



NETL Life Cycle Inventory Data

Process Documentation File

Section II: Process Description

Associated Documentation

This unit process is composed of this document and the data sheet (DS) *DS_Stage1_O_NG_Sweetening_2010.01.xls*, which provides additional details regarding relevant calculations, data quality, and references.

Goal and Scope

The scope of this unit process encompasses the energy inputs and material outputs for the processing of natural gas to remove hydrogen sulfide. The unit process is based on the reference flow of 1 kg of sweetened natural gas. The relevant flows of this unit process are described below and shown in **Figure 1**.

The inputs to this unit process are natural gas, ground water, and diethanolamine (DEA) solvent. Ground water is a natural resource and thus enters the boundary of this unit process with no upstream environmental burdens. The inputs of natural gas and diethanolamine represent upstream processes that have material and energy flows that are not included in this unit process but are accounted for by other unit process. The output of this unit process is sweetened natural gas that is suitable for long-distance pipeline transmission and subsequent combustion by utilities, industry, or consumers. This unit process also accounts for environmental emissions that are directly released by the natural gas sweetening operations.

Boundary and Description

Raw natural gas contains varying levels of hydrogen sulfide (H_2S), a toxic gas that reduces the heat content of natural gas and causes fouling when combusted in equipment. The removal of H_2S from natural gas is known as "sweetening". Amine-based processes are the predominant technologies for the sweetening of natural gas.

The H_2S content of raw natural gas is highly variable, with typical concentrations ranging from $5.7E-05$ kg of H_2S per kg of natural gas to 0.16 kg of H_2S per kg of natural gas. This analysis assumes an H_2S concentration of $2.3E-05$ kg of H_2S per kg of natural gas (which is equivalent to 1 mole of H_2S per kg of natural gas).

The energy consumed by the amine reboiler accounts for the majority of energy consumed by the sweetening process. Reboiler energy consumption is a function of the amine flow rate, which, in turn, is related to the amount of H_2S removed from natural gas.

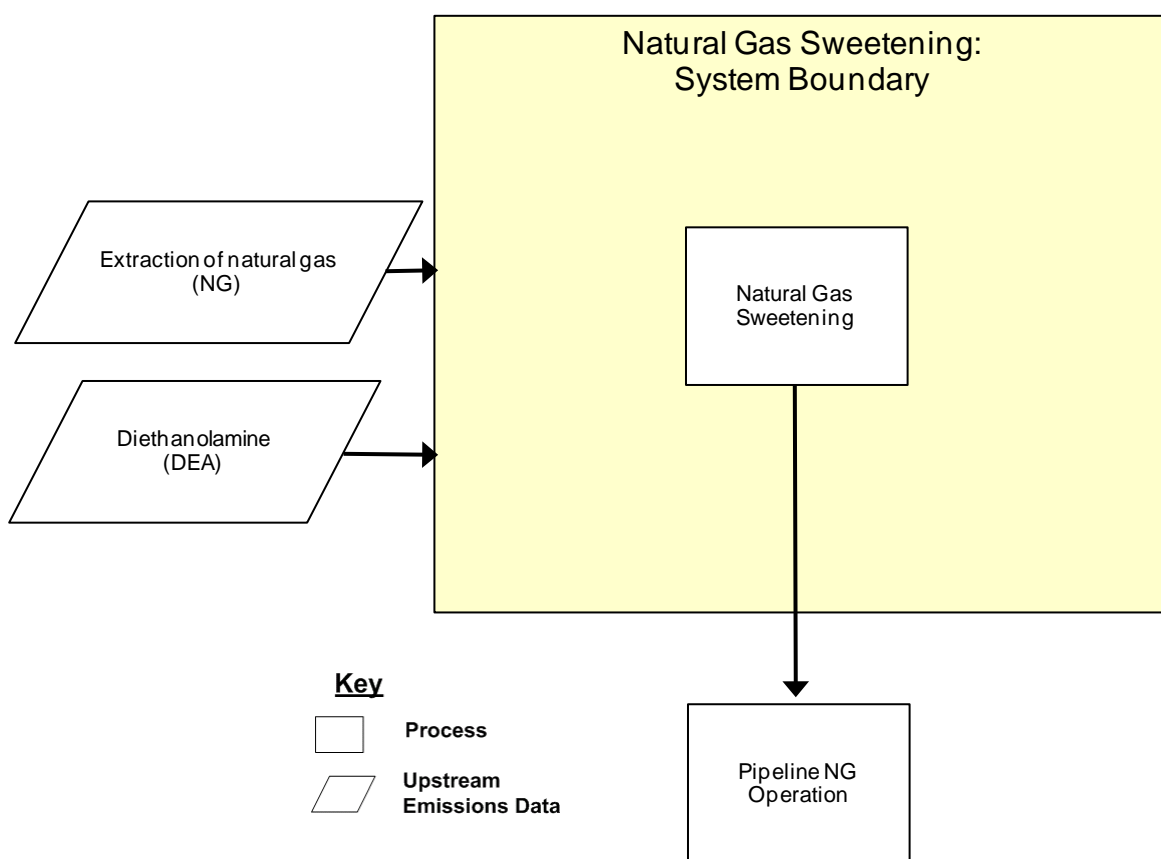
Approximately 0.30 moles of H_2S are removed per 1 mole of circulated amine solution (Polasek, 2006), and the reboiler duty is approximately 1,000 Btu per gallon of amine (Arnold, 1999).

The amine reboiler combusts natural gas to generate heat for amine regeneration. This analysis applies EPA emission factors for industrial boilers (EPA, 1996) to the energy consumption rate discussed in the above paragraph in order to estimate the combustion emissions from amine reboilers.

The sweetening of natural gas is also a source of vented methane emissions. In addition to absorbing H₂S, the amine solution also absorbs a portion of methane from the natural gas. This methane is released to the atmosphere during the regeneration of the amine solvent. The venting of methane from natural gas sweetening is based on emission factors developed by the Gas Research Institute; natural gas sweetening releases 2.8E-05 per kg of natural gas sweetened (API, 2009).

The loss rate of amine solvent is 2.4E-05 kg per kg of natural gas sweetened (Stewart, 1994). The loss rate of water is 2.8E-03 kg per kg of natural gas sweetened (Lungsford, 2006).

Figure 1: Unit Process Scope and Boundary



Key properties of the amine-based natural gas sweetening technology are summarized in **Table 1**. These properties include the solvent type, energy requirements, and material losses. These variables are expressed on the same bases as reported in literature and do not necessarily match the bases as described above.

The inputs and outputs of this unit process are summarized in **Table 2**.

Table 1: Properties of Amine-Based Natural Gas Sweetening Technology

| Property | Value | Source |
|---|---|---------------------------|
| Solvent type | Diethanolamine | Polasek 2006 |
| Reboiler duty | 1,000 Btu/gal amine | Polasek 2006; Arnold 1999 |
| Molar loading | 3.3 mol H ₂ S/mol amine | Polasek 2006 |
| Default H ₂ S composition of raw natural gas | 1 mol H ₂ S per kg raw natural gas | EPA 1995; TOTAL SA 2006 |
| Amine loss rate | 0.1 lb per million cubic feet of natural gas | Stewart 1994 |
| Water loss | 115 lb per million cubic feet of natural gas | Lunsford 2006 |

Table 2: Unit Process Input and Output Flows

| Flow Name* | Value | Units (Per Reference Flow) |
|---|----------|----------------------------|
| Inputs | | |
| Natural gas, unsweetened | 1.0016 | kg |
| Diethanolamine (DEA) [Organic intermediate products] | 2.38E-06 | kg |
| Water (ground water) [Water] | 2.75E-03 | kg |
| Outputs | | |
| natural gas (sweetened) | 1.00 | kg |
| Carbon dioxide [Inorganic emissions to air] | 1.60E-06 | kg |
| Methane [Organic emissions to air (group VOC)] | 2.75E-05 | kg |
| Nitrous oxide (laughing gas) [Inorganic emissions to air] | 8.73E-09 | kg |
| Nitrogen oxides [Inorganic emissions to air] | 3.66E-06 | kg |
| Sulphur dioxide [Inorganic emissions to air] | 2.20E-08 | kg |
| Carbon monoxide [Inorganic emissions to air] | 3.07E-06 | kg |
| NMVOC (unspecified) [Group NMVOC to air] | 2.01E-07 | kg |
| Dust (PM10) [Particles to air] | 2.78E-07 | kg |
| Lead (+II) [Heavy metals to air] | 1.83E-11 | kg |
| Water (Evaporated) [Water] | 2.75E-03 | kg |

* **Bold face** clarifies that the value shown *does not* include upstream environmental flows. Upstream environmental flows were added during the modeling process using GaBi modeling software, as shown in Figure 2.

Embedded Unit Processes

None.

References

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Section III: Document Control Information

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