

CO₂ Compression Using Supersonic Shock Wave Technology

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Forward Looking Statement



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The Company – Brief Background

- Privately held since 1993, headquartered in Bellevue, WA
- Development and test of supersonic turbo-components for process gas and power generation applications
- 1998-present, \$30 M in private funds and \$25.0 M in DOE, DOD and CEC PIER support
- 2008-Dresser-Rand investment of up to \$49M to commercialize supersonic compression technology
- Novel technology permits high pressure ratios and efficiencies
- DOE Supporting commercial scale compressor demonstration (10 khp)
- 26 full-time employees
 - Ingersoll-Rand, CAT/Solar, P&W, Boeing, Honeywell, Rocketdyne
 - 3 PhD & 9 MS Degreed Engineers



DRESSER-RAND



Project Overview

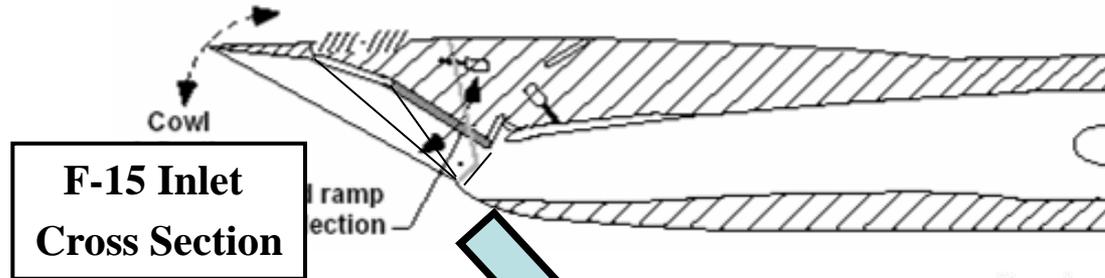
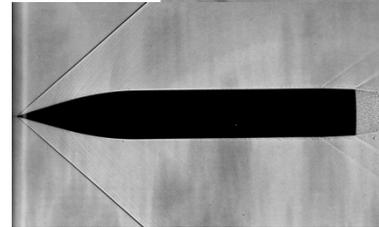
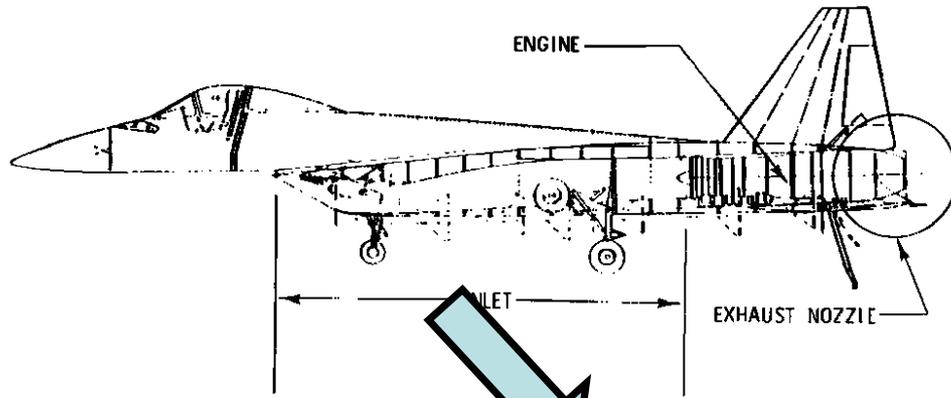
- **Funding (DOE and Cost Share)**
 - Total Funding – Current Contract \$42.2M (DE-FE0000493)
 - DOE – \$20.0M
 - Ramgen – \$22.2M
- **Overall Project Performance Dates**
 - August 1, 2009 – November 30, 2012
- **Project Participants**
 - DOE
 - Ramgen
 - Dresser-Rand – Integrated demonstration tests
 - Naval Post Graduate School Turbo Machinery Laboratory – static component testing
 - Consulting engineering organizations
- **Overall Project Objectives (SOPO)**
 - Incorporate lessons learned from previous Ramgen shock compression test programs and recommendations from industry partner Dresser-Rand to define and execute improvements in development plan for large scale demonstration of novel CO₂ compression technology

World Class Test Facilities

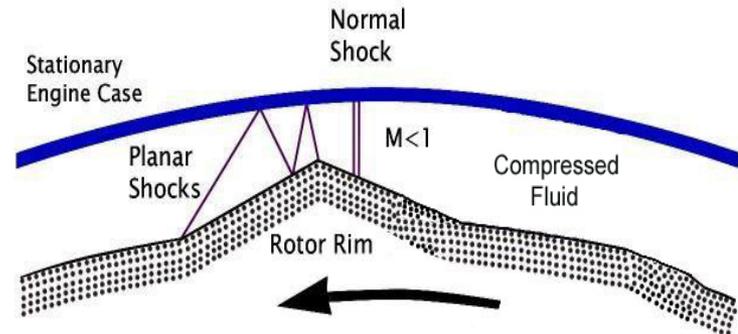


DRESSER-RAND.

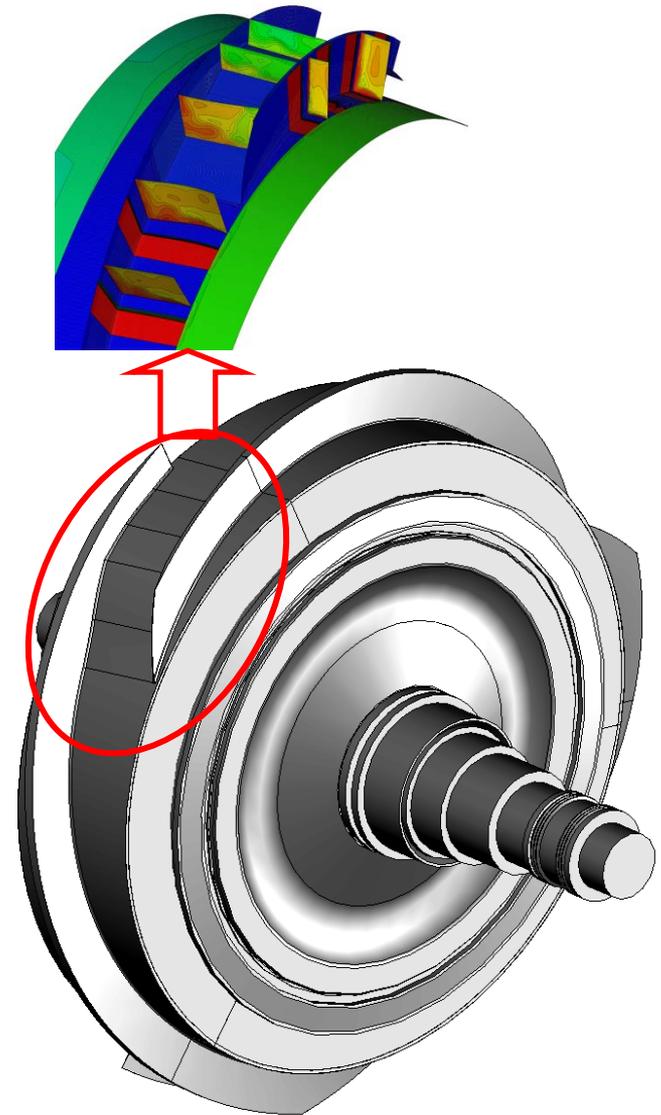
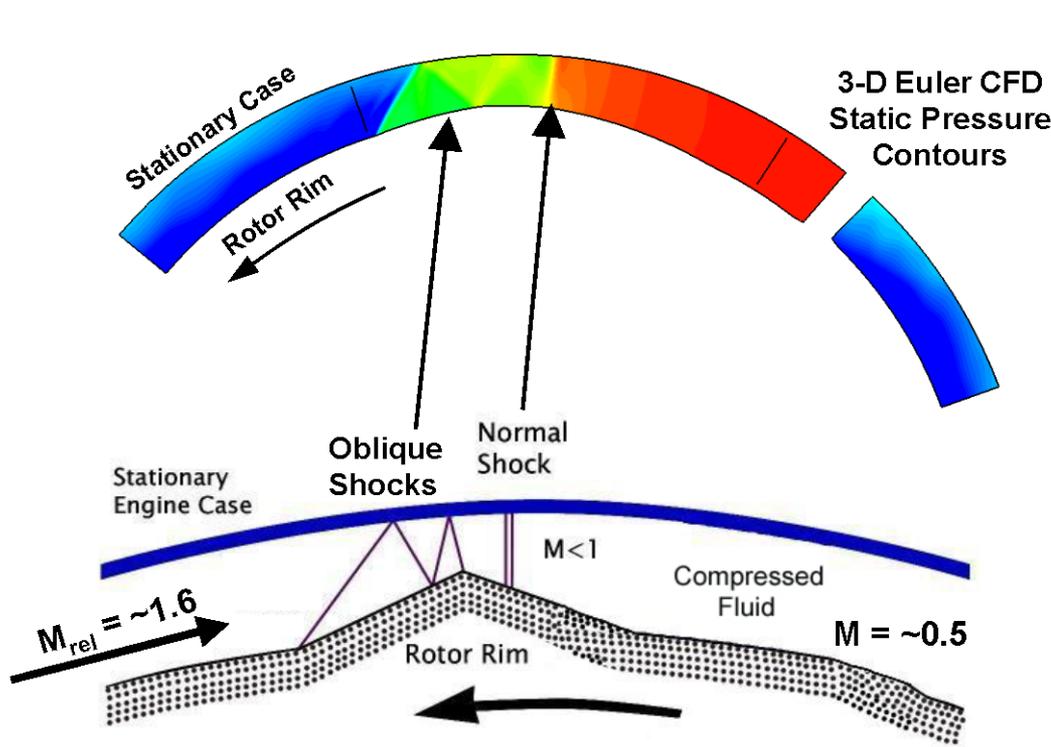
Technology Fundamentals/Background



Rampressor Rotor

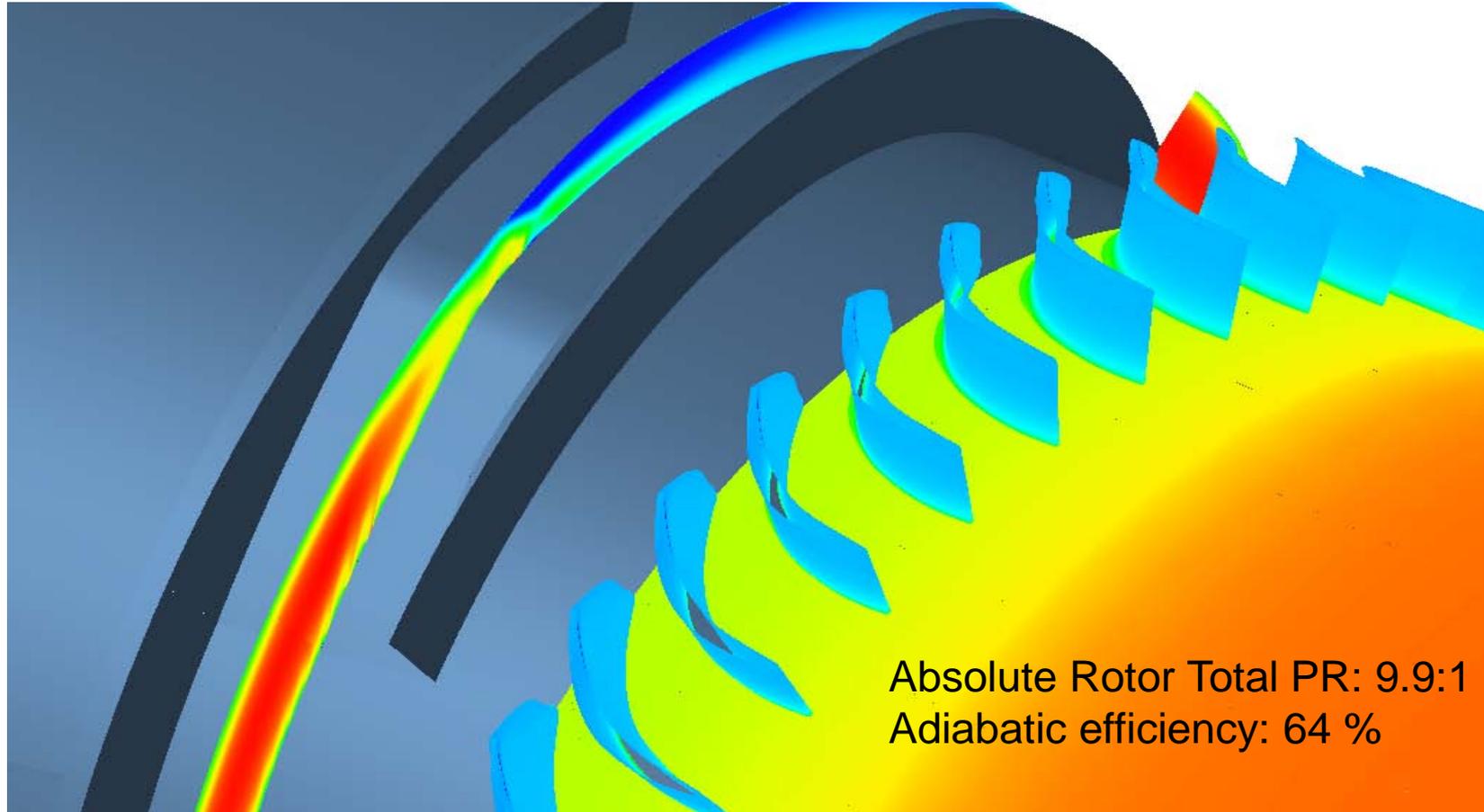


Rampressor 3-D Geometry & Flowfield



- Compressive flowpaths integrated onto rim of rotor at shallow helix angle
- Strakes form sidewalls for shock compression ducts & separate high pressure discharge from low pressure suction

Effect of IGV Losses on Rotor PR



Absolute Rotor Total PR: 9.9:1
Adiabatic efficiency: 64 %

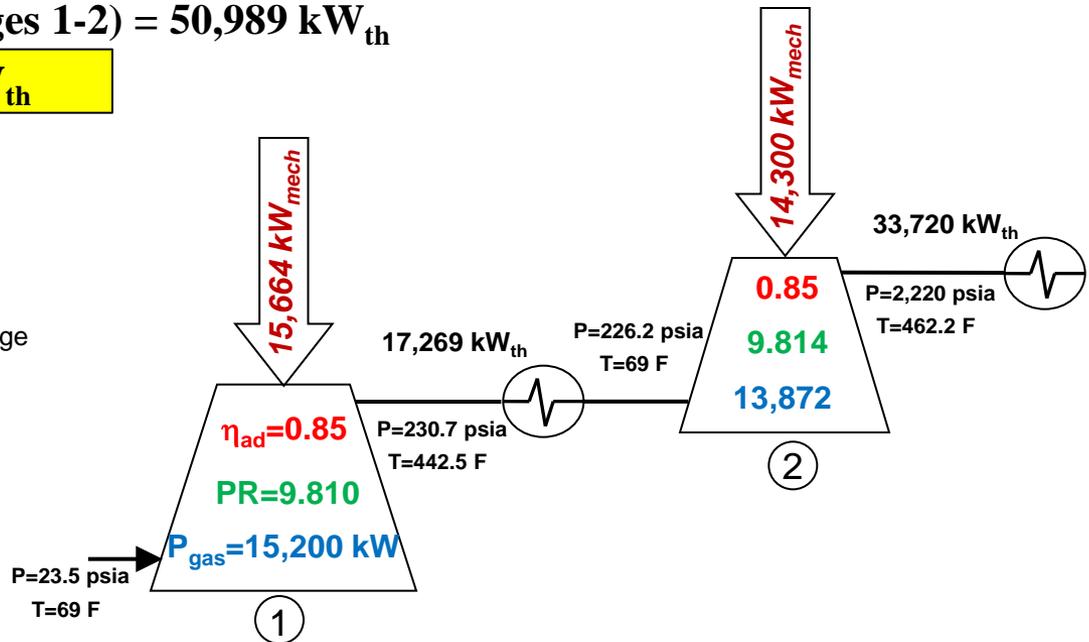
| | July rotor, 0.001 in TC, adiabatic shroud | As built rotor, 0.001 in TC, adiabatic shroud | As built rotor, 0.001 in TC, isothermal shroud dist. | As built rotor, 0.001 in TC, isothermal shroud dist., +4 strake slots |
|----------|---|---|--|---|
| Max PR | 8.2:1 | 7.3:1 | 8.2:1 | 8.9:1 |
| Max effy | 69.8 | 66.1 | 69.9 | 72.3 |

Ramgen 2-Stage Process – Discrete Drive

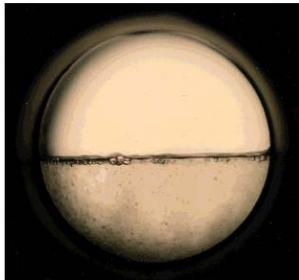
- Shaft power (stages 1-2)
 - Gas-path power = 29,072 kW_{mech}
 - Total shaft power = 29,964 kW_{mech}
- Heat of compression
 - Total rejected into coolers (stages 1-2) = 50,989 kW_{th}
 - Total recoverable¹ = 28,986 kW_{th}

Notes:

- 1) 60°F Cooling Water / 9°F Approach / 69°F Interstage
- 2) Recovery to 200°F



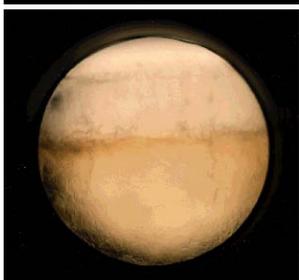
PT Diagram & Supercritical Phase



*Separate Phases
Visible-
Meniscus Clearly
Observed*



*Increase in
Temperature-
Diminished
Meniscus*

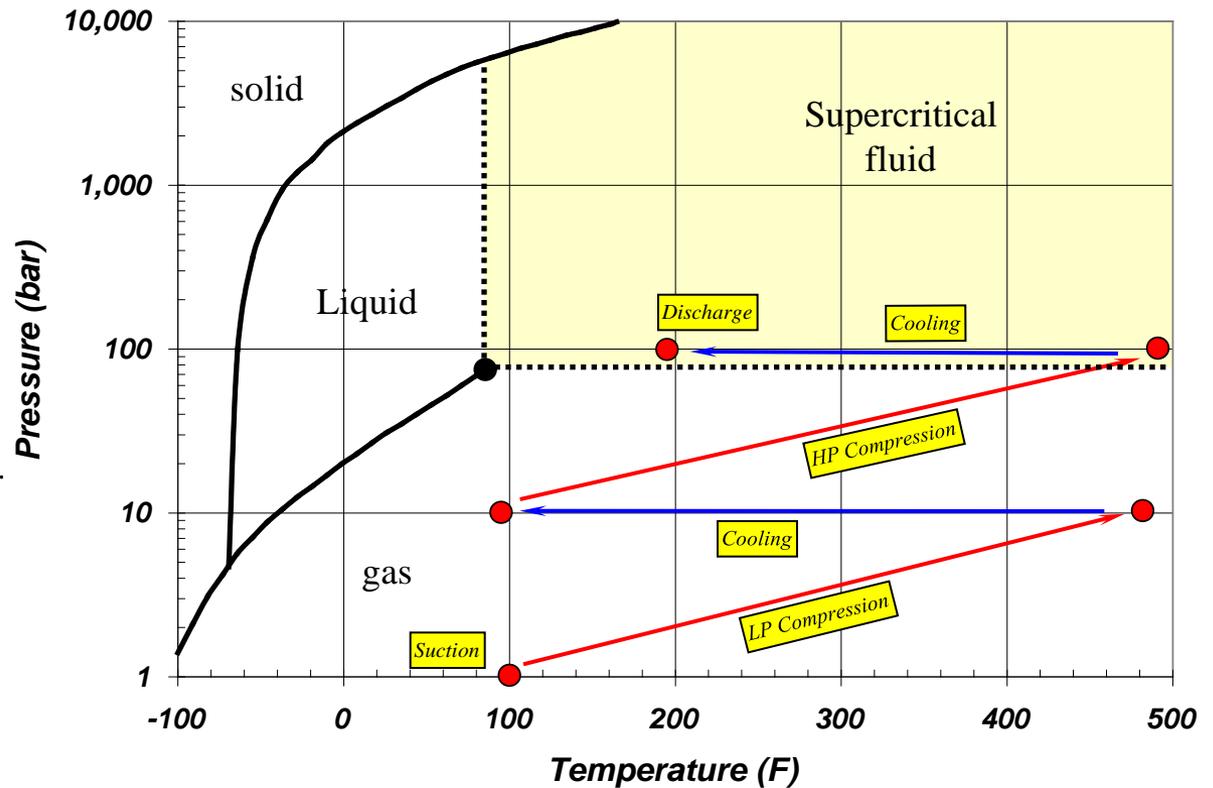


*Further Increase in
Temperature-
Gas & Liquid
Densities more Similar*

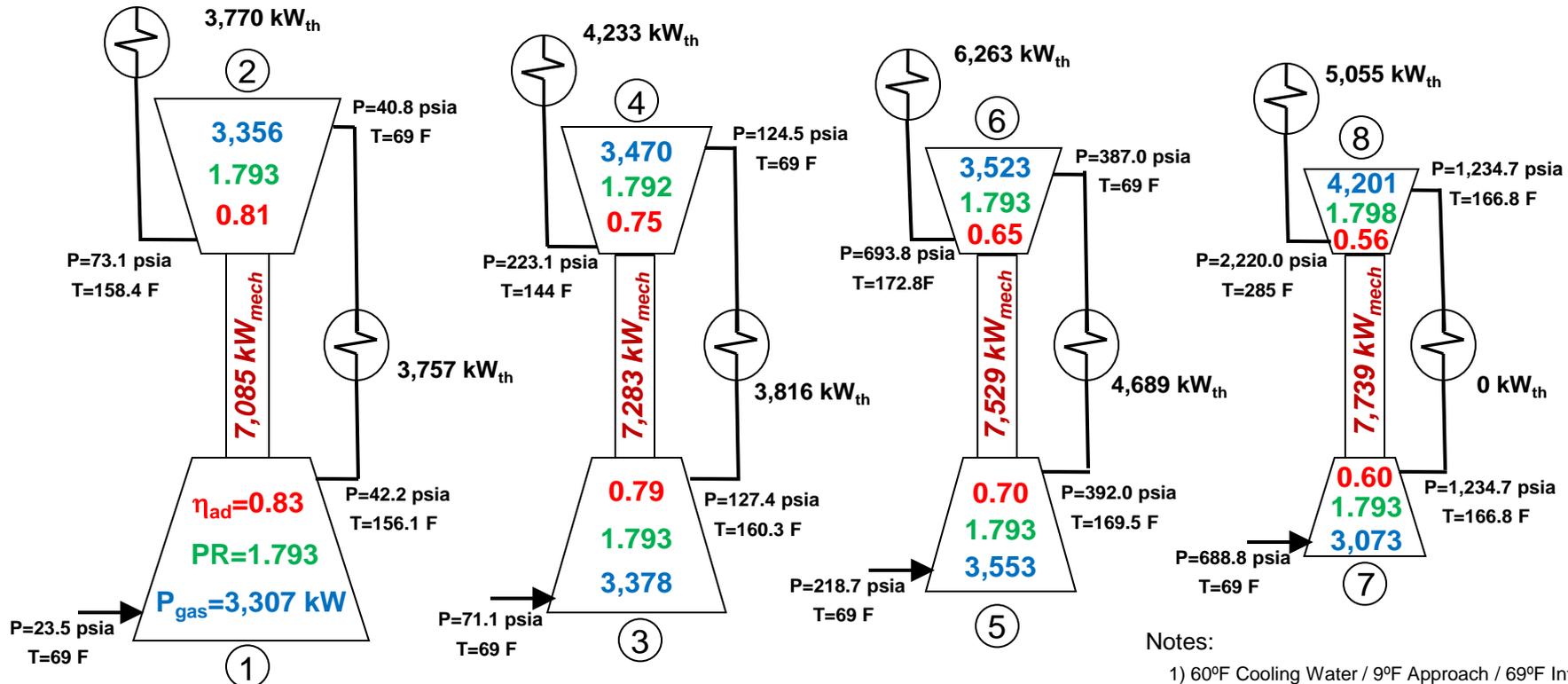


*At Critical P & T-
Distinct Gas & Liquid
Phases no Longer
Visible "Supercritical
Fluid" with Properties
of Both Liquids & Gases*

- Compression process transitions from superheated to supercritical phases
- Avoids liquid (sub-cooled) phase



Advantages Over Conventional Designs



Notes:
 1) 60°F Cooling Water / 9°F Approach / 69°F Interstage
 2) Recovery to 200°F

- **Shaft power (stages 1-8)**
 - Gas-path power = $27,862$ kW_{mech}
 - Total shaft power = $29,636$ kW_{mech}
- **Heat of compression**
 - Total rejected into coolers (stages 1-8) = $45,614$ kW_{th}
 - Total recoverable² = 224 kW_{th}

- **Ramgen (stages 1-2)**
 - Total shaft power = $29,964$ kW_{mech}
 - Total recoverable² = $28,986$ kW_{th}

Conventional Design Practices

- **Combined PR, turndown and specific speed effects limit maximum achievable stage pressure ratios (PR ~1.7 – 1.9)**
- **Increasing suction pressure and rotor pair speed matching results in decreasing rotor sizes through system**
- **Decreased rotor sizes result in decreased efficiency – Reynolds number effects become dominant**



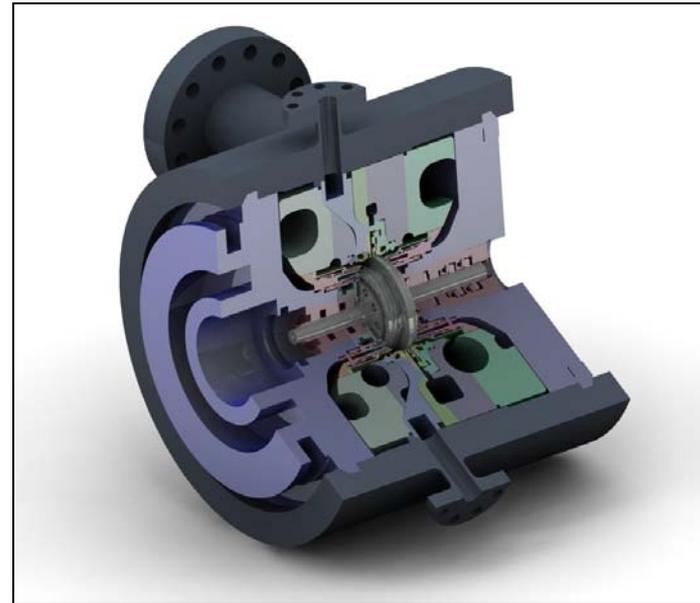
Benefits - Reduce CC(C)&S COE Penalty

MAN Turbo CO₂ Compressor



- **10-stage 6000 hp**
 - \$8.0 million ⇒ \$1350/hp
 - Pr 200:1 ⇒ 1.70 per stage
- **8-stage 20,000 hp**
 - \$15.0 million ⇒ \$750/hp
 - \$23.0 million installed ⇒ \$1150/hp
 - Pr 143:1 ⇒ 1.86 per stage

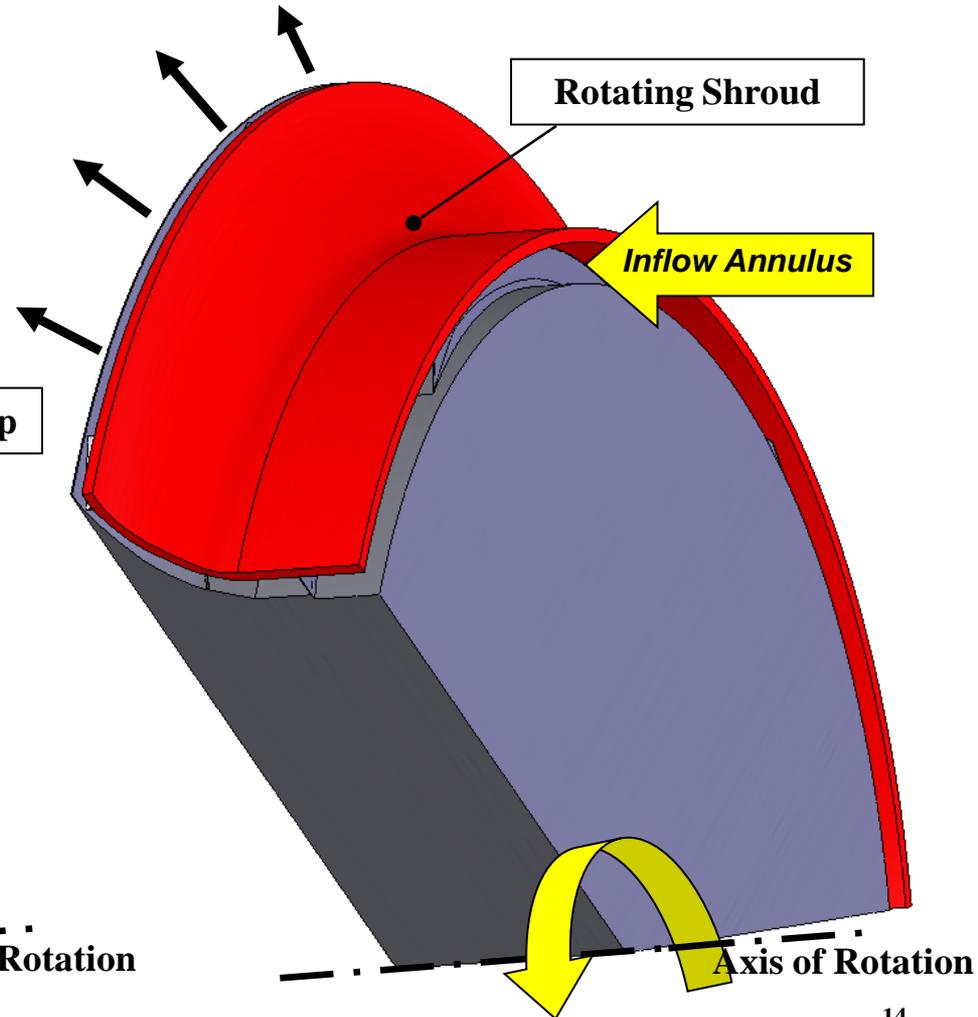
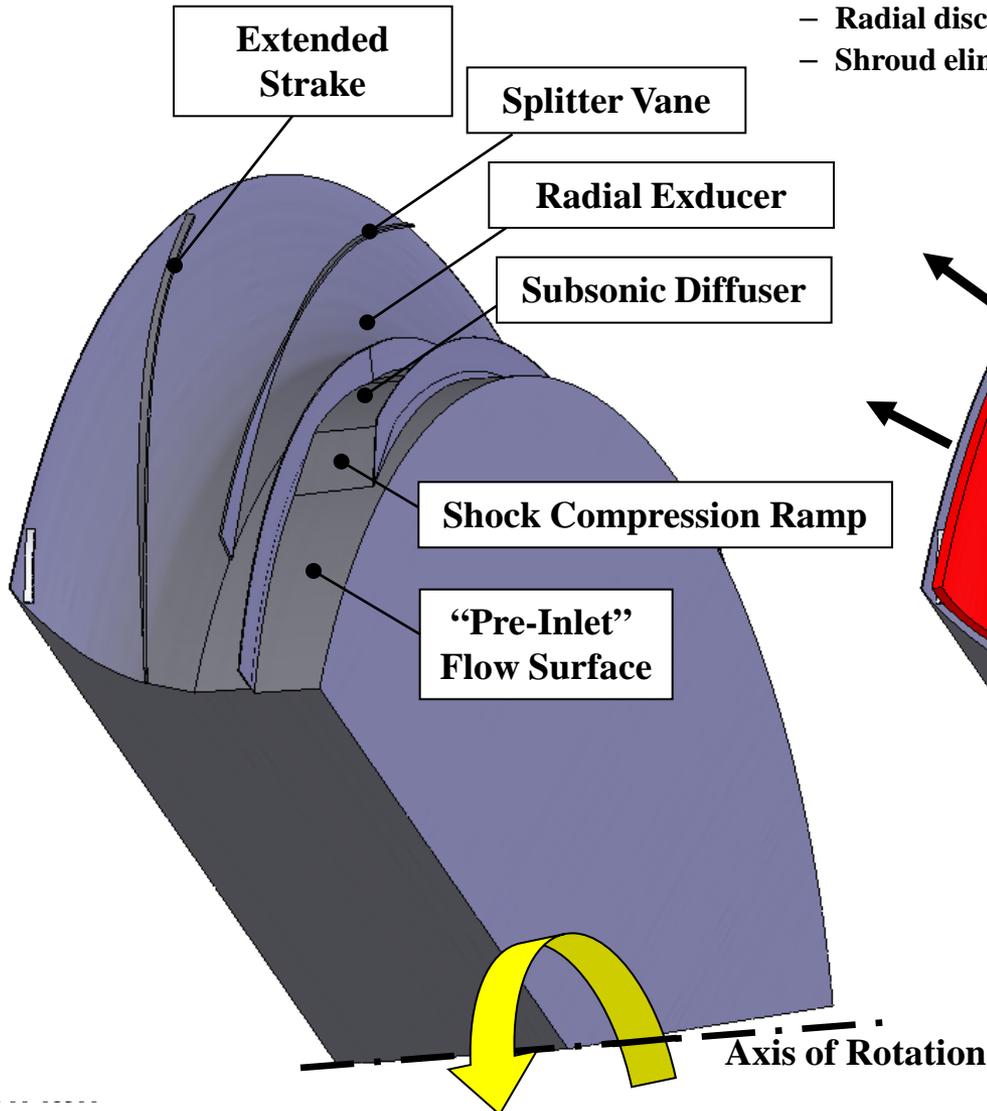
Ramgen CO₂ Compressor



- **Pr 10+:1 per stage; Intercooled**
- **1/10th the physical size**
- **50-60% of the installed capital cost**
- **Same shaft input power requirements**
- **Recover of 80% of the input Btu at 500°F**
 - Improve CCS efficiency
 - Reduce power plant de-rate

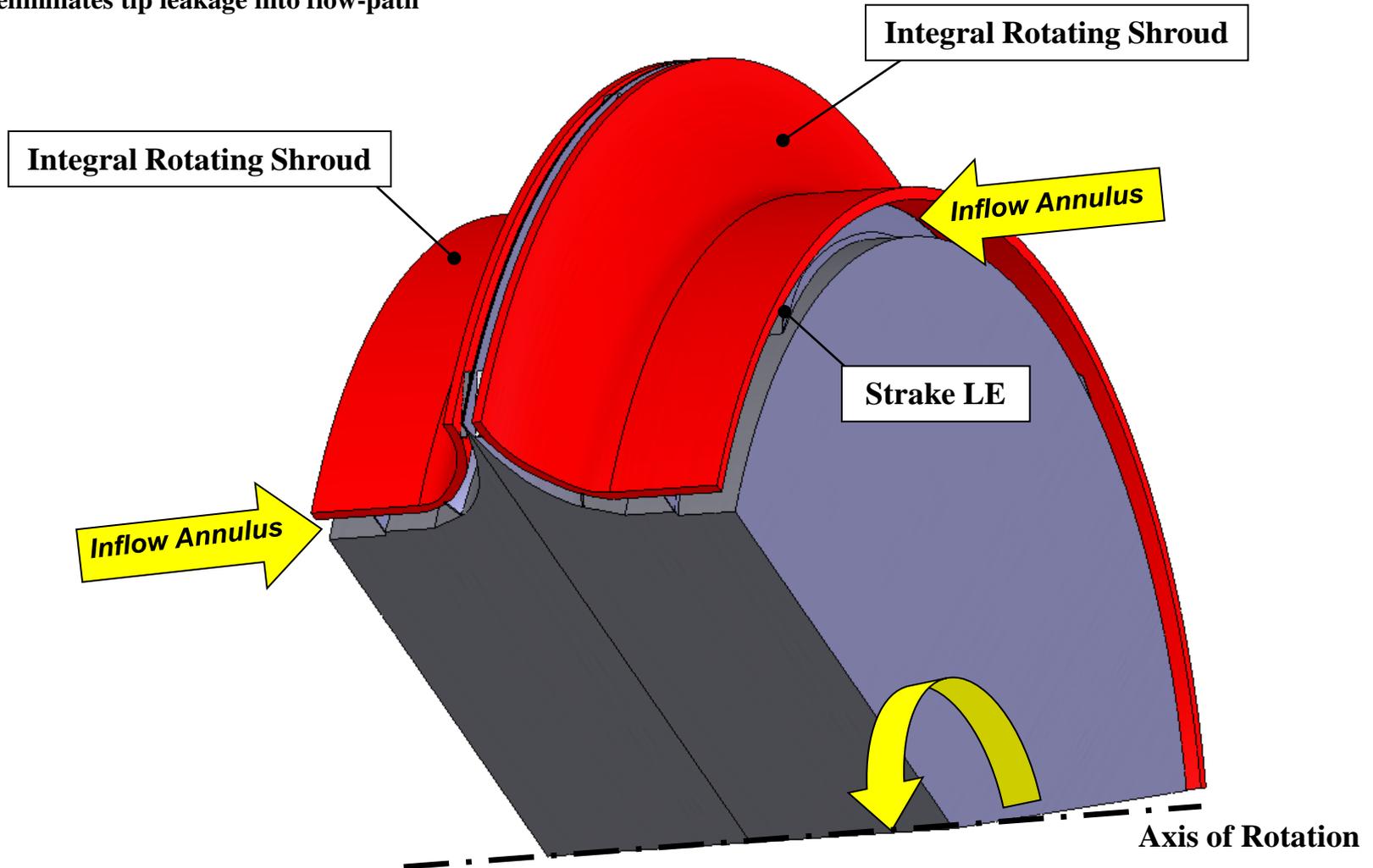
Rotor Design Evolution – Radial Discharge

- Shrouded rotor - radial discharge
 - Radial discharge improves diffuser performance
 - Shroud eliminates tip leakage into flow-path



Dual Entry – Back to Back Configuration

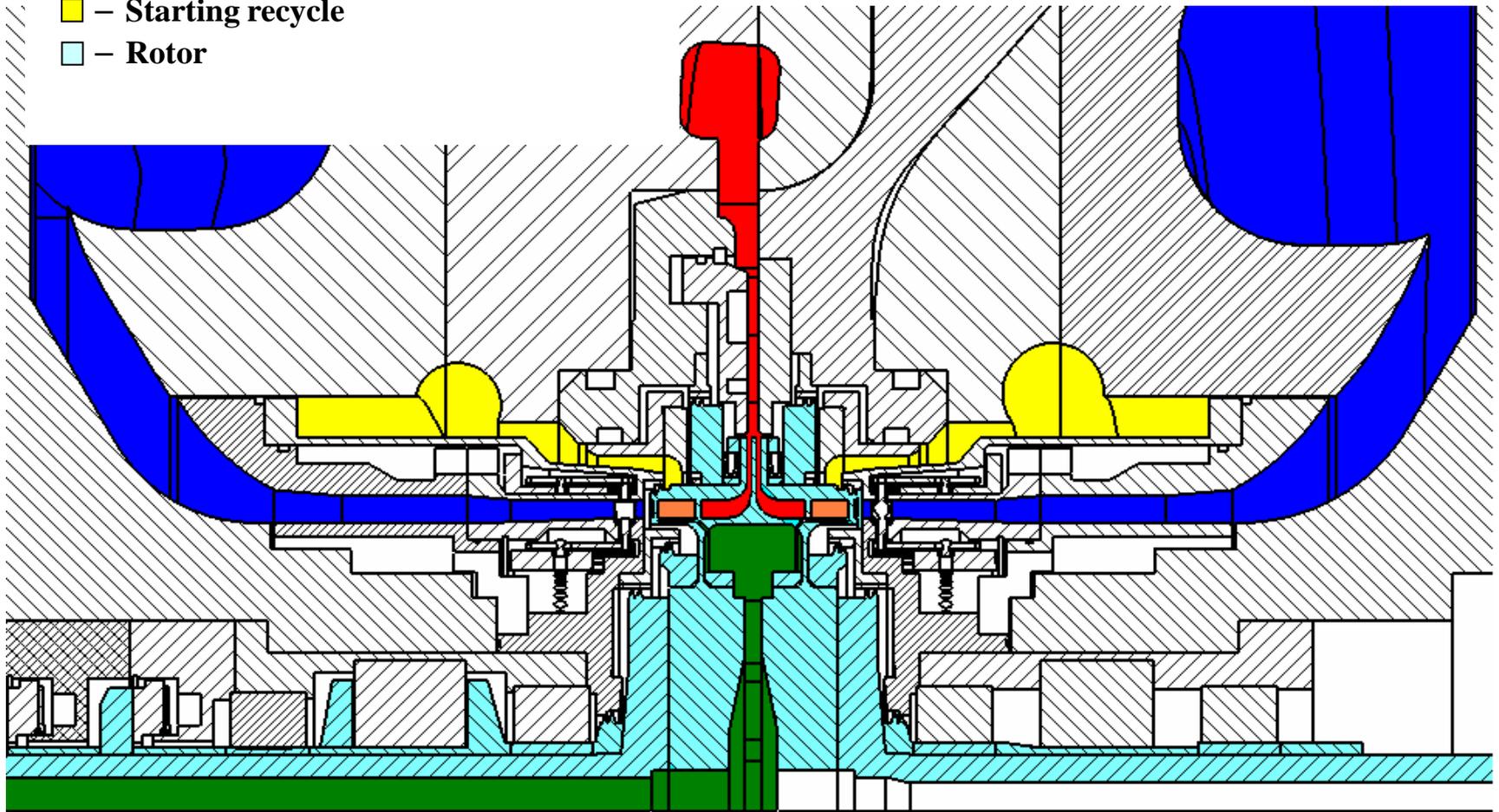
- Shrouded back-to-back rotor
 - Eliminates rotor thrust –significant for HP stage
 - Shroud eliminates tip leakage into flow-path



HP Stage Schematic

- Key stage features

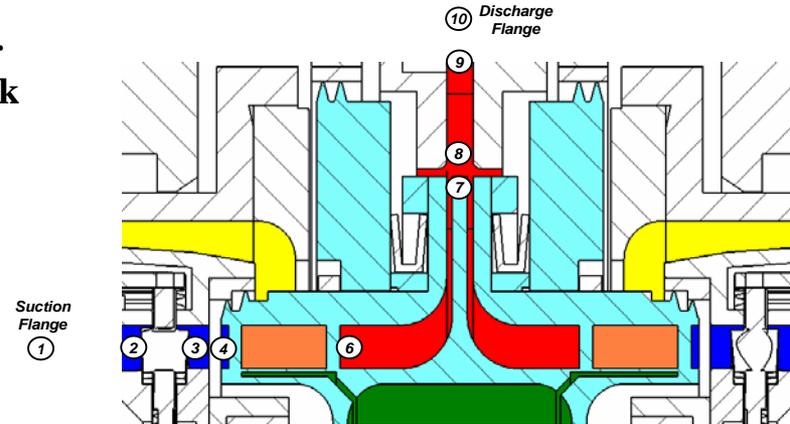
- – Suction (inflow)
- – Discharge (outflow)
- – Starting recycle
- – Rotor



Demo Unit Performance Approaching Goals with DOE Super-Computer Support

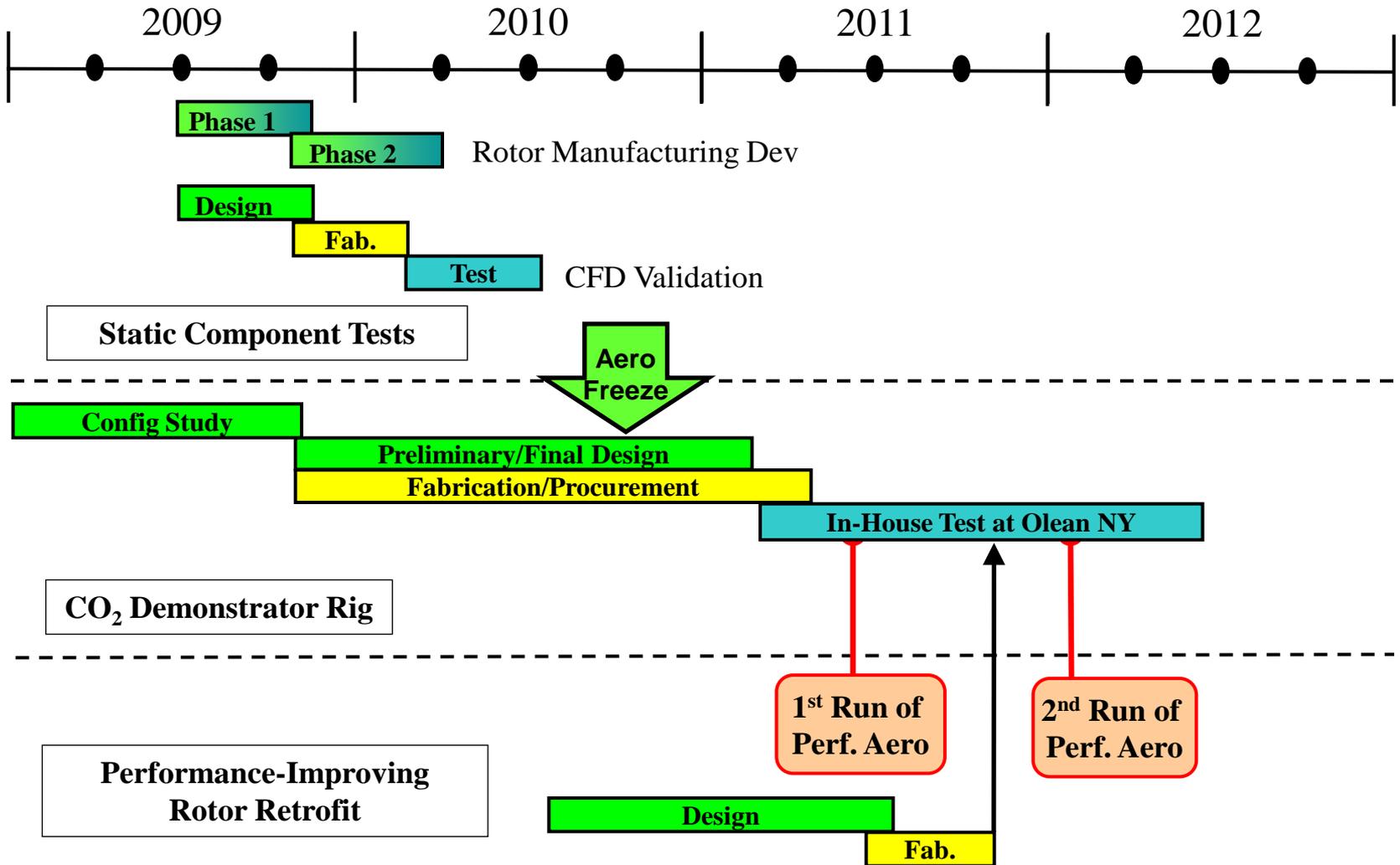


- DOE Support with access to ORNL super-computer resources has been critical to rapid progress in shock compression CFD modeling and optimization
 - Details of Ramgen shock compression geometry require large CFD grids
 - Capturing critical shock boundary layer interactions complicates simulations
 - Need for time-accurate simulations to evaluate aero-stability issues important to system optimization



| Station Number => | | | 1 | 2 | 3 | On Rotor - Relative Conditions | | | | 8 | 9 | 10 |
|-------------------|---------|-----------------------------|----------------|------------------------------------|------------------------------------|--------------------------------|--------------------------------------|------------------------------------|------------|-------------------|--------------------------------------|---------------------------------------|
| | | | | | | 4 | 5 | 6 | 7 | | | |
| | | | Suction Flange | IGV Inflow | IGV Exit | Rotor Inflow | Ramp Base | End Shock Comp | Rotor Exit | Diffuser Entrance | Diffuser Exit | Discharge Flange |
| Demo | High | P_t (psia) Loss Metric | 212.0 | 211.8 P_{t2}/P_{t1} 0.9991 | 208.9 P_{t3}/P_{t2} 0.9863 | 1,073.5 | 1,019.8 P_{t5}/P_{t4} 0.9500 | 968.8 P_{t6}/P_{t5} 0.9500 | 2,190.0 | 2,520.1 | 2,319.0 P_{t9}/P_{t8} 0.9202 | 2,289.1 P_{t10}/P_{t9} 0.9871 |
| | Nominal | P_t (psia) Loss Metric | 212.0 | 211.8 P_{t2}/P_{t1} 0.9991 | 208.9 P_{t3}/P_{t2} 0.9863 | 1,073.5 | 1,030.1 P_{t5}/P_{t4} 0.9395 | 923.9 P_{t6}/P_{t5} 0.8800 | 2,115.0 | 2,574.0 | 2,318.8 P_{t9}/P_{t8} 0.9008 | 2,289.1 P_{t10}/P_{t9} 0.9872 |
| | Low | P_t (psia) Loss Metric | 212.0 | 211.8 P_{t2}/P_{t1} 0.9991 | 208.9 P_{t3}/P_{t2} 0.9863 | 1,073.5 | 1,030.1 P_{t5}/P_{t4} 0.9395 | 923.9 P_{t6}/P_{t5} 0.8800 | 2,115.0 | 2,574.0 | 2,246.8 P_{t9}/P_{t8} 0.8728 | 2,218.1 P_{t10}/P_{t9} 0.9872 |
| Current Status | | P_t (psia) Loss Metric | 212.0 | 211.8 P_{t2}/P_{t1} 0.9991 | 208.9 P_{t3}/P_{t2} 0.9863 | 1,073.5 | 1,030.1 P_{t5}/P_{t4} 0.9395 | 923.9 P_{t6}/P_{t5} 0.8800 | 2,115.0 | 2,574.0 | 2,246.8 P_{t9}/P_{t8} 0.8728 | 2,218.1 P_{t10}/P_{t9} 0.9872 |

Project Milestones



Questions