

# Coal Combustion and Gasification Science



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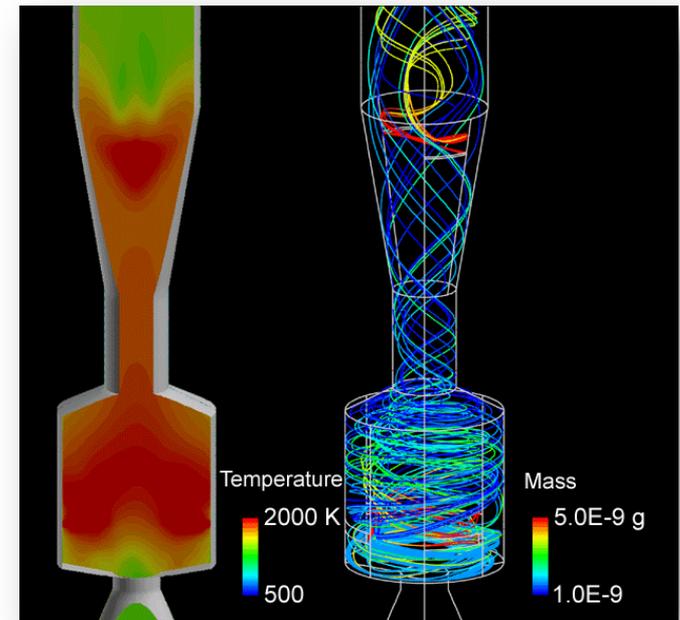


# Outline

- Motivation
- Research Approach
- Recent Research Results
  - Model Evaluation for Oxy-Fuel Combustion
    - $\text{CO}_2/\text{CO}$  production ratio
    - Single-film vs. double-film models
    - Apparent kinetics and gas diffusivity
    - Ash inhibition
  - Pressurized Gasification Kinetics
- Future Plans
- Summary

# Motivation

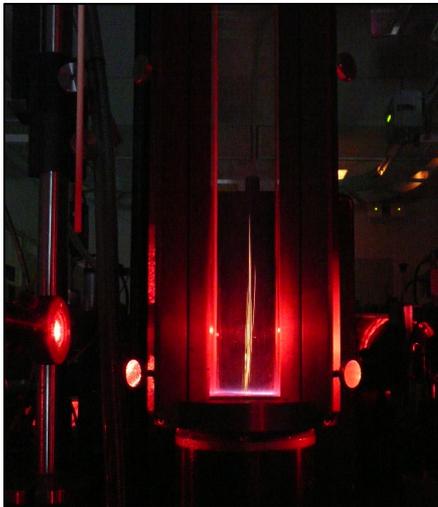
- Improvements in energy efficiency, availability, fuel flexibility, and capital effectiveness of oxy-fuel coal boilers and coal gasifiers increasingly rely on CFD modeling
- Accuracy of CFD modeling limited by
  - poor knowledge of fundamental coal conversion *rate parameters*
    - ignition delay
    - volatile loss
    - char combustion/gasification rate
  - limitations of *simplified models* used to predict coal conversion in CFD simulations



Simulation of 2-stage coal gasifier

# Our Research Approach – Experimental

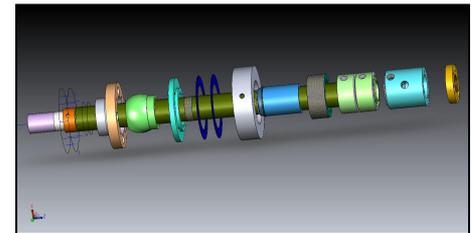
- Utilize unique experimental facilities that recreate relevant reaction conditions, while allowing for optical measurements
- Perform both optical and sampling-based diagnostic measurements to collect data on critical rate parameters
- Use well-controlled particle sizes and particle feed rates



1-atm entrained flow reactor



pressurized entrained flow reactor

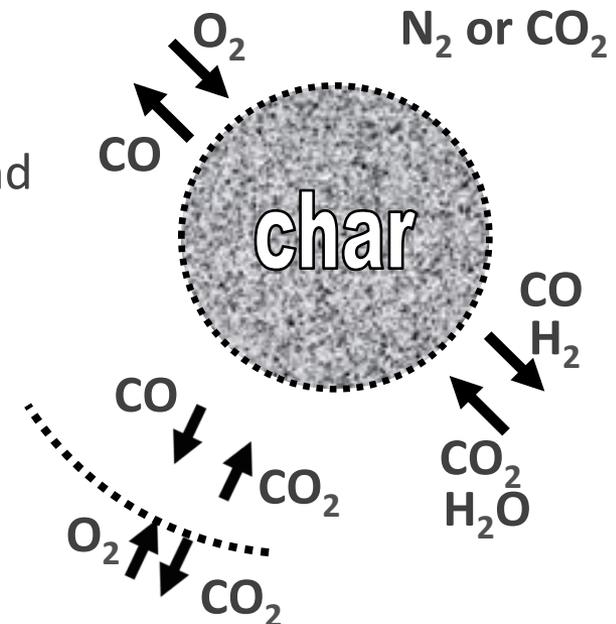


exploded diagram of optical probe

# Our Research Approach – Modeling

Use detailed reacting porous particle model to *interpret* experimental trends and *guide* the application of simplified reacting particle models

- **SKIPPY** (Surface Kinetics in Porous Particles) model, initially developed by Prof. Brian Haynes (Univ. Sydney)
- Detailed surface kinetics and gas-phase kinetics provided through links to CHEMKIN II
- Heterogeneous mechanism, char properties and combustion environment specified by user
- Allows evaluation of *boundary layer reactions* and *different kinetic mechanisms or rate parameters*



Reaction	A (g/cm <sup>2</sup> s)	E (kJ/mol)
<b>Heterogeneous oxidation:</b>		
(R1) C <sub>s</sub> + O <sub>2</sub> => CO + O <sub>s</sub>	3.3E+15	167.4
(R2) O <sub>s</sub> + 2C(b) => CO + C <sub>s</sub>	1.0E+08	0.
(R3) C <sub>s</sub> + O <sub>2</sub> => O <sub>2s</sub> + C(b)	9.5E+13	142.3
(R4) O <sub>2s</sub> + 2C(b) => C <sub>s</sub> + CO <sub>2</sub>	1.0E+08	0.
<b>CO<sub>2</sub> gasification reaction:</b>		
(R5) C <sub>s</sub> + CO <sub>2</sub> => CO + O <sub>s</sub> + C(b)	variable	251.0
<b>Steam gasification reaction:</b>		
(R6) C <sub>s</sub> + H <sub>2</sub> O => H <sub>2</sub> + O <sub>s</sub> + C(b)	variable	222.8



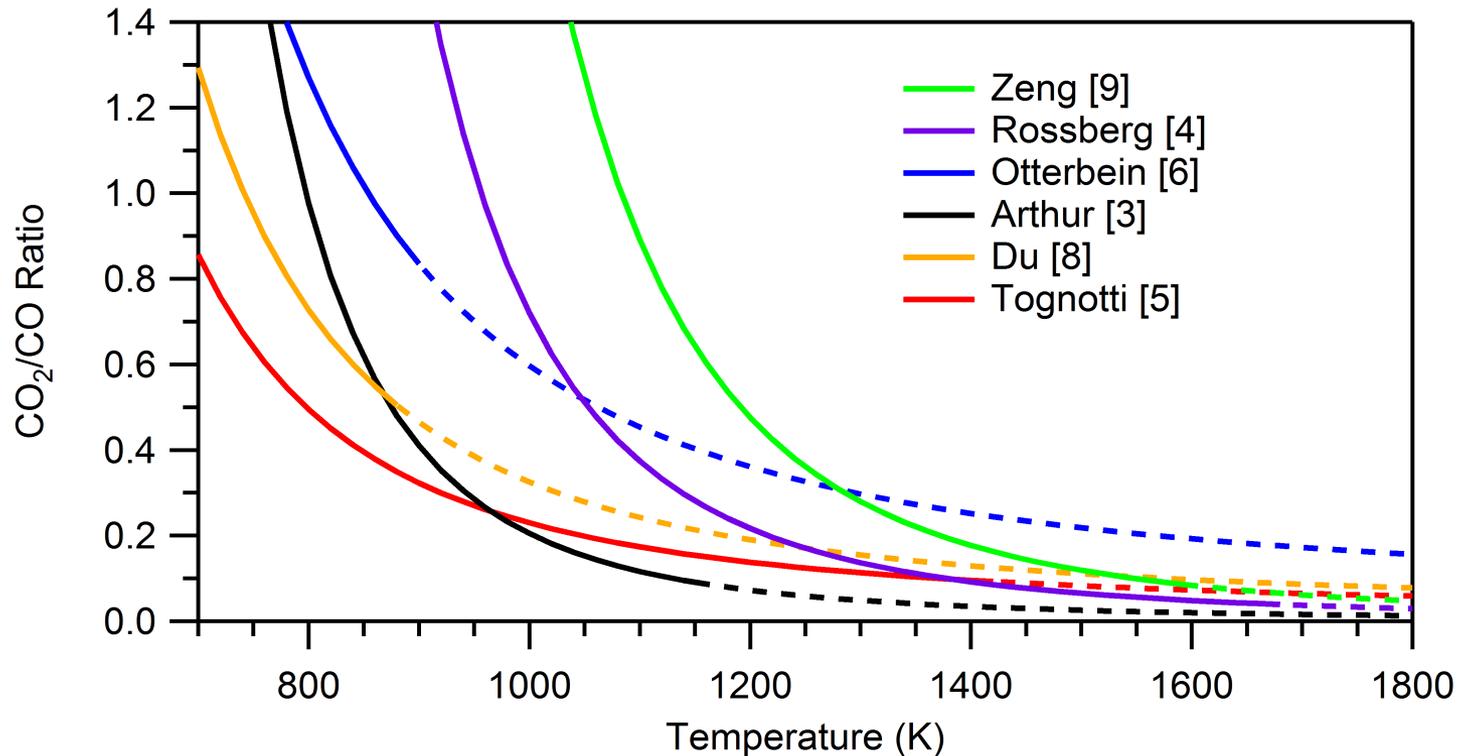
# Recent Results – CO<sub>2</sub>/CO Production Ratio

## Motivation:

- reaction of O<sub>2</sub> with C produces mostly CO<sub>2</sub> at low temperatures and CO at high temperatures
  - Important effect on char combustion rates due to difference in heat release (394 kJ/mol-C<sub>s</sub> vs 110 kJ/mol-C<sub>s</sub>) and difference in O<sub>2</sub> consumption

# Recent Results – CO<sub>2</sub>/CO Production Ratio

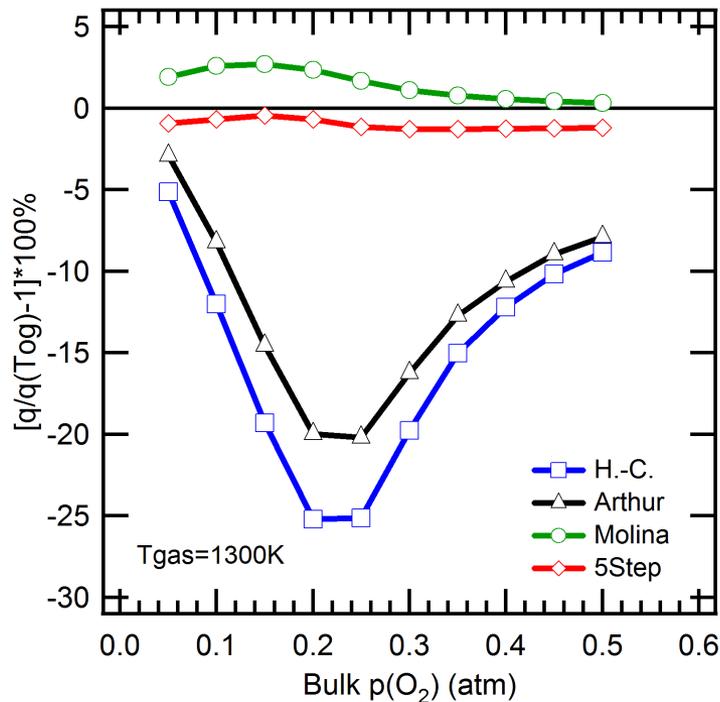
Published studies of CO<sub>2</sub>/CO production ratio



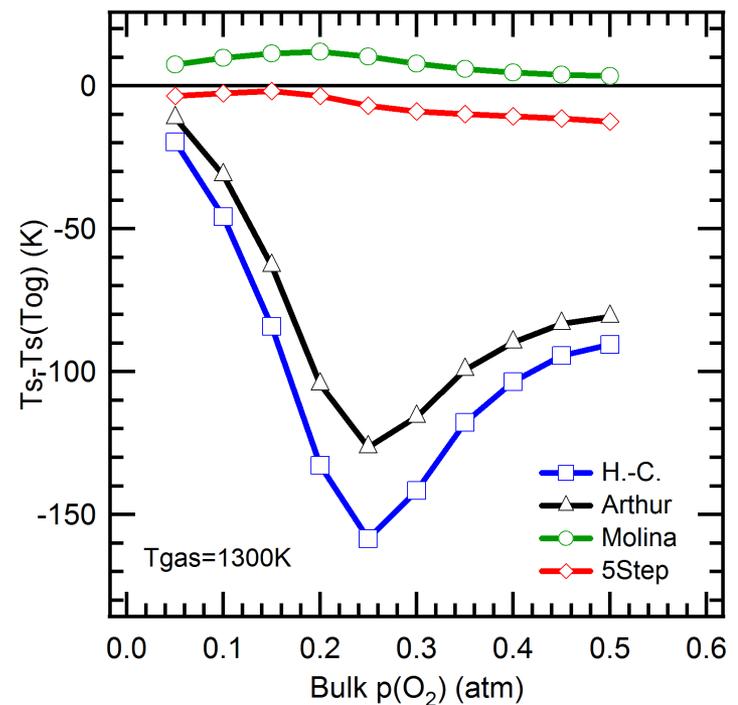
# Recent Results – CO<sub>2</sub>/CO Production Ratio

Assessment of importance of assumed CO<sub>2</sub>/CO production ratio

Error in burning rate predictions\*



Error in char particle T predictions\*



\* relative to Tognotti correlation

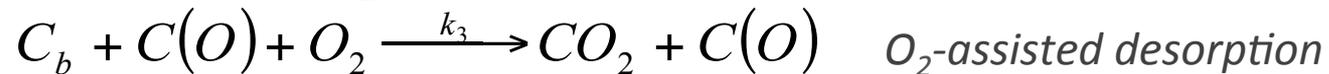
-- calculations based on measured kinetics for 50 um subbituminous (N. Antelope) char particles

# Recent Results – CO<sub>2</sub>/CO Production Ratio

## Motivation (cont'd):

- most commonly employed relationships in CFD are Arrhenius expressions from Arthur (with  $E_a = -52$  kJ/mol) and Tognotti et al. ( $E_a = -26$  kJ/mol + weak power law dependence on surface O<sub>2</sub>)

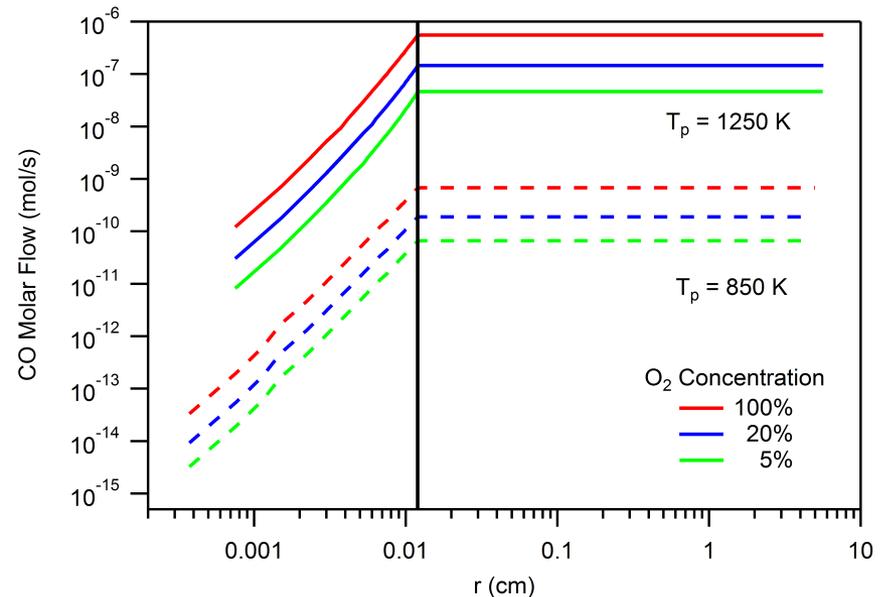
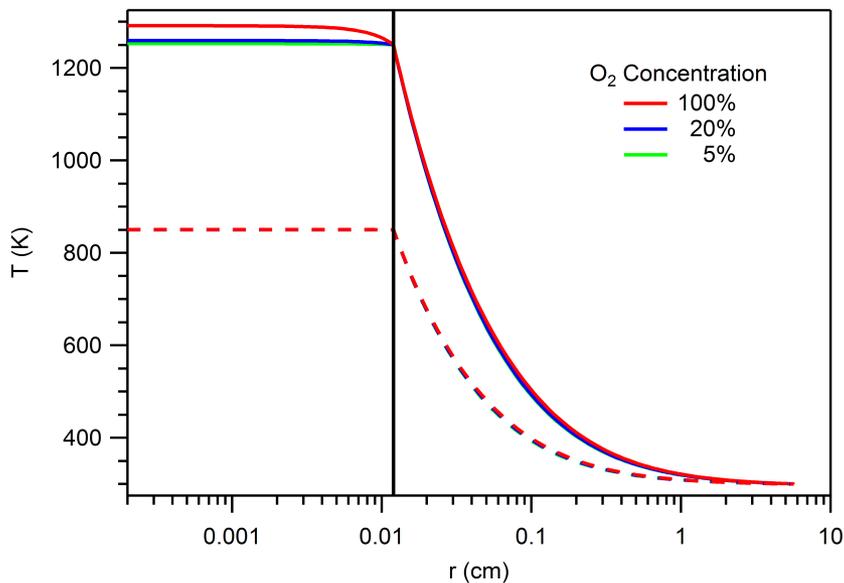
- dependence on O<sub>2</sub> is expected



- Tognotti levitated individual spherocarb particles ( $\approx 200$   $\mu\text{m}$  diameter) at room temperature, heated them with a laser, measured particle T with pyrometry, mass loss by virtue of balance voltage, and CO<sub>2</sub>/CO ratio in combustion products
- Tognotti assumed Zone I combustion conditions (uniform particle T, no CO conversion in particle or in boundary layer, negligible O<sub>2</sub> gradient)

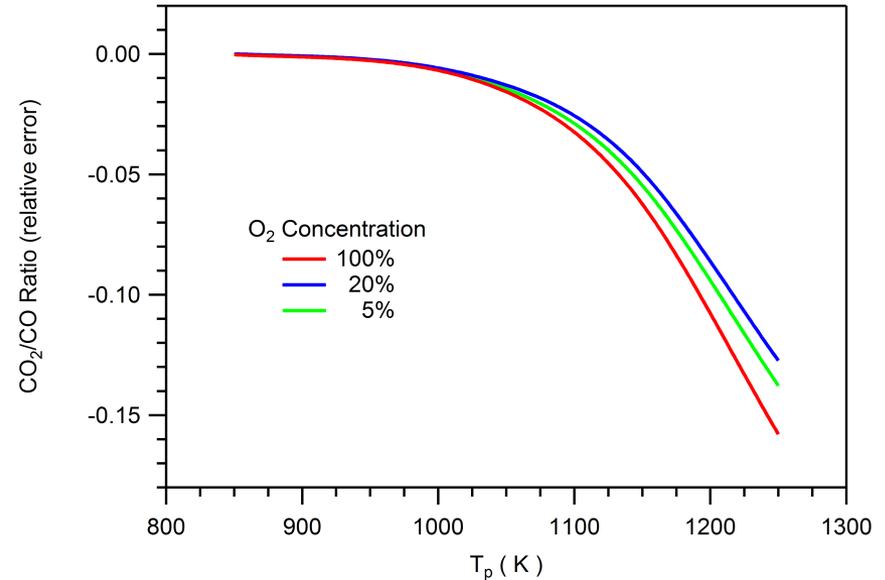
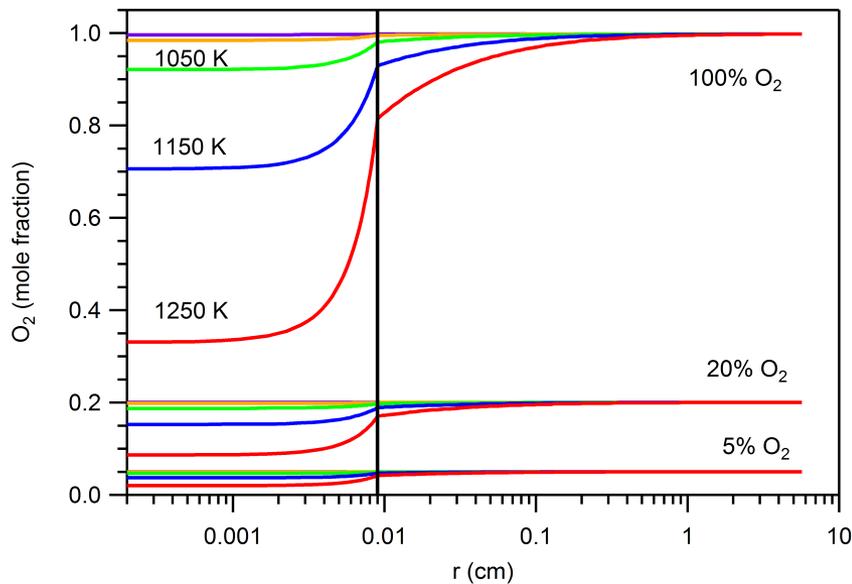
# Recent Results – CO<sub>2</sub>/CO Production Ratio

- Approach: use SKIPPY to assess Tognotti experiments
- Results:
  - Particle temperature is uniform (for experiments up to 1250 K)
  - Negligible CO consumption in the boundary layer (for  $T \leq 1250$  K) nor within the particle



# Recent Results – CO<sub>2</sub>/CO Production Ratio

- Results (cont'd):
  - Diffusional resistance becomes significant for  $T > 1050$  K
  - Because of weak sensitivity of CO<sub>2</sub>/CO production ratio to [O<sub>2</sub>], Zone I interpretation of Tognotti measurements is valid to 1150 K

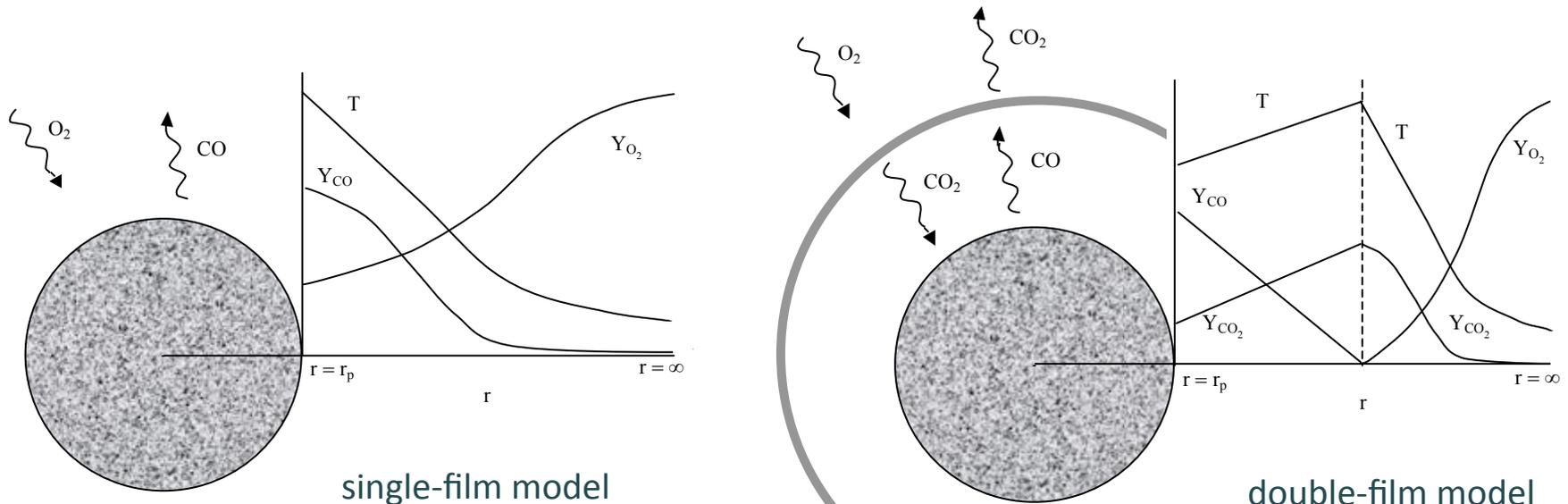


Results support use of Tognotti expression:  $CO_2/CO = 0.02 p_{O_{2,s}}^{0.21} \exp(3070/T_p)$

# Recent Results – Single-Film and Double-Film Models

## Motivation:

- most CFD modelers use so-called ‘single-film’ apparent kinetics model of char combustion, whereas others use ‘double-film’ model
  - both neglect effect of different extents of reactant penetration
  - single-film model neglects CO conversion in particle boundary layer
  - double-film model assumes all of the CO emitted from the particle is consumed at a flamefront in the boundary layer





# Recent Results – Single-Film and Double-Film Models

## Motivation (cont'd):

- our previous results demonstrate that CO is partially converted in the boundary layer (continuous film) for high particle/gas temperatures, e.g. during oxygen-enriched combustion
- our previous results demonstrate char gasification reactions with CO<sub>2</sub> and steam are important and lead to partial reactant penetration during oxy-fuel combustion
- unclear which of the two models is most accurate under oxy-fuel combustion conditions



# Recent Results – Single-Film and Double-Film Models

## Approach:

- Use SKIPPY to assess predictions of single-film and double-film models
  - employ combination of oxidation and gasification reactions
  - analyze range of particle sizes burning in both  $N_2$  and  $CO_2$  diluent environments with 14 vol-%  $H_2O$  and 12 – 60 vol-%  $O_2$
  - use particle reactivity corresponding to a PRB subbituminous coal char



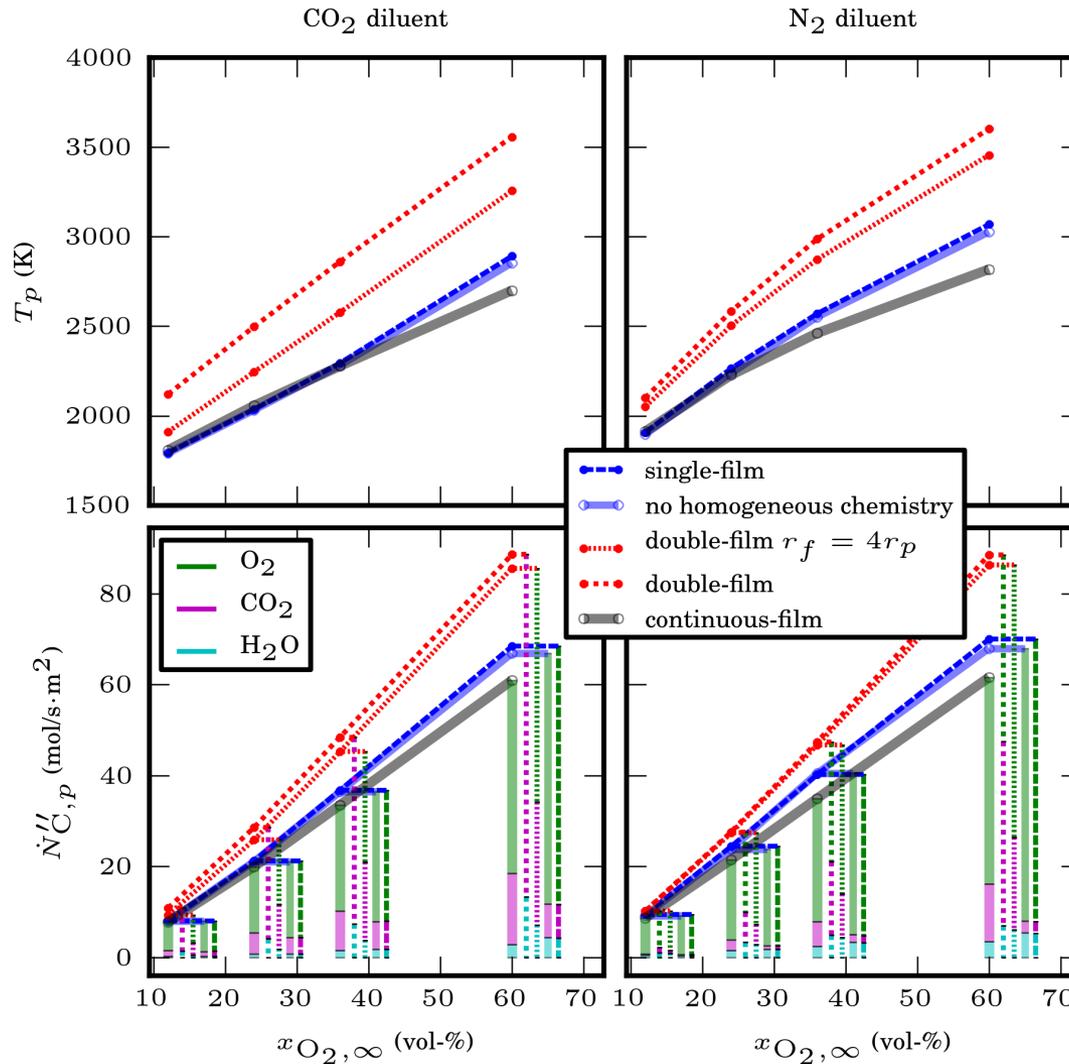
# Recent Results – Single-Film and Double-Film Models

## Results:

- Over evaluated range of  $d_p$  (60 – 135  $\mu\text{m}$ ), single-film model is always superior to double-film model, no matter where the flame sheet is assumed to occur in the boundary layer
  - heat release from CO flame in double-film model always leads to overpredicted  $T_p$  and carbon burning rate
- $\text{CO}_2$  and steam gasification reactions must be included to give accurate prediction of  $T_p$  and, to a lesser extent, carbon burning rate (in agreement with our previous analyses)
- Stefan flow must be included to give accurate predictions for high reaction rate conditions (e.g. oxygen-enriched char combustion)

# Recent Results – Single-Film and Double-Film Models

Results:





# Recent Results – Single-Film and Double-Film Models

## Conclusions:

- Use of the single-film model appears to be generally warranted
- For broad applicability in oxy-fuel combustion environments, gasification reactions and Stefan flow should be included



# Recent Results – Apparent Kinetics and Gas Diffusivity

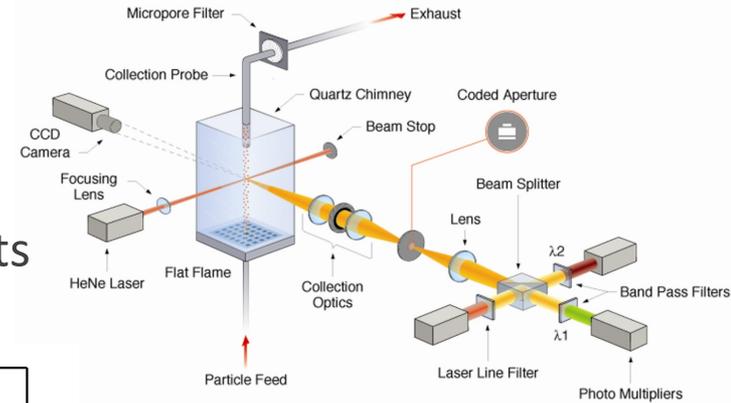
## Motivation:

- CFD modelers almost always use apparent Arrhenius kinetics model of char combustion, neglecting effect of different extents of reactant penetration
- during oxy-fuel combustion with FGR, char combustion occurs in a CO<sub>2</sub> background gas, rather than N<sub>2</sub>
- the 20% lower diffusivity of O<sub>2</sub> in CO<sub>2</sub> has been shown to reduce apparent char burning rates, attributed to slower diffusion through the external boundary layer
- unclear how much lower gas diffusivity *through the char pores* also reduces the burning rate

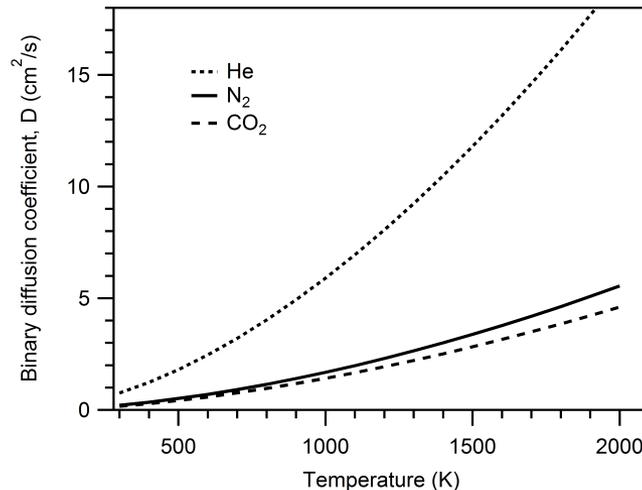
# Recent Results – Apparent Kinetics and Gas Diffusivity

## Approach:

- use laminar entrained flow reactor to produce same T combustion environments with N<sub>2</sub>, CO<sub>2</sub>, and He diluents
  - He has very high diffusivity



Diffusivity of O<sub>2</sub> in Diluent Gases



$$D_{O_2-He} \approx 3.5 D_{O_2-N_2}$$

- measure 70 μm PRB subbituminous char particle combustion temperatures and burnout rates in different environments
- compare measurements against intrinsic and apparent kinetics models

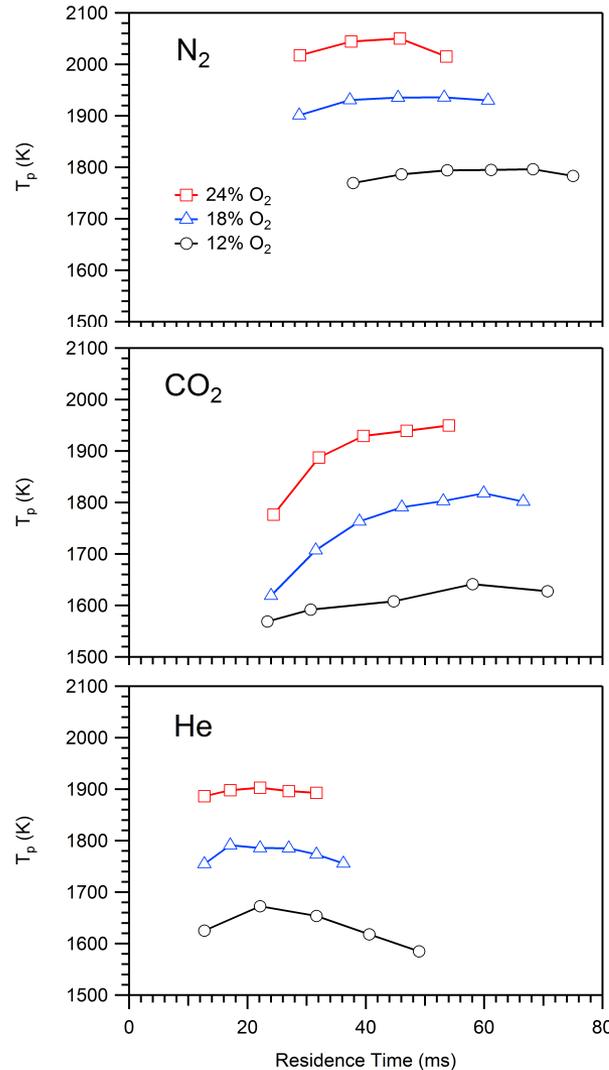
# Recent Results – Apparent Kinetics and Gas Diffusivity

## Results:

mean  $T_p$  of 100 – 150  
single-particle data  
points

Particles burn 100 –  
150 K cooler in  $\text{CO}_2$   
than in  $\text{N}_2$  (as seen  
previously)

Particles ignite much  
faster in He, but burn  
cooler (relative to  $\text{N}_2$ )

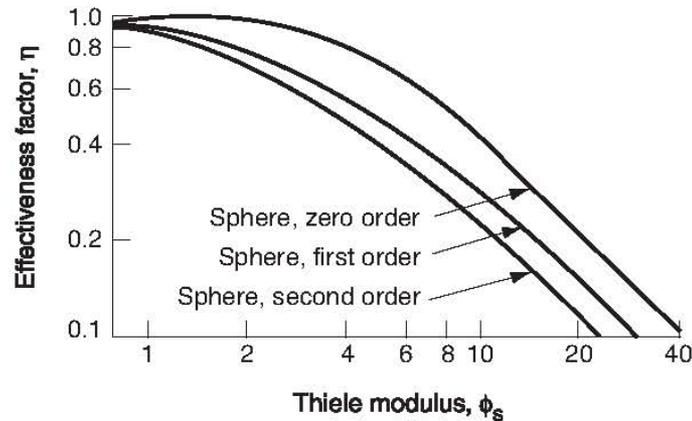


$$\lambda_{\text{O}_2\text{-He}} \approx 5 \lambda_{\text{O}_2\text{-N}_2}$$

# Recent Results – Apparent Kinetics and Gas Diffusivity

## Results:

- preliminary application of apparent kinetics model to the data suggests > 2X greater reactivity in He
- from catalyst theory, greatest variation in effectiveness factor (extent of char particle participating in reaction) with thiele modulus is for high modulus, with a slope of  $\eta \sim 1/\phi_n$ , so maximum difference in apparent rate one would expect for He vs. N<sub>2</sub> would be a factor of 1.9 (= sqrt(3.5))

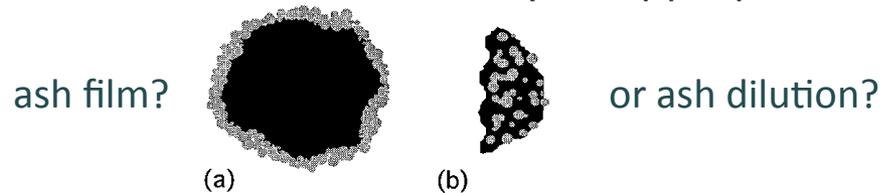


- extension to CO<sub>2</sub> vs N<sub>2</sub> suggests maximum apparent kinetics rate decrease of 11%, for same actual intrinsic kinetic rate

# Recent Results – Ash Inhibition of Char Combustion

## Motivation:

- final burnout of char always occurs with carbon embedded in ash
- in some parts of the world (e.g. India and Brazil), coals with high ash content are increasingly being mined and used
- ash inhibition of pulverized coal combustion has always been modeled (when it has been modeled) as an ash film effect, despite little evidence that ash films are commonly formed
- our previous experimental measurements have suggested mineral components exposed at pore surface can diffuse back into char matrix (Lunden et al., PCI 27:1695-1702, 1998)
  - suggests ‘ash dilution’ model may be appropriate



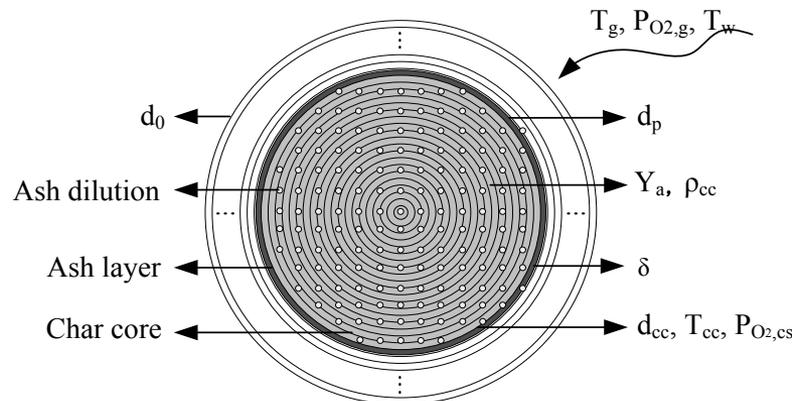
- we previously showed that ash dilution will result in low apparent reaction order (Murphy and Shaddix, CNF 157:535-539, 2010)

# Recent Results – Ash Inhibition of Char Combustion

## Approach:

- develop robust transient, intrinsic kinetics model of ash inhibition that can treat ash film effect as well as ash dilution, and which can assign a user-specified fraction of liberated ash to either effect
- compare model predictions against experimental measurements of char combustion temperatures and C burnout over range of  $O_2$  concentrations (all previous ash film models only compared against burnout data, and for small variation in  $O_2$ )

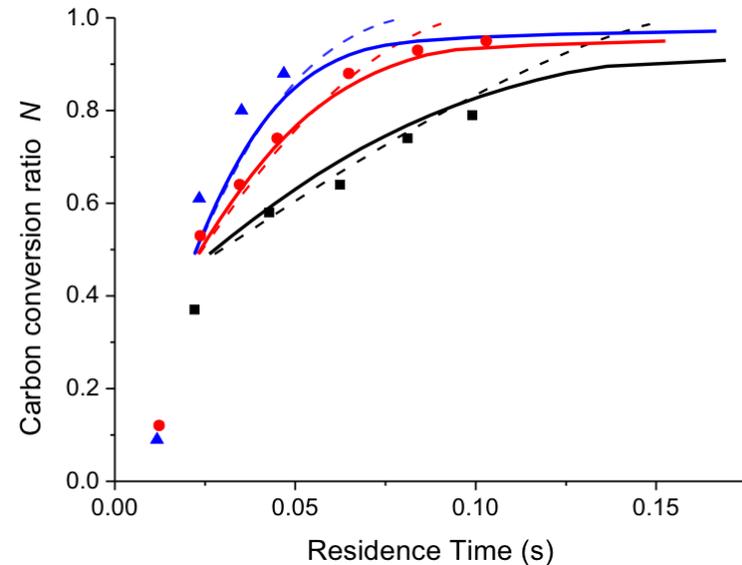
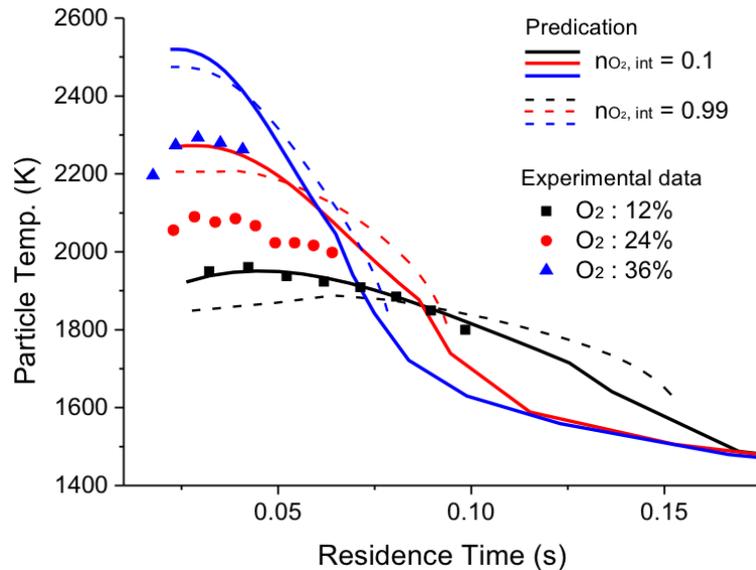
schematic of ash inhibition model



presence of ash reduces internal diffusivity and available surface area, as well as external diffusion to the char particle

# Recent Results – Ash Inhibition of Char Combustion

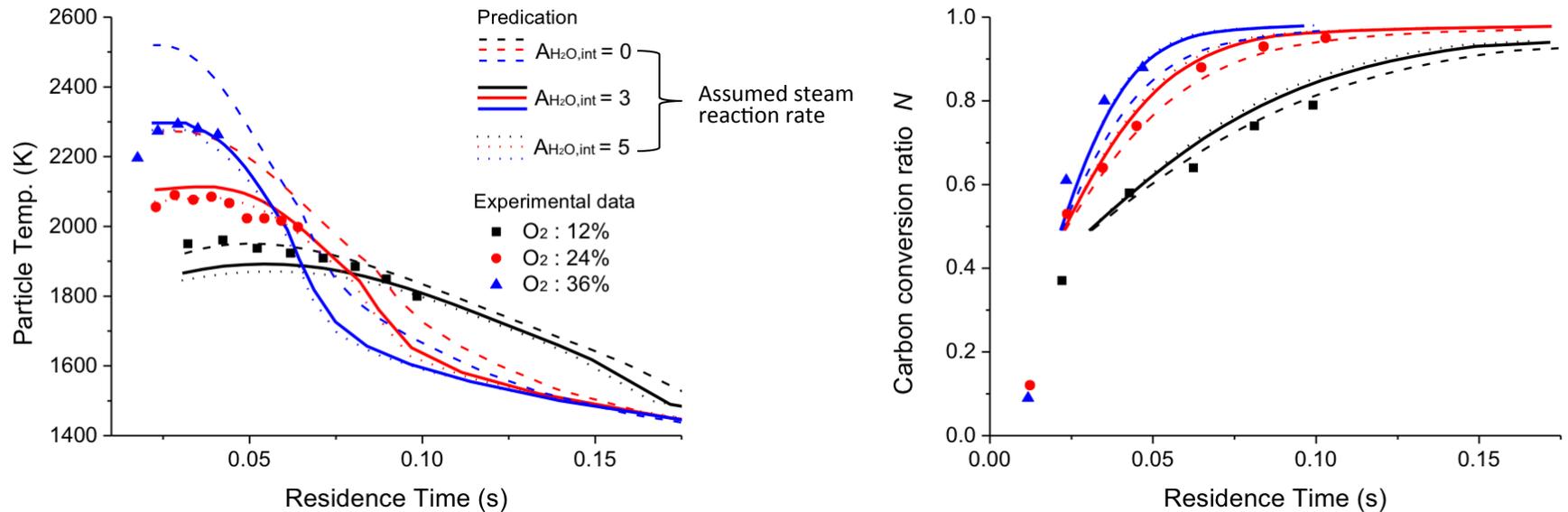
Results (modeling char oxidation only):



- predicted char combustion temperatures increase too rapidly as  $p_{O_2}$  increases
- assumed intrinsic reaction order has minor influence on trends
- burnout predictions are quite accurate

# Recent Results – Ash Inhibition of Char Combustion

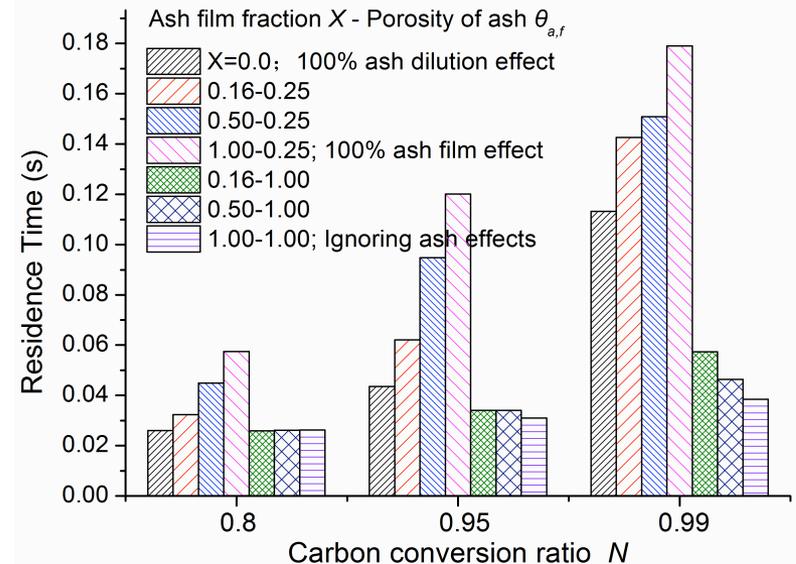
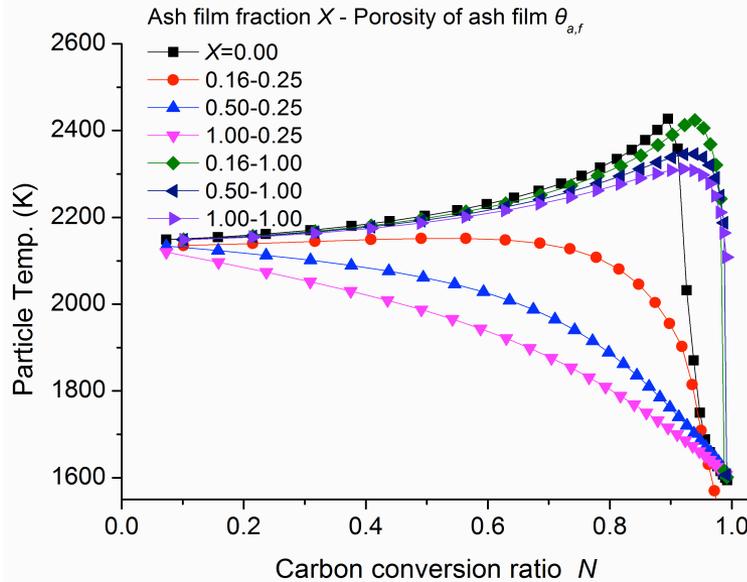
Results (modeling char oxidation + steam gasification):



- inclusion of steam gasification reaction improves predicted char combustion temperatures (consistent with our previous findings for oxy-fuel combustion)
- burnout predictions are still accurate – inclusion of gasification rate slightly increases burnout

# Recent Results – Ash Inhibition of Char Combustion

Results (ash film vs. ash dilution effects):



- ash film cools particle throughout char conversion, resulting in slower burnout
- ash dilution effect is primarily manifested at large extents of burnout
- char kinetic reactor data are *inconsistent* with model results assuming dominant fraction of liberated ash contributes to external ash film



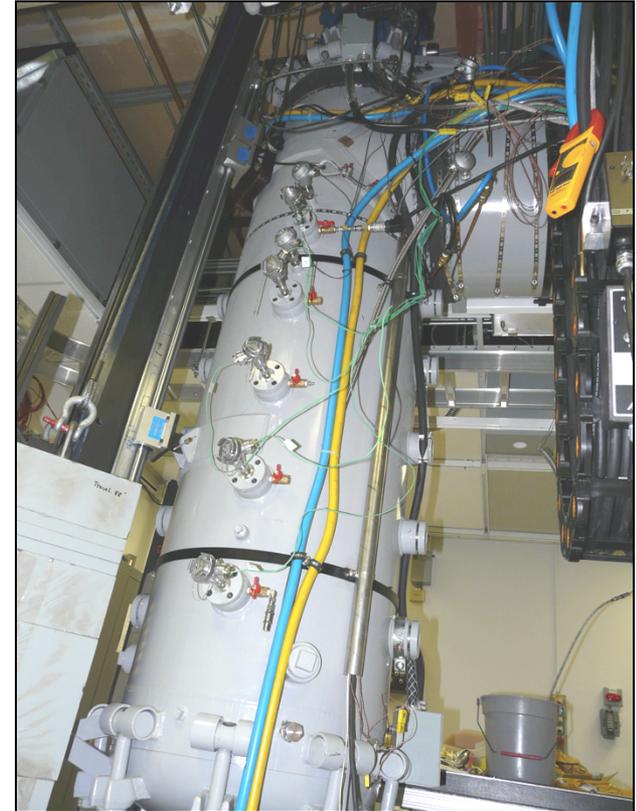
# Recent Results – Pressurized Gasification Kinetics

## Motivation:

- carbon conversion is inherently a limiting factor in gasifier design and operation – is closely linked to minimum operating T of gasifier and to refractory wear
- dearth of quality data and rate information at high temperatures at which gasifiers operate
- high activation energy of char gasification means extrapolating rates from TGA measurements (at 1000-1100 K) gives erroneous results
- gasification kinetics are complicated at pressure, because of action of reverse reactions involving gasification products (CO and H<sub>2</sub>)

## Approach:

- perform experiments in specially designed, turbulent entrained flow reactor – low particle loading, isothermal conditions
- separate char formation step from char gasification, to clearly quantify rates – i.e. pre-form chars
- perform optical measurements of char particle temperatures, as well as extractive measurements of carbon conversion, to quantify rates
- build-up kinetic knowledge sequentially: measure char gasification in  $\text{CO}_2$  only, and in  $\text{H}_2\text{O}$  only, then in mixtures of  $\text{CO}_2$  and  $\text{H}_2\text{O}$ , then add in  $\text{H}_2$  and  $\text{CO}$



Pressurized entrained flow reactor

## Results:

- developed procedure for generating high heating rate char particles – 1200 °C, 250 ms
- designed, fabricated, and calibrated fiber-optic probe for in situ particle T measurements



SEM of generated coal char

cold target probe

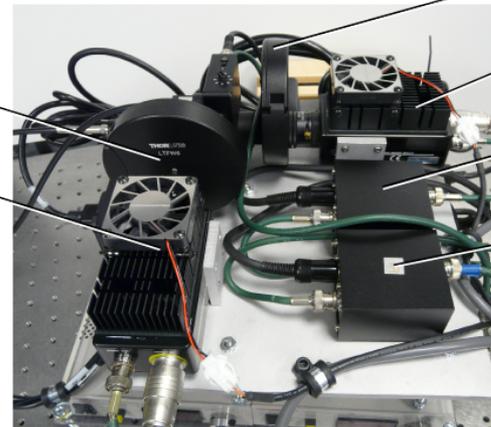


optical collection probe



IR ND filter wheel

IR PMT module



visible ND filter wheel

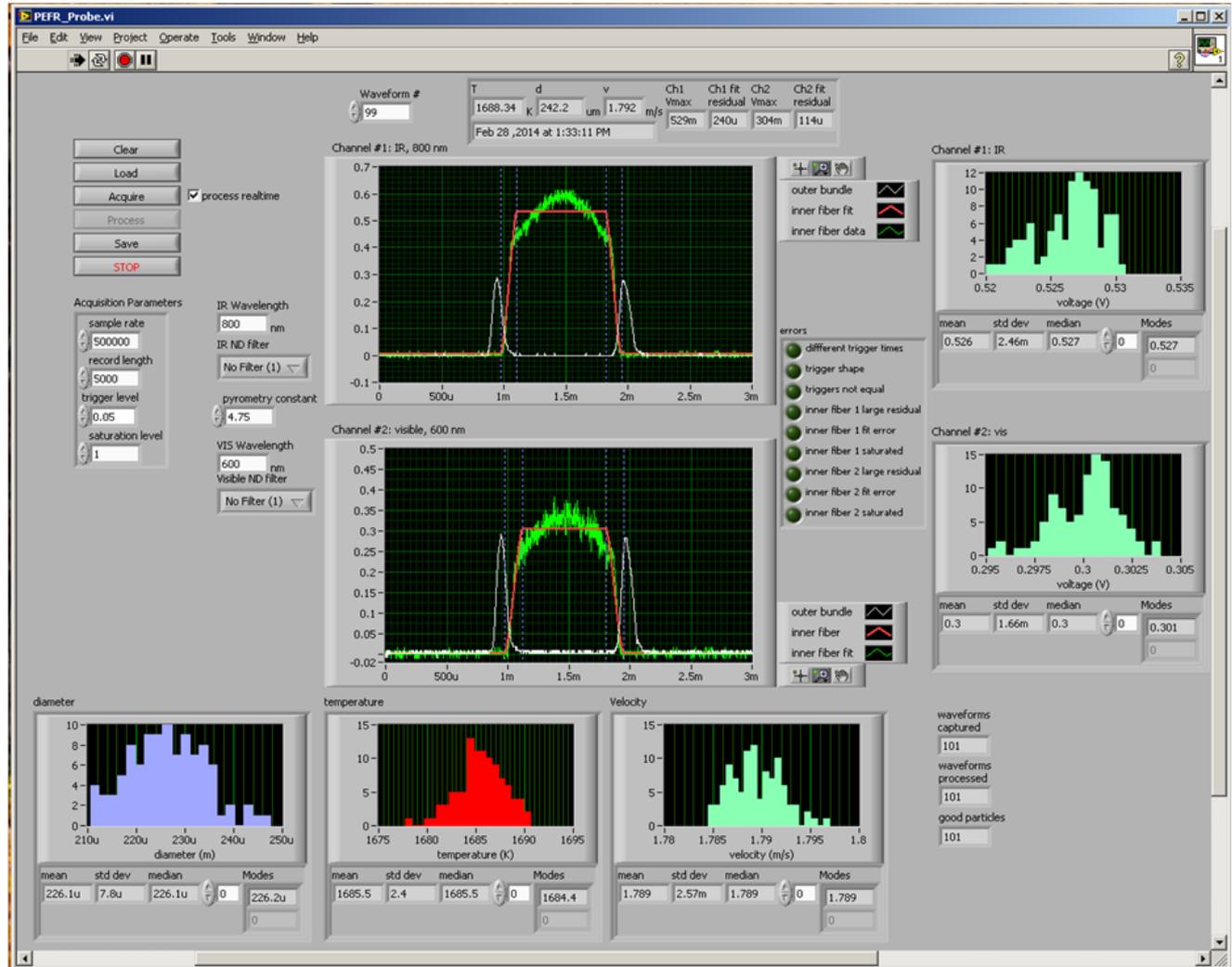
visible PMT module

visible current-voltage amplifier

IR current-voltage amplifier

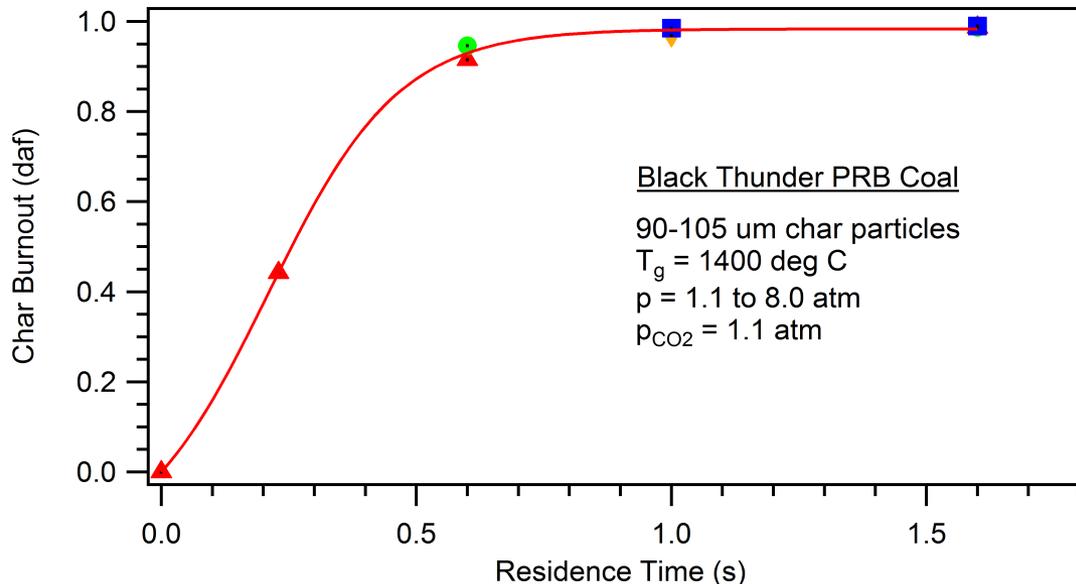
Results:

Labview display of optical probe calibration data



## Results:

- performed char gasification experiments with various CO<sub>2</sub> concentrations at 1400 °C and pressures up to 8 atm (improved heating and thermal management will allow experiments up to 20 atm)



Measured char burnout for partial pressure of CO<sub>2</sub> of 1.1 atm, over total pressure range of 1 – 8 atm



# Continuing and Future Work

- Measurement of gas temperature profile in 2200 K CO<sub>2</sub> environments – to complete quantification of char gasification kinetics at 1 atm
- Complete analysis of apparent and intrinsic kinetics in 'He study'
- Additional char gasification kinetic measurements in high-p entrained flow reactor, utilizing new optical pyrometry probe
- Oxy-fuel char combustion kinetics at elevated p



## Summary of Recent Progress

- Tognotti expression for  $\text{CO}_2/\text{CO}$  production at char surface has been numerically justified, based on Tognotti data (for  $T < 1150 \text{ K}$ )
- The single-film char combustion model, when accounting for Stefan flow and combined oxidation/gasification kinetics, has been shown to give reasonably accurate predictions for a wide range of oxy-fuel combustion environments
- Lower diffusivity of  $\text{O}_2$  in  $\text{CO}_2$  has been shown to result in lower apparent kinetic rates (by up to 11%)
- Ash inhibition of char burnout has been shown to *not* be accurately modeled as due to ash film formation, but to a mix of ash film and ash dilution effects
- A new optical probe has been developed for application to pressurized gasification and oxy-fuel combustion environments
- $\text{CO}_2$  gasification kinetics of pc char has been quantified from 1 – 8 atm



# Acknowledgments

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- Funding provided through FE Crosscutting Research Program



# Recent Publications

## *Refereed journal articles*

- M. Schiemann, M. Geier, C.R. Shaddix, N. Vorobiev, V. Scherer, “Determination of char combustion kinetics parameters: Comparison of point detector and imaging-based particle-sizing pyrometry,” submitted to *Review of Scientific Instruments*.
- Y. Niu, C.R. Shaddix, “A sophisticated model to predict ash inhibition during combustion of pulverized char particles,” accepted for publication in *Proceedings of the Combustion Institute*.
- D. Kim, S. Choi, M. Geier, C.R. Shaddix, “Effect of CO<sub>2</sub> gasification reaction on char particle combustion in oxy-fuel conditions,” *Fuel* 120 (2014) 130-140.
- C.R. Shaddix, F. Holzleithner, M. Geier, B.S. Haynes, “Numerical assessment of Tognotti determination of CO<sub>2</sub>/CO production ratio during char oxidation,” *Combustion and Flame* 160 (2013) 1827-1834.
- E.S. Hecht, C.R. Shaddix, J.S. Lighty, “Analysis of the errors associated with typical pulverized coal char combustion modeling assumptions for oxy-fuel combustion,” *Combustion and Flame* 160 (2013) 1499-1509.
- M. Geier, C.R. Shaddix, F. Holzleithner, “A mechanistic char oxidation model consistent with observed CO<sub>2</sub>/CO production ratios,” *Proceedings of the Combustion Institute* 34 (2013) 2411-2418.
- E.S. Hecht, C.R. Shaddix, M. Geier, A. Molina, B.S. Haynes, “Effect of CO<sub>2</sub> and steam gasification reactions on the oxy-combustion of pulverized coal char,” *Combustion and Flame* 159 (2012) 3437-3447.
- C.R. Shaddix, “Coal combustion, gasification, and beyond: Developing new technologies for a changing world,” invited article, *Combustion and Flame* 159 (2012) 3003-3006.
- M. Geier, C.R. Shaddix, K.A. Davis, H.-S. Shim, “On the use of single-film models to describe the oxy-fuel combustion of pulverized coal char,” *Applied Energy* 93 (2012) 675-679.