

Hybrid Optical Sensors for Power Generation Systems

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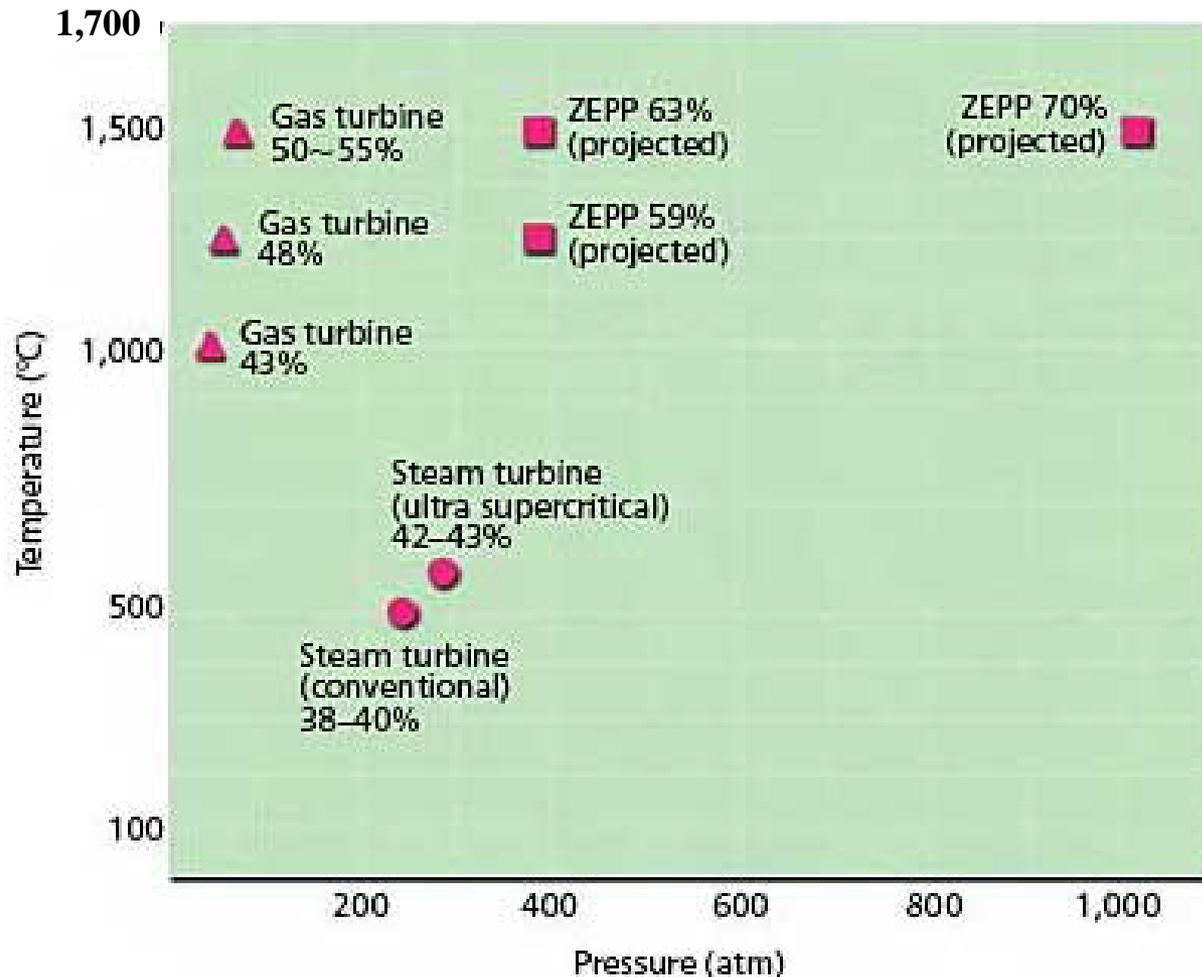
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Why is Extreme Temperature Sensing Needed --- Greener & More Efficient



Ultimate Goal--ZEPP: Zero Emission Power Plant

Burn Less Fuel

↓
**Less Hazardous
Waste & CO₂**

Higher Pressures

↓
**Liquify CO₂ -Easier
To Transport/Store
Waste**

↓
Greener Plant

* J. H. Ausubel, "Big Green Energy Machines," The Industrial Physicist, AIP, pp.20-24, Oct./Nov., 2004.

GE's H system Gas Turbine



System Test had 3500 gauges and sensors

Uses Firing Temperature of 1430 C

R. Matta, et.al, "Power Systems for the 21st Century," GE Power Systems Publication GER3935B, Oct. 2000.

**THE NEED:
PRECISION RELIABLE SENSORS for GAS Temperature and Pressure
Measurement to Keep
Plants at Operating at Super Critical Conditions**

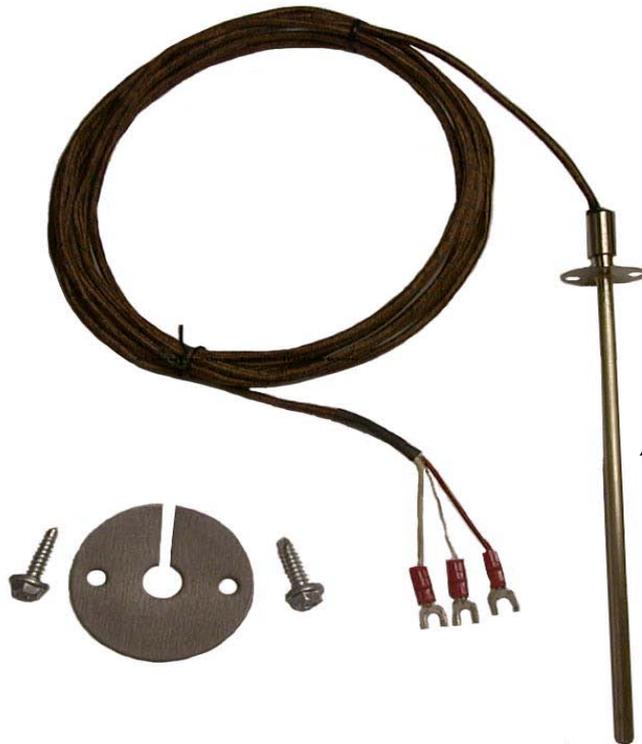
Any Options?

-- ALL Electronic Sensor Chips ? Fail after ~ 500 °C (Insulation Breakdown)

-- Silica/Glass Fiber Optics (Single Mode) – Fail after ~ 900 °C (Grating Erasure)

How does Extreme temperature Measurement get done today?

Platinum/Rhodium High Temperature Thermo-Couple (TC)
All-Electrical Technology is used to Measure Extreme
Temperature



Note:
Need to Encase in Custom
Magnesia (MgO) or Alumina
Insulating Ceramics – Can
Reach 1900 C

Image courtesy: Cybernetics Technical Industries Inc.

What are the limitations of the Best TC Technology?

Present **TC Technology** under extreme engine conditions are:

- Structurally unreliable (develop cracks in the ceramic insulation – moisture retention making it conductive, can explode)
- Give inaccurate and erratic readings
- Readings intrinsically depend on a % of measured extreme temperature, i.e., gets worse at higher temperatures- caused by Compositional variations in wire alloy – varying EMF properties along length

| Type | Combination | | Working Temperature Range/°C | | | Tolerance/°C |
|------|-------------|-----------|------------------------------|------------------|-----------------|------------------------|
| | -ve | +ve | Bare wire only | | Metal Clad form | |
| | | | Continuous use | Intermittent use | | |
| S | Pt | 10% Rh/Pt | 200-1500 | 200-1650 | 200-1300 | IEC 584-2 Class 1 or 2 |
| R | Pt | 13% Rh/Pt | 200-1500 | 200-1650 | 200-1300 | IEC 584-2 Class 1 or 2 |
| B | 6% Rh/Pt | 30% Rh/Pt | 200-1600 | 200-1750 | 200-1450 | IEC 584-2 Class 1 or 2 |
| | 20% Rh/Pt | 40% Rh/Pt | 200-1700 | 200-1850 | 200-1450 | 8.0 |
| | Iridium | 40% Ir/Rh | 1000-2100 | - | N/A | 10.0 |
| | 0.03% Fe/Au | Chromel | 1-300K | - | N/A | - |

Tolerance Classes

Class 1 = +/- 1°C or +/- {1 + (t - 1100) x 0.0003}°C

Class 2 = +/- 1.5°C or +/- 0.0025t°C

Class 3 = +/- 4°C or +/- 0.005t°C

Whichever is the greater and where t is temperature in °C

Table of tolerance values

| Temperature °C | Class 1 | Class 2 | Class 3 |
|----------------|---------|---------|---------|
| | +/- °C | +/- °C | +/- °C |
| 0 - 600 incl. | 1.0 | 1.50 | 4.0 |
| 700 | 1.0 | 1.75 | 4.0 |
| 800 | 1.0 | 2.00 | 4.0 |
| 900 | 1.0 | 2.25 | 4.5 |
| 1000 | 1.0 | 2.50 | 5.0 |
| 1100 | 1.0 | 2.75 | 5.5 |
| 1200 | 1.3 | 3.00 | 6.0 |
| 1300 | 1.6 | 3.25 | 6.5 |
| 1400 | 1.9 | 3.50 | 7.0 |
| 1500 | 2.2 | 3.75 | 7.5 |
| 1600 | 2.5 | 4.00 | 8.0 |
| 1700 | - | 4.25 | 8.5 |

Availability

| Type | Class 1 | Class 2 | Class 3 |
|------|---------|---------|---------|
| S | x | x | |
| R | x | x | |
| B | | x | x |

The temperature scale used in ITS-90 for which the fixed points are as follows:-

Zinc point = 419.53°C

Gold point = 1064.18°C

Palladium Point = 1553.5°C

Platinum Point = 1768.1°C

~ +/- 0.2% →

Who does TC Probes?

Engine/Turbine Manufacturers design custom Temperature Probes based on Highly Packaged / Protected TC Technology

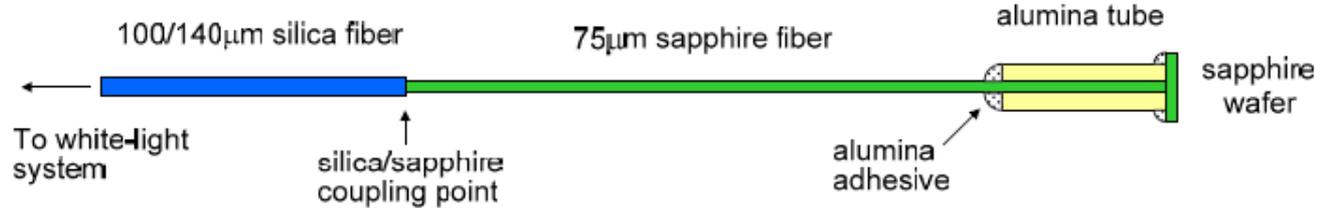


Image courtesy: L&L Kilns Inc.

Fiber-Optic Probes?

Same Packaging Problem as TCs – Protect the Flexible and Thin/Brittle Optical Fiber and related frontend optics generally requiring a mix of packaging materials- CTE Mismatches

Multi-Mode Fiber-Optics for Robust Coupling – Causes Multi-Mode Interference/Noise



Is There An Extreme
Temperature Sensor Design
Without
the TC & Optical Fiber Probe
Packaging
& Reliability Issues?

What is new about our approach?

Wireless



Extremely Hot

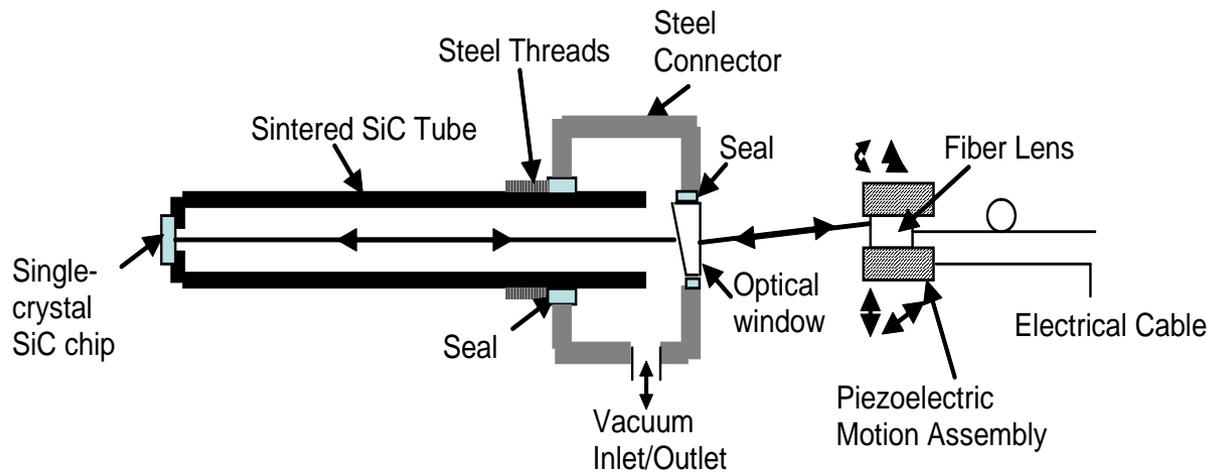
+

Wired Optics



Cool Section

Thermal Isolation



What is new about our approach?

- Single Crystal SiC + Sintered SiC Probe
- Single material (CTE matched) – Robust frontend for extreme zone
- Temperature Reading Independent of Intrinsic % Increasing Temperature Error

Eliminated Fundamental TC Limitations

Front-End Probe

Unassembled

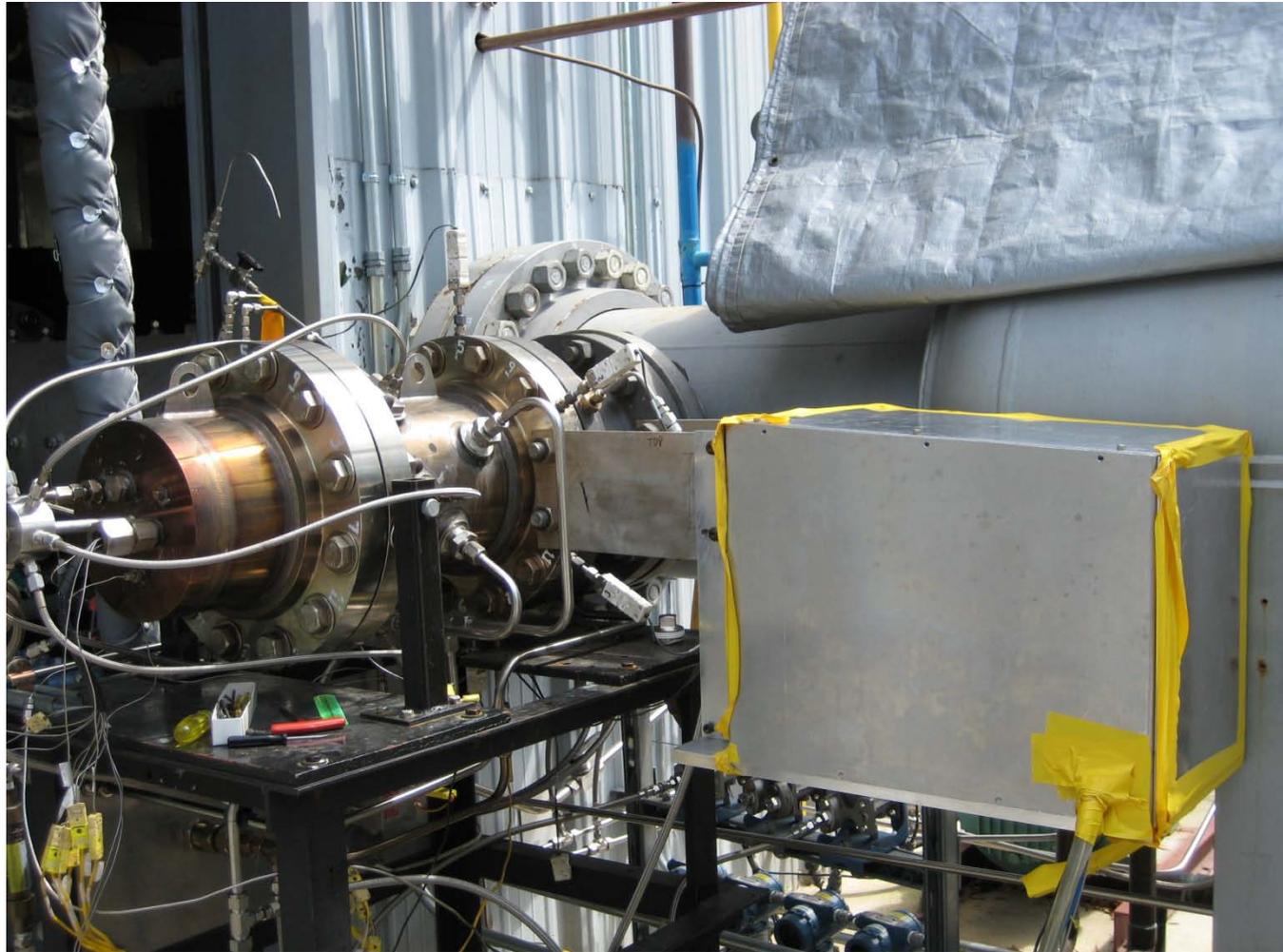


Assembled



Images courtesy: Nuonics, Inc.

INSTALLED OPTICAL SENSOR AT GAS TURBINE TEST RIG



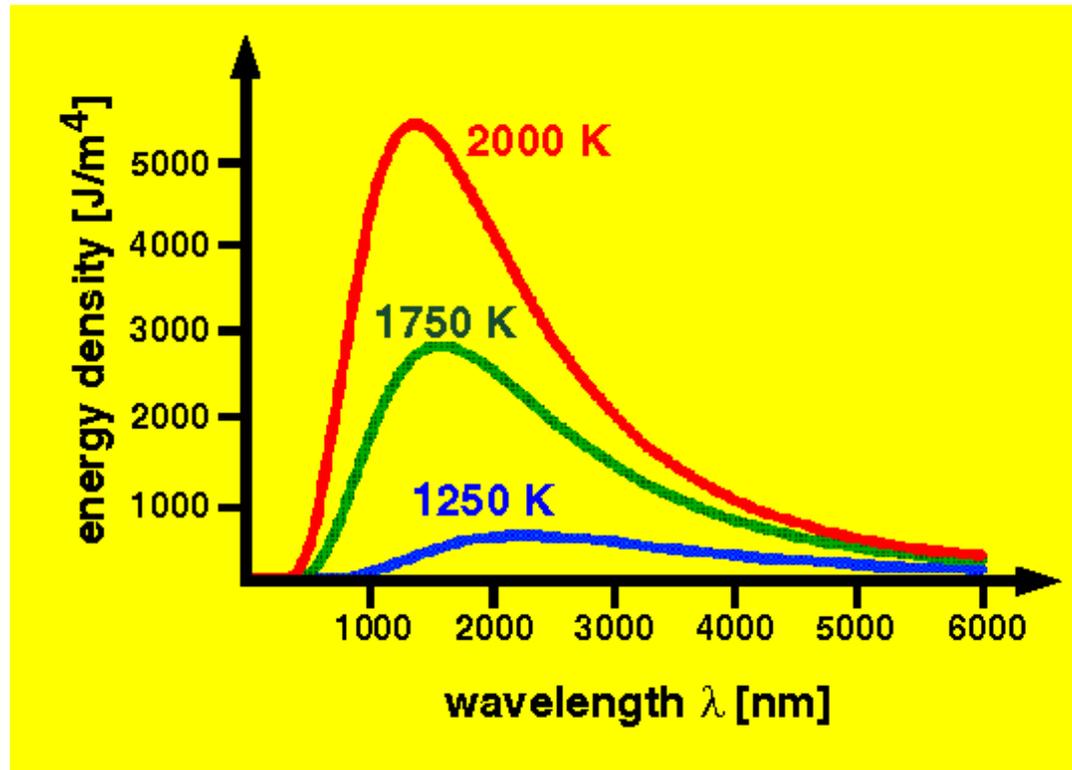
6 Thermo-Couples (TCs) Placed in Circular Ring Format At Exit of Combustor

Optical Probe about 6 inches From TC positions in Combustor Exhaust Section

GAS TURBINE RIG TESTING SUMMARY

| | |
|---|--|
| COMBUSTION RIG FLAME ACTIVE OPERATION | 6 DAYS |
| NO. OF TIMES PROBE EXPERIENCED FLAME LIGHT AND THERMAL SHOCK (TEMPERATURE RAMP OF 1000 DEG-C IN 3 SECONDS) | 8 (1 DAY 3 FLAME LIGHTS, 5 DAYS 1 FLAME LIGHT/DAY |
| OPERATION WITH FLAME ON | 26 HOURS |
| OPERATION WITH FLAME OFF AND BLOWER ON | 13.5 HOURS |
| NUMBER OF COMBUSTION HEAT AND COOL CYCLES | 8 |
| DAYS IN EXTERNAL RIG ENVIRONMENT | 28 DAYS |

+100 years of Blackbody Radiation & Temperature Dependence



Max Planck

$$I(\lambda, T) = \frac{2hc^2}{\lambda^5} \frac{1}{e^{\frac{hc}{\lambda kT}} - 1} \cdot \varepsilon(\lambda, T)$$

Radiation Thermometry - Pyrometers

- Options:

--- **Direct View of Near BB radiation** – Problem- Changing Gas/Combustor Wall Emmissivity Issue

- **Emmissivity Calibration via 2-wavelength** – Problem – Optical Window Dirty

- **OK for fixed clean material production- Steel Melts Production Factory**
(Pioneer: Prof. of Chemical Engg. Hoyt Hottel- 1924-68 at MIT)

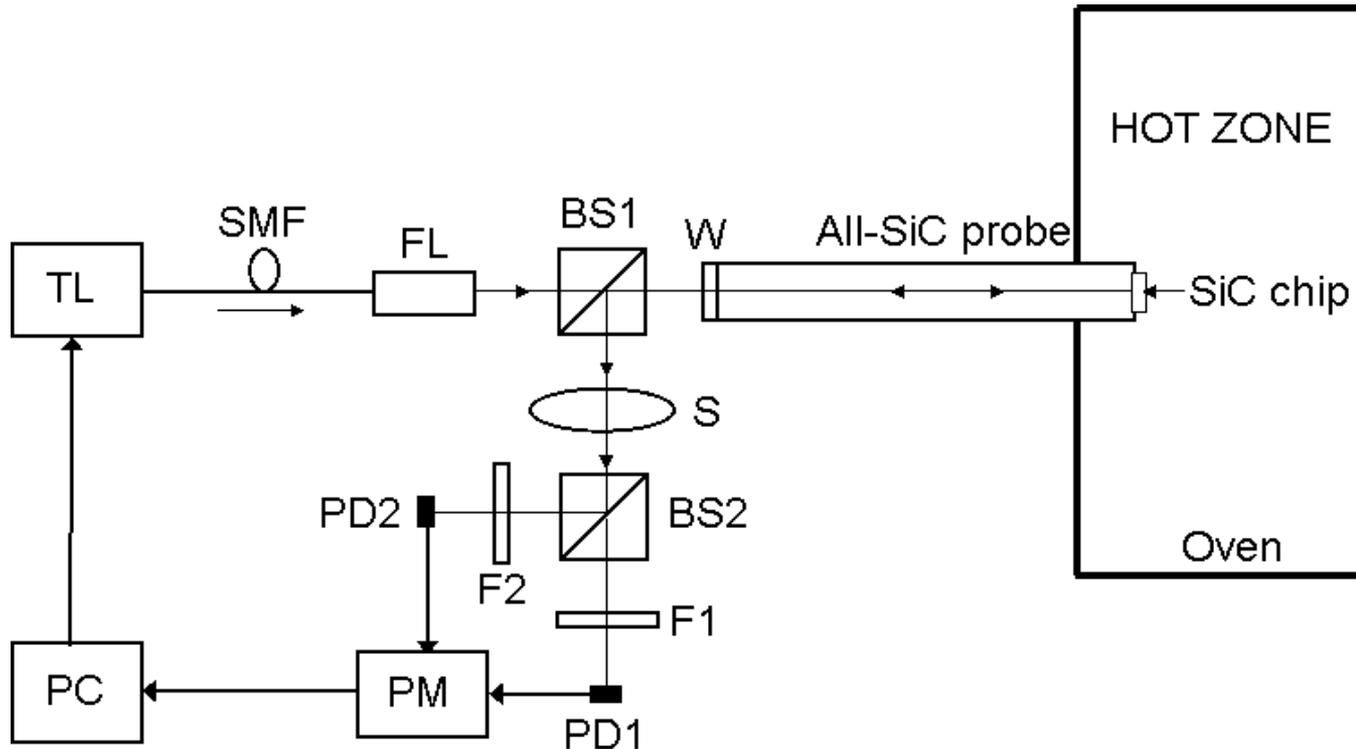
--- **Indirect View of Protected Target Material BB radiation**

- **OK as No window and changing emmissivity issue BUT Problem of light coupling and Multi-material issue (couple light to optical fiber – NASA– Coarse Temperature Resolution and Multi-Material Design – Mechanical Breakdown issues)**

**Can Pyrometry Positively Impact
The Proposed All-SiC Hybrid Sensor?**

Proposed Dual-Signal Processing-Mode Sensor Design

A First Hybrid Design: Pyrometry + Laser Interferometry



F1, F2: Optical Bandpass Filters

Two-Color Pyrometer

- Measure radiation power at two wavelengths and take the ratio

Wein Approximation $I(\lambda, T) = \frac{2hc^2}{\lambda^5} e^{-\frac{hc}{\lambda kT}} \cdot \varepsilon(\lambda, T)$

$$R = \frac{P_{\lambda_1}}{P_{\lambda_2}} = A_s \left(\frac{\lambda_2}{\lambda_1} \right)^5 \frac{\varepsilon(\lambda_1, T) + a(\lambda_1, T)}{\varepsilon(\lambda_2, T) + a(\lambda_2, T)} \exp \left[-C_2 \left(\frac{1}{\lambda_1} - \frac{1}{\lambda_2} \right) \frac{1}{T} \right]$$

A_s : system-specific constant – takes into account optical and detection components

$a(\lambda, T)$: specific emissivity of the background

$C_2 = hc/k$

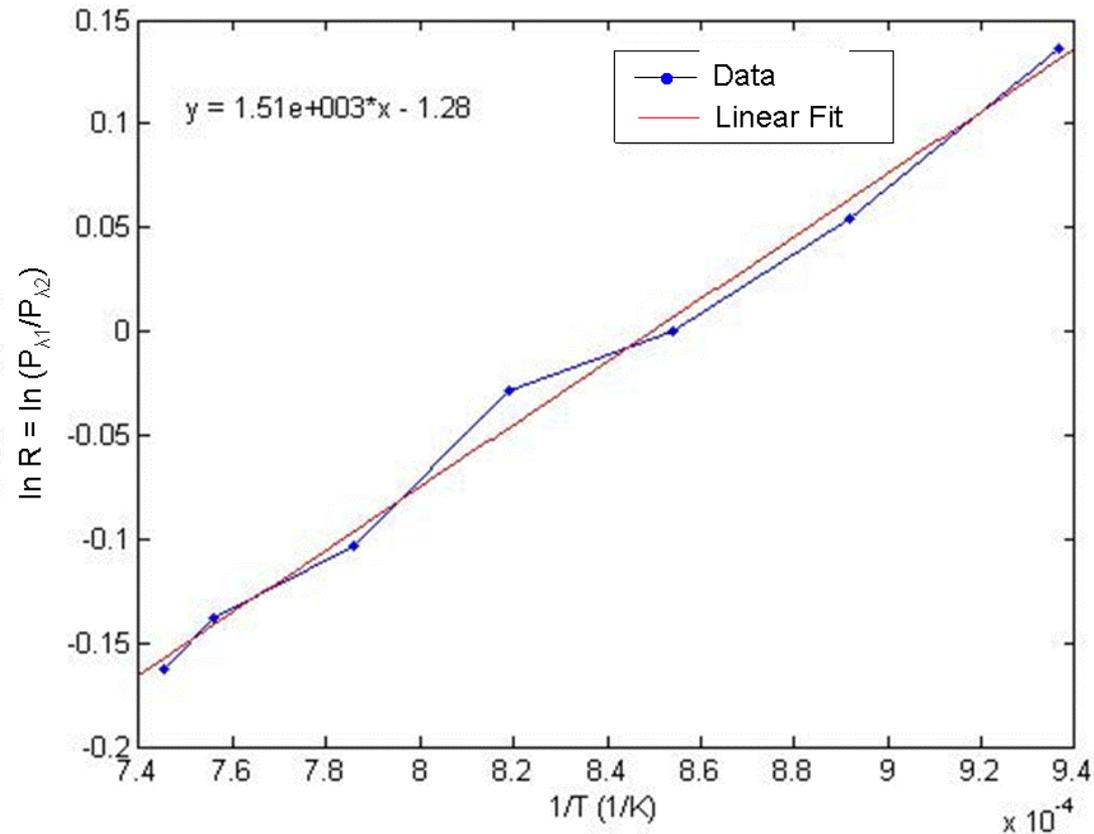
Two-Color Pyrometer

- Specific emissivity has a weak dependence on wavelength
- If the two wavelengths are selected close to each other, then the emissivity ratio can be approximated to a constant

$$R = \frac{P_{\lambda_1}}{P_{\lambda_2}} = A_s \left(\frac{\lambda_2}{\lambda_1} \right)^5 \frac{\varepsilon(\lambda_1, T) + a(\lambda_1, T)}{\varepsilon(\lambda_2, T) + a(\lambda_2, T)} \exp \left[-C_2 \left(\frac{1}{\lambda_1} - \frac{1}{\lambda_2} \right) \frac{1}{T} \right]$$

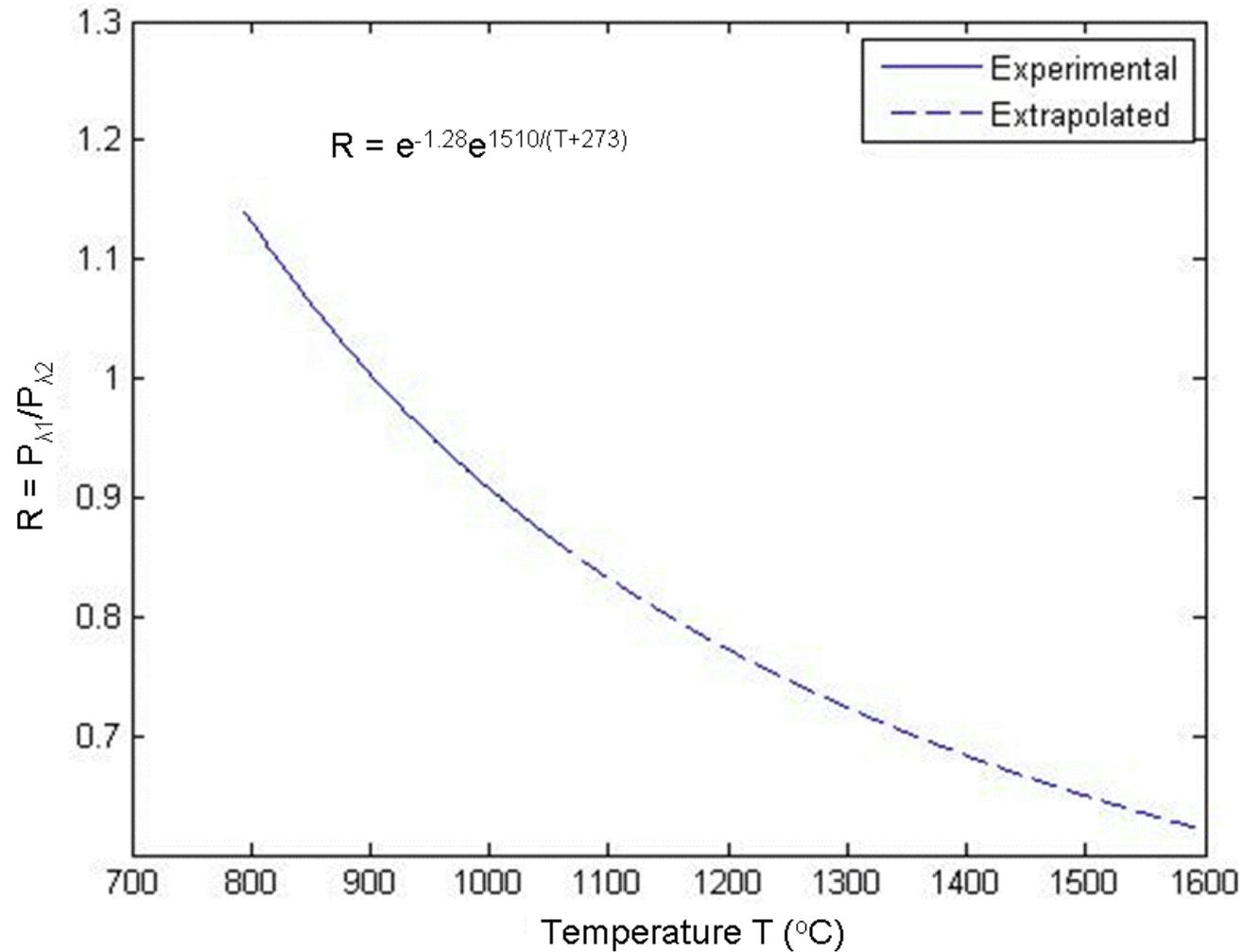
$$\ln R = \alpha + \frac{\beta}{T}$$

Proposed SiC Sensor Calibration Experimental Results



F1: Center wavelength: 1550 nm, FWHM: 30 nm
F2: Center wavelength: 1300 nm, FWHM: 30 nm

Calibration Curve from Data



Discussion on Results

- Works best beyond ~ 800 °C
- Resolution depends on the smallest change in radiation power that can be detected
- Estimated resolution varies between 5.8 °C at 795 °C to 2.7 °C at 1077 °C
- Can be used to give a coarse value of temperature

Proposed Fine Temperature Sensing Technique using Fixed Wavelength Power and Power Slope Measurement

Classic Fabry-Perot Etalon Reflectance

$$R_{FP} = \frac{R_1 + R_2 + 2\sqrt{R_1 R_2} \cos \varphi}{1 + R_1 R_2 + 2\sqrt{R_1 R_2} \cos \varphi} \quad \varphi = \frac{4\pi}{\lambda} n(\lambda, T) t(T)$$

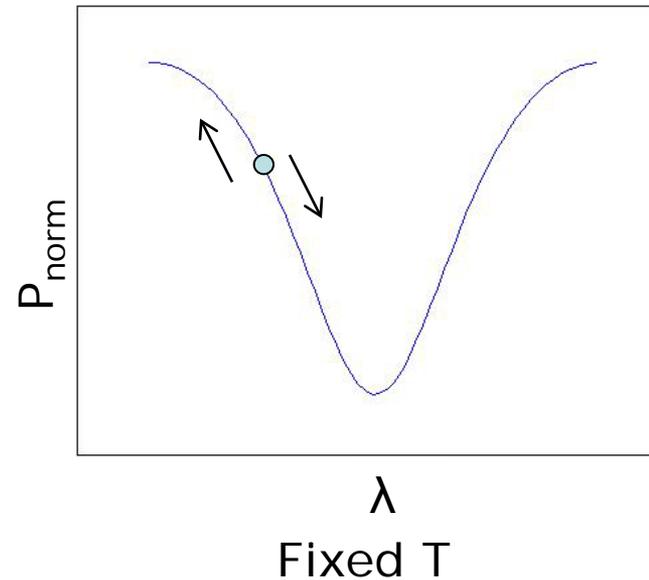
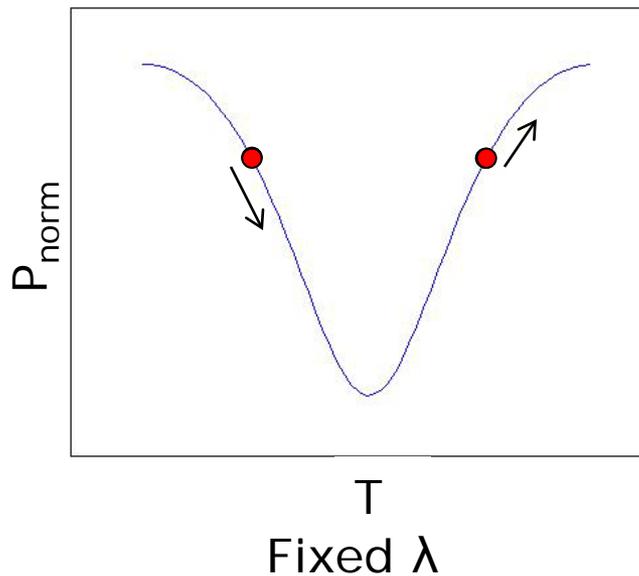
Detected Power $P \propto R_{FP}$

$$P_{norm} = \frac{P - P_{min}}{P_{max} - P_{min}}$$

$$\frac{dP}{d\lambda} = \frac{dP}{d\varphi} \frac{d\varphi}{d\lambda} = -\frac{4\pi}{\lambda^2} n(T) t(T) \frac{dP}{d\varphi}$$

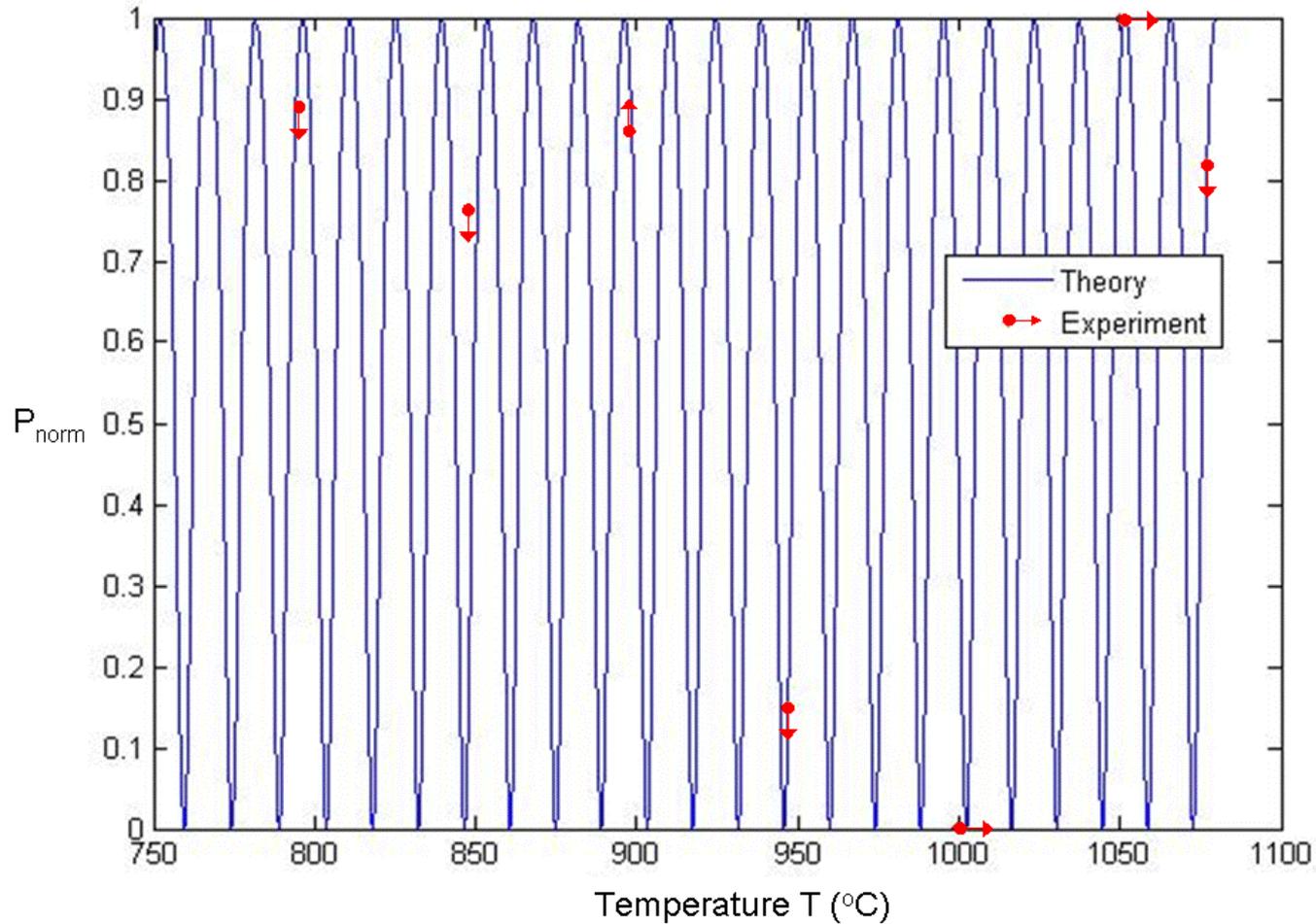
- If $dP/d\lambda$ is positive, then $dP/d\varphi$ would be negative and vice versa
- φ at a fixed wavelength changes only because of temperature

Normalized Power vs. Temperature Curve



Within each cycle, for any P_{norm} value, there are two possible values of temperature

Experiment



Fixed Wavelength λ : 1550 nm
Arrows denote the sign of $dP/d\lambda$

Summary of Hybrid Temperature Sensing Approach

- Find a coarse value of temperature using two-color pyrometry
- Measure laser reflected power
- Measure P_{\max} and P_{\min} by tuning the wavelength and use these to find P_{norm}
- Find the sign of $dP/d\lambda$ to find which half of the 2π cycle is the temperature
- Resolution is 0.1 °C
- Comparable to TC

Conclusion- Technology has Potential for Success

- Both single-crystal SiC and sintered SiC are tried and tested materiald
- Single-crystal SiC is used by US DoD for all high temperature power electronics
- Sintered SiC is used by NASA / ESA as a lightweight material for space platforms and for giant mirrors for telescopes



Ref: Seme Lab



Ref.: ESA