

# **Sealing Stresses and Deformations -SECA CTP-**

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# Critical questions

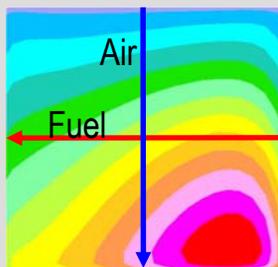
- ▶ What are the PEN stresses as a function of boundary stiffness during steady state or transient conditions?
- ▶ What are the cell edge displacements as a function of PEN stresses?
- ▶ What are the effects of stack B.C.s on stresses?
- ▶ What is the state of stress and displacement in the seal area?
- ▶ How does a dead load distributes throughout the stack, especially sealing areas?

# PEN Stresses during Steady State as a function of Boundary Compliance

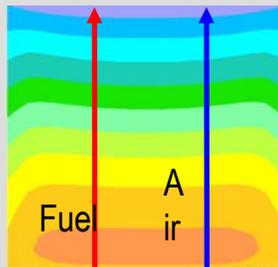
CROSS-FLOW

CO-FLOW

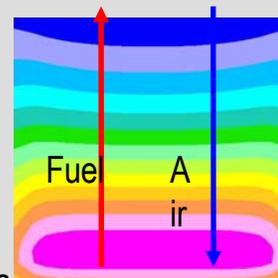
COUNTER-FLOW



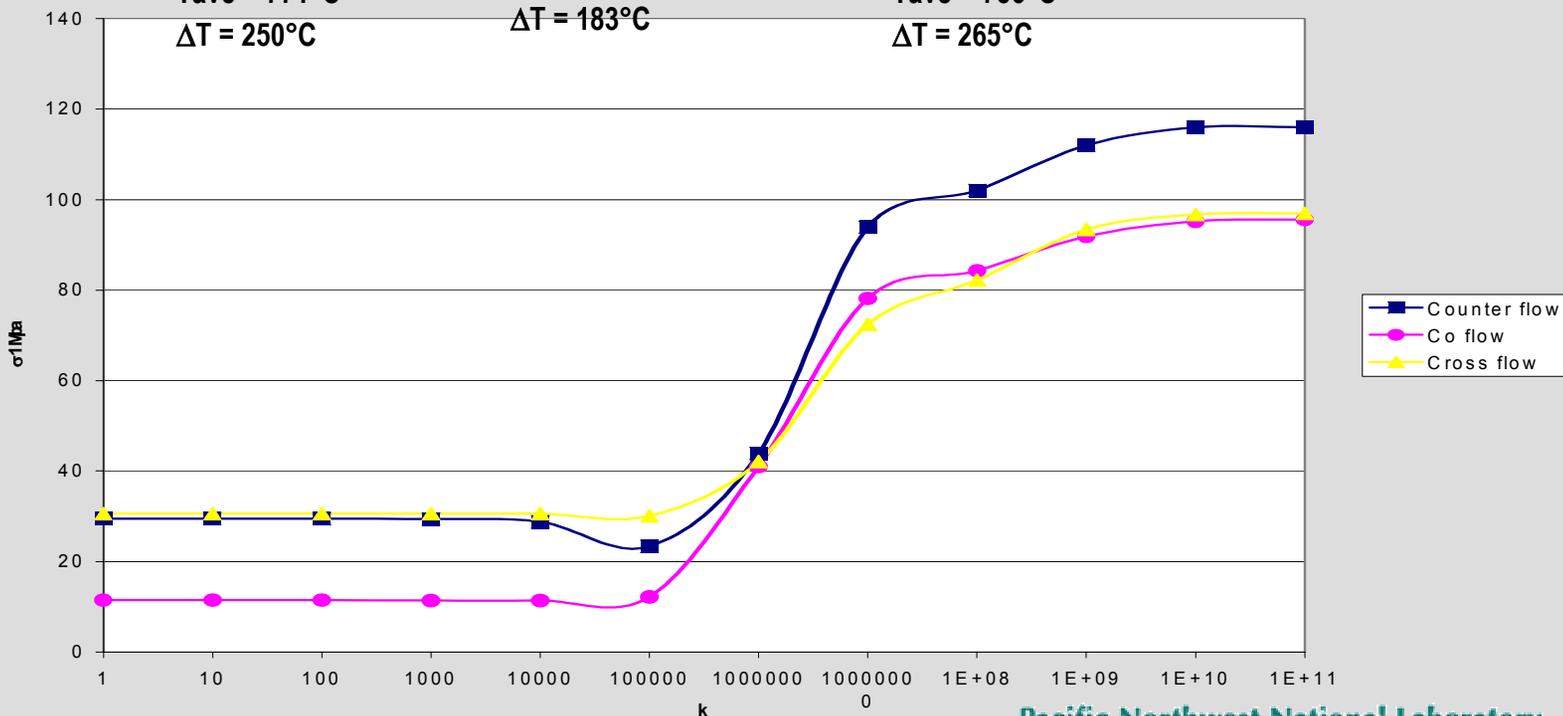
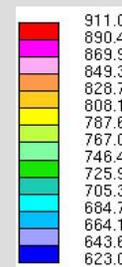
Tave = 771°C  
ΔT = 250°C



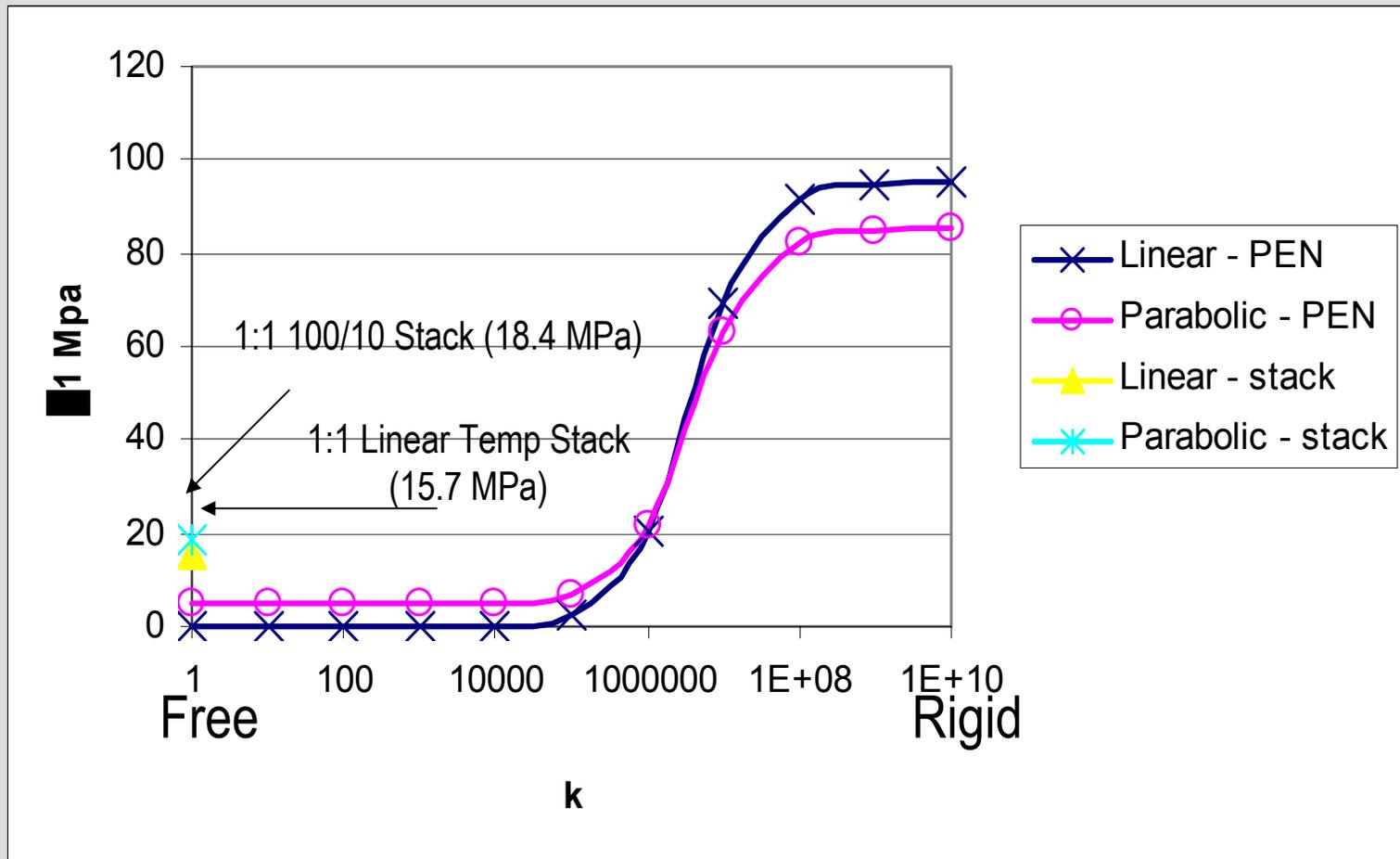
Tave = 761°C  
ΔT = 183°C



Tave = 756°C  
ΔT = 265°C



# PEN Stresses during Transient State as a function of Boundary Compliance

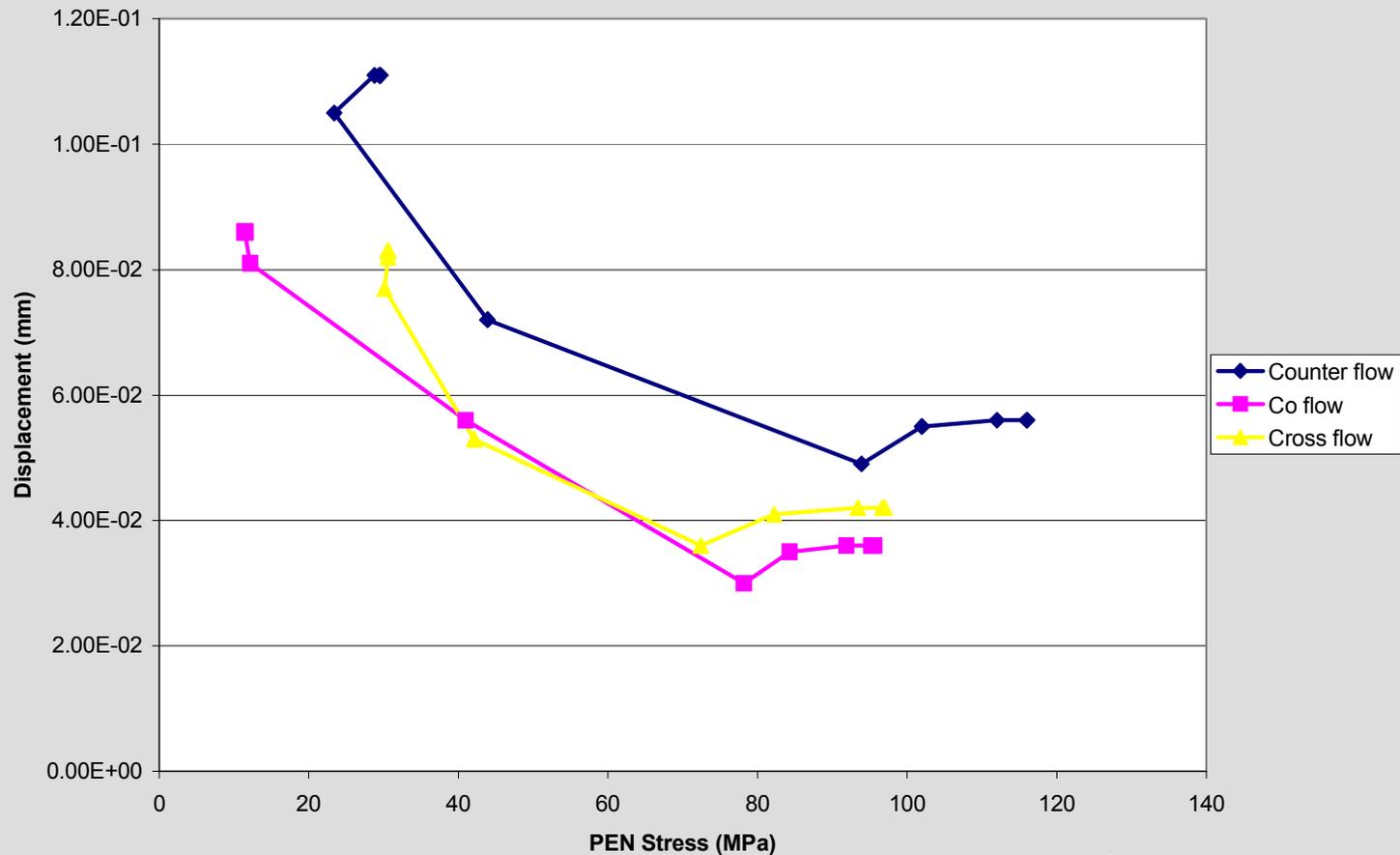


# Pure Shear and Axial Loading

	E (GPa)	nu	G (GPa)	K/L Shear	K/L Axial	K shear	K axial
YSZ	175	0.3	67.30769	1.7E+12	7.0E+09	1E+10	4E+07
Steel	120	0.3	46.15385	1.2E+12	4.8E+09	7E+09	3E+07
Glass	9	0.3	3.461538	8.7E+10	3.6E+08	5E+08	2E+06
Nylon	1.7	0.3	0.653846	1.6E+10	6.8E+07	1E+08	4E+05
Rubber	0.002	0.3	0.000769	1.9E+07	8.0E+04	1E+05	5E+02

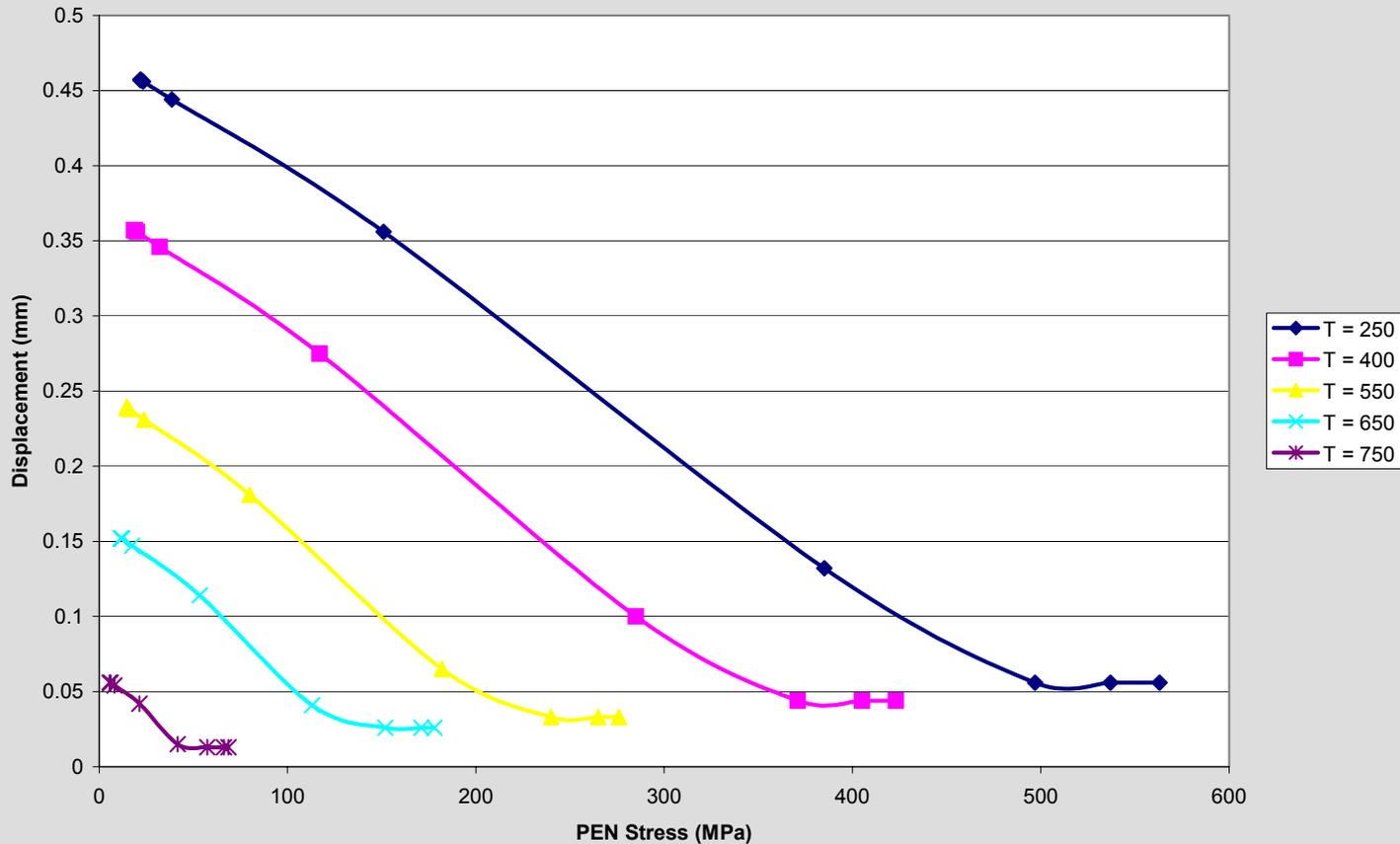
# Cell Edge Displacement During Steady State

Steady State Stress



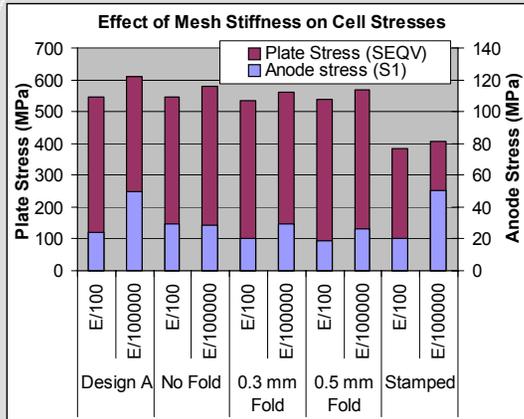
# Cell Edge Displacement During Transient Loading

Start-up Transient



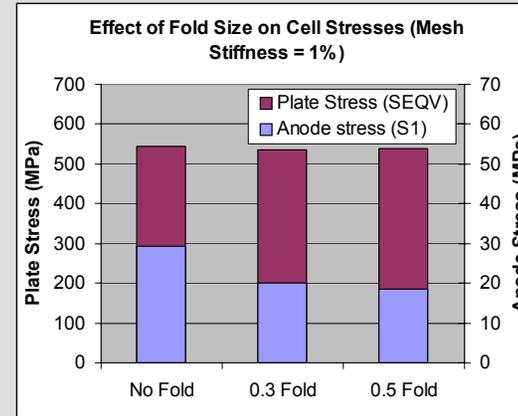
# Thermal-Structural Stress Analysis: Influence of Design Variables on Cell Stresses

## Mesh Stiffness



A more compliant mesh material generally increased the stresses in both the anode and the plate.

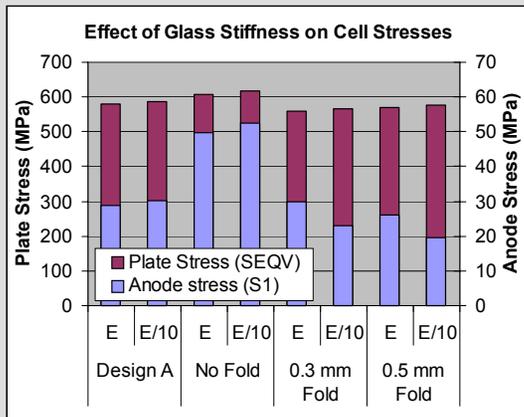
## Fold Size (rigid+compliance in fold)



Addition of fold reduced the anode stress significantly and the plate stresses slightly.

*(Note: Fold reduces the active area of PEN)*

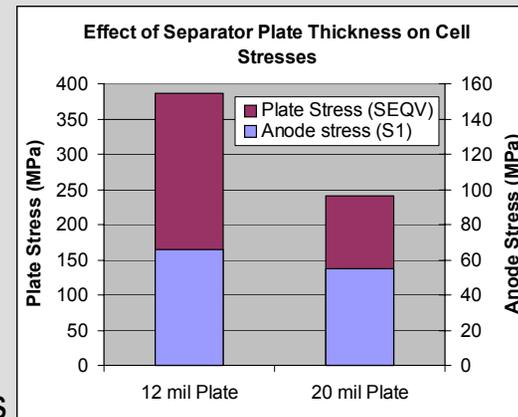
## Glass Stiffness



Reduced stiffness for the glass increased plate stresses.

Reduced glass stiffness also reduced anode stress in designs w/ a fold, but increased anode stress in designs w/o a fold.

## Separator Plate Thickness

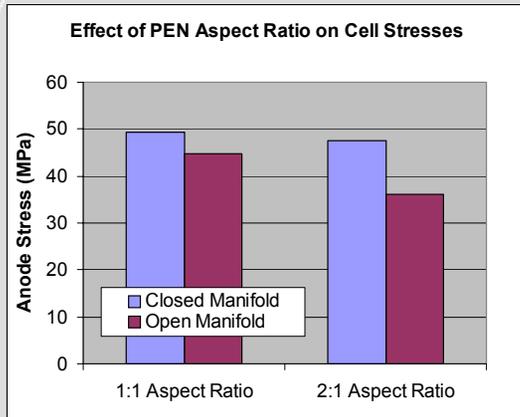


A thicker separator plate decreased the stresses in both the anode and the plate.

*(Note: Thicker plate gives slower thermal response for start-up)*

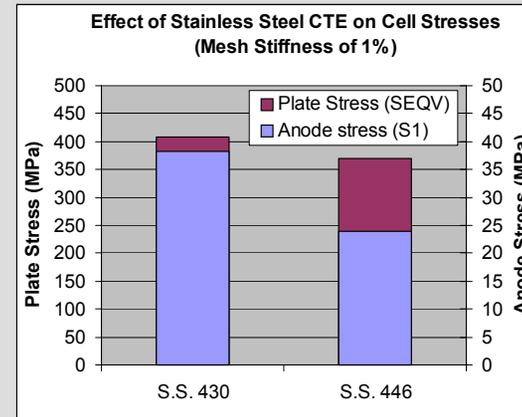
# Thermal-Structural Stress Analysis: Influence of Design Variables on Cell Stresses

## PEN Aspect Ratio



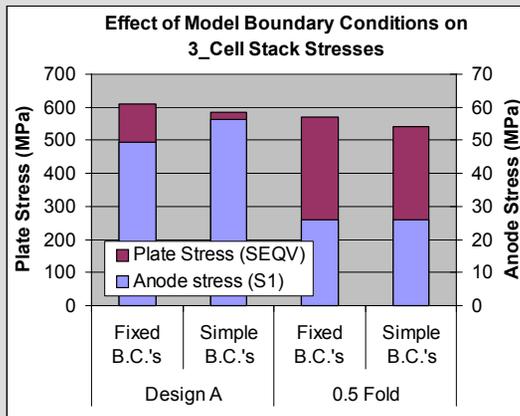
A rectangular PEN had lower stresses than a square PEN during start-up.

## CTE



Lower coefficient of thermal expansion (CTE) for 446 stainless steel significantly reduced anode and plate stresses.

## Model B.C.'s



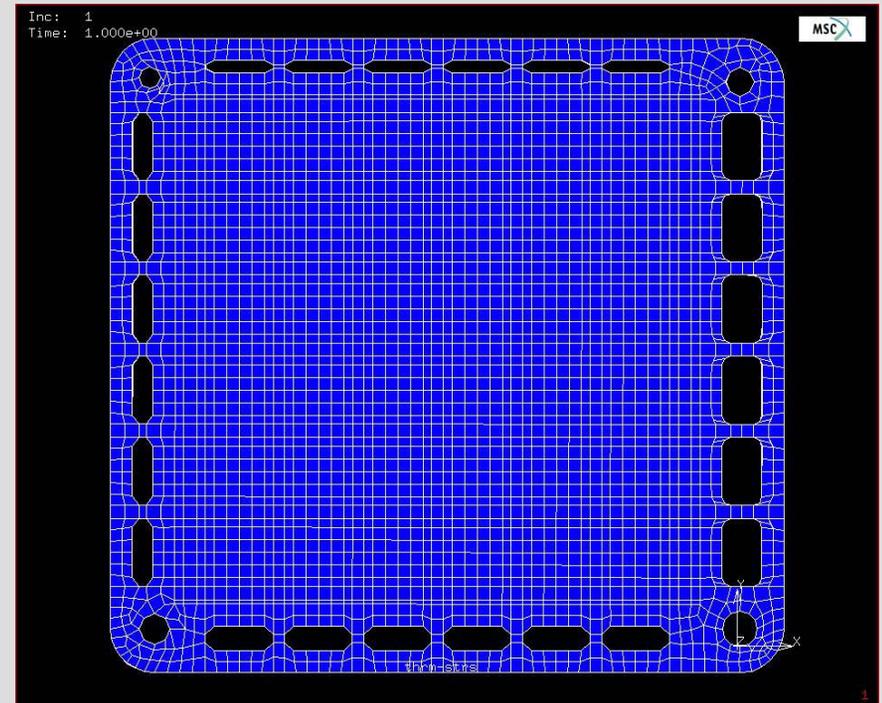
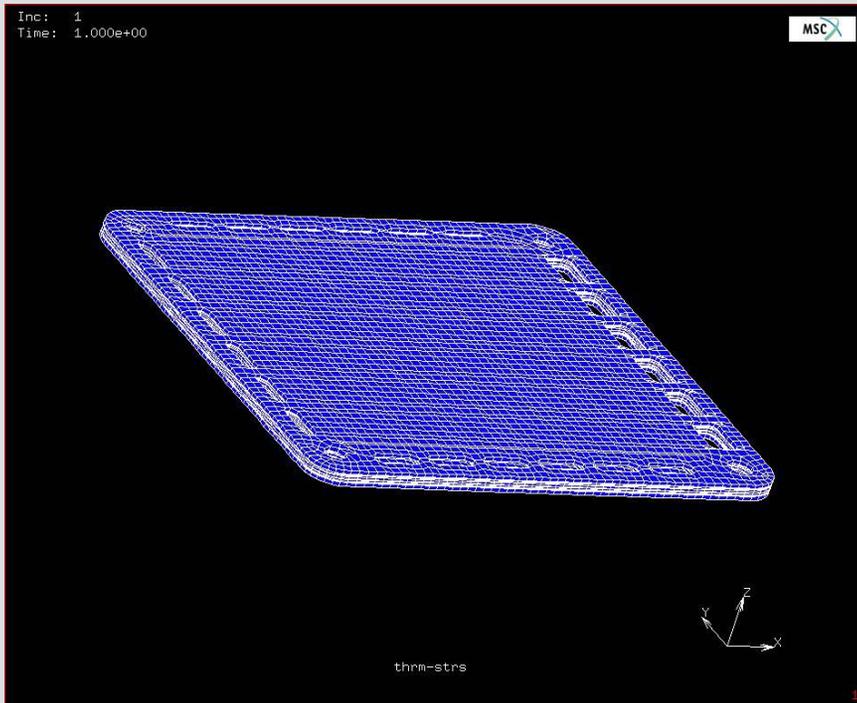
The stack stiffness can be accounted for with boundary conditions. The effect of the model B.C.'s on stresses was found to be dependent on the cell design.

# Results 3-Stack Simulations

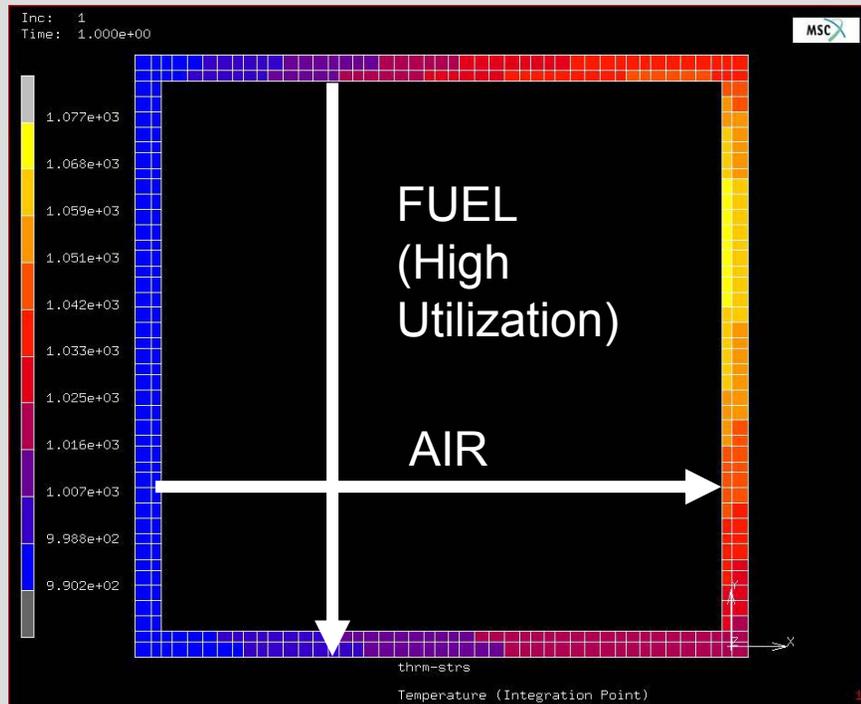
		Anode $\sigma_1$ MPa	SS $\sigma_{eqv}$ MPa
1% (A)	Bottom	24	370
	Top	22	547
0.001% (D)	Bottom	49.6	313
	Top	32.4	609
0.001% (E) Simple BC	Bottom	56.4	410
	Top	33.8	585
0.001% (F) 10% glass	Bottom	52.5	326
	Top	28.9	617

- Will the stack survive thermal stresses? (based on stress/strength failure criteria)
- What is the effect of out of plane stiffness?
- Will softer glass reduce stresses?
- How do the B.C.'s change stress profiles?

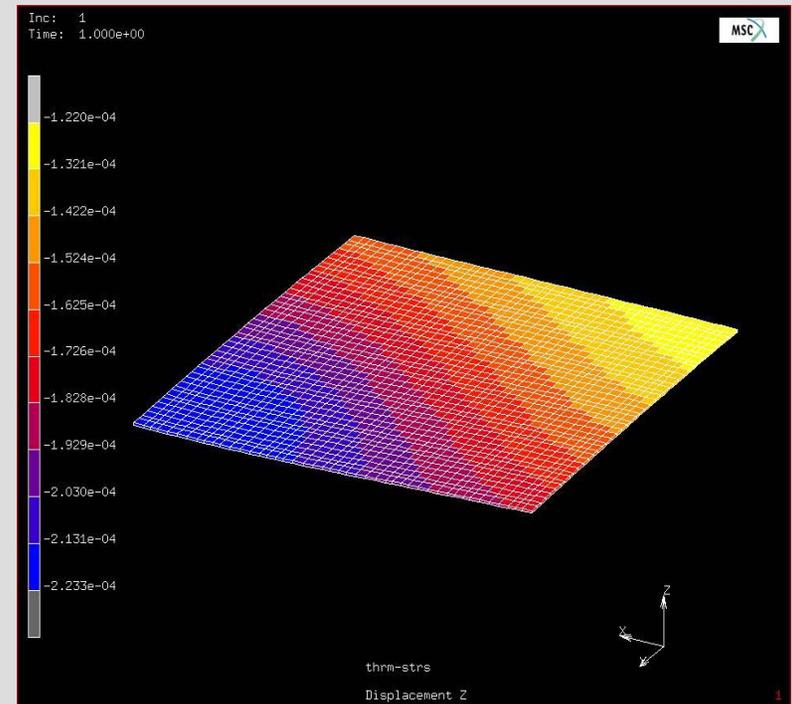
# 1- Cell Stack (Picture Frame)



# Seal Temperature Profile and PEN out-Plane Deformation

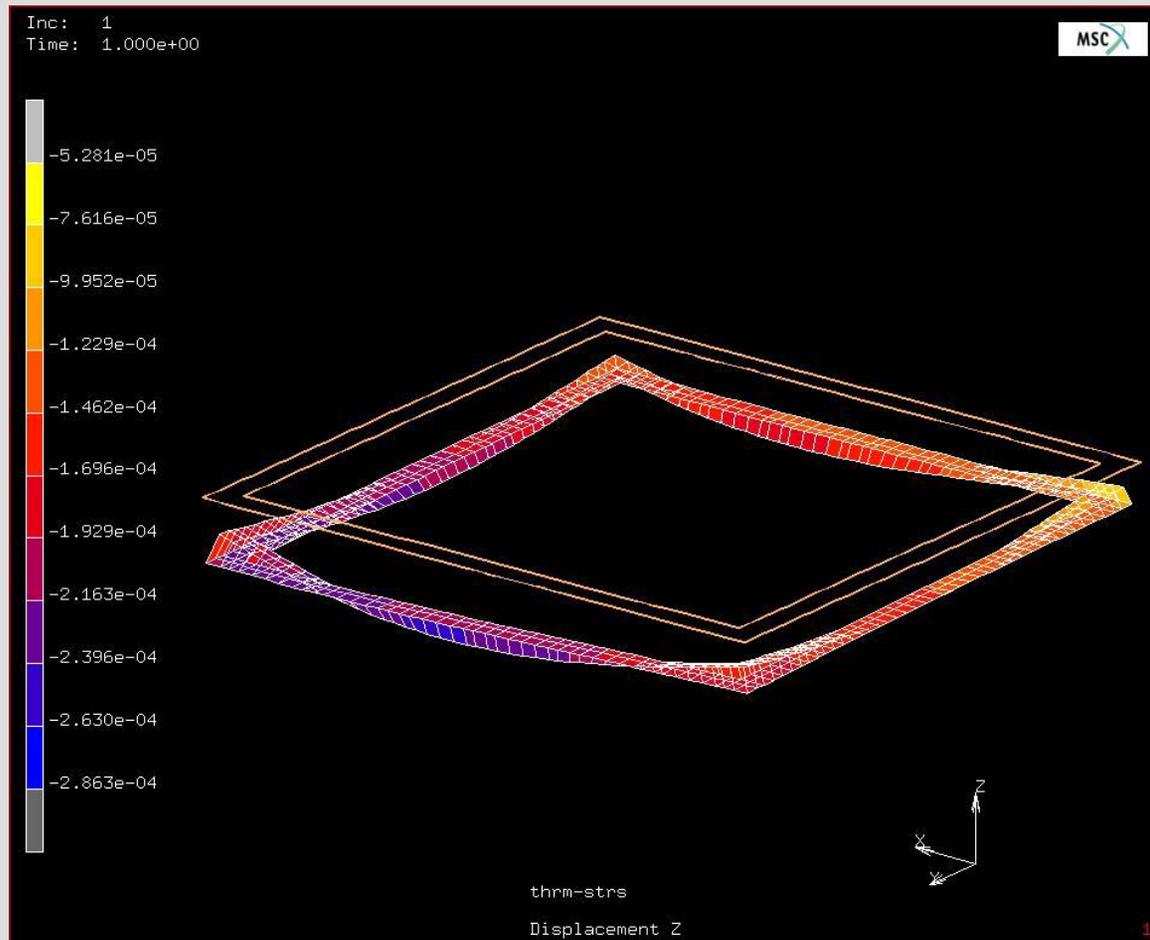


Seal Temperature



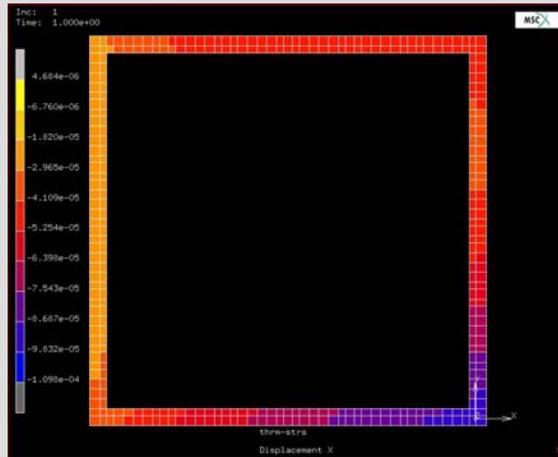
PEN UZ  
Deformation

# Seal Deformations

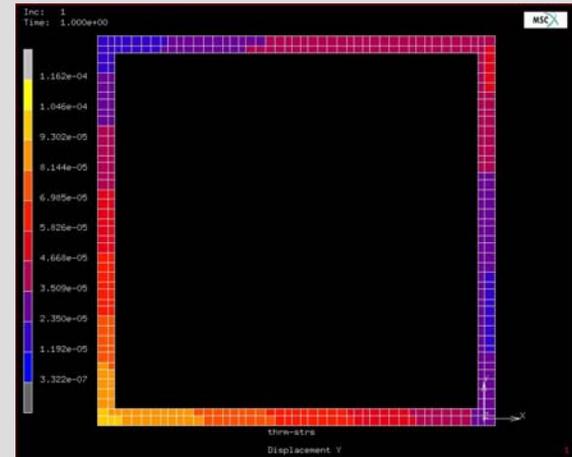


# Displacement Components in Seal

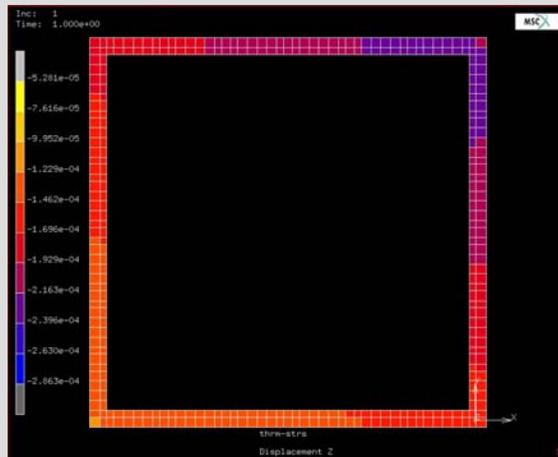
UX



UY

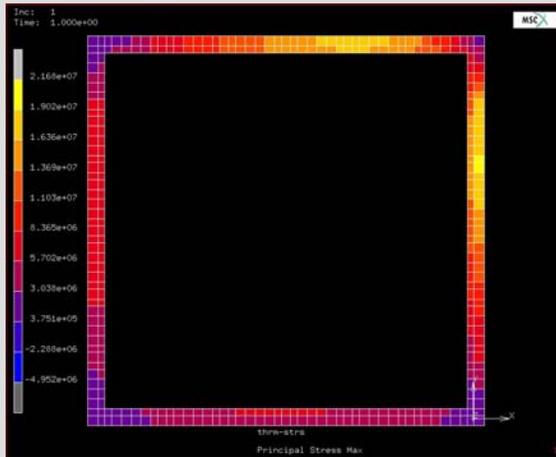


UZ

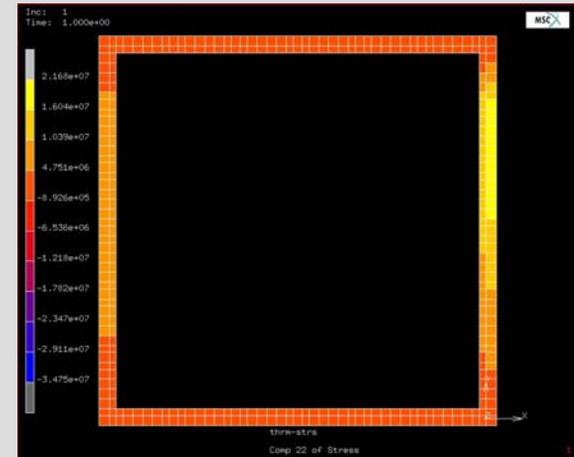


# Seal – Principal Stresses

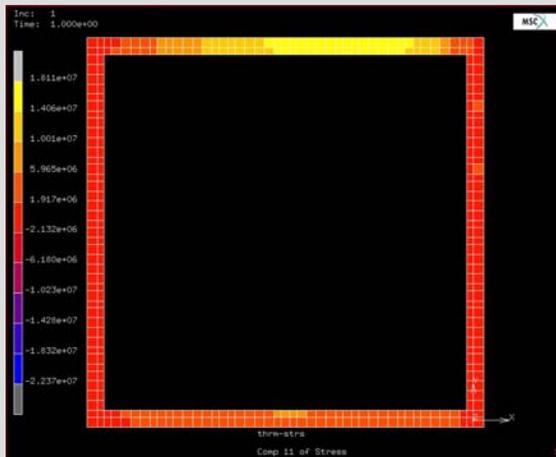
SMAX



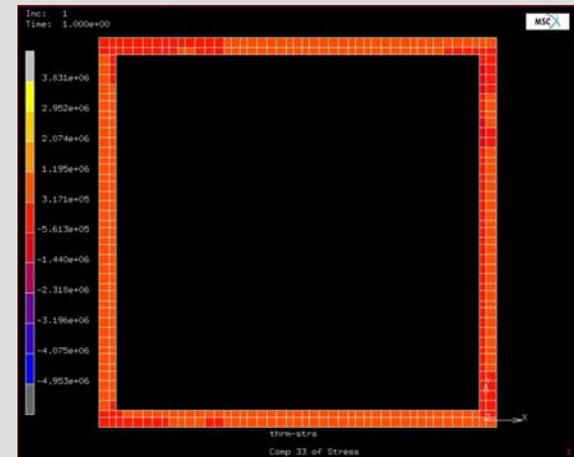
SY/S22



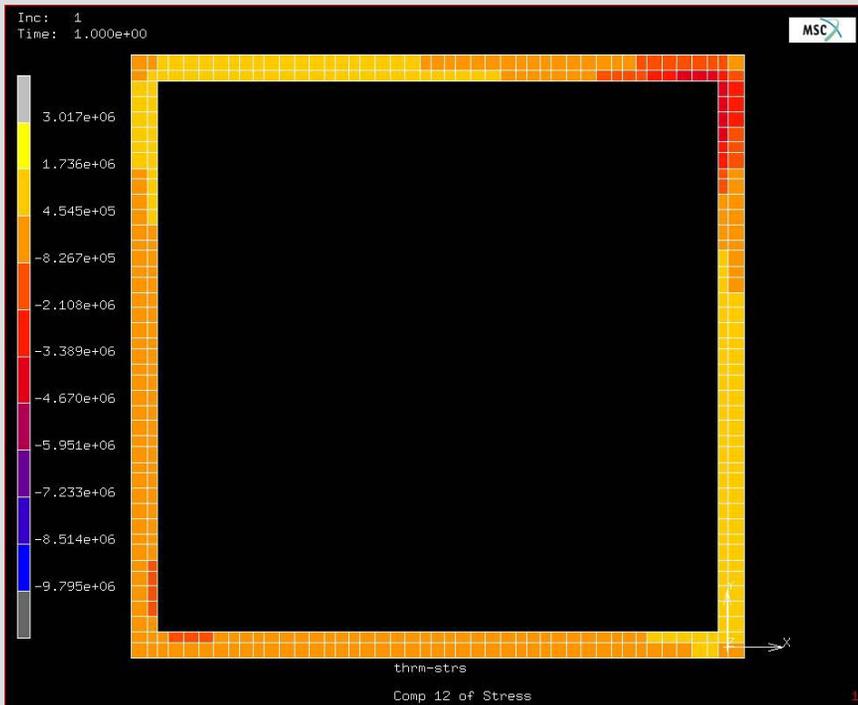
SX/S11



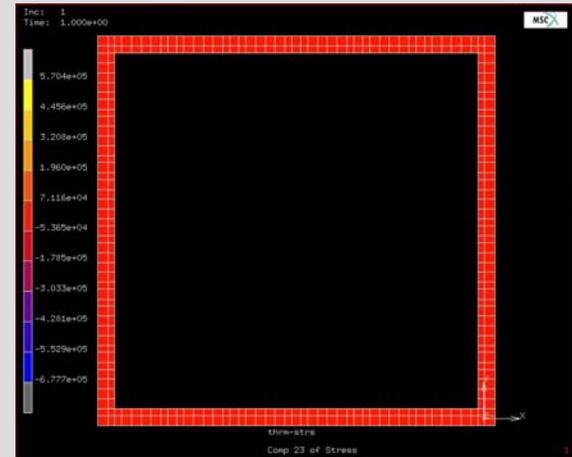
SZ/S33



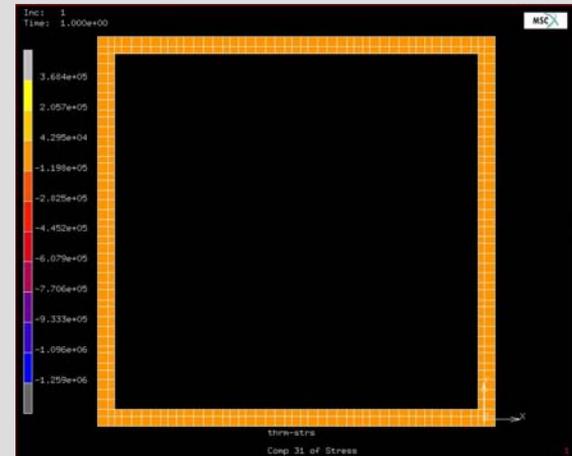
# Seal- Shear Stresses



SXY/S12

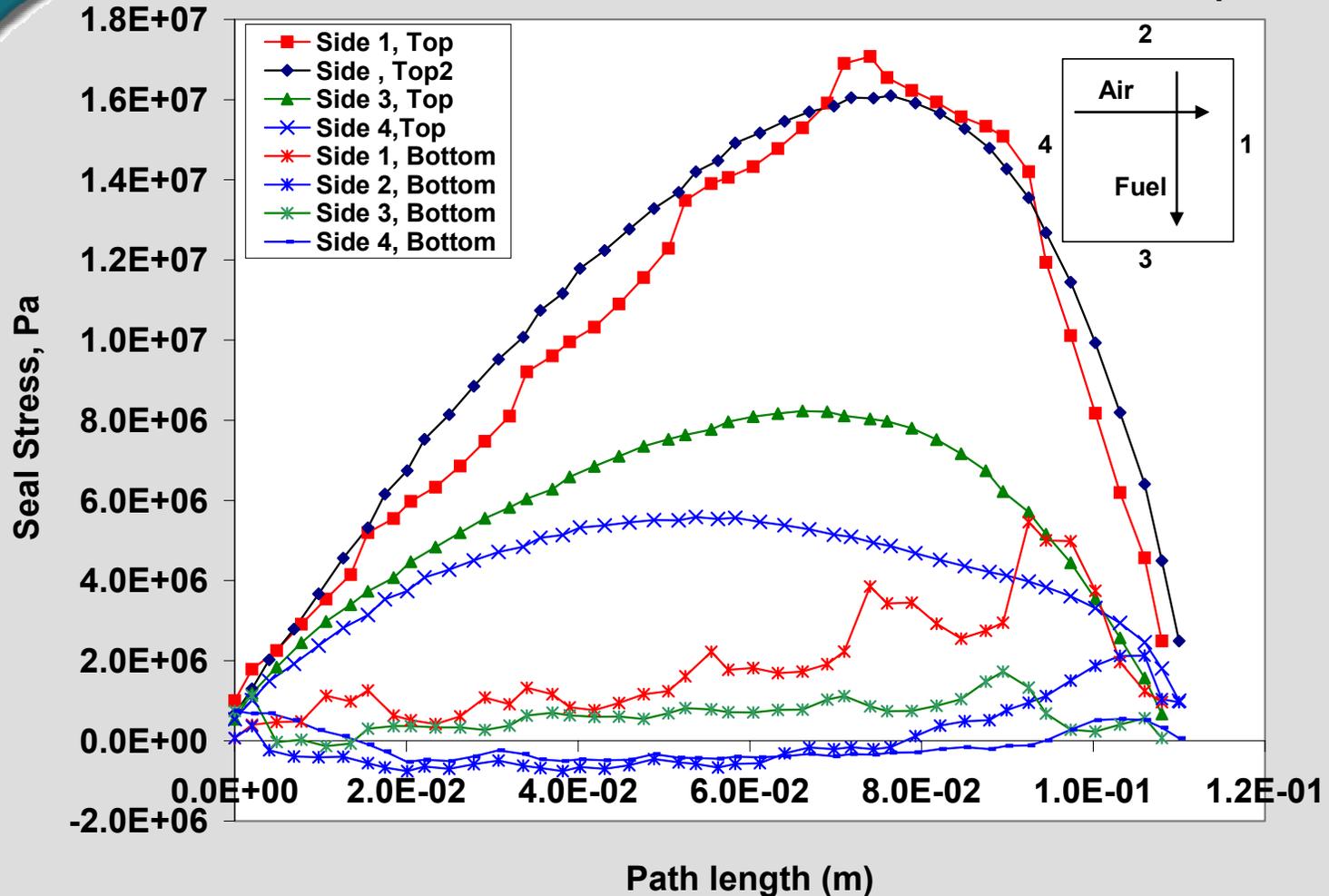


SYZ/S23



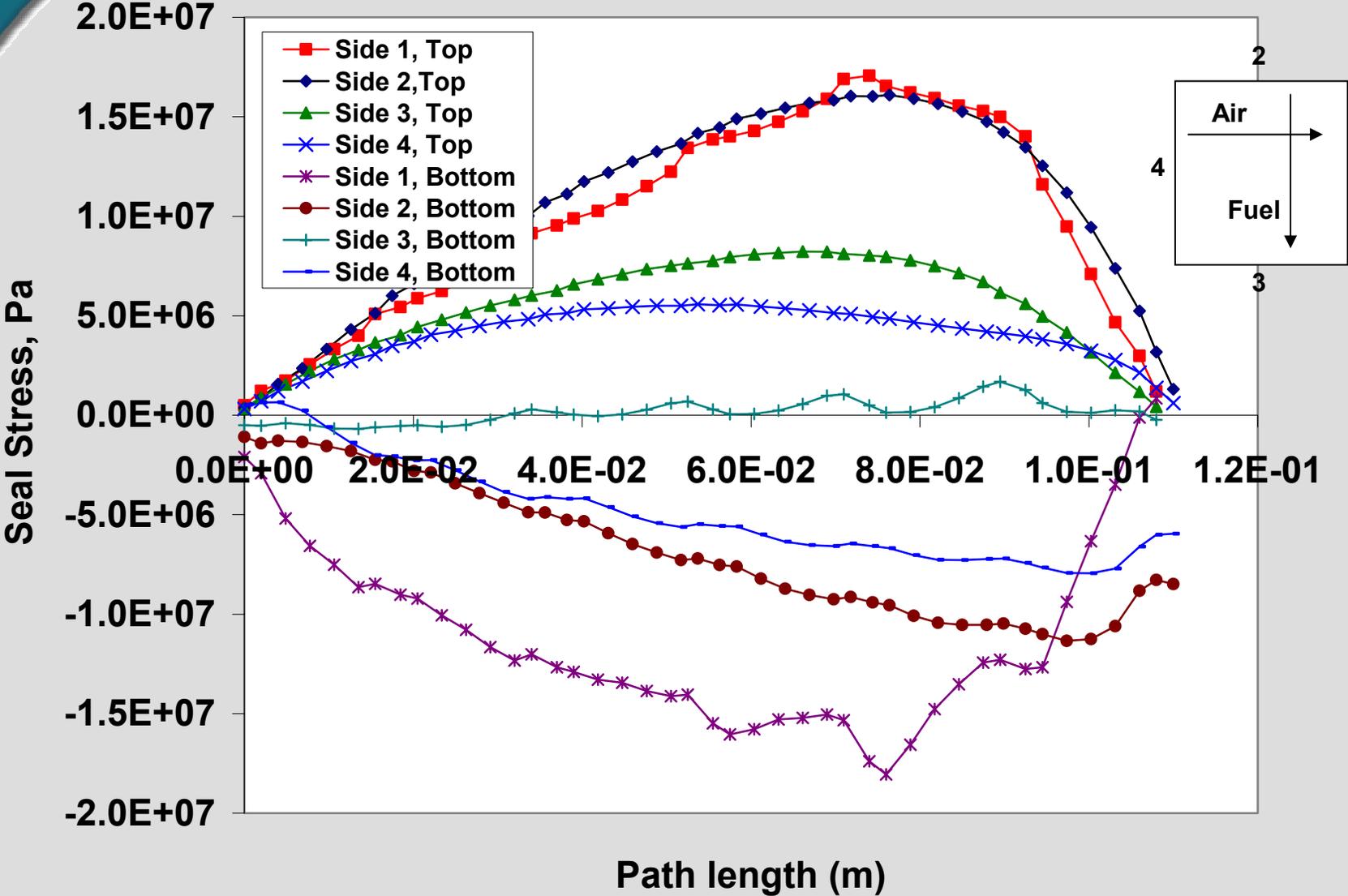
SXZ/S31

## Seal Stress - Maximum Principal

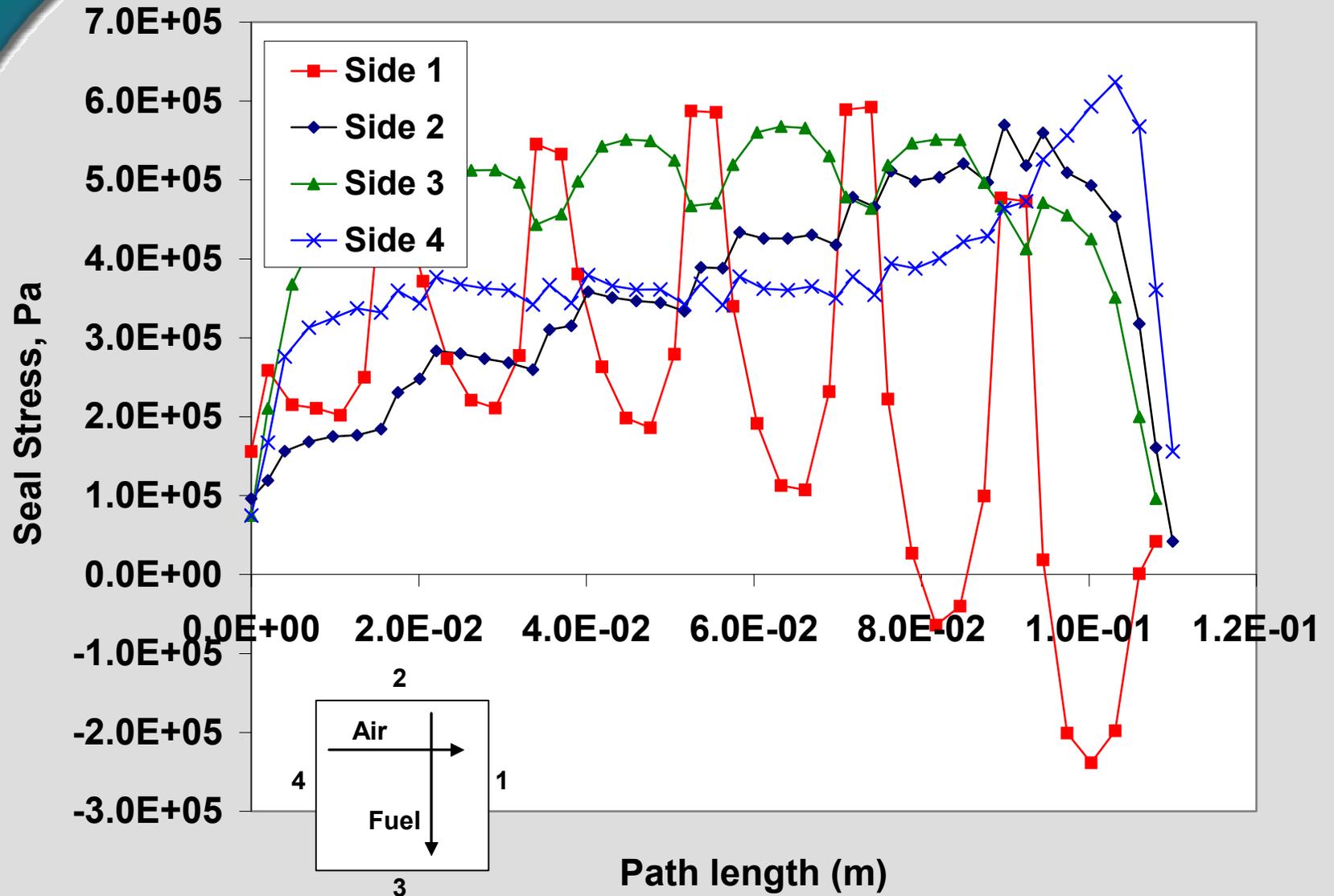


Max principal much larger on one side than other- bending dominated. 17 Mpa max.  
 Caveat- This is only a 1 cell model with simple support, much more flexible than stuck to a manifold.

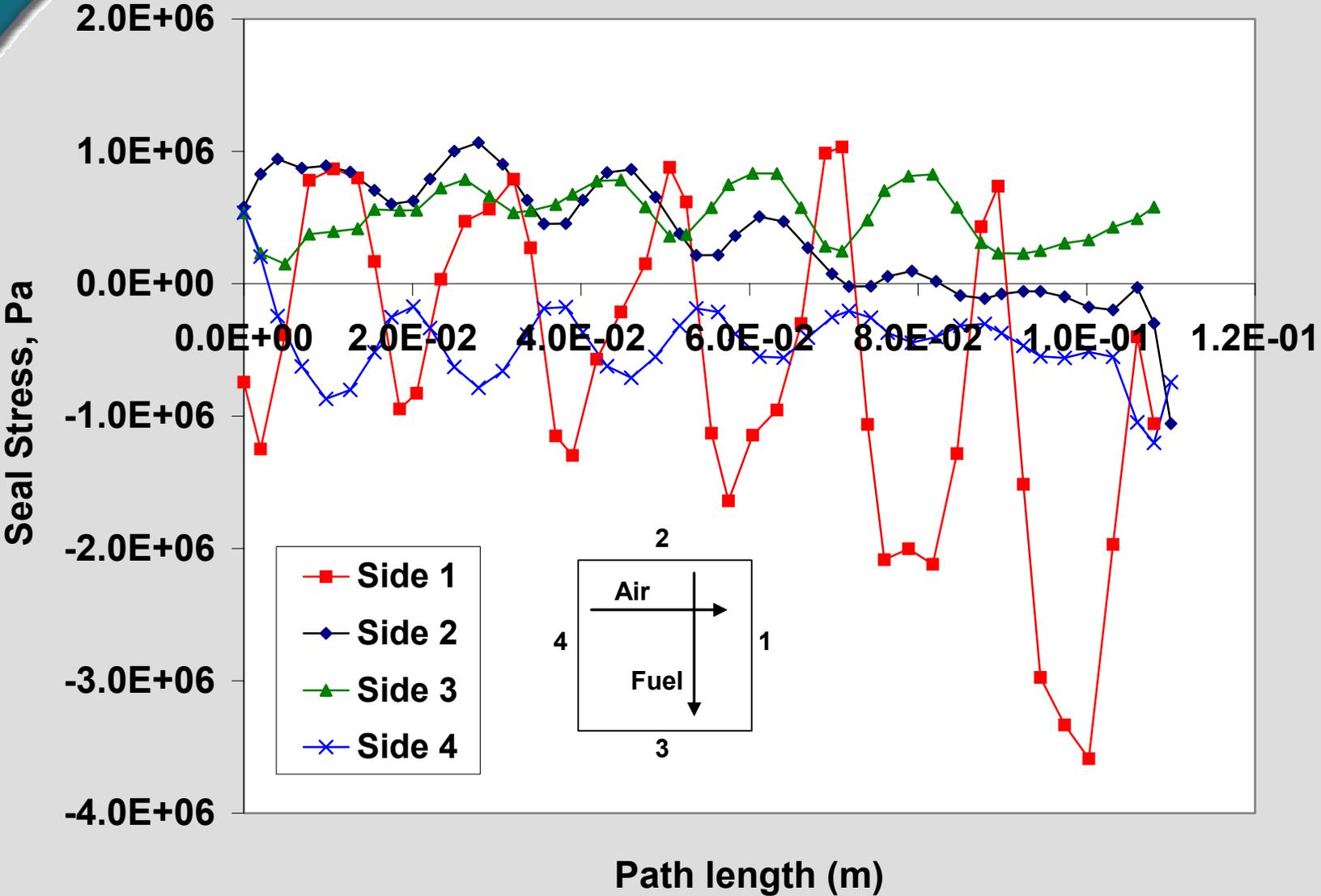
### Seal Stress - Parallel to PEN Edge



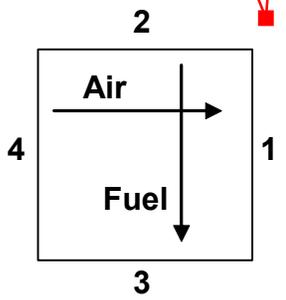
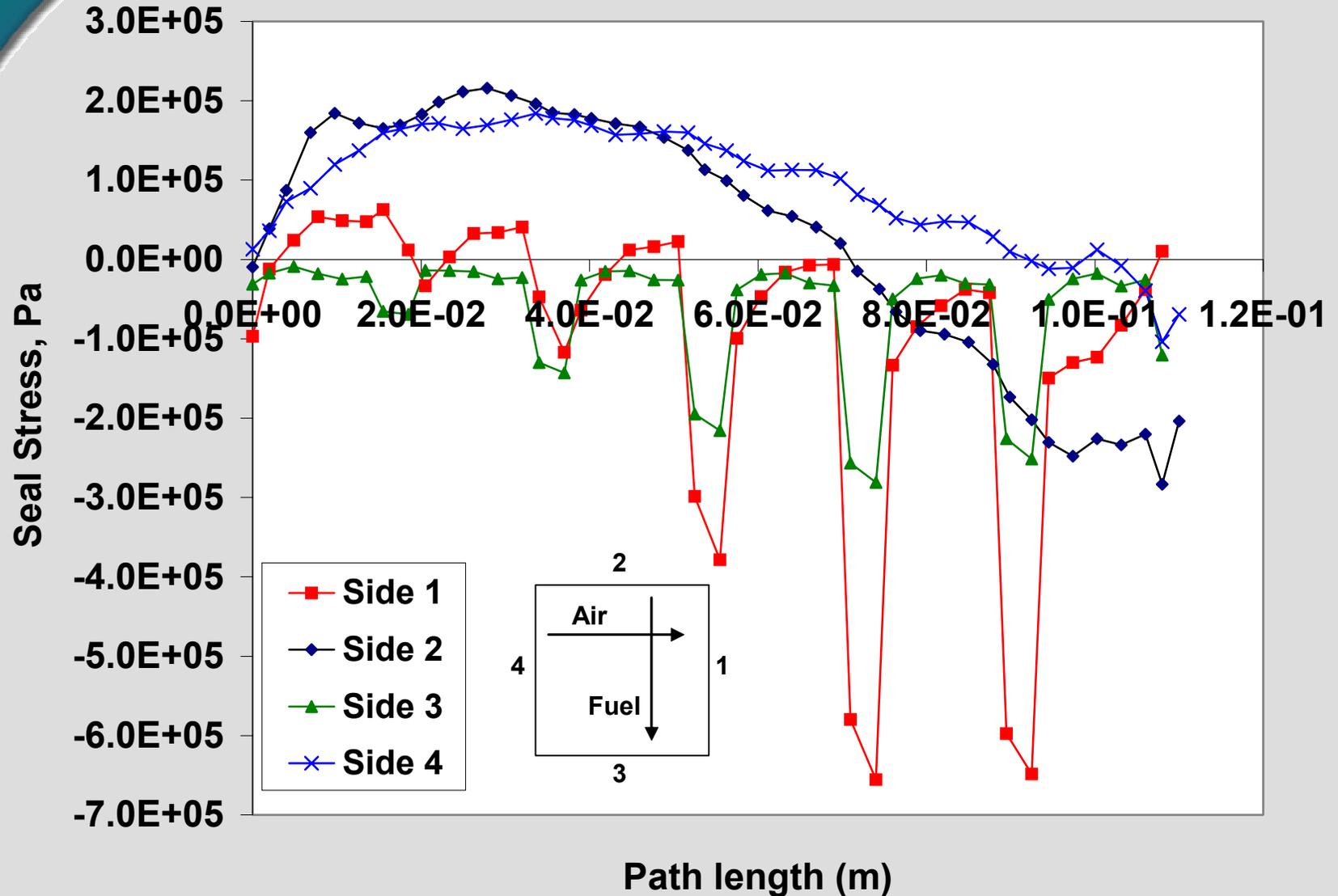
# Seal Stress - Out of Plane



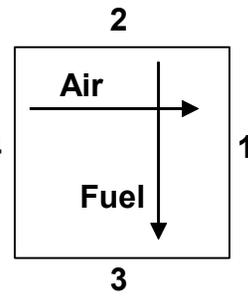
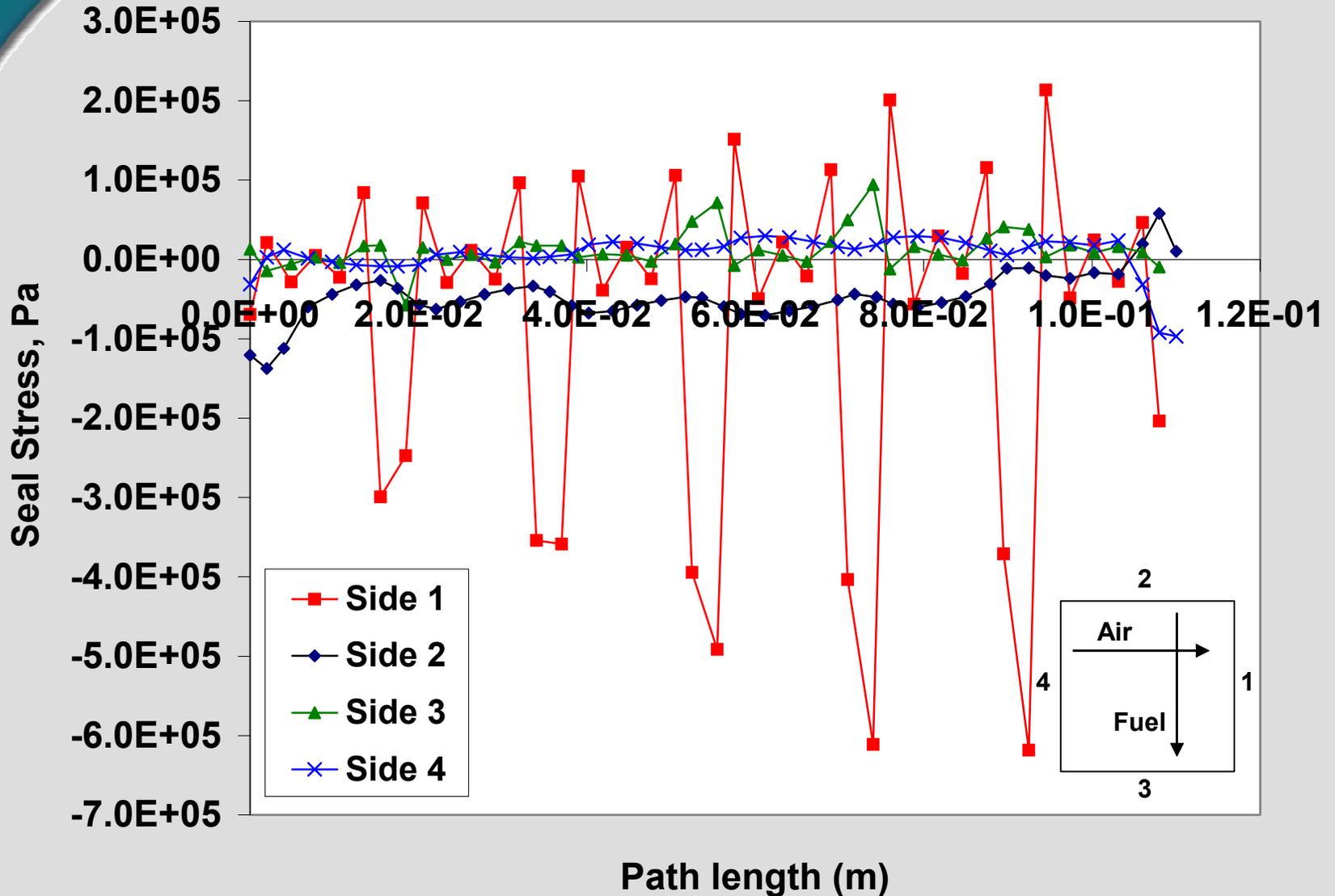
# Seal Shear Stress - InPlane



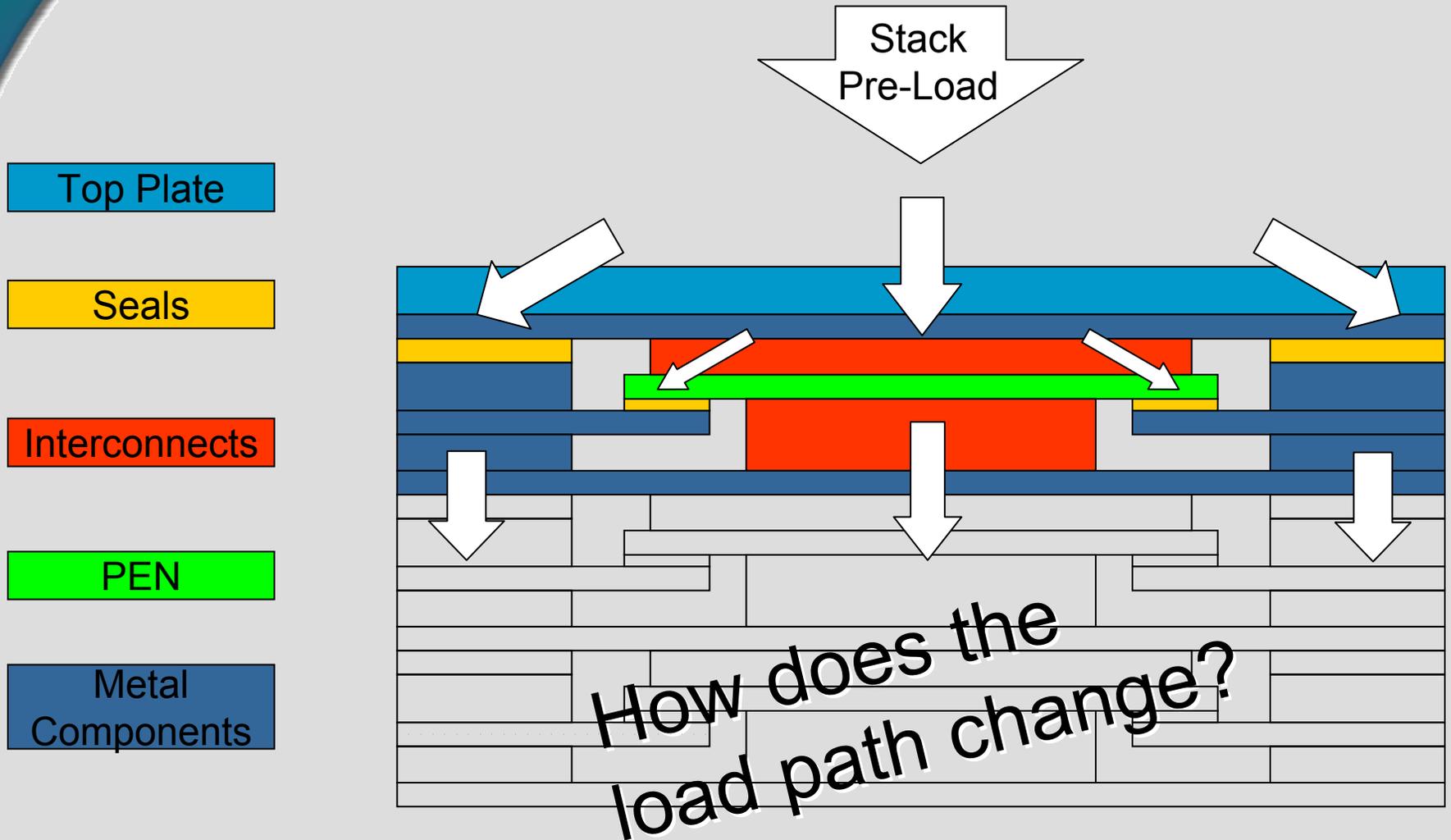
## Seal Shear Stress - Tangent to PEN Edge



# Seal Shear Stress - Normal to PEN Edge



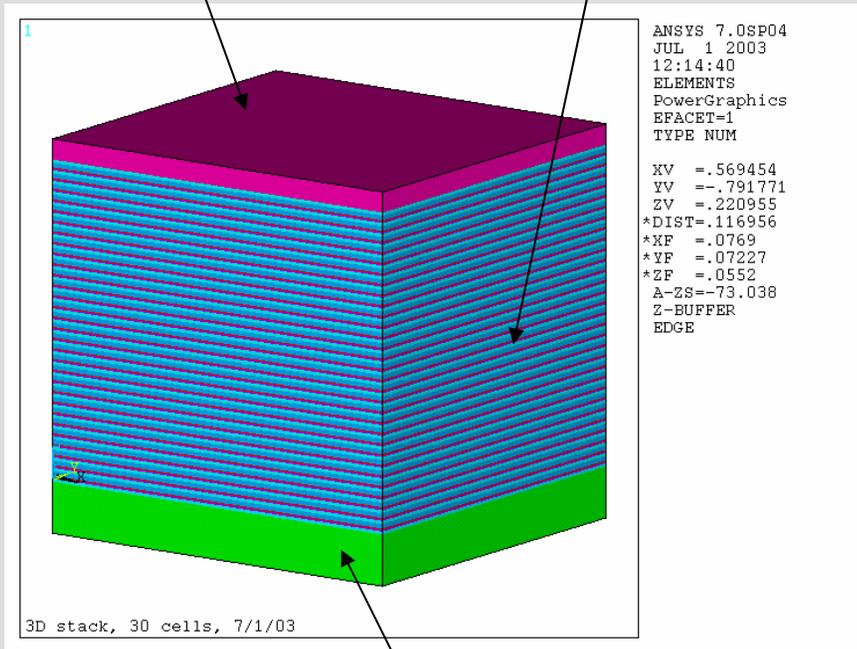
# Load Paths for Multiple Planar Cell Stack



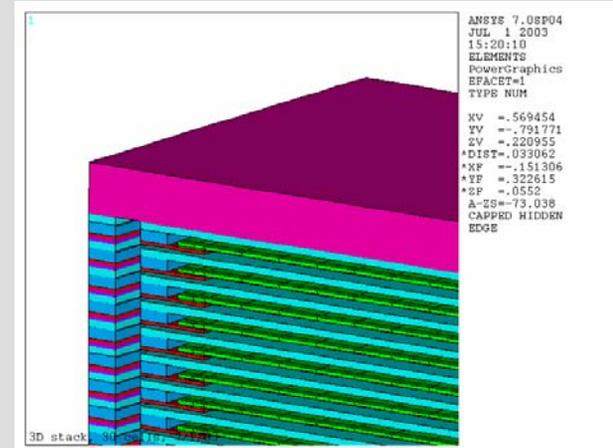
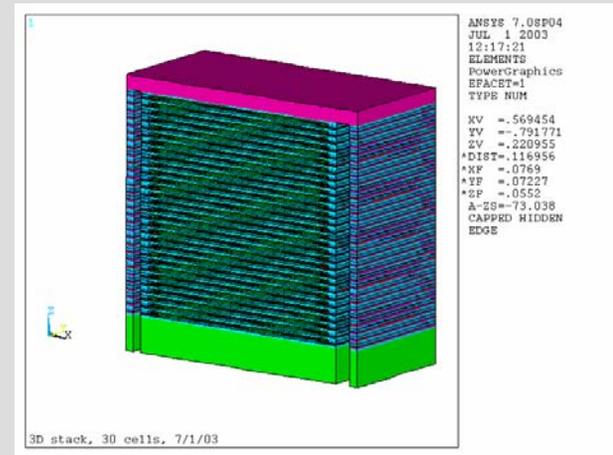
# Load Paths for Multiple Planar Cell Stack

Top Plate

30 Cells

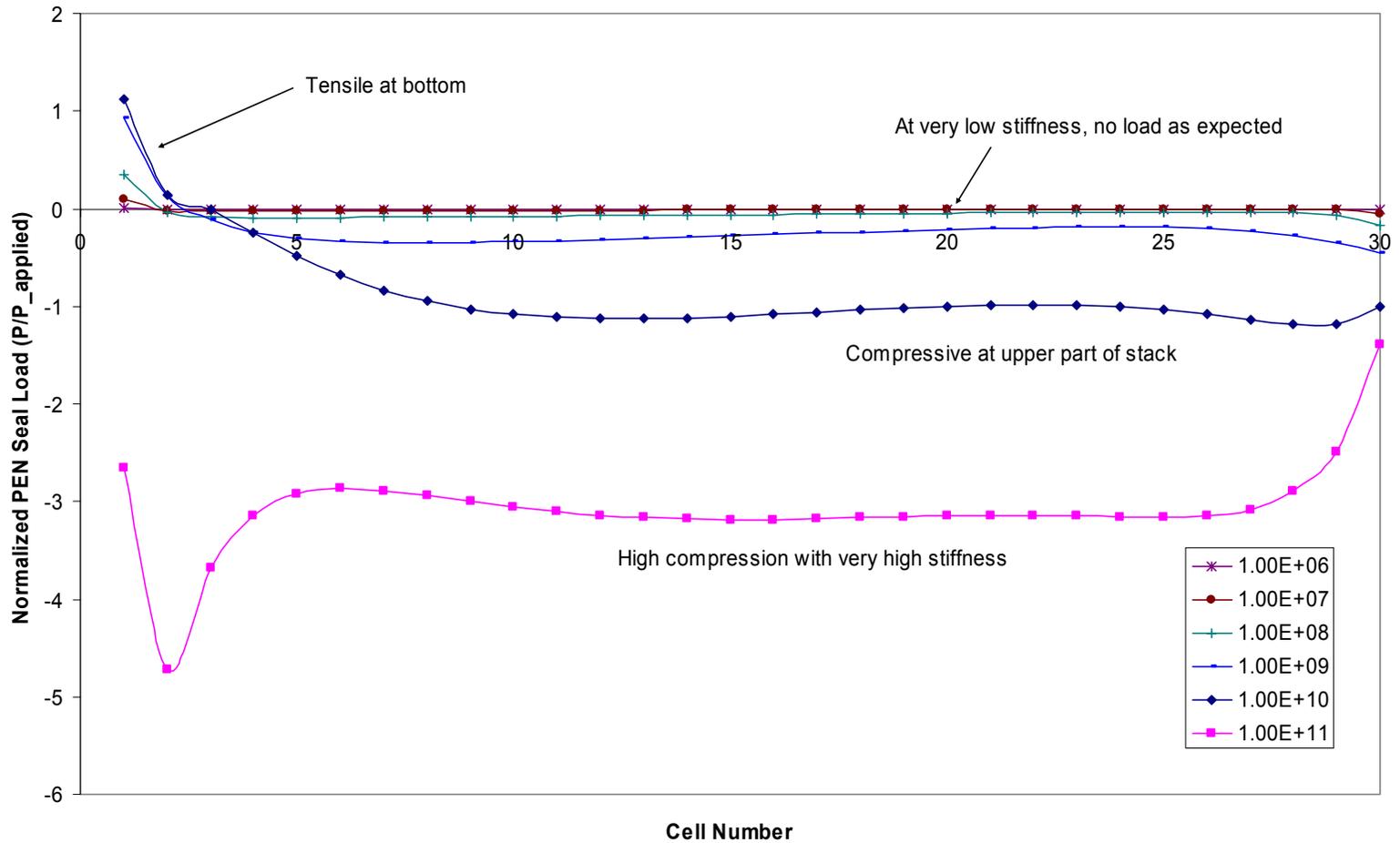


Manifold



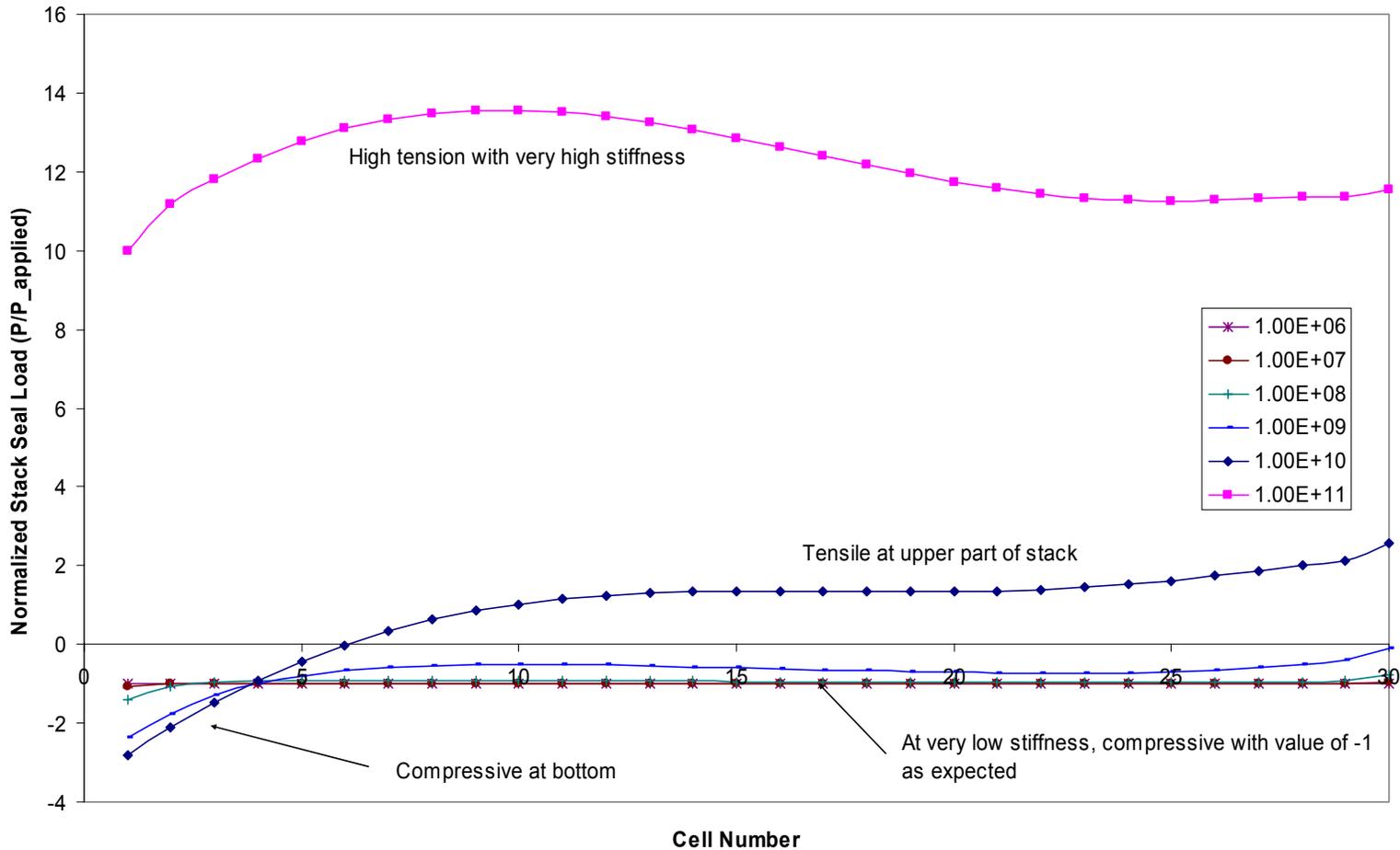
# Load Paths for Multiple Planar Cell Stack

Average Load for PEN Seals as a Function of Interconnect Stiffness

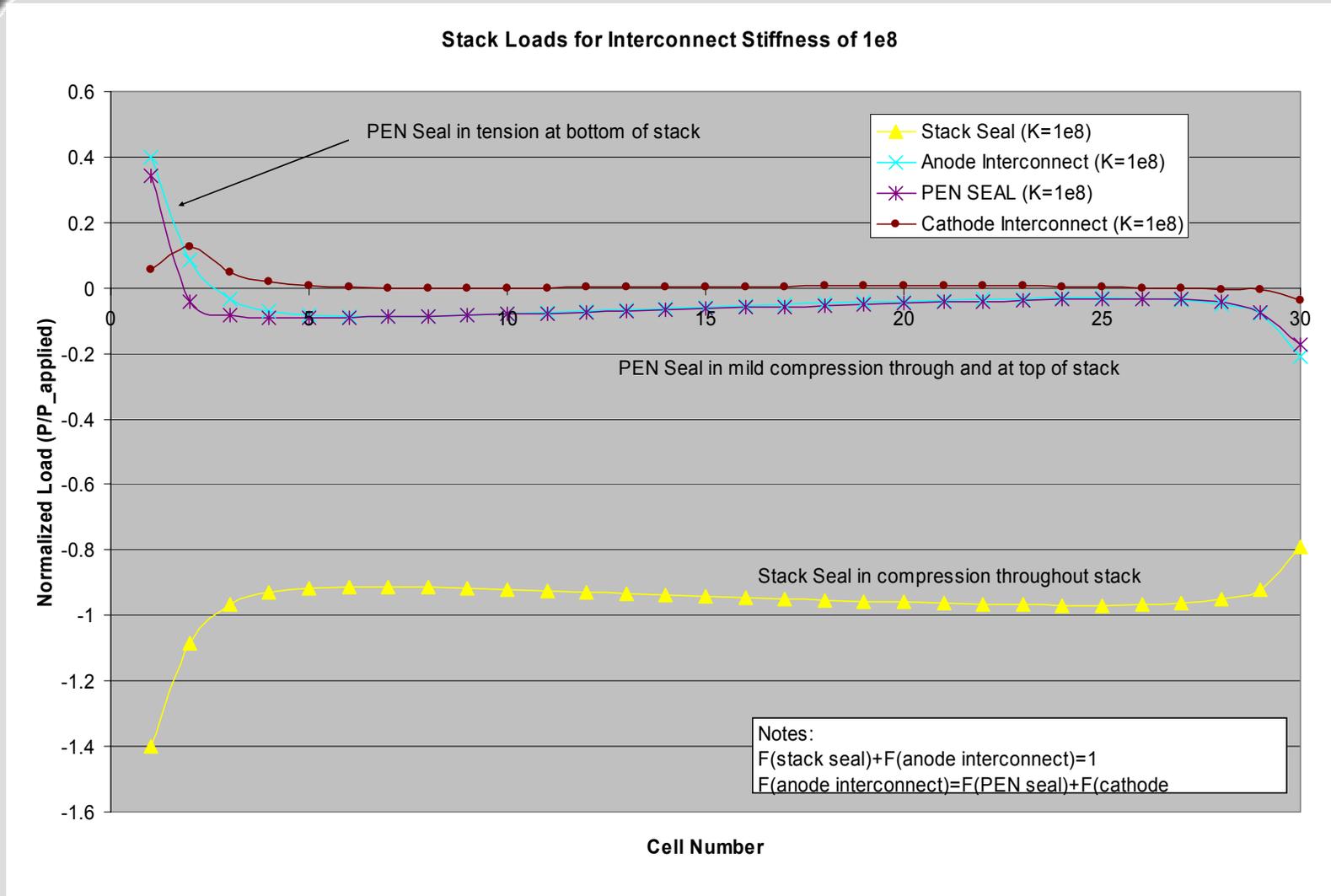


# Load Paths for Multiple Planar Cell Stack

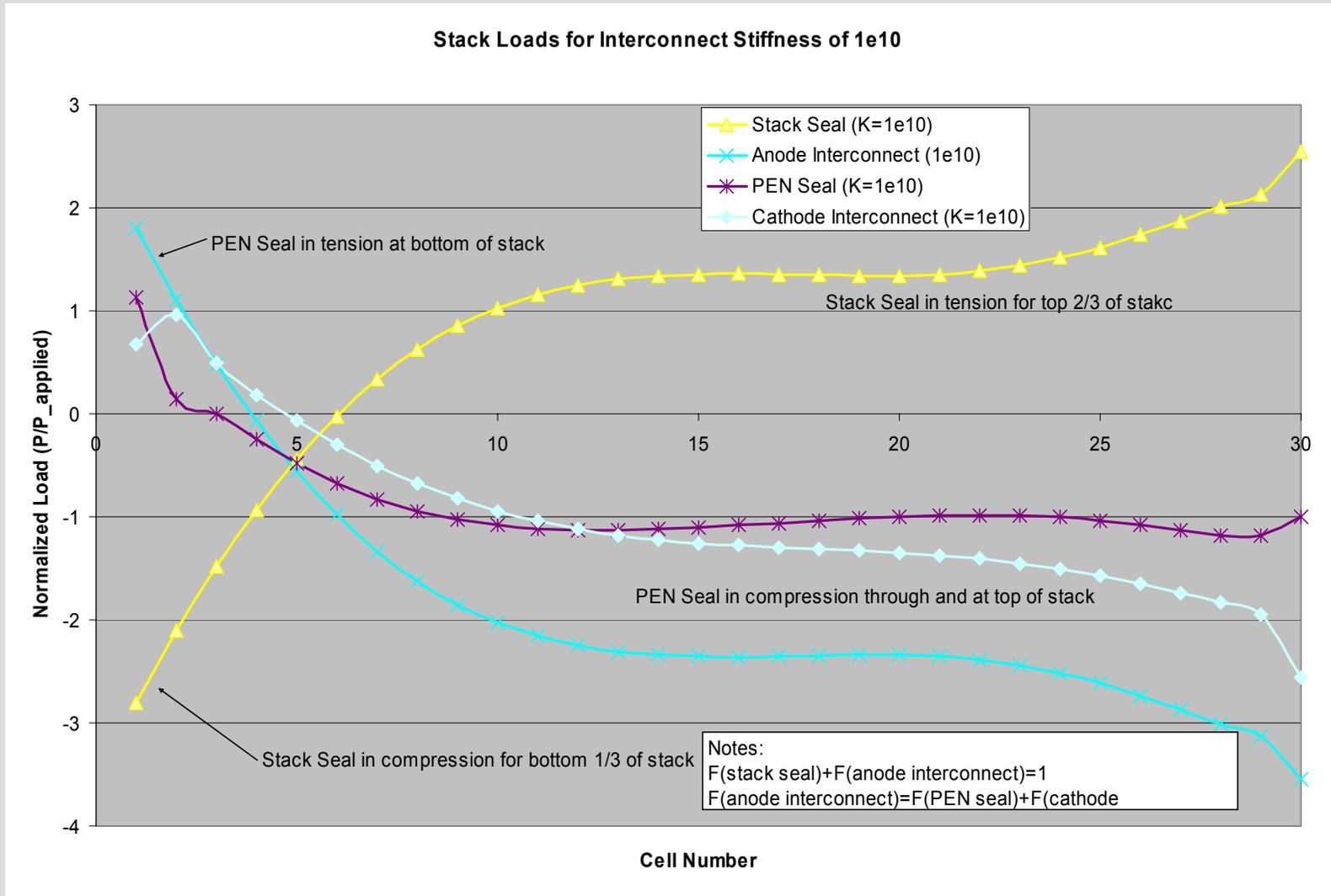
Average Load for Stack Seals as a Function of Interconnect Stiffness



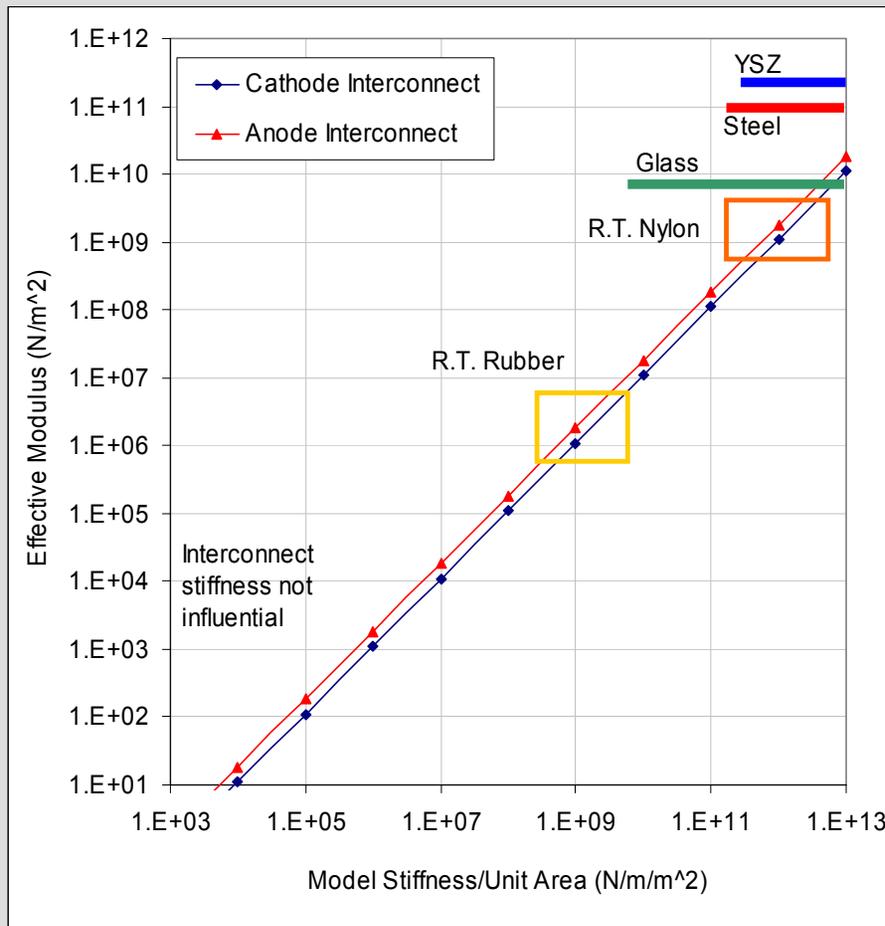
# Load Paths for Multiple Planar Cell Stack



# Load Paths for Multiple Planar Cell Stack



# Load Paths for Multiple Planar Cell Stack



This chart tries to relate the "stiffness" used in the model for the cathode and anode mesh to a modulus. This will help give a feel for what these stiffnesses actually mean.

The stiffness  $K$  is actually stiffness per unit area, so  $K \cdot t$  where  $t$  is the spring length (thickness) would give the effective modulus for the interconnect material if it was a solid layer.