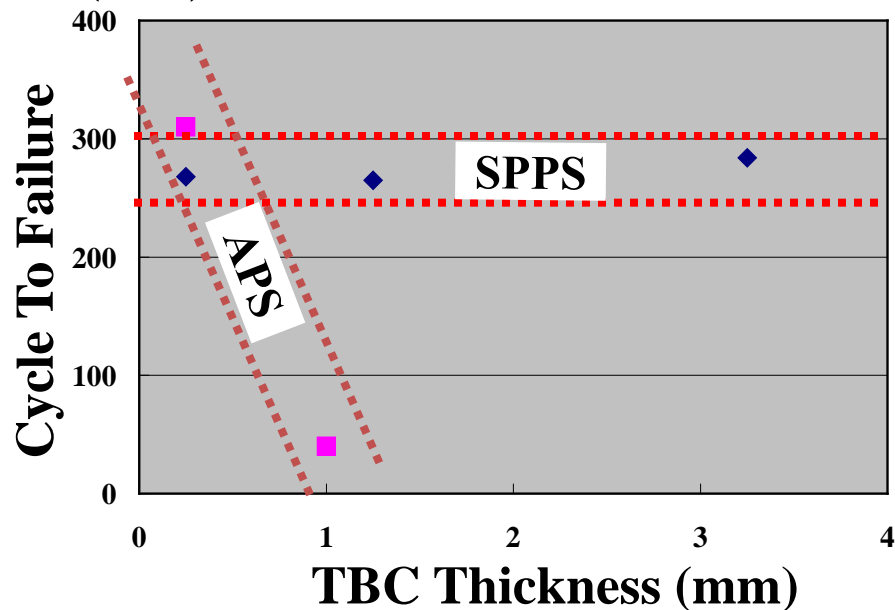
- Vertical stress relieving Cracks- Critical when thick
- Higher Fracture Toughness
- Rapid Composition Exploration (100X)
- Structured Porosity leading to low K coatings

# Effect of SPPS TBC Thickness On Durability



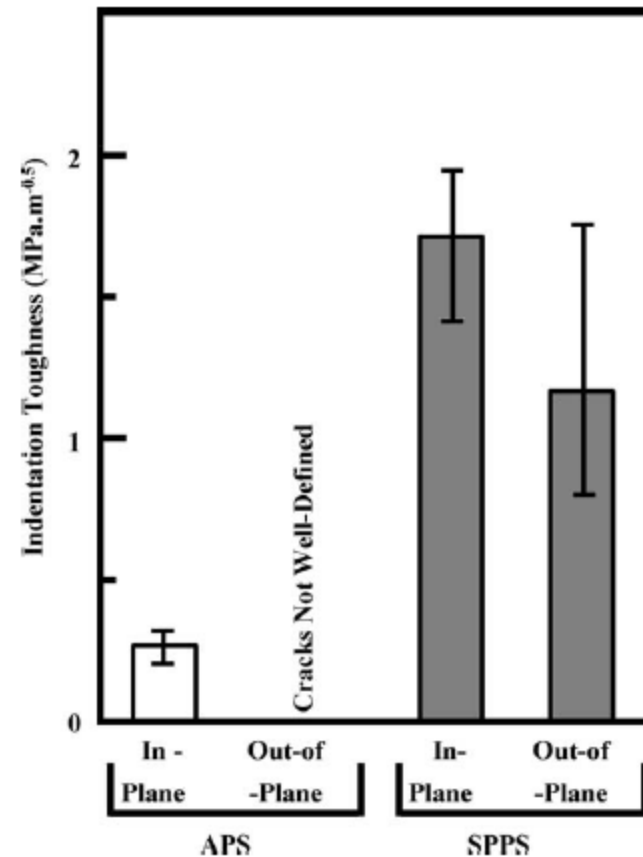
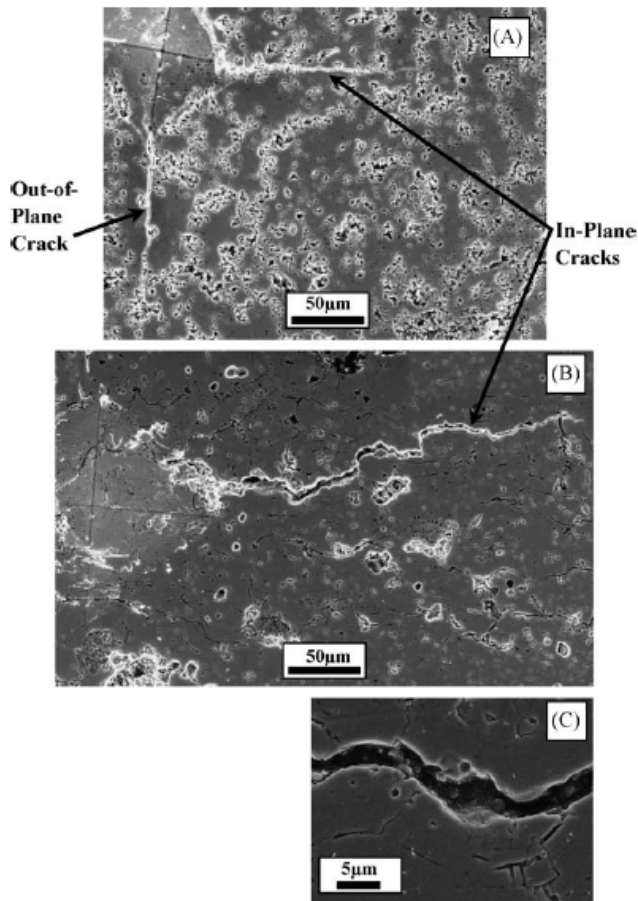
**Substrate: CMSX-4**

**Bond Coat: Co210**

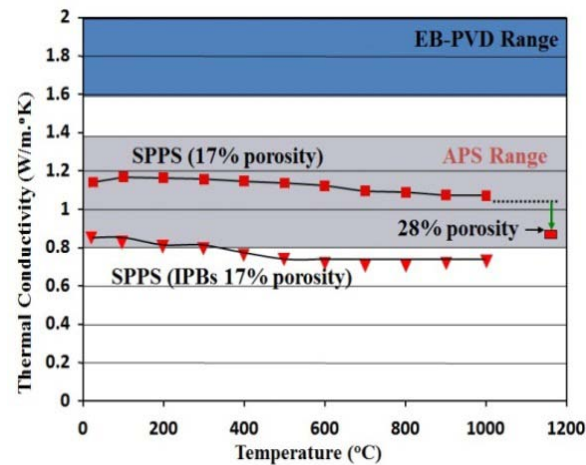
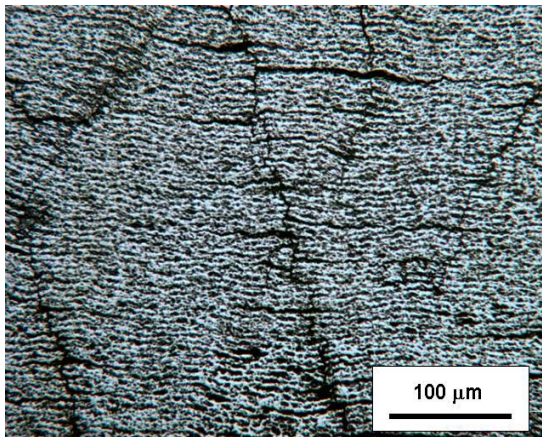


# SPPS Coating have 5X higher In Plane Toughness

Fig. 4. SEM micrographs of Vickers indentation (49N load) sites in: (A) SPPS coating and (B) APS coating. Arrows indicate in-plane and out-of-plane cracks. (C) High-magnification SEM micrograph showing the in-plane indentation crack following a "splat" boundary in the APS coating.



# Structured Porosity Lead to Lower Thermal Conductivity



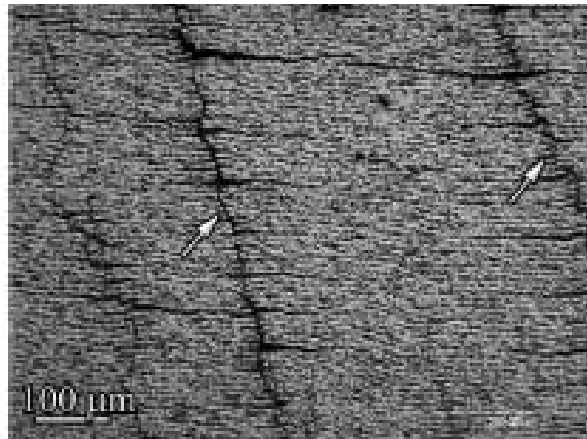
**Figure 3.** (a) SPPS YSZ TBC with IPBs (a) and resultant, reduced thermal conductivity



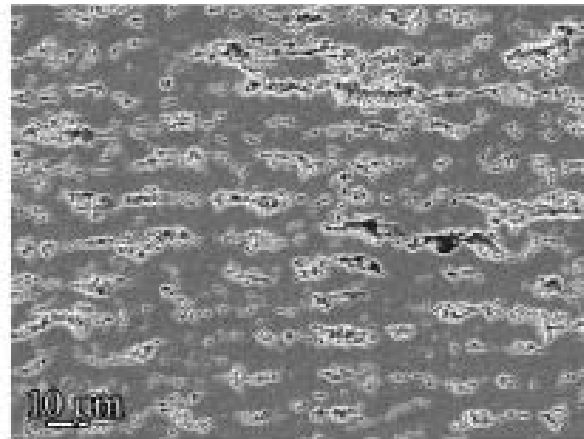


# IPB Microstructure

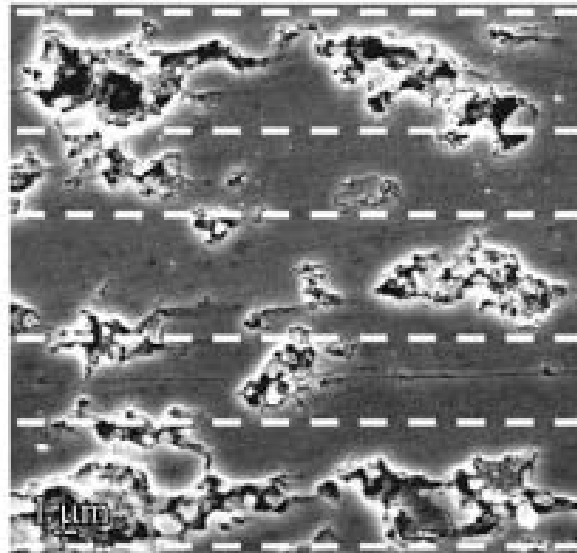
*A.D. Jadhav et al. / Acta Materialia 54 (2006) 3343–3349*



(a)

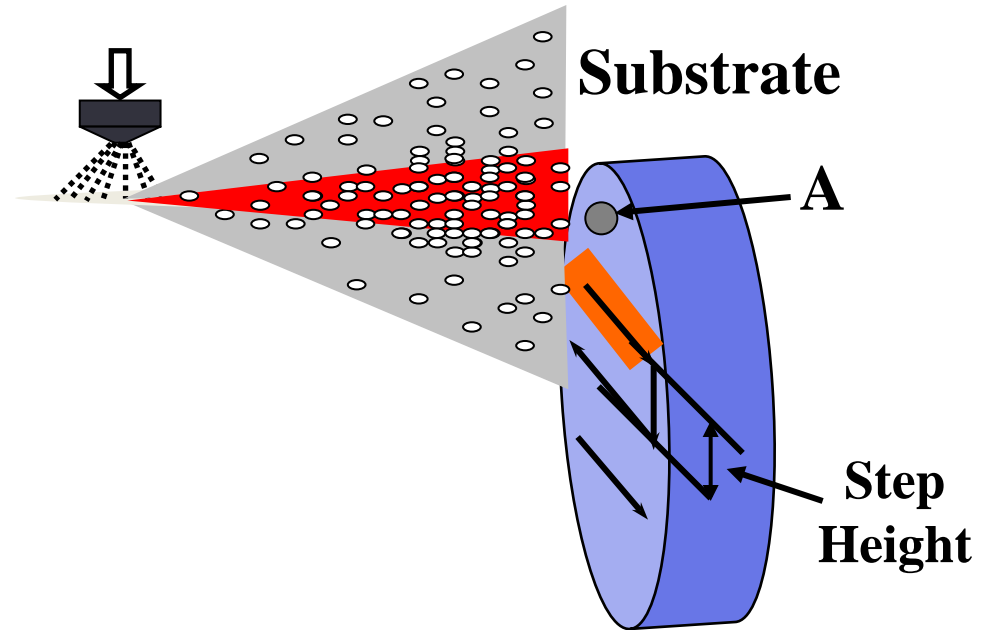
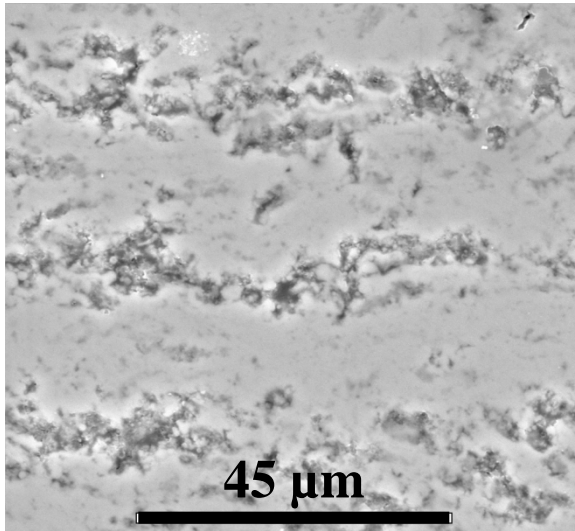


(b)



(c)

# Formation of Inter-Pass Boundaries



# UConn Thermal Spray Facility



# Metco 9MB Plasma Spray System



**Metco 9MC Control**



**4MP Dual Powder Feeder**



**9MB Plasma Gun**

# Liquid Delivery Options



**Standard Inframat System**



**Unique High Pressure System (33 atm)**



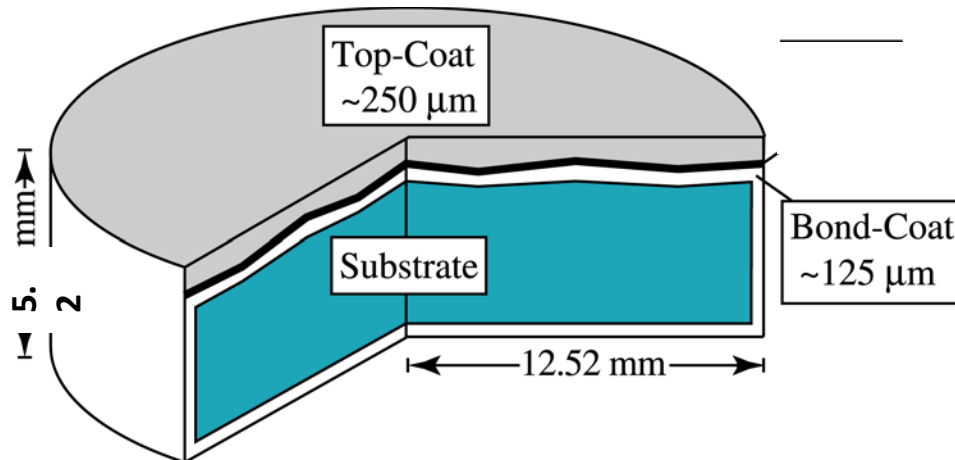
# Cyclic Furnace Test Facility



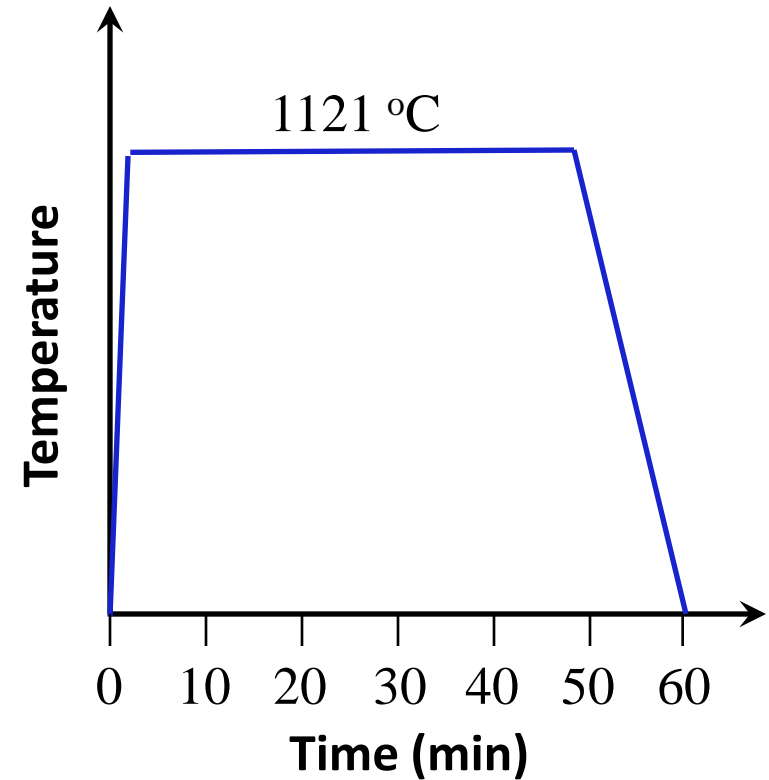


# Specimen Shape & Furnace Cycle

- **Disk-Shape Samples**



- **Thermal Cycling Life Test**



- **Substrate: SC superalloy**
- **Bond-Coat: APS NiCoCrAlY**
- **Top-Coat: SPPS Layered**

# Vast Reference Data Base

- GTD 111- GE DV
- HY 230 with Ni Co Cr Al Y and SPPS
- Rene N-5 Pt-Al BC with EB-PVD
- CMSX-4, Pt Al with EB-PVD
- CMSX-4 , MCrAlY+Si,Hf-EB-PVD
- PWA 1484- APS Ni Cr Al Y -APS

# 10 More Types Tested

#	S1	S2	S3	S4	S5	S6	S7	S8	A1	E1
Top Coat Process	SPPS	SPPS	SPPS	SPPS	SPPS	SPPS	SPPS	SPPS	DVC/APS	EB-PVD
Bond Coat Category	MCrAlY	MCrAlY	MCrAlY	MCrAlY	MCrAlY	MCrAlY	MCrAlY	MCrAlY	MCrAlY	Pt-Al
Bond Coat Process	APS	APS	APS	HVOF	HVOF	LPPS	LPPS	LPPS	APS	CVD
Substrate	H230	H230	NA	H230	CMSX-4	CMSX-4	MARM509	NA	GTD-111	CMSX-4

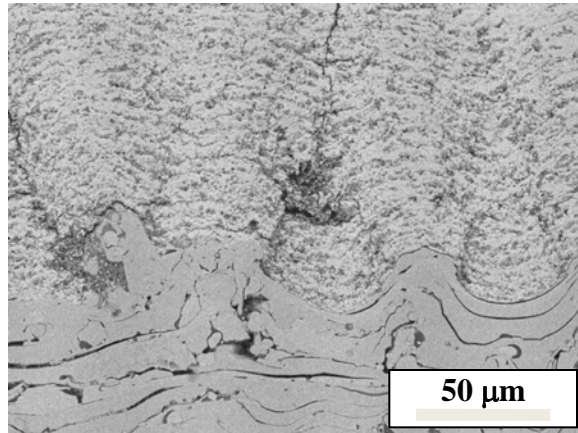
# Bond Coat Composition

	Co	Ni	Cr	Al	Y	Si	Hf
S1, S2		bal	20	10	1		
S4	23-26	Bal.	15-19	9-11	0.2-0.4		
S5, S6	Bal	32	21	8	0.5		
S7	20	Bal	18	12.5	0.6	0.4	0.25
?S8	Bal	32	21	8	0.5		

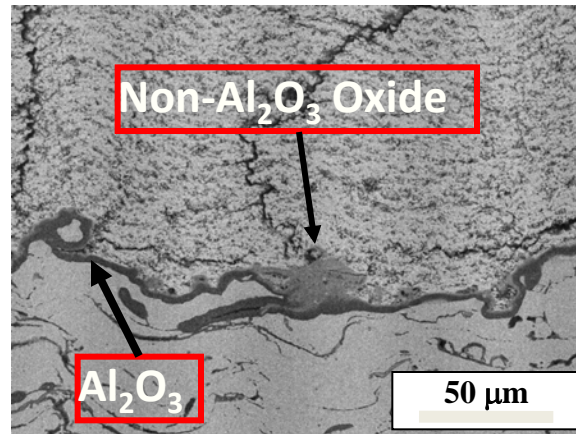
# Test Results at 1121 C 1 Hour Cycles

#	S1	S2	S3	S5	S6	S7	S8	A1	E2
Cycle Life	1140 1140* 1230 1230	573, 595* 785* 1049* 1206	697*	300* 350	245, 270* 290	220, 245*	125 140*	Ave. 300	Ave. 458
Failure % in ceramic	70%	60-75%	50%	60%	25%	50%	30%	-	-

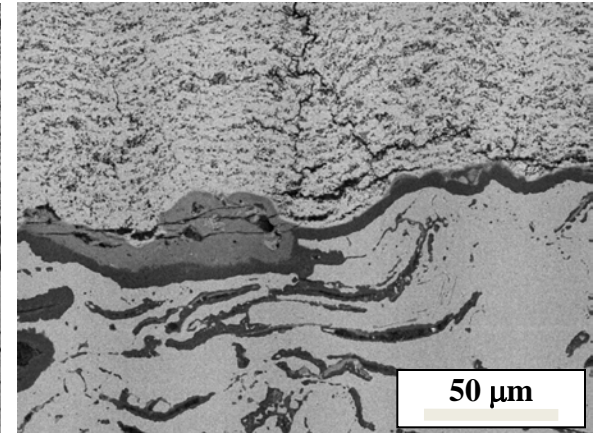
# Change of Microstructure with Thermal Cycling



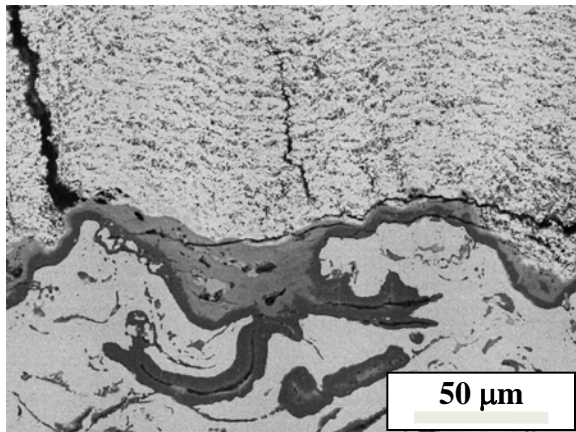
As-Sprayed



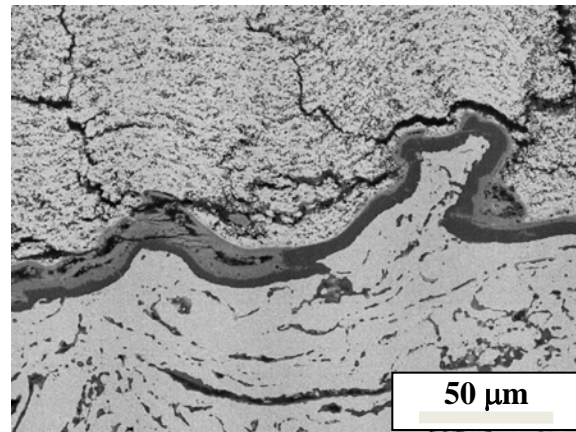
40 Cycles



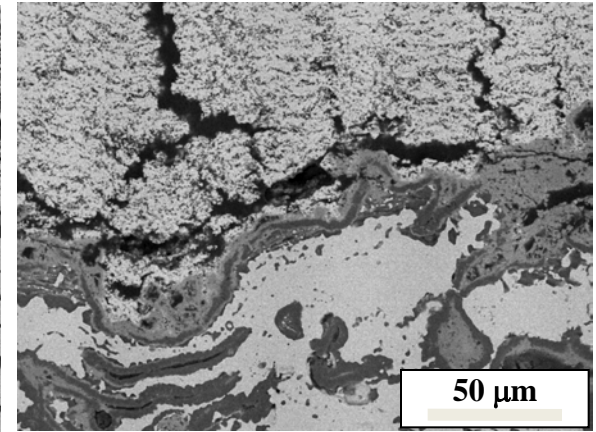
200 Cycles



400 Cycles



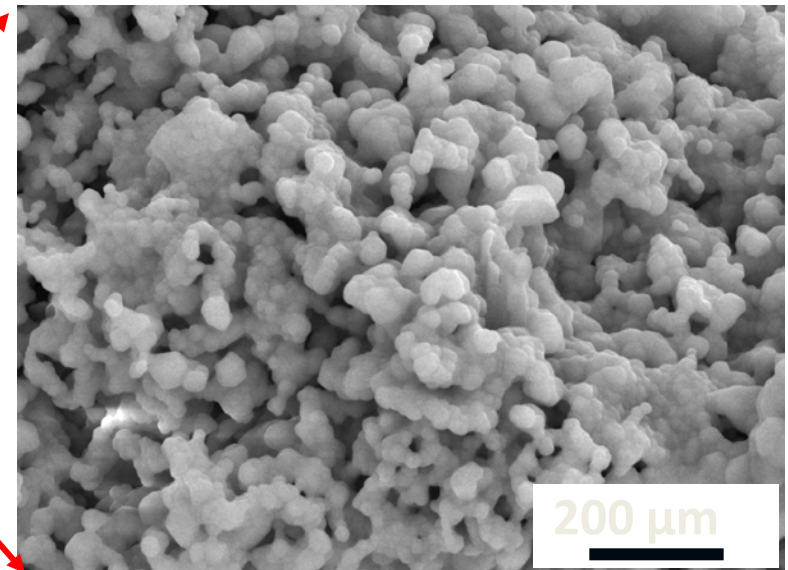
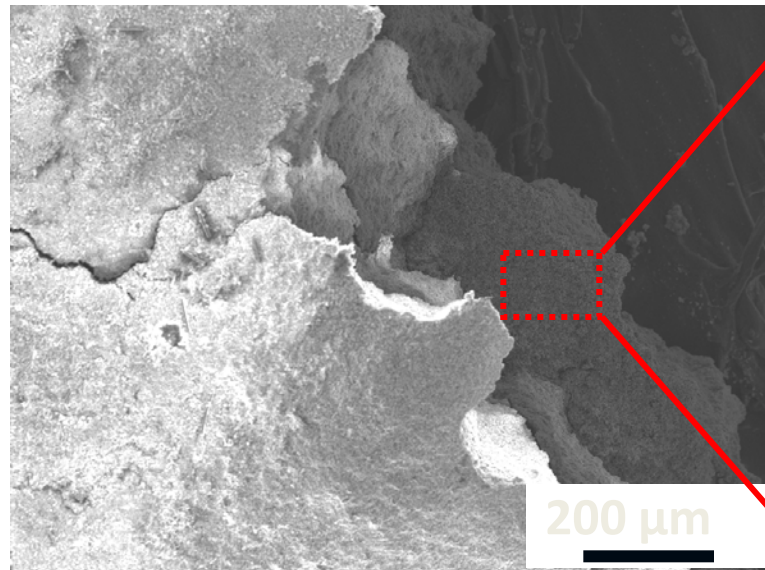
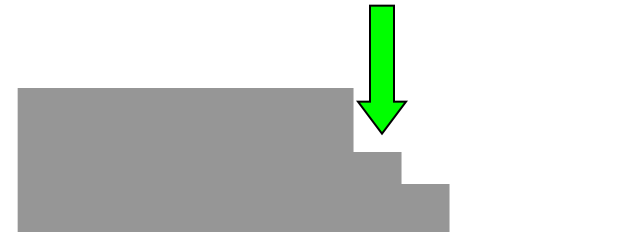
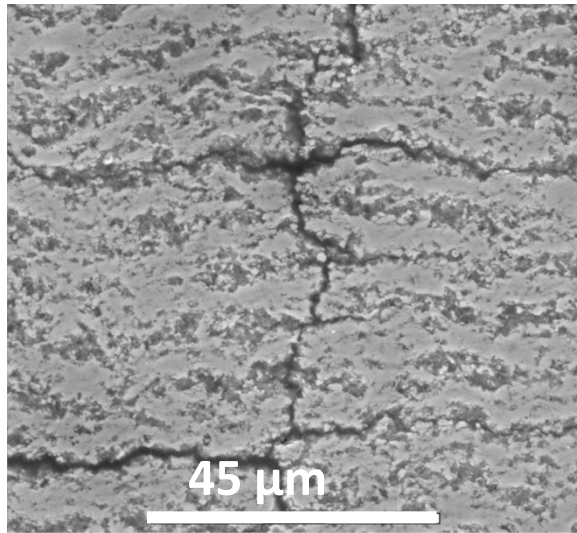
600 Cycles



800 Cycles

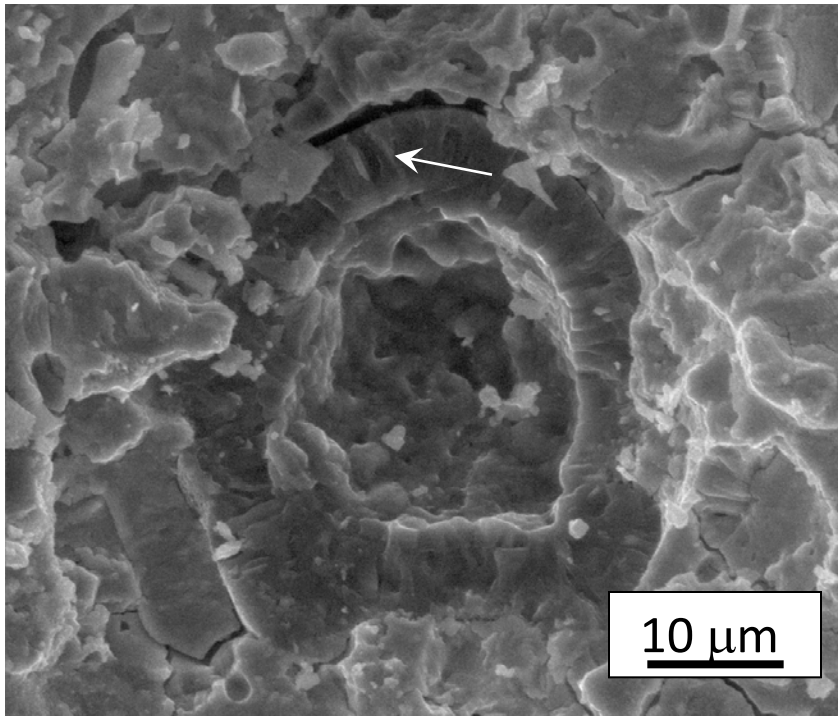


# Morphology of Inter-Pass Boundary

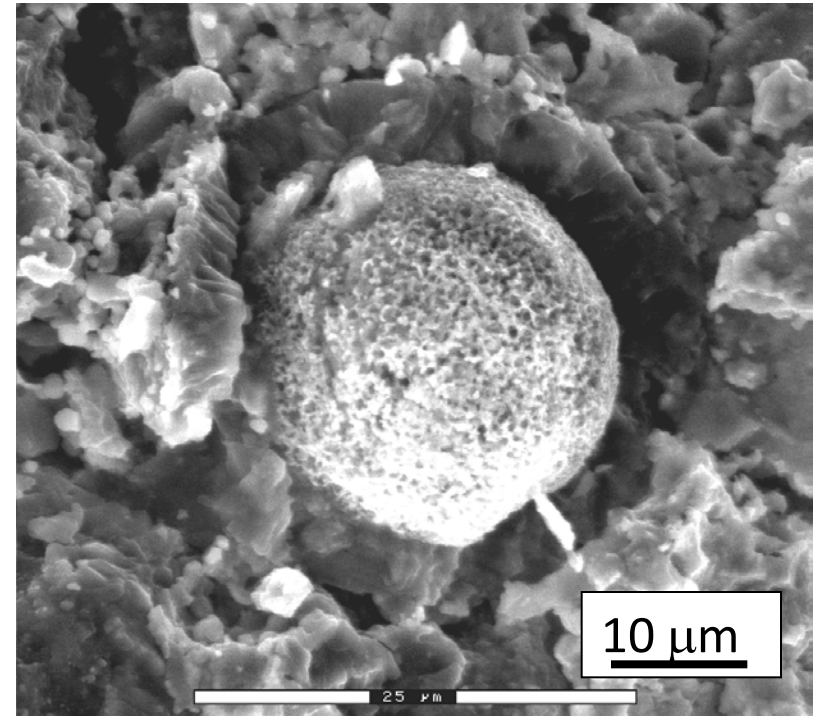


# Spallation Surface Features

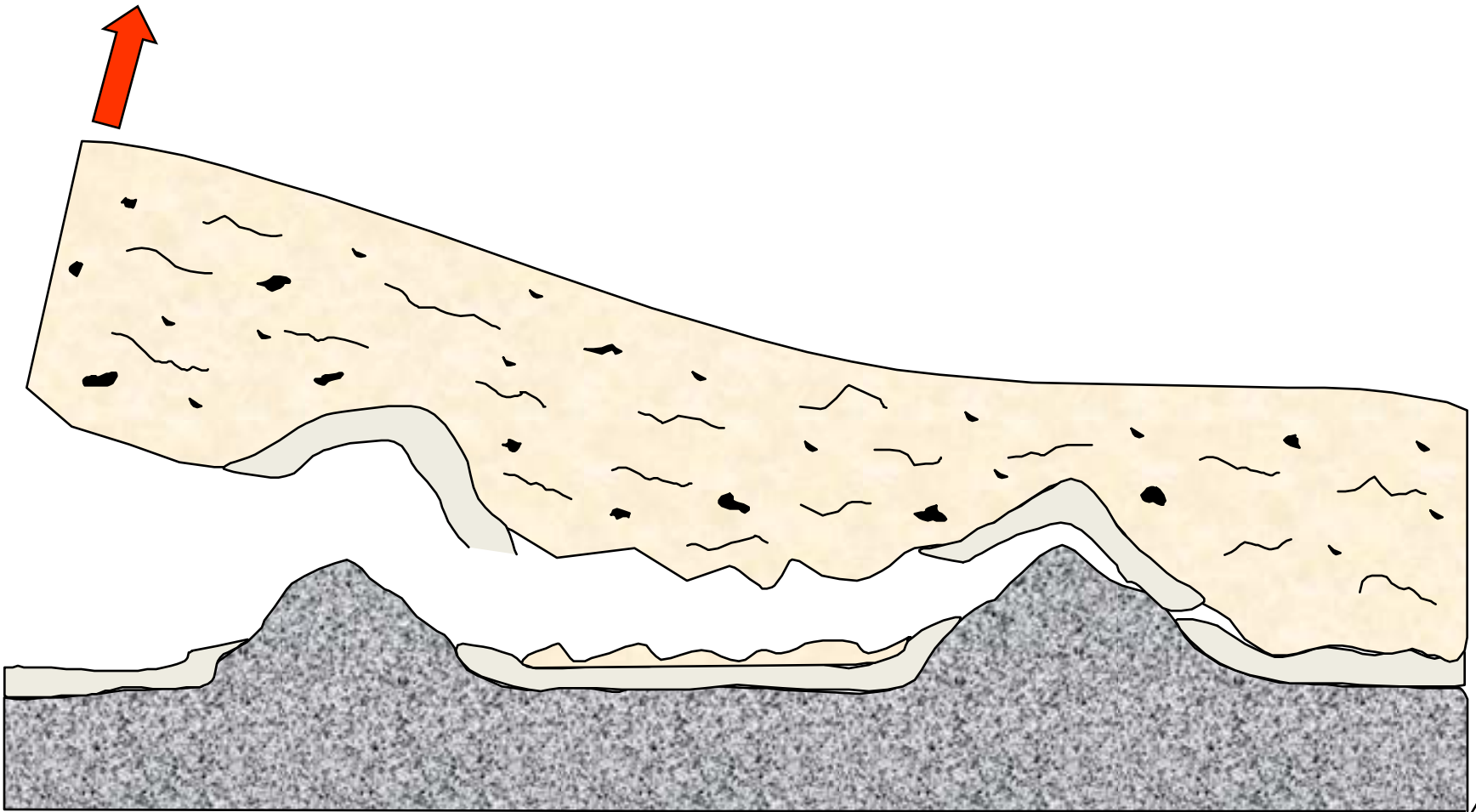
- Ceramic “Bottom” Side



- Metal “Top” Side



# Failure Mode of Plasma Sprayed TBCs



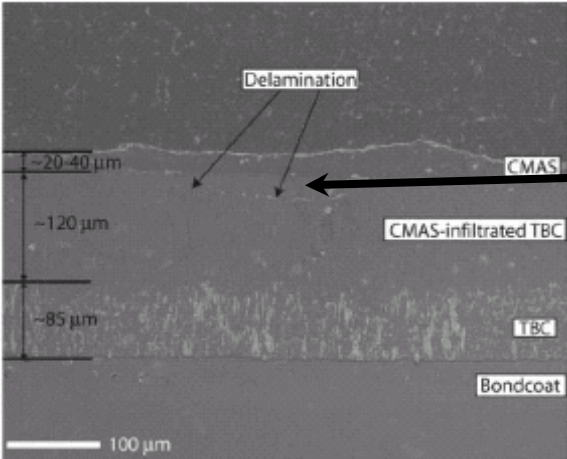
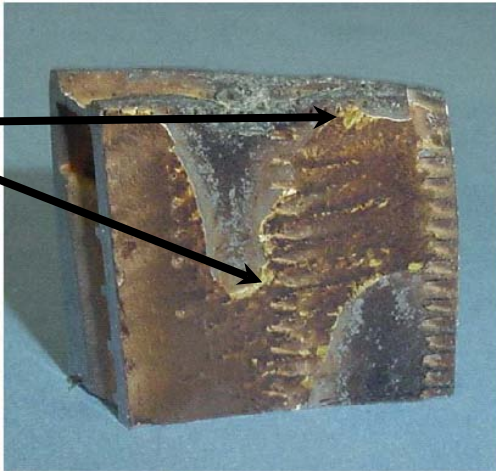
# Contaminants Affect Failure

Calcium, Magnesium, Aluminum  
Silicon= CMAS

# CMAS Infiltration of 7YSZ Thermal Barrier Coating

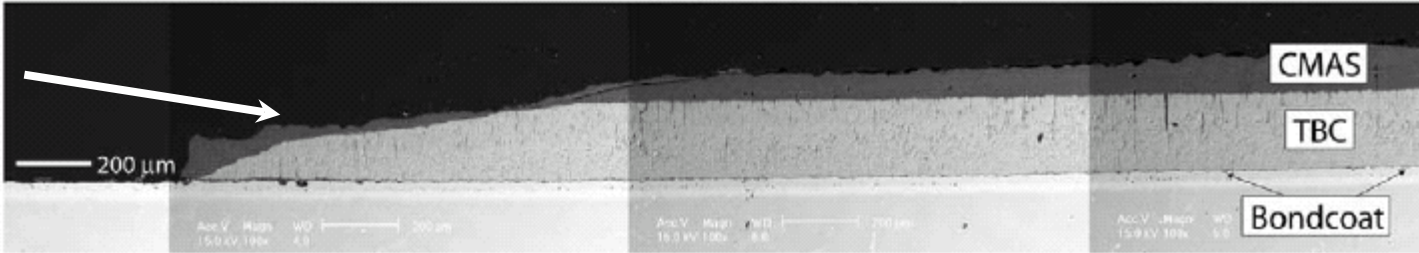
## Field Observation of CMAS Attack

CMAS  
Deposits



Transverse Cracks  
that Lead to  
Shedding of  
Topcoat

Coating Loss  
Due to CMAS  
Infiltration



Mercer et al. 2005

Most Aggressive Attack Tends to Occur in Hottest Regions



# 1. Loss of Strain Tolerance-Mechanical Effect

*A.G. Evans, J.W. Hutchinson / Surface & Coatings Technology 201 (2007) 7905–7916*

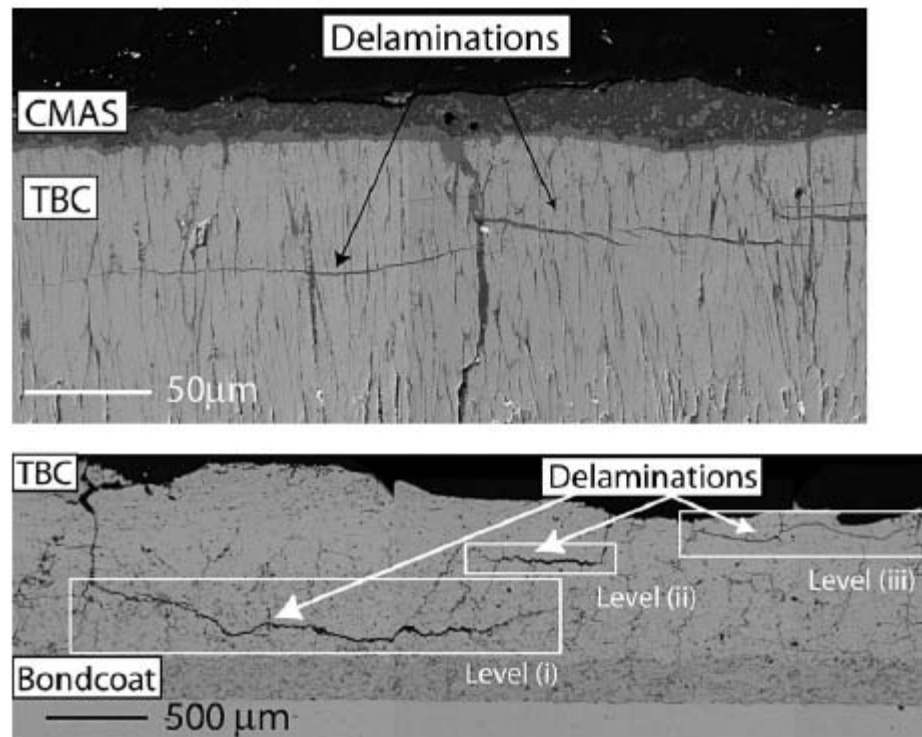


Fig. 1. Examples of delaminations in thermal barrier coatings obtained from components removed from engines subjected to CMAS penetration: (a) Sub-surface mode I delaminations in an airfoil with a TBC made by electron beam physical vapor deposition; the delaminations are within the penetrated zone [9]. (b) Delaminations at several locations within a shroud penetrated by CMAS; the TBC is 1 mm thick and deposited by air plasma spray (APS) [10].



# Mechanics Modes for Loss of Strain Tolerance Developed by Hutchinson and Evans

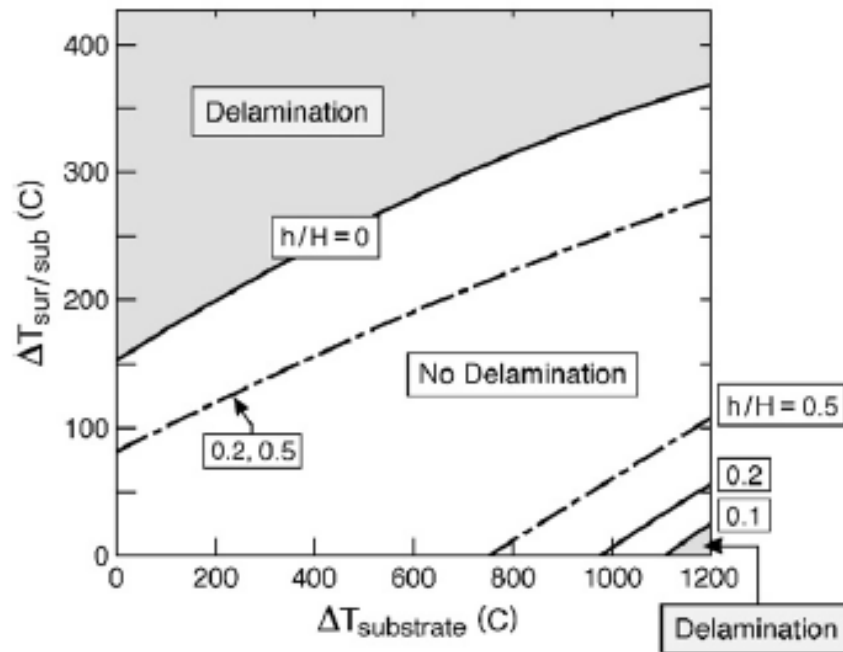


Fig. 10. A map for deep delamination in an APS-TBC on a superalloy substrate with CMAS infiltration to depth,  $h/H$ . The mixed mode toughness parameter is,  $\lambda=0.25$ .

## 2. Many types of chemical and Phase Effects for example Y loss and destabilization of t phase $\text{ZrO}_2$ to Monoclinic with a destructive volume change

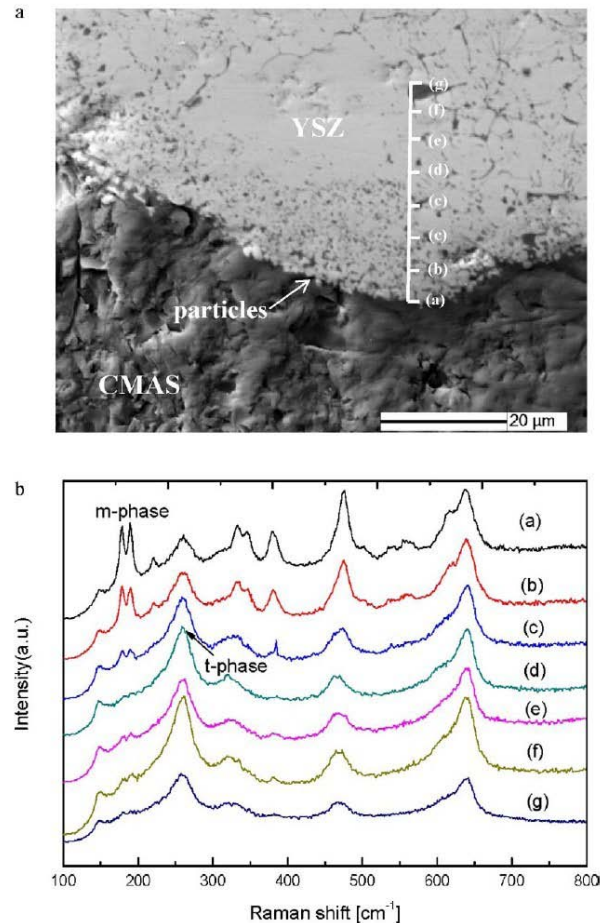


Fig. 4. (a) Micrograph of the interaction zone of CMAS deposit and YSZ coating after 4 h heat-treatment at 1250 °C, and (b) Raman spectra obtained from the positions marked in (a).

# **Proposed Work Plan**

1

# **Minimization of Thermal Conductivity Using IPBs**

- Experimental Design of spray trials
- Outcome assessment by thermal conductivity calculation verified by measurement

# Base Line System



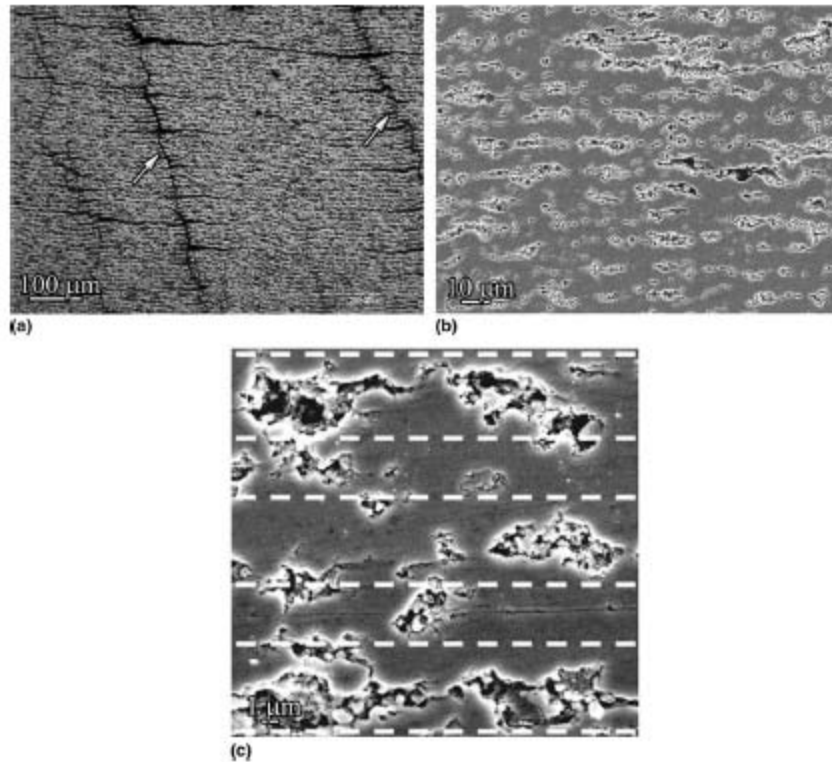
**Figure 6.** TBC #1, a Low K SPPS YSZ TBC using IPBs and porosity

# **Rapid Measurement of Thermal Conductivity**

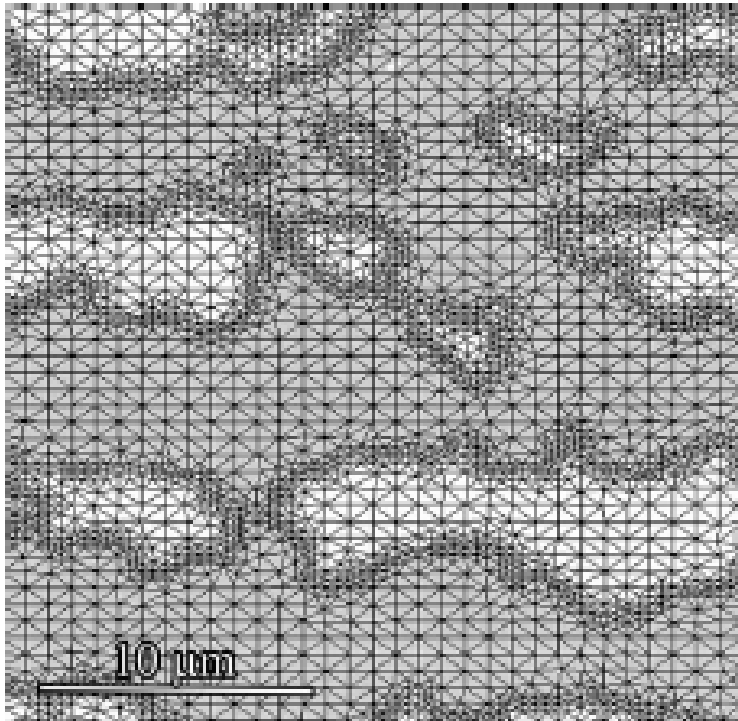


# Calculating Thermal Conductivity

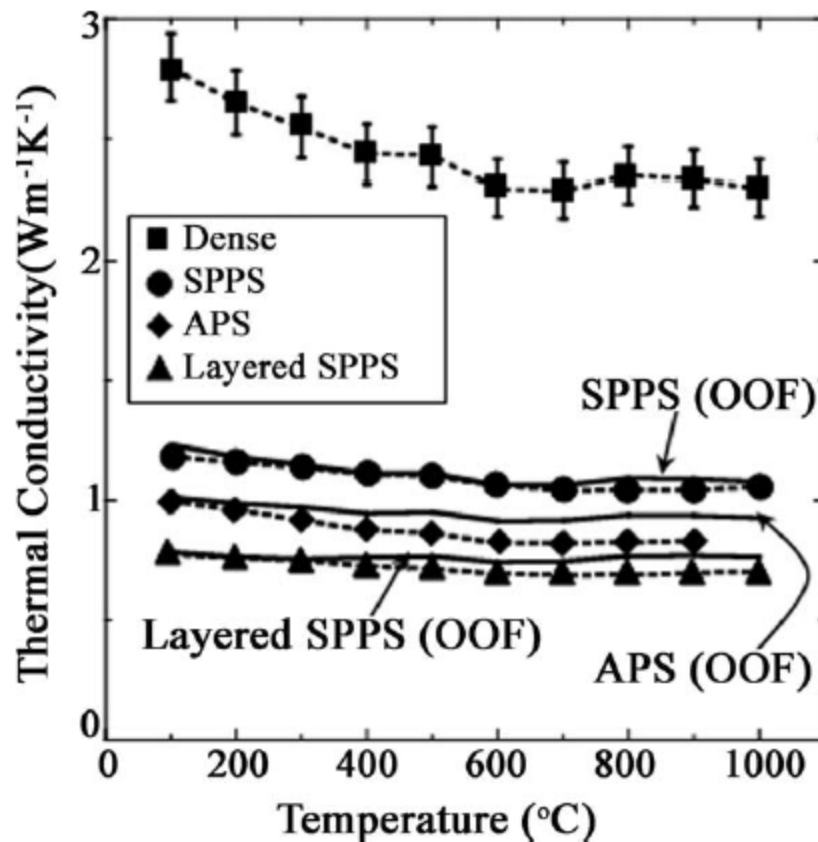
*A.D. Jadhav et al / Acta Materialia 54 (2006) 3343–3349*



# Finite Element Mesh Generated from Micrograph Using OOF Program



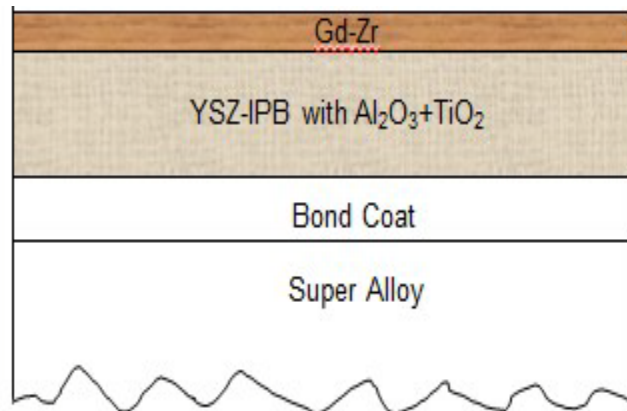
# Calculated Conductivity Agrees Well with Experiments



# **CMAS Damage Mitigation to be Implemented**

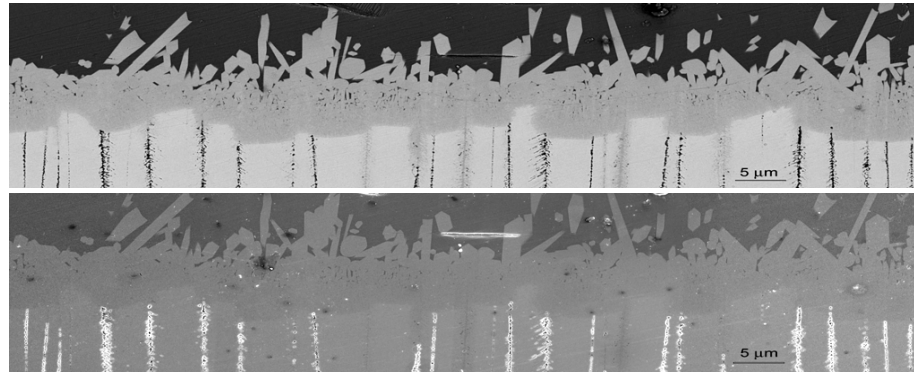
Three Approaches

# 1. Add Gd-Zr to baseline system for higher temperature phase stability and CMAS



**Figure 7.** TBC system #2 with low conductivity solution plasma sprayed YSZ with IPBS and CMAS resistant high temperature tolerant Gd-Zr protective surface layer (PSL).

# CMAS Resistance of GdZr



# Add Metastable $\text{Al}_2\text{O}_3$ + to block CMAS in the YSZ layer

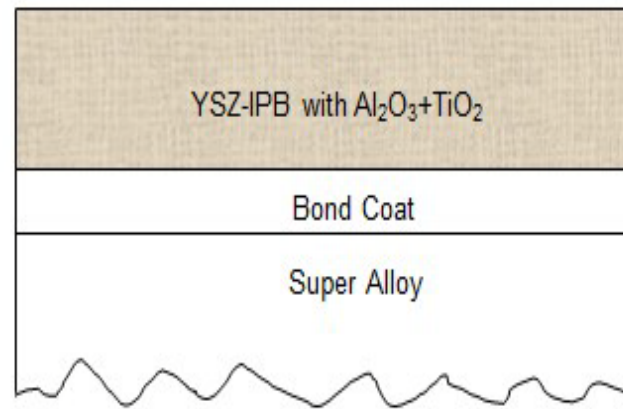
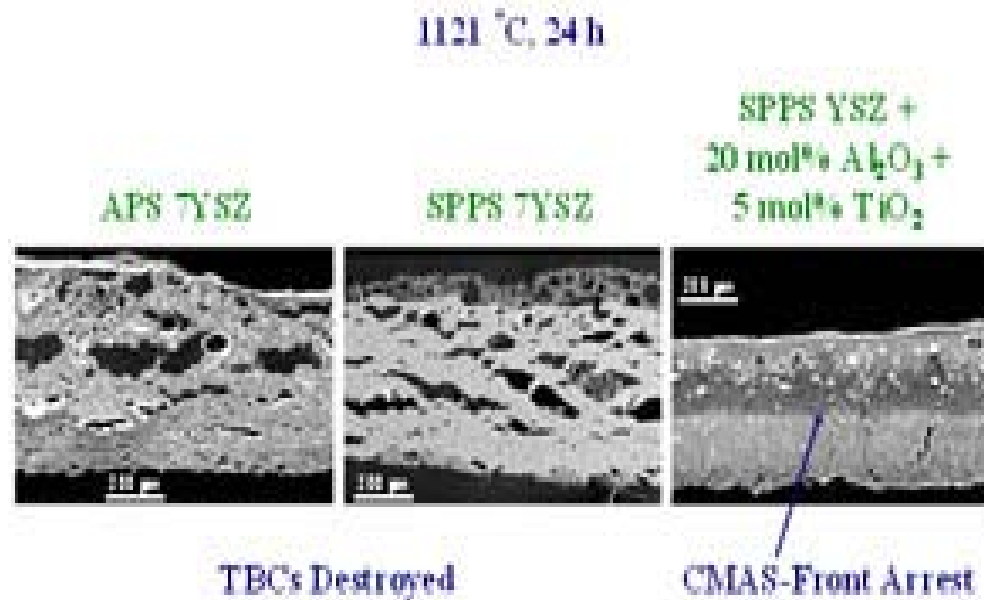


Figure 9. TBC system #4 has features of TBC #1-3 with calcium sulfate infiltration.

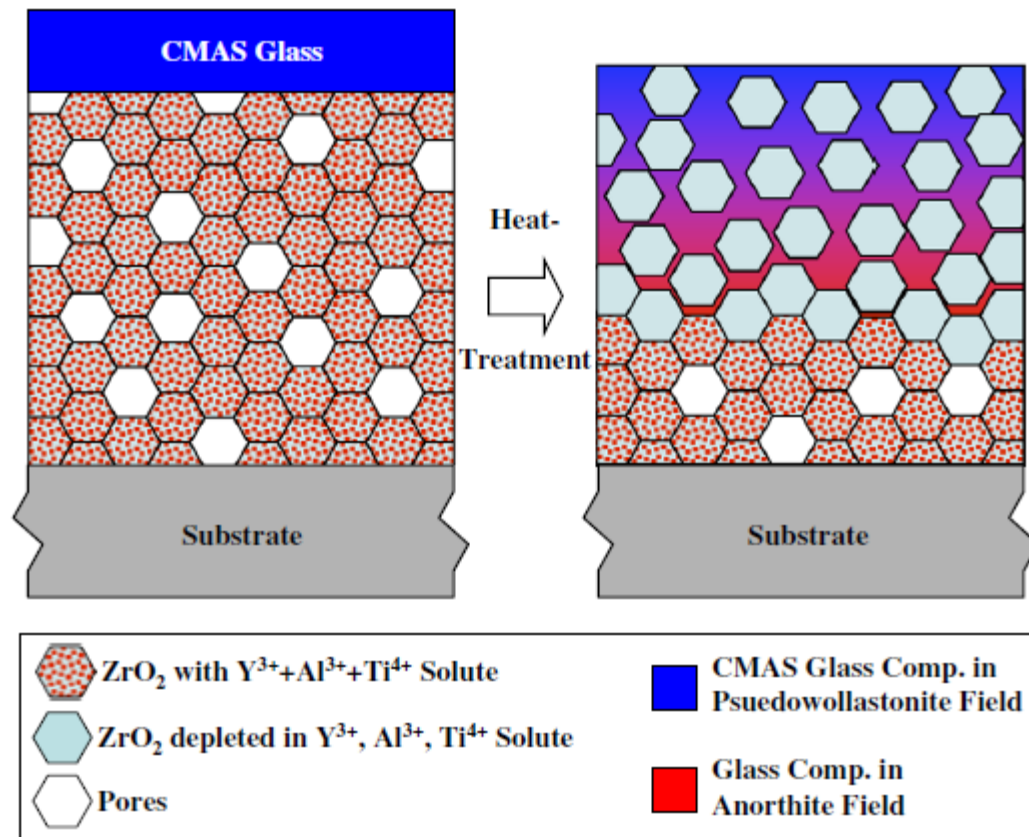


## 2. Addition of metastable Al + more

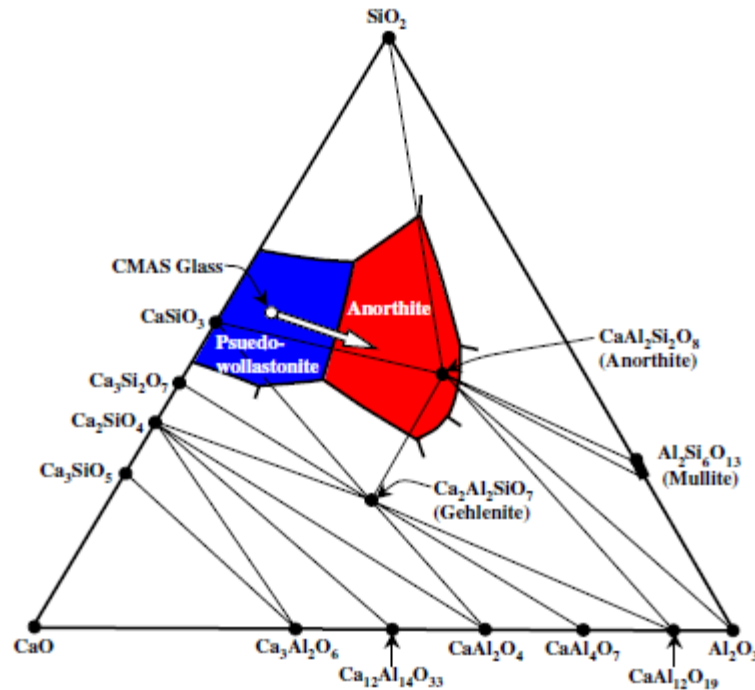


# CMAS composition is altered to Anorthite Filed

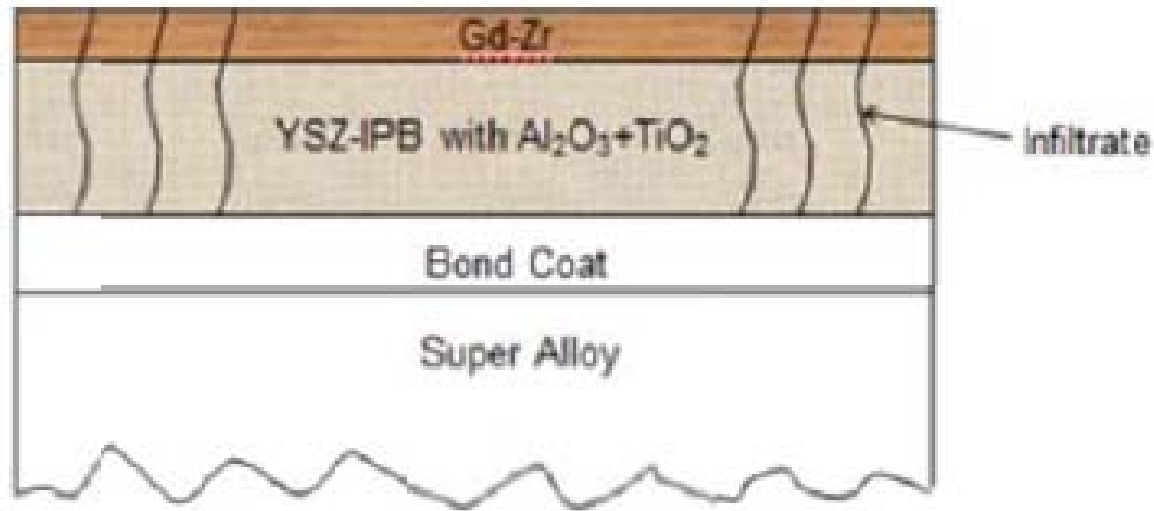
*A. Aygun et al. / Acta Materialia 55 (2007) 6734–6745*



# Microscopy Shows Anorthite phase is blocking

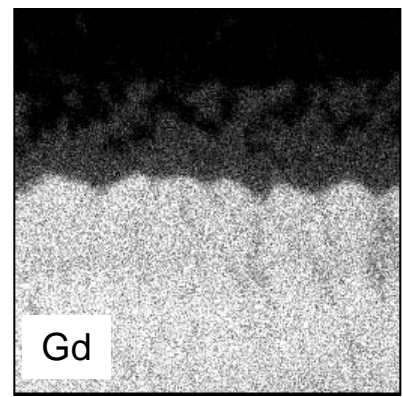
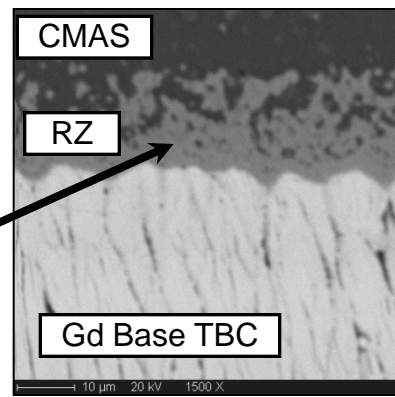
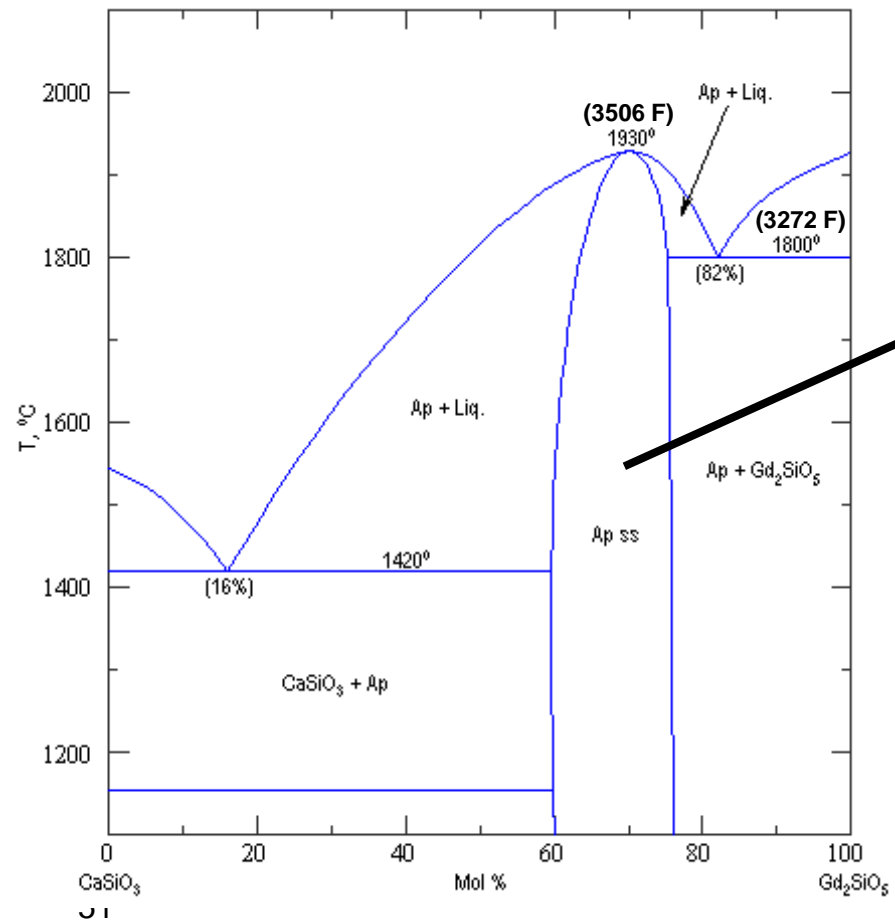


### 3. Infiltration of $\text{CaSO}_4$ via a low melting eutectic of $\text{NaSO}_4$ - $\text{CaSO}_4$ - $\text{MgSO}_4$



# Analysis of $\text{Gd}_2\text{Zr}_2\text{O}_7$ /CMAS Reaction Product

## Sealant Layer Identified as Hexagonal Apatite Phase, $\text{CaGd}_4(\text{SiO}_4)_3\text{O}$



**Coating System Needs to be Designed Such That Coating/CMAS Constituents Form Stable Refractory Compound**

### 3. Infiltration with $\text{CaSO}_4$ found in the field by Breau

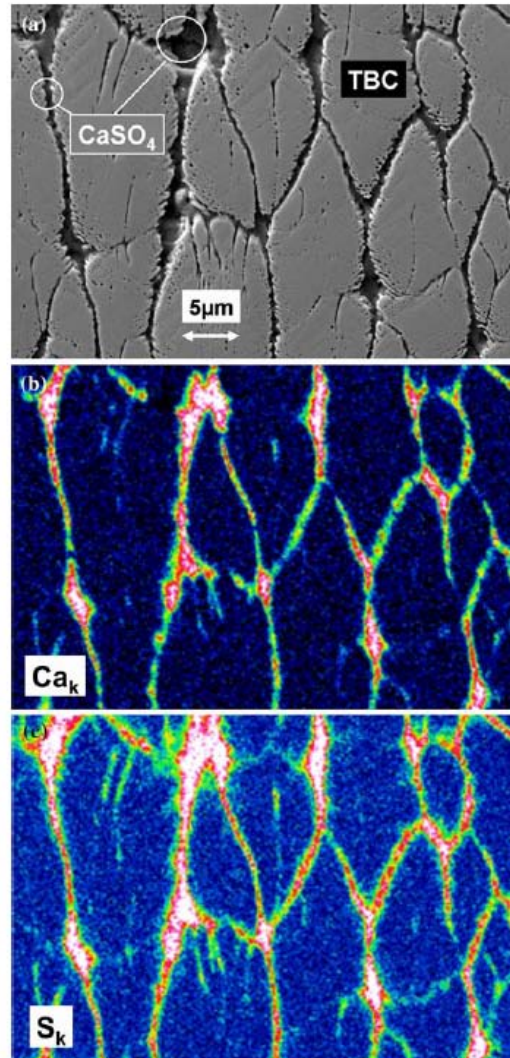


Fig. 3 a middle section of the YSZ top coat displaying  $\text{CaSO}_4$  infiltration of open porosity (suction-surface/region B, SEM, secondary electron image), b and c elementary mapping ( $\text{Ca}_k$ ,  $\text{S}_k$ ) proving that  $\text{CaSO}_4$  is continuous within the intercolumnar pore network of the coating



# Composition of the CMAS blocking Ca-Mg-Si materials found

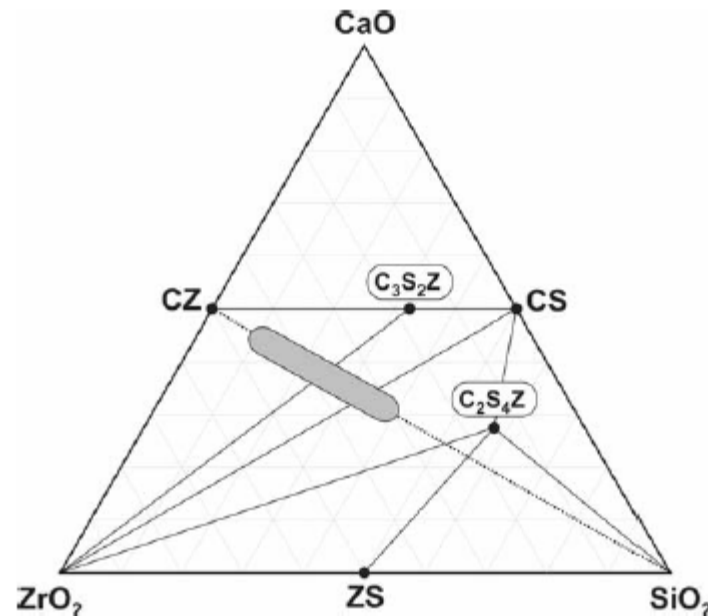


Fig. 13 Compatibility triangles in the ternary CaO–ZrO<sub>2</sub>–SiO<sub>2</sub> (mol%) at 1,300 °C (modified after [39, 40]) serving as a first approximation for pertinent phase assemblages at the CMAS/YSZ interface. Shaded area represents the compositional variation of the Ca–Zr–Fe–silicate which plots close to the join CZ–SiO<sub>2</sub> (given by dotted line). Abbreviations: C = CaO, S = SiO<sub>2</sub>, Z = ZrO<sub>2</sub>, CZ = CaZrO<sub>3</sub>, C<sub>3</sub>S<sub>2</sub>Z = Ca<sub>3</sub>ZrSi<sub>2</sub>O<sub>9</sub>, C<sub>2</sub>S<sub>4</sub>Z = Ca<sub>2</sub>ZrSi<sub>4</sub>O<sub>12</sub>, CS = CaSiO<sub>3</sub>, ZS = ZrSiO<sub>4</sub>. Compatibility triangles in the subsystem CaO–CZ–CS are omitted

# Summary

- Project Goals are;
  - Reduce thermal conductivity 0.5 watt/m<sup>°K</sup>
  - Increase surface temperature allowable by 100C
  - Significantly improve CMAS resistance
- Inter-Pass Boundaries will be used and optimized to lower thermal conductivity
- A top layer of GdZr will be used to:
  - Allow +100°C surface temperature + high purity SPPS
  - Reduce CMAS attack
- Al-Ti Metasable solutes+ will be added to the YSZ to reduce CMAS infiltration.
- CaSO<sub>4</sub> will be used for the first time to arrest CMAS infiltration.

# Summary

- Results will be validated with CMAS testing in cyclic furnace tests and high moisture tests
- Detailed mechanism of failure will be evaluated for the test run and Modification of the TBC will be made as mechanisms suggest.
- Substrates are to be supplied by Siemens and Pratt and Whitney

Questions ?