

Engineering Assessment of CO₂ Recovery, Transport, and Utilization*

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Introduction

The need to establish benchmarks for available power-generating cycles having reduced atmospheric emissions of CO₂ served as the basis for this study. Innovative process technologies need this benchmark so they can be appreciated in their proper perspective. An oxygen-blown KRW coal-gasification plant producing hydrogen, electricity, and supercritical-CO₂, was studied in a full-energy cycle analysis extending from the coal mine to the final destination of the gaseous product streams. A location in the mid-western United States 100 mi from Old Ben #26 mine was chosen. Three parallel gasifier trains, each capable of providing 42% of the plant's 413.5 MW nominal capacity use 3,845 tons/day of Illinois #6 coal from this mine. The plant produces a net 52 MW of power and 131 MMscf/day of 99.999% purity hydrogen which is sent 62 mi by pipeline at 34 bars. The plant also produces 112 MMscf/day of supercritical-CO₂ at 143 bars, which is sequestered in enhanced oil recovery operations 310 mi away.

Objective

This project emphasizes CO₂-capture technologies combined with integrated gasification combined-cycle (IGCC) power systems that produce both merchant hydrogen and electricity. Comparisons of energy penalties, capital investment, and CO₂ emission reductions are based on the full-energy cycle including mining, coal transportation, coal preparation, gasification, gas treatment, power generation, infrastructure to transfer power or hydrogen to end users, and pipeline transport of CO₂ to enhanced-oil recovery. Technical and economic aspects of H₂ pipelines and supercritical CO₂ pipelines, as well as issues relating to CO₂ sequestering in EOR are considered so that process conditions and energy use are accounted for by the study.

Approach

Oxygen-blown gasification is used to convert Illinois #6 coal to synthesis gas [Fig. 1]. After

particulate removal, a shift reactor uses steam to convert the CO component of the gas to CO₂ and hydrogen (H₂). Next, H₂S is removed from the stream and processed to produce marketable sulfur. Carbon dioxide is then recovered in a glycol-based process and transported by pipeline for enhanced oil recovery. The gas stream after CO₂ recovery is processed using pressure-swing adsorption (PSA) to recover H₂ at a purity suitable for fuel cells, although there is no restriction on the actual hydrogen end-use. The H₂ stream is transported to end users via pipeline, while the residual gas from PSA - a combination of hydrogen, methane, and light hydrocarbons - is used to generate electricity by combustion turbine combined cycle. Part of the electricity generated supplies the internal needs of the plant, and the excess is sent to the grid.

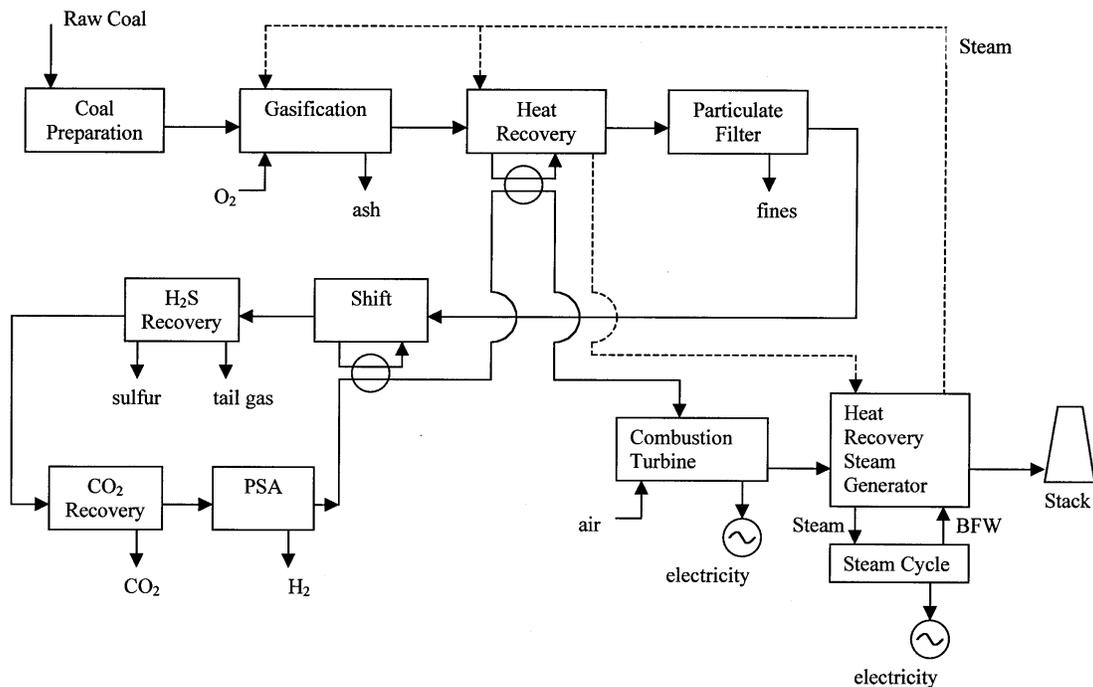


Fig. 1. Integrated Gasification Combined-Cycle Producing Electricity, CO₂ and H₂

Description

Mining: The assumed power plant location is 100 mi (160 km) by diesel-rail transport from the Old Ben #26 underground mine in Sesser, Illinois. The plant receives 4,112 tons/day (155.4 metric tonnes/h) of 2 x 4-in. coal, which is prepared to 0 x 1/4-in. with 3.5% weight loss. A summary of this portion of the power cycle appears in Table 1.

Conversion: Previous process design studies to characterize integrated gasification combined-cycle (IGCC) power systems with CO₂-capture technologies were modified using ASPEN[®] modeling to evaluate a configuration producing both merchant hydrogen and electricity [1,2,3,4,5]. The power plant configuration employs three parallel gasifier trains, each capable of providing 42% of the plant's 413.5 MW nominal capacity (for the base case with no CO₂ recovery.) After modification, the plant produces 131 MMscf/day (3.71 million standard cubic m/day) of 99.999% purity hydrogen at 287.7 Btu/scf; 119.9 KJ/g (LHV) which is sent 100 km by pipeline at 34 bars.

At 100% efficiency, this could yield 460 MW of power. The plant also produces 112 MMscf/day (3.18 million standard cubic m/day) of supercritical-CO₂ at 143 bars, which is sent 500-km for sequestering in enhanced oil recovery. PSA reject gas goes to a turbine cycle to produce 118 MW. After supplying 66 MW for internal power use this yields 52 MW Net power.

H₂ pipeline: A 100-km pipeline design was prepared and costs were estimated for a high purity hydrogen flow of 131 MMscf/day through a 343 mm pipe at 30 bar. There appears to be no economic justification for going to higher pipeline pressures and an internal study of the costs for delivering energy as methane vs. energy as H₂ showed a 13% advantage for methane at 500 psi rising to a 46% advantage at 800 psi. Economic assumptions were for a capacity factor of 95% and capital recovery of 12% to yield transmission costs of 0.171 \$/Mscf; 0.564 \$/GJ.

Table 1. Energy Use in Coal Mining, Preparation, and Transportation

	Electricity	Diesel Fuel #2	CO ₂ Emissions	Electricity	Losses	Coal	CO ₂
metric units	kWh/tonne	tonne-km/liter	kg/tonne coal	MW	%	kg/h	kg/h
MINING (a)							
Methane emissions (b)			9.63		0.0%	178,981	1,724
Hoisting	6.12		6.12				
Drilling	2.03		2.03				
Ventilation	2.20		2.20				
Dewatering	2.67		2.67				
Break and convey	0.73		0.73				
Ancillary	0.46		0.46				
subtotal	14.21		14.21	2.54	0.0%	178,981	2,543
PREPARATION 2x4-in.	0.44		0.44	0.07	10.0%	161,083	71
TRANSPORT - 161 km							
Mine to IGCC by rail		135	3.27				
General service	0.98		0.98	0.15			
Return to mine		50	1.22				
General service	0.36		0.36	0.06			
subtotal			5.83	0.21	3.5%	155,445	905
PREPARATION 1/4-in. (c)	5.85				6.5%	145,341	

(a) Operations of 250 days/yr at 13 hr/day

(b) Methane emissions of 175 scf/ton counted only as conversion to CO₂ within a 14-yr life

(c) Accounted for in IGCC plant balance

CO₂ pipeline: Design and economic assumptions for a supercritical-CO₂ pipeline were compared against current plans for Dakota Gasification Company, Beulah, ND [6] and Shell estimates of CO₂ purchase costs at \$3.25/bbl of oil recovered [7] with a reasonable CO₂ utilization of 5.6 Mscf/bbl oil [8], which would come to a purchase price of about \$0.60/Mscf. Since, the 30-in. Shell Cortez line is unusually large D resulting in economies of scale D previously determined pipeline costs of \$0.77/Mscf CO₂ still appear reasonable.

RESULTS: Full-Energy Cycle Balances

The energy costs of delivering electricity 100-km from the IGCC plant are presented for three cases; the IGCC base case with no CO₂ recovery (Table 2); the IGCC system with CO₂ recovery (Table 3); the IGCC system developed for this study with H₂ production and CO₂ recovery (Table 4). For the Base-case with no CO₂ recovery; delivered power was 396-MW full-cycle with emissions of 0.83 kgCO₂/kWh.

There is a derating with CO₂ recovery. Delivered power becomes 366-MW full-cycle at 0.20 kgCO₂/kWh. An additional derating takes place in the present case with both H₂ production and CO₂ recovery where the hydrogen goes to 3-stage solid-oxide fuel cells. The delivered power now becomes 344-MW full-cycle at 0.22 kgCO₂/kWh. This is the combination of 52-MW busbar at the plant and 298-MW from fuel cells and a steam generator topping cycle.

Table 2. KRW O₂-blown IGCC - Base Case

Basis: Electric power delivery 100 km from station

	nm ³ /d	tons/d	kg/h	Power MW	CO ₂ kg/h	CH ₄ kg/h	N ₂ O kg/h
MINING AND TRANSPORT							
Coal methane emissions						566	
Mining operations & preparation				-2.61	2,614		0.00003
Transport by rail - 161 km				-0.21	905		0.66265
Subtotal				-2.82	3,520	566	0.66267
POWER PLANT							
Coal preparation (0-in. x 1/4-in.)		3,845	145,341	-0.85			
O ₂ by cryogenic separation	8,937,000	2,347	88,717	-29.29			
Steam from heat recovery generator			17,254				
Gasifier island				-2.90			
Solid waste		492	18,598				
Sulfur		78	2,948	-4.64			
SO ₂ (gasifier only)		6.92	262		6,157		unknown
Power island				-7.02	320,383		
Miscellaneous (5%)				-2.24			
Subtotal				-44.70	326,540		
Power - gas turbine				627.40			
Power - air compressor and losses				-328.60			
Power - steam turbine				159.40			
GROSS Power Subtotal				458.20			
NET Power				413.50			

CO₂ PIPELINE AND SEQUESTERING			0.00	0		
H₂ PIPELINE			0.00	0		
TRANSMISSION LOSS-3.5%			-14.47	0		
NET ENERGY CYCLE -Base Case	0.833	kg CO₂/kWh	396.20	330,060	566	0.66267

Table 3. O₂-blown IGCC with CO₂

Glycol CO₂ and H₂S recovery; turbine topping
 Basis: Electric power delivery 100 km from station

	nm ³ /d	tons/d	kg/h	Power MW	CO ₂ kg/h	CH ₄ kg/h	N ₂ O kg/h
MINING AND TRANSPORT							
Coal methane emissions						566	
Mining operations & preparation				-2.61	2,614		0.00003
Transport by rail - 161 km				-0.21	905		0.66265
Subtotal				-2.82	3,520	566	0.66267
POWER PLANT							
Coal preparation (0-in. x 1/4-in.)		3,845	145,341	-0.85			
O ₂ by cryogenic separation	8,937,000	2,347	88,717	-29.29			
Steam from heat recovery generator			17,254				
Gasifier island				-2.90			
Solid waste		492	18,598				
Sulfur		78	2,948				
SO ₂ (gasifier only)		6.92	262		6,157		unknown
Glycol circulation				-5.80	320,383		
Glycol refrigeration				-4.50			
Power recovery turbines				3.40			
CO ₂ compression to pipeline (143 bar)	3,178,000			-17.30	-260,055		
Power island				-6.90			
Miscellaneous (5%)				-2.86			
Subtotal				-67.01	66,485	0	unknown
Power - gas turbine				580.78			
Power - air compressor and losses				-325.51			
Power - steam turbine				195.30			
GROSS Power Subtotal				450.57			
NET Power				383.56			
CO₂ PIPELINE AND SEQUESTERING							
	3,178,000				260,055		
Pipeline booster stations				-1.64	1,637		0.00002
Geological reservoir (1% loss)					-257,454		
Subtotal				-1.64	4,238	0	0.00002
H₂ PIPELINE							
				0.00			

TRANSMISSION LOSS-3.5%

-13.42

NET ENERGY CYCLE	0.203	kg CO₂/kWh	365.67	74,242	566	0.66269
NET ENERGY CYCLE -Base Case	0.833	kg CO₂/kWh	396.20	330,060	566	0.66267

Table 4. KRW O₂-blown IGCC

Glycol CO₂ and H₂S recovery; PSA H₂ recovery; turbine topping; 3-stage solid oxide fuel cell

	nm ³ /d	tons/d	kg/h	Power MW	CO ₂ kg/h	CH ₄ kg/h	N ₂ O kg/h
MINING AND TRANSPORT							
Coal methane emissions						566	
Mining operations & preparation				-2.61	2,614		0.00003
Transport by rail - 161 km				-0.21	905		0.66265
Subtotal				-2.82	3,520	566	0.66267
POWER PLANT							
Coal preparation (0-in. x 1/4-in.)		3,845	145,341	-0.85			
O ₂ by cryogenic separation	8,937,000	2,347	88,717	-29.29			
Steam from heat recovery generator			17,254				
Gasifier island				-2.90			
Solid waste		492	18,598				
Sulfur		78	2,948				
SO ₂ (gasifier only)		6.92	262		6,157		unknown
Glycol circulation				-5.80	320,383		
Glycol refrigeration				-4.50			
Power recovery turbines				3.40			
CO ₂ compression to 143 bar	3,178,000			-17.30	-260,055		
H ₂ PSA purification to 31 bar	3,710,000			-3.18			
H ₂ cryo-storage for pipeline				-0.92			
Power island				-1.81			
Miscellaneous (5%)				-3.07			
Subtotal				-66.22	66,485	0	unknown
Power - gas turbine				244.53			
Power - air compressor and losses				-169.48			
Power - steam turbine				42.93			
GROSS Power Subtotal				117.98			
NET Power				51.76			
CO₂ PIPELINE & SEQUESTERING							
Pipeline booster stations				-1.64	1,637		0.00002
Geological reservoir (1% loss)					-257,454		
Subtotal				-1.64	4,238	0	0.00002

H₂ PIPELINE OUTLET (21 bar)	3,710,000					
H ₂ 3-stage SOFC (58% of 460.0 MW)			266.80			
Steam Generator (85% of 36.8 MW)			31.28			
Subtotal			298.08	0	0	0.00000
TRANSMISSION LOSS-3.5%			-1.81			
NET ENERGY CYCLE	0.216	kg CO₂/kWh	343.56	74,242	566	0.66269
NET ENERGY CYCLE -Base	0.833	kg CO₂/kWh	396.20	330,060	566	0.66267

Applications

Carbon dioxide as a supercritical product (143 bar) can be recovered from coal gasification and power production. Where there is an enhanced oil recovery market, this actually is profitable.

The need for high-pipeline utilization is critical. Hydrogen can be recovered at high purity (99.999%) for sale from coal gasification, however the need for high pipeline-utilization is critical. Pressures of 35 bar are optimal. Fuel-cell conversion efficiencies need to approach 77% to match the base-case output. At present, solid-oxide fuel cell efficiencies are 53-58%; while alkaline fuel cell efficiencies are near 70%.

Future Work

Costs for the current study have been prepared for the pipelines, but changes to the IGCC plant itself must be reviewed and finalized to yield the comparative costs of electricity.

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