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*Very High Temperature Heat Exchange
Performance When Firing Low-Grade Fuels*

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Technology to Support National Energy Needs, Orlando, FL

January 14–16, 2002

Goal

Development of a radiant air heat that can provide very high temperature at ($\sim 2000^{\circ}\text{F}$) using a range of low grade fuels including coal and biomass.

Performance and Economics of HiPPS with Bare Tube HITAF



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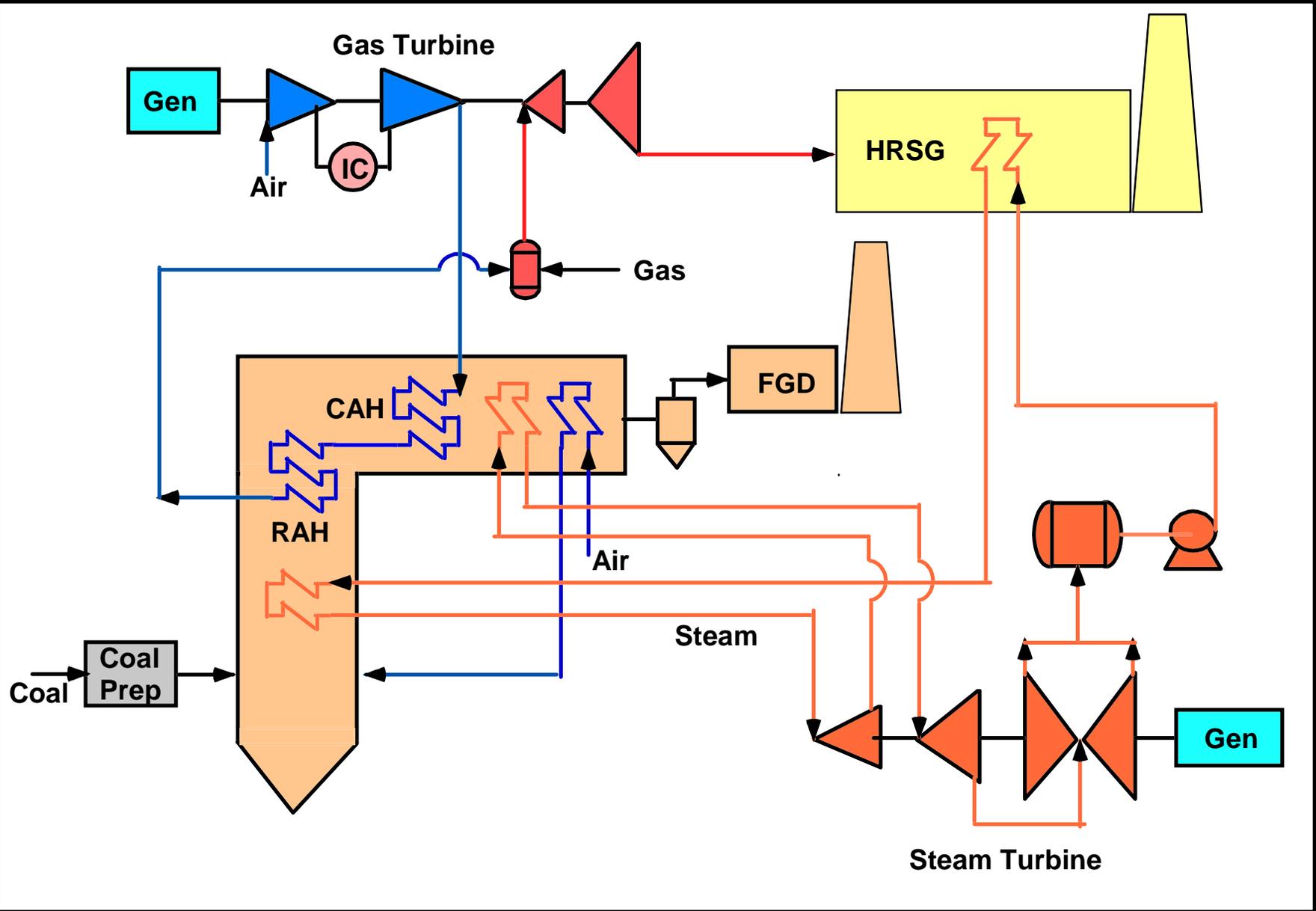
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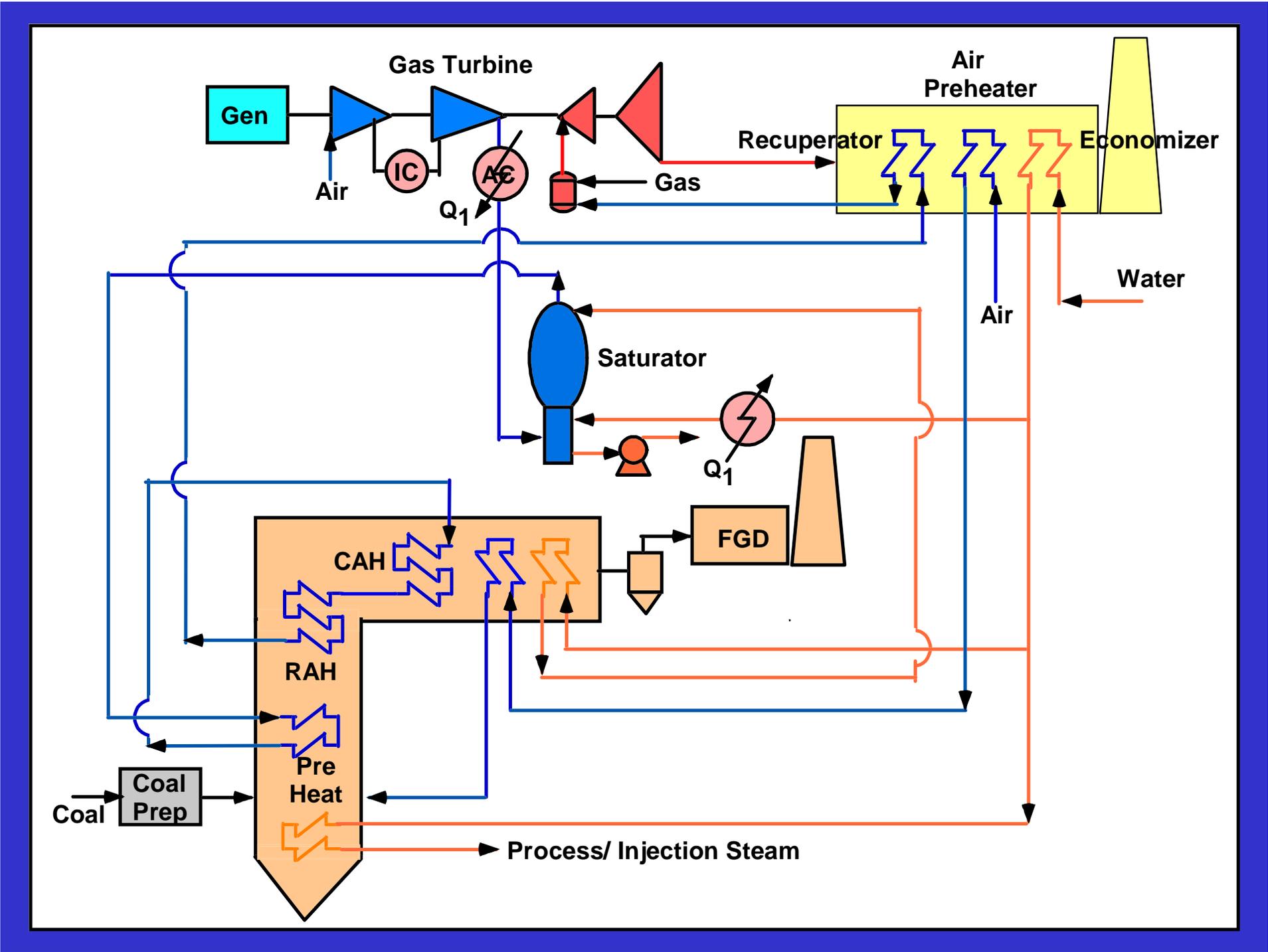
Background

- UTRC HiPPS had refractory protection in RAH
- RAH required approximately 20,000 ft² for 300 MW
- Bare tube has five times heat transfer
- Assume 4,000 ft² RAH for 300 MW
- HITAF now more closely resembles conventional steam generator

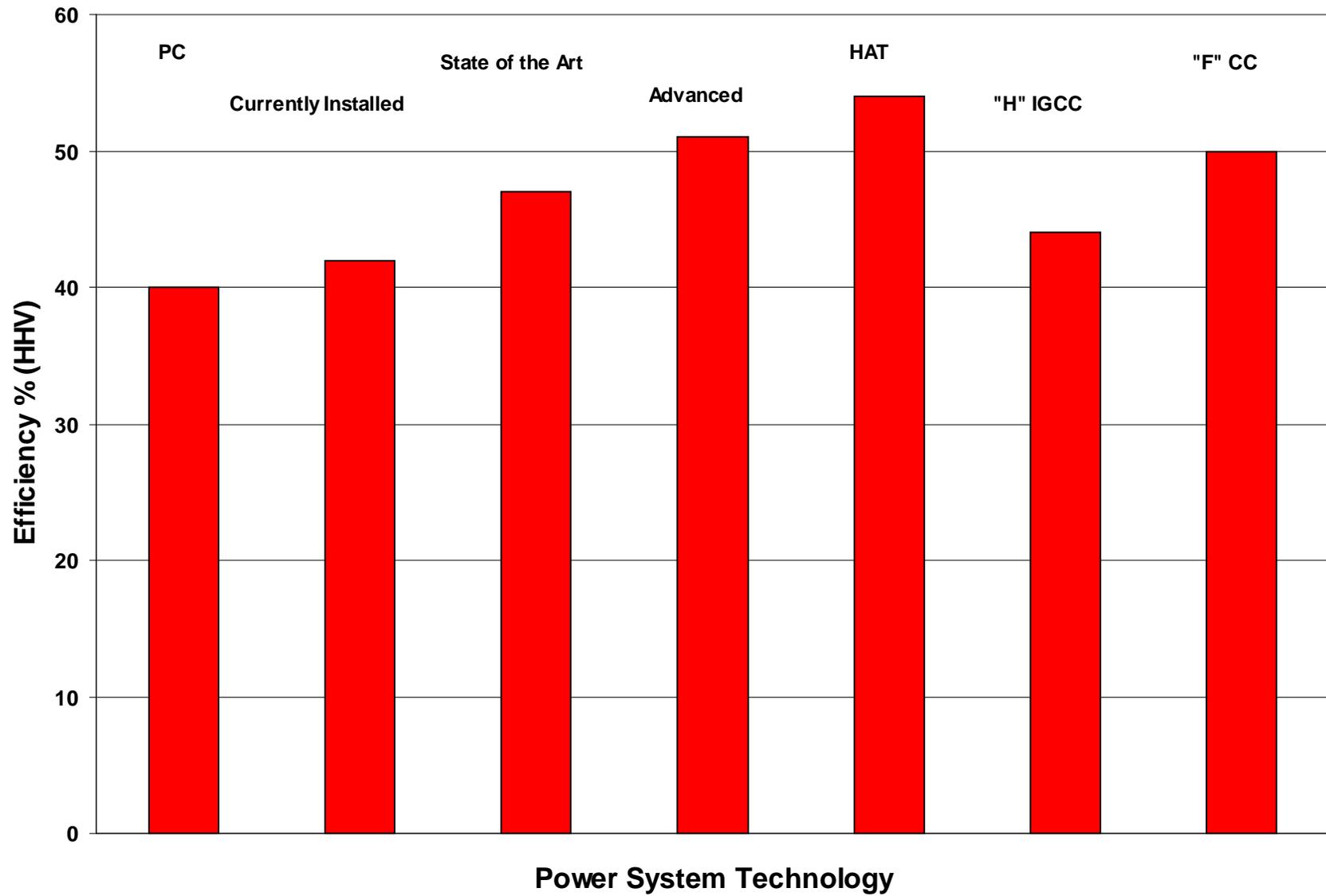
Method of Analysis

- Performance estimates for 4 HiPPS configurations
- Performance estimates for PC plant, IGCC, and NGCC
- Cost for HiPPS with bare tubes
 - Based on Bechtel/Nexant estimates
- Costs for other systems from literature adjusted to Bechtel/Nexant assumptions

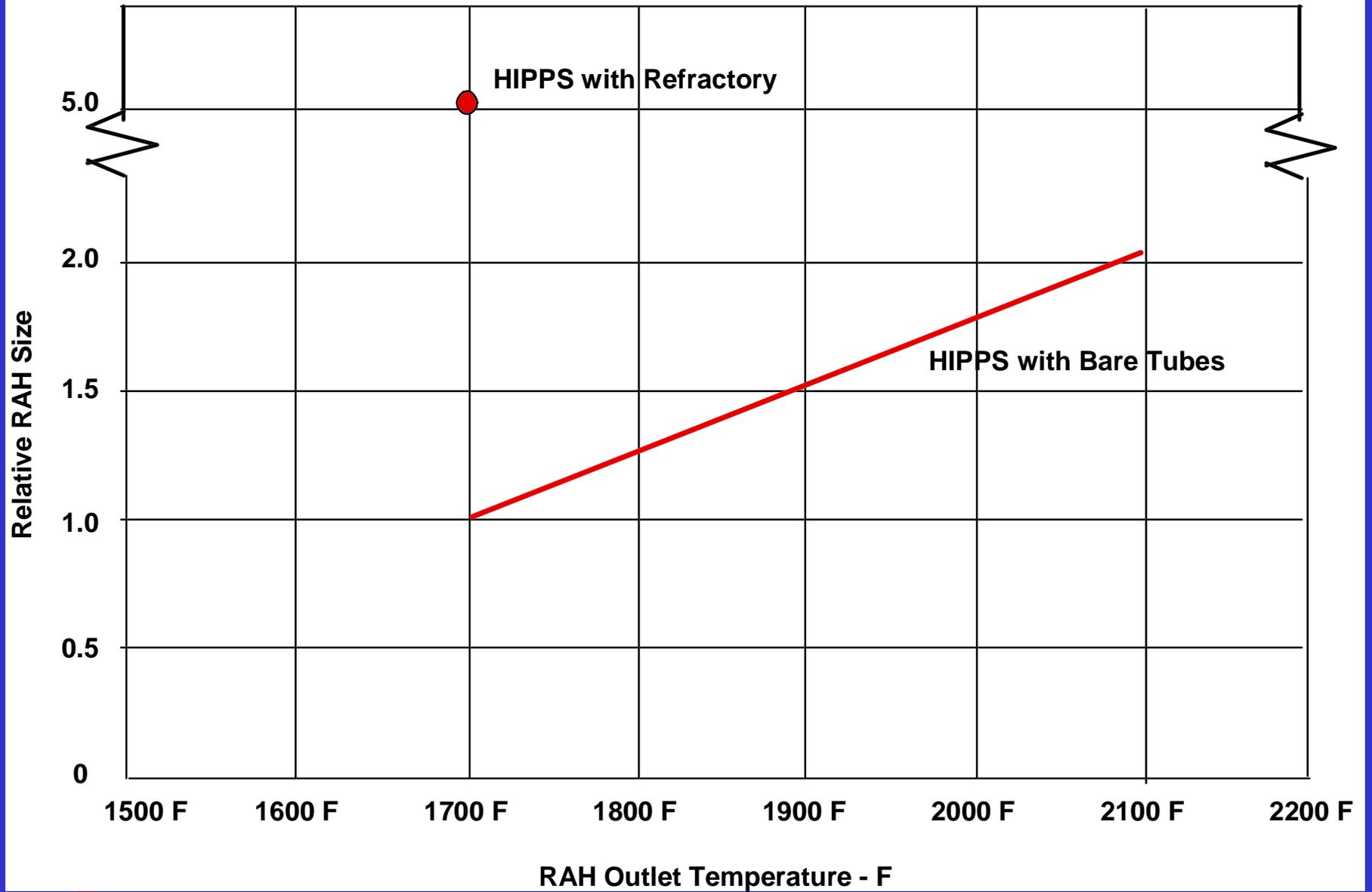




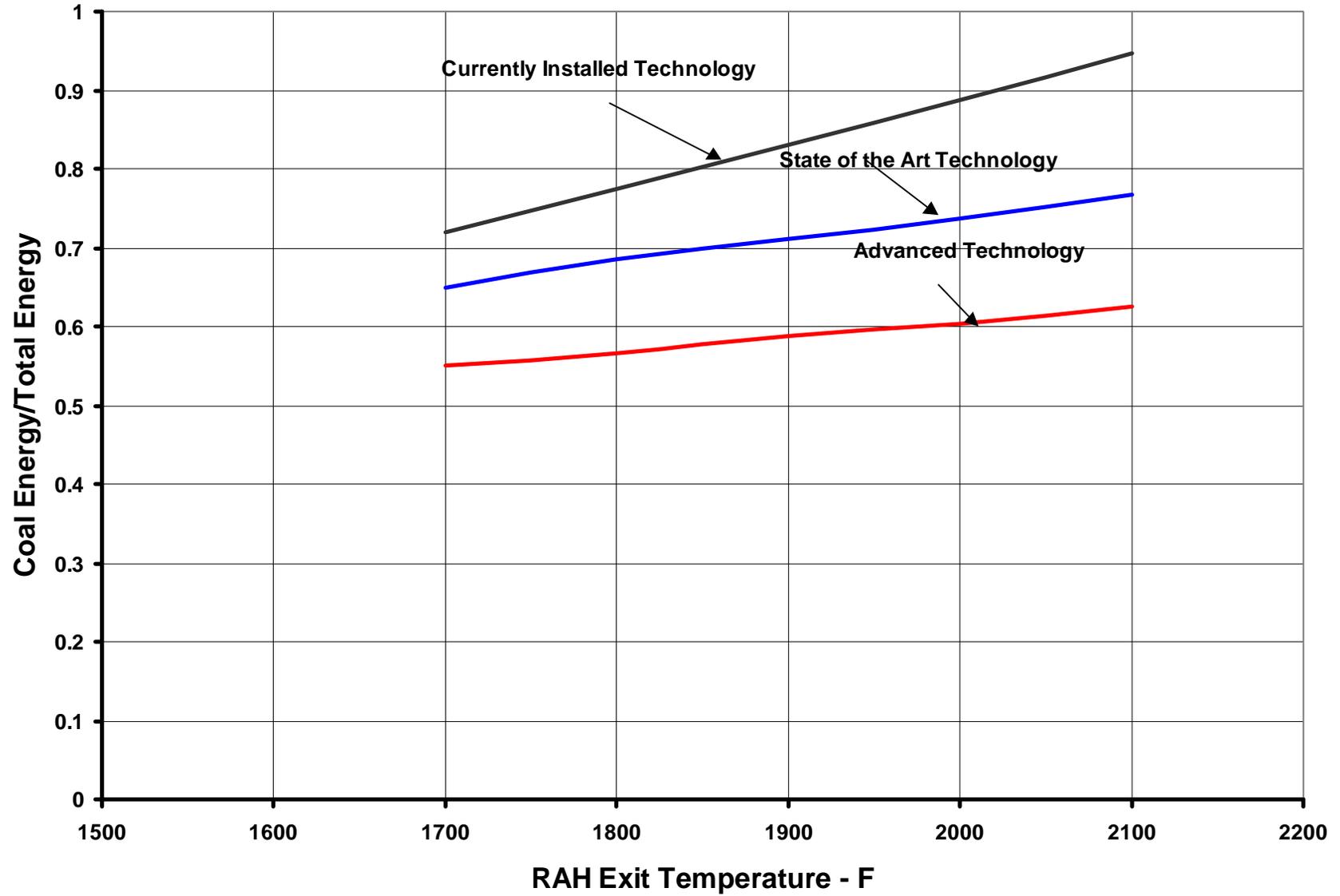
Power System Efficiency



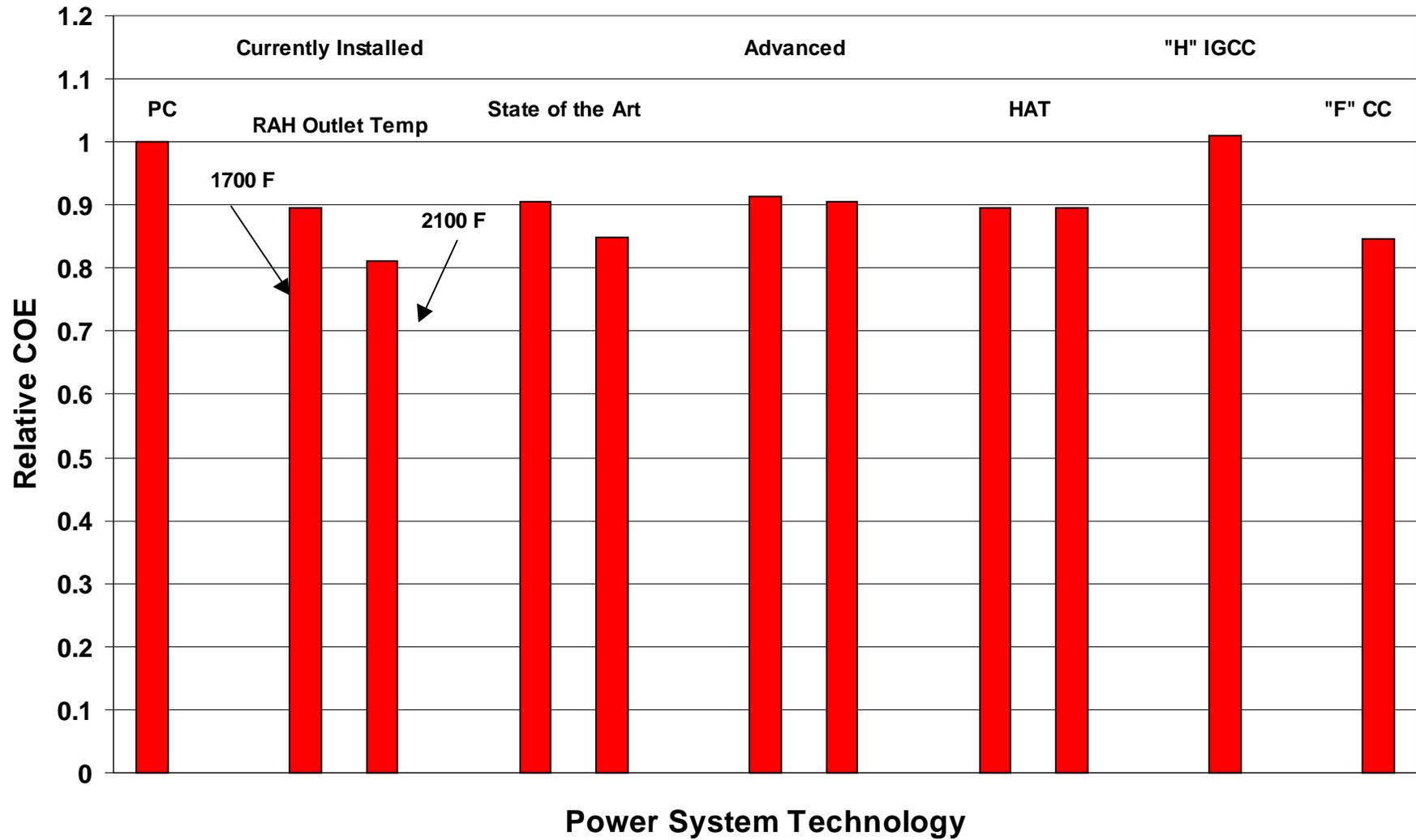
Relative RAH Size



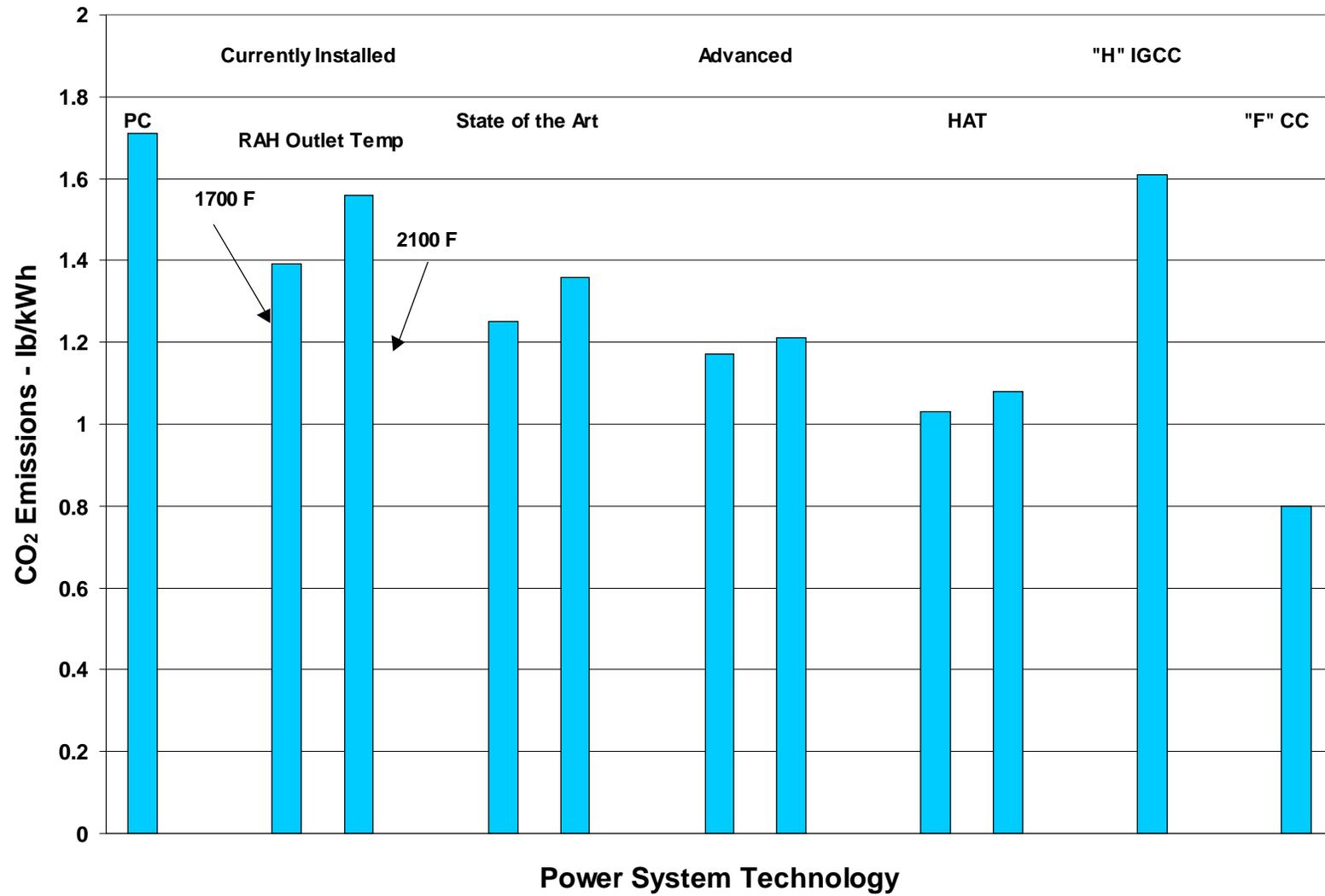
Coal Fraction



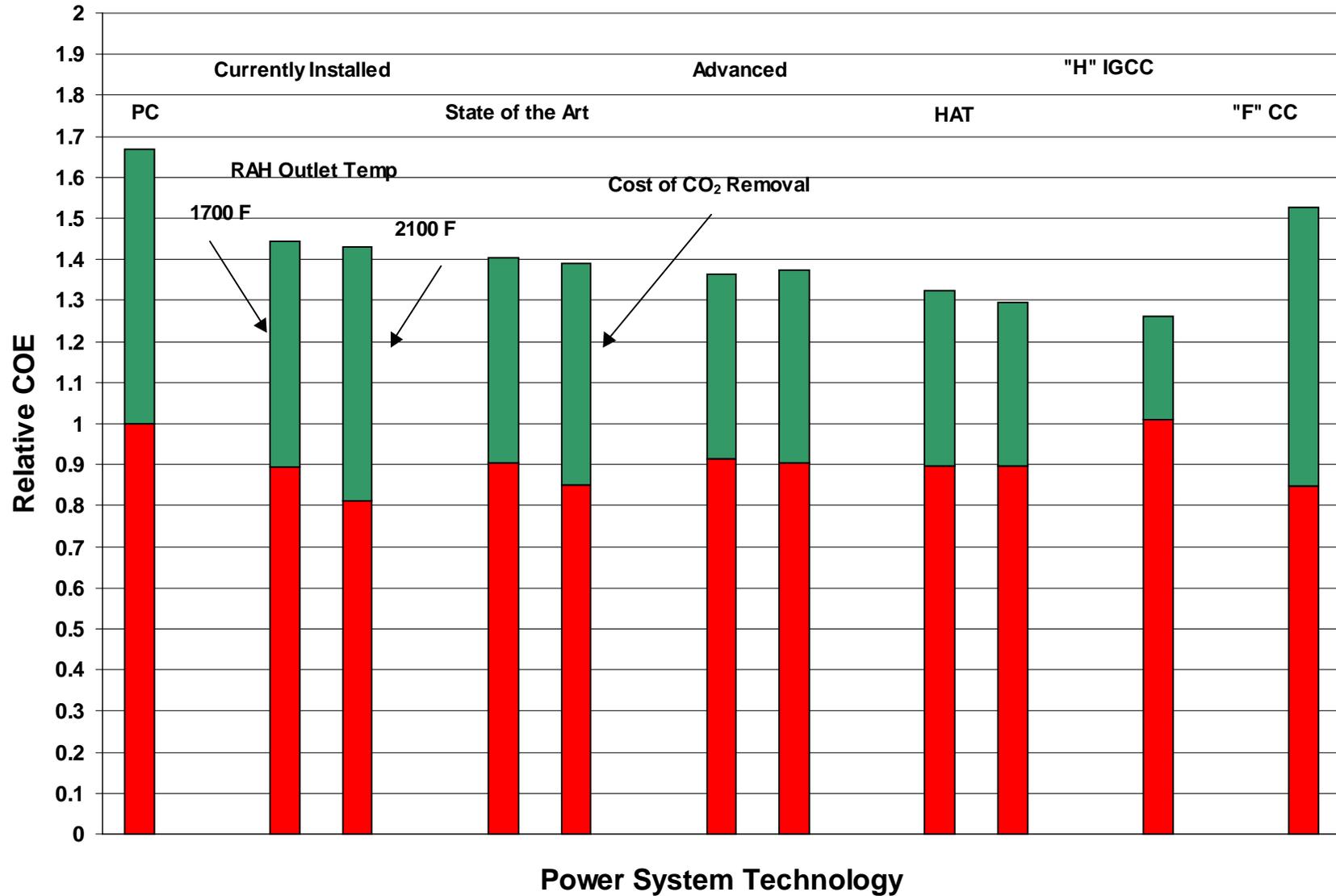
Relative Cost of Electricity



CO₂ Emissions



Relative Cost of Electricity with CO₂ Capture



Summary

- Bare tube HiPPS has advantage over other HiPPS and conventional coal-based systems.
- Nearer term systems are very attractive and potentially could meet market demand for efficient, low cost coal-fired plants in Third World countries

Preliminary Conclusions

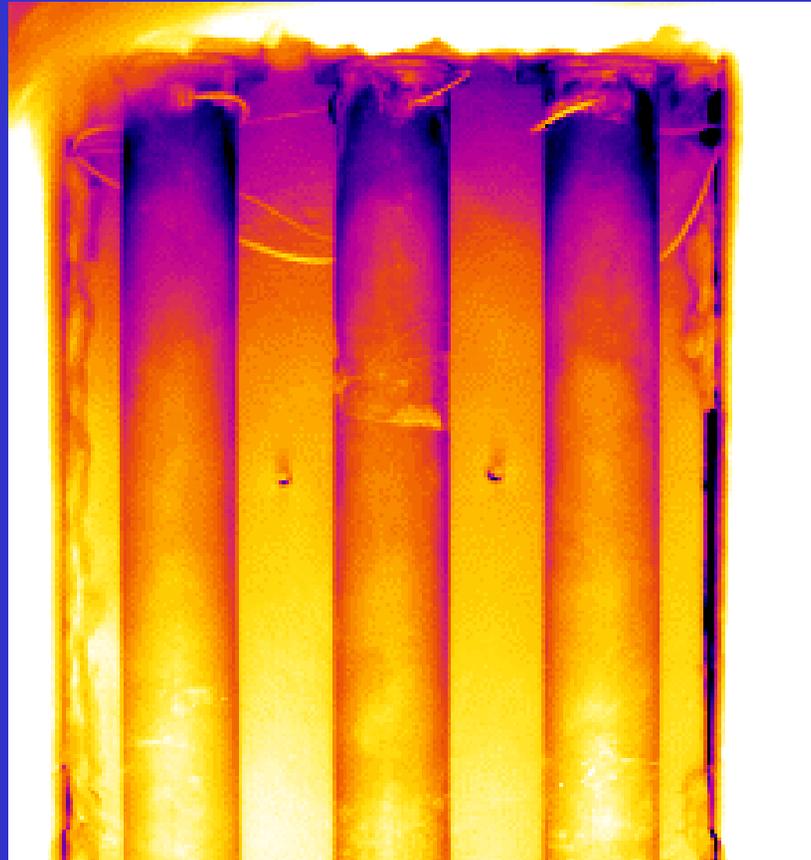
- Heat removal rates are increased by a factor of 4 to 6 by removing the ceramic panels.
- This change will lower the cost of the heat exchanger by a factor of 10 over the UTRC design.
- Initial ash deposit is thin and sintered which protects the tube from rapid corrosion with a minimum of insulation.
- A flowing slag layer is created within a few millimeters of the surface, minimizing insulating value and becoming self-cleaning.
- Most likely industries interested in first trying the technology are fossil-energy intensive industries, not the power sector.

Future Work

- With much lower levels of funding, pilot testing will not be possible.
- Corrosion testing of alloys with different flowing slags and temperatures will continue.
- Laboratory tests of joining MA 956 alloy.
- Construction of six foot tall, three tube heat exchanger using MA 956 alloy.

Infrared Image of RAH Tubes Before Coal-Fire – August 2001

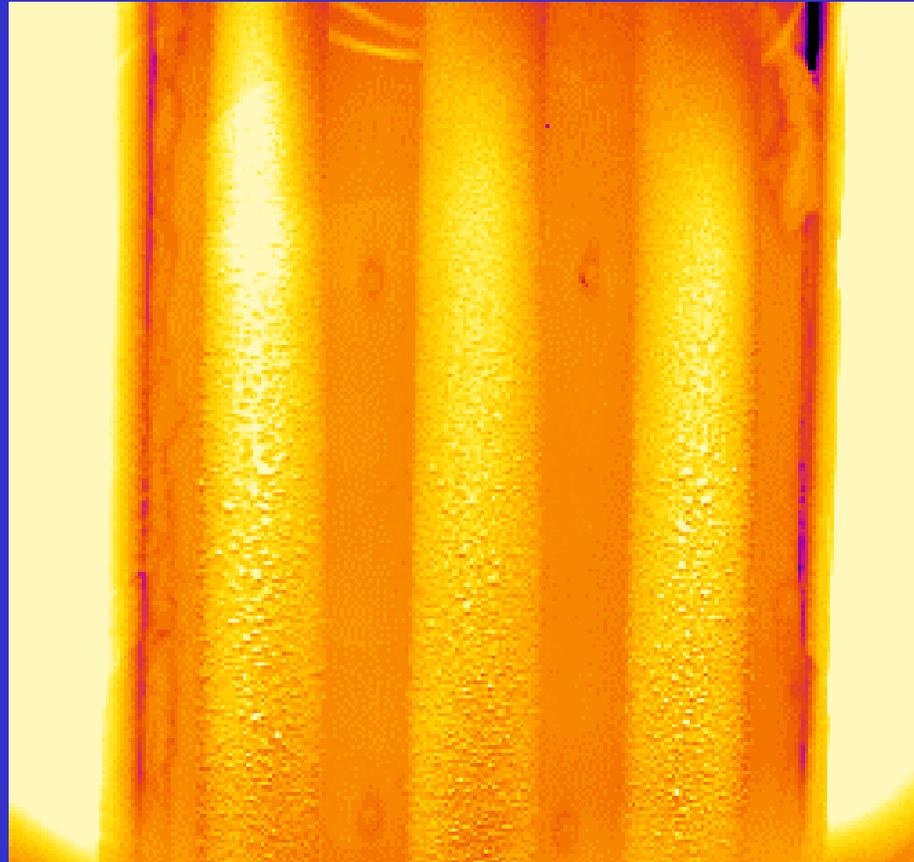
Upper Portion



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Infrared Image of RAH Tubes After 24 hr on Coal-Fire – August 2001



RAH Exchanger Tubes

Before August 2001 Test



After August 2001 Test



RAH Exchanger Tubes After August 2001 Test

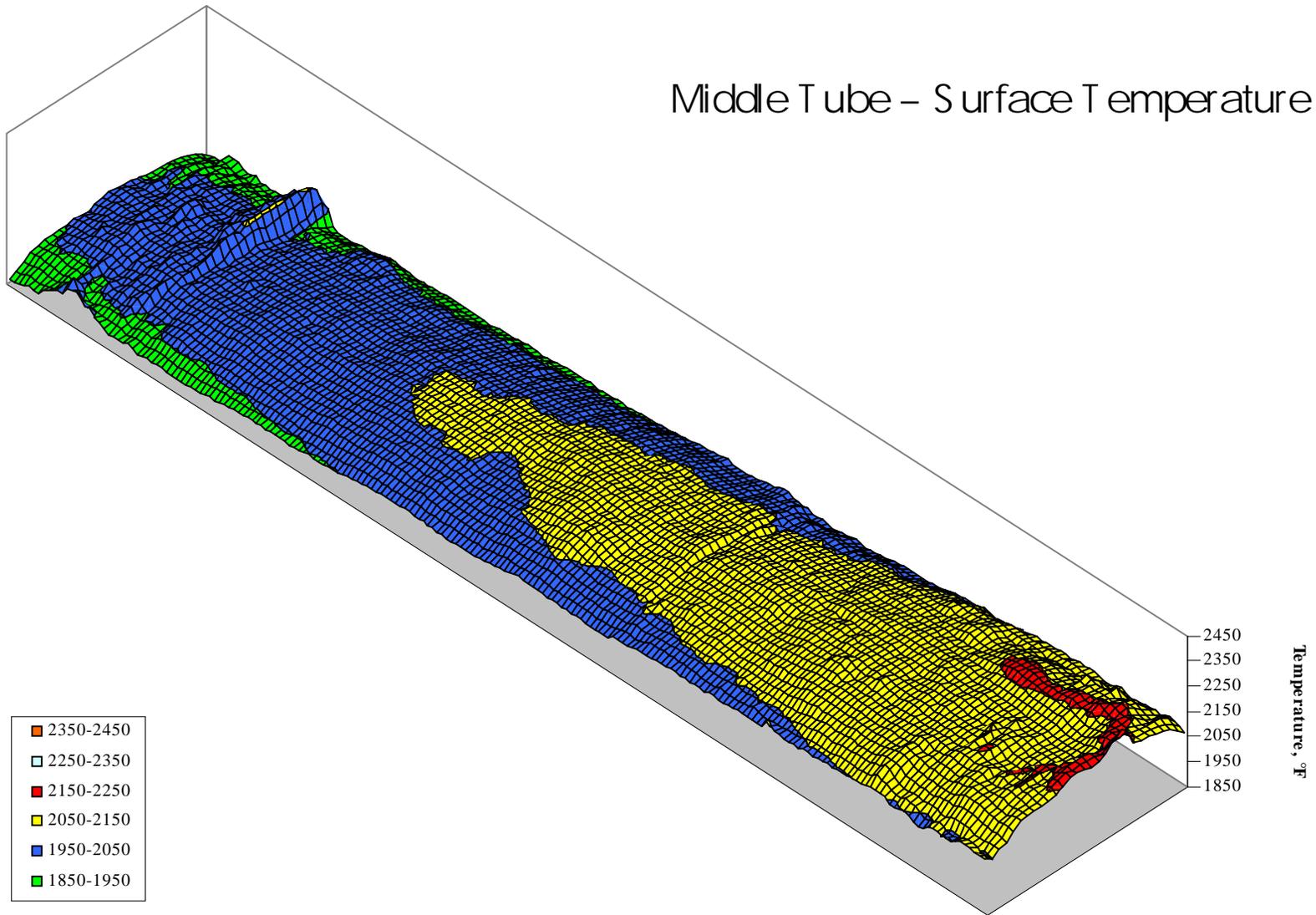


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AM Images 02-04 Test 6 Before Coal-Fire – August 29, 2001

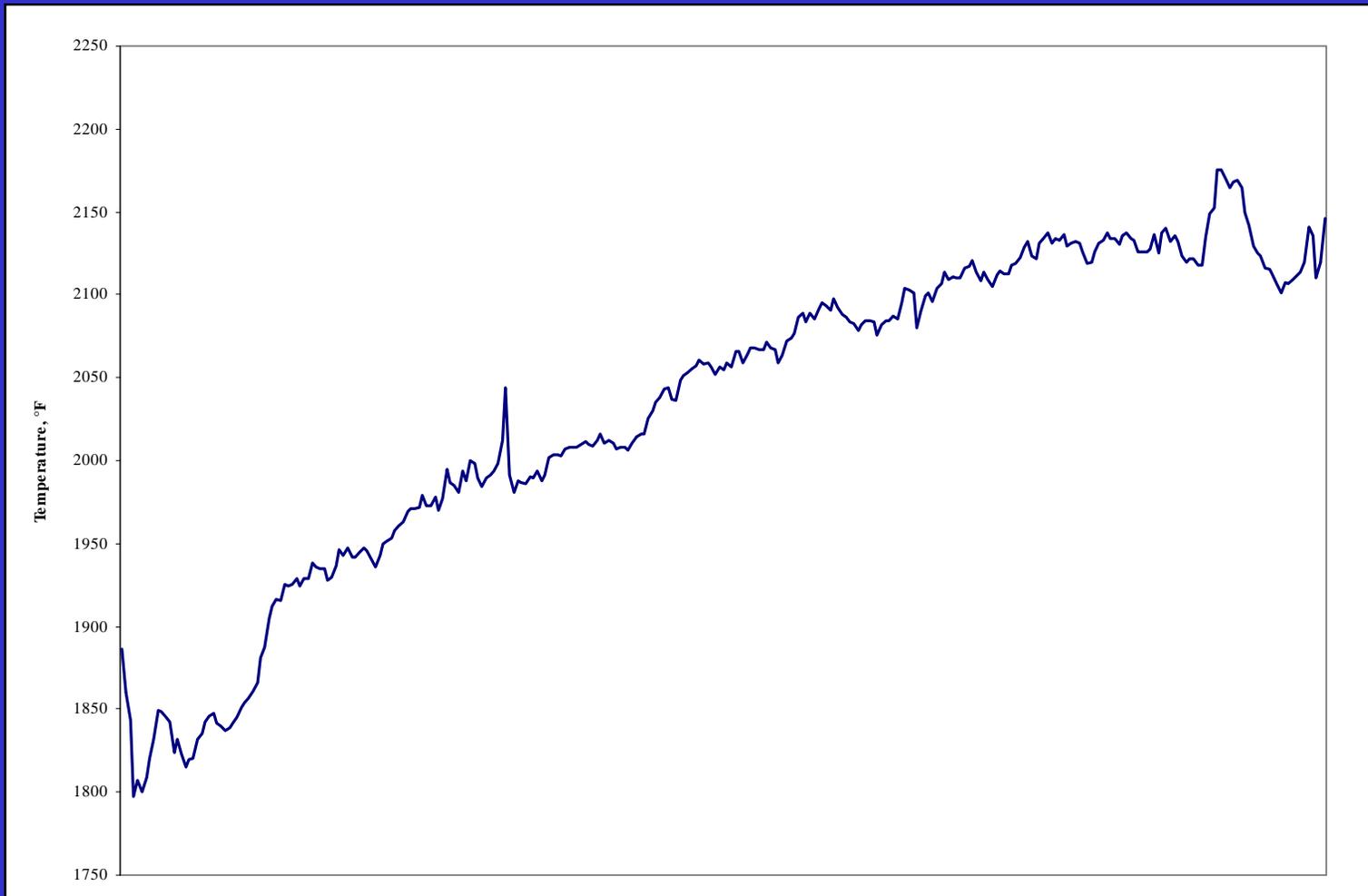
Middle Tube – Surface Temperature



AM Images 02-04 Test 6

Before Coal-Fire – August 29, 2001

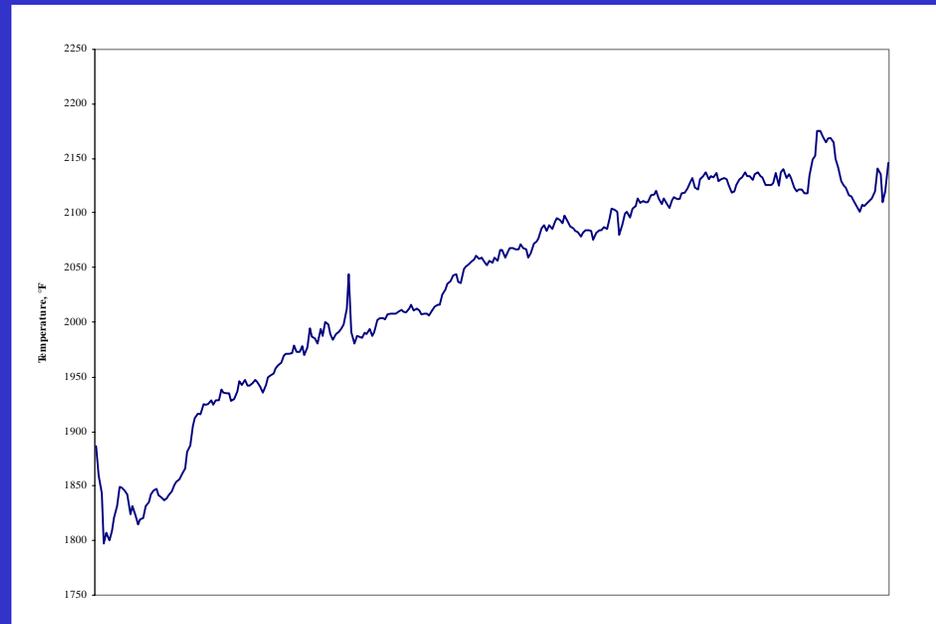
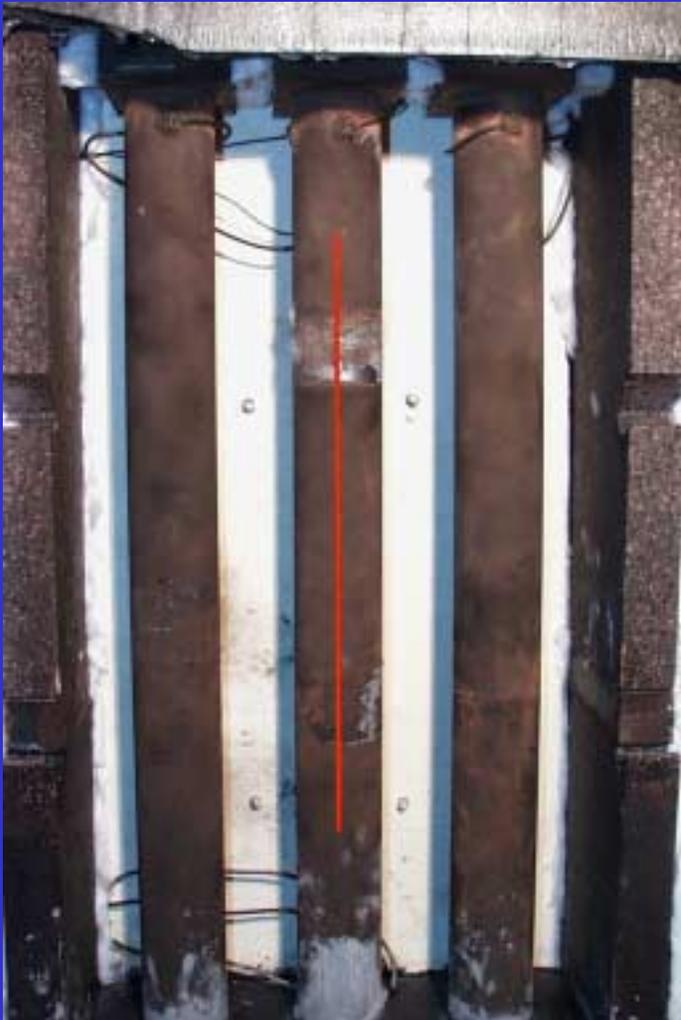
Middle Tube – Centerline Temperature



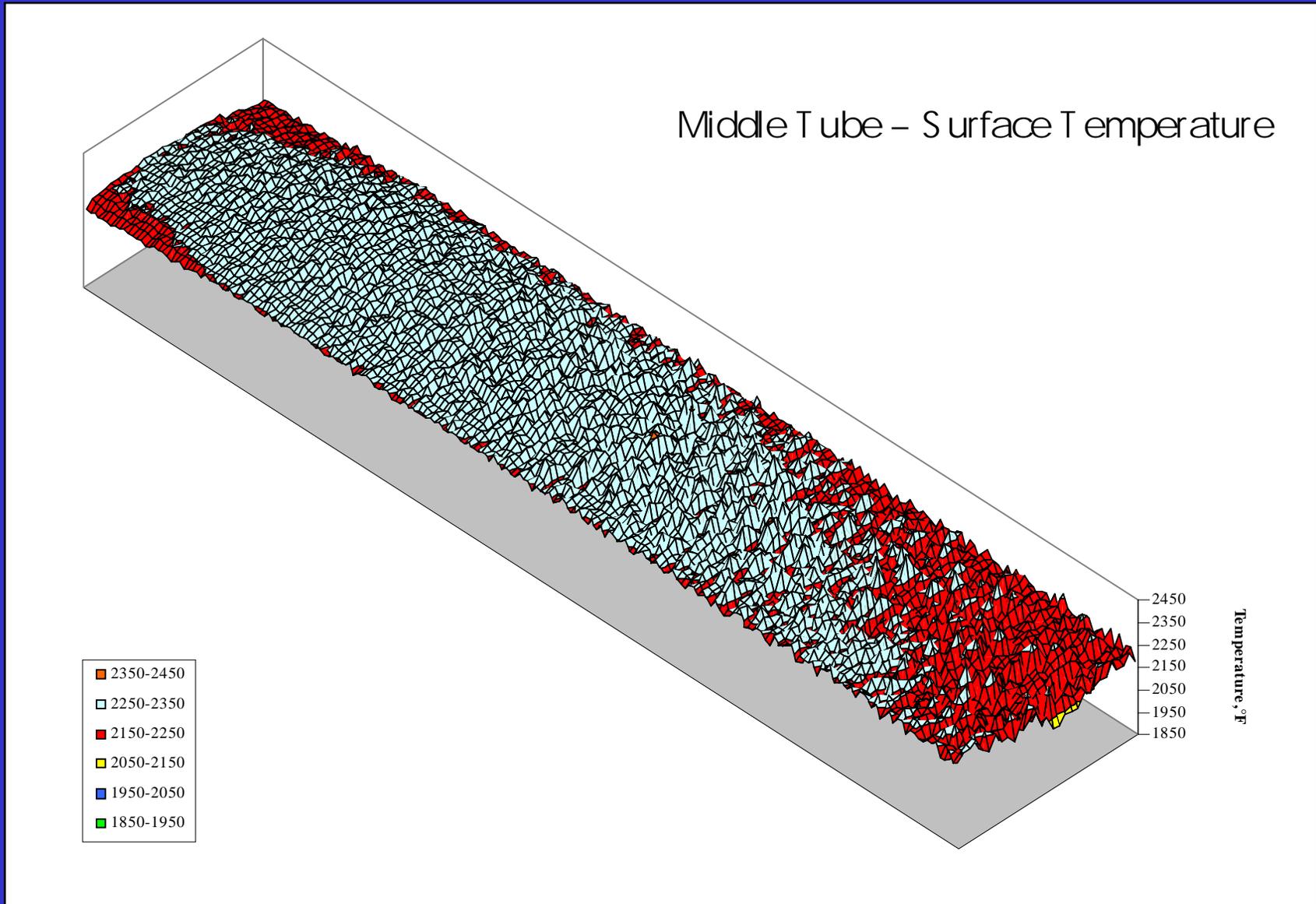
AM Images 02-04 Test 6

Before Coal-Fire – August 29, 2001

Middle Tube – Centerline Temperature

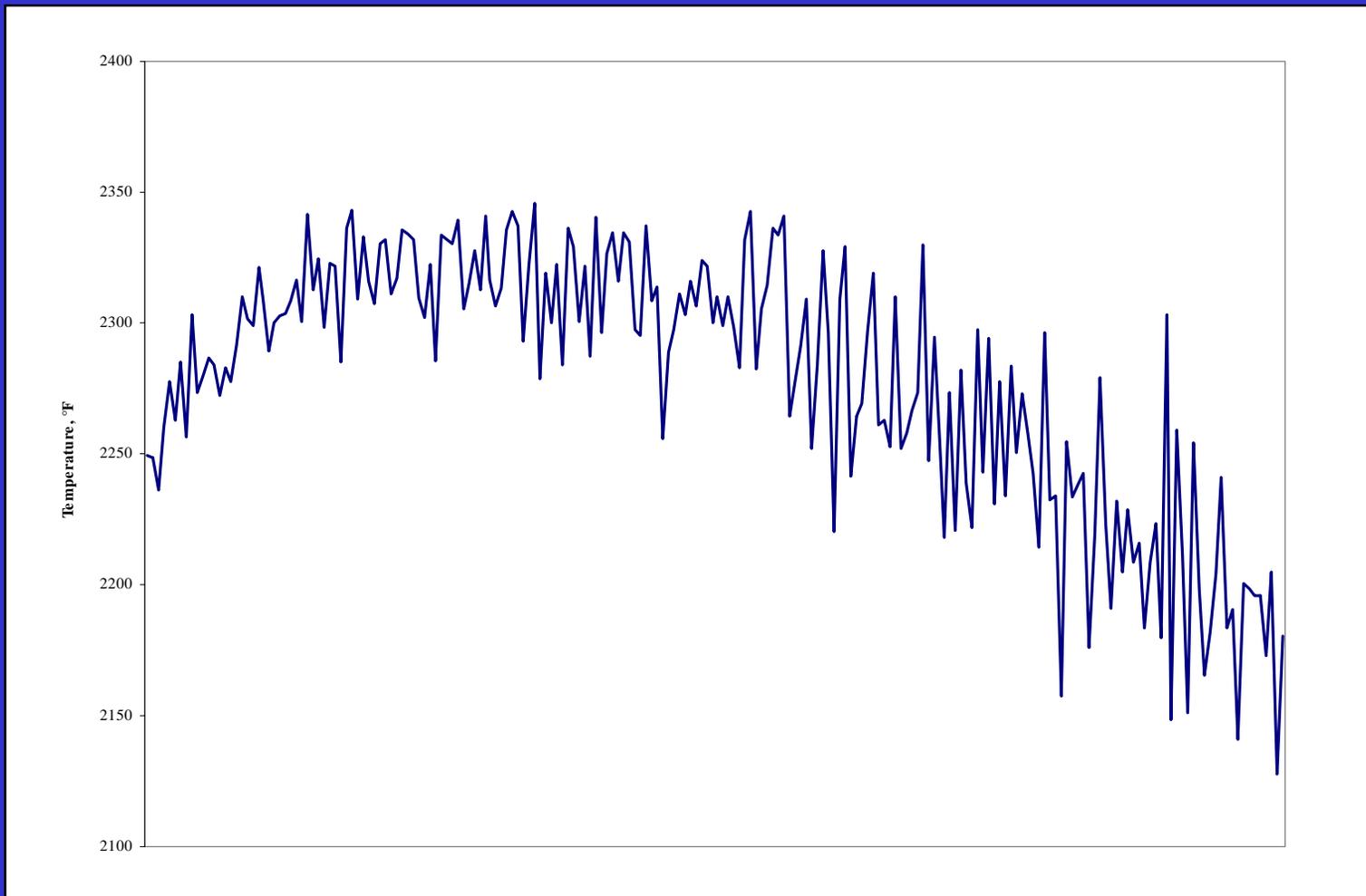


4PM Image 03 Test 7 After Coal-Fire – August 30, 2001



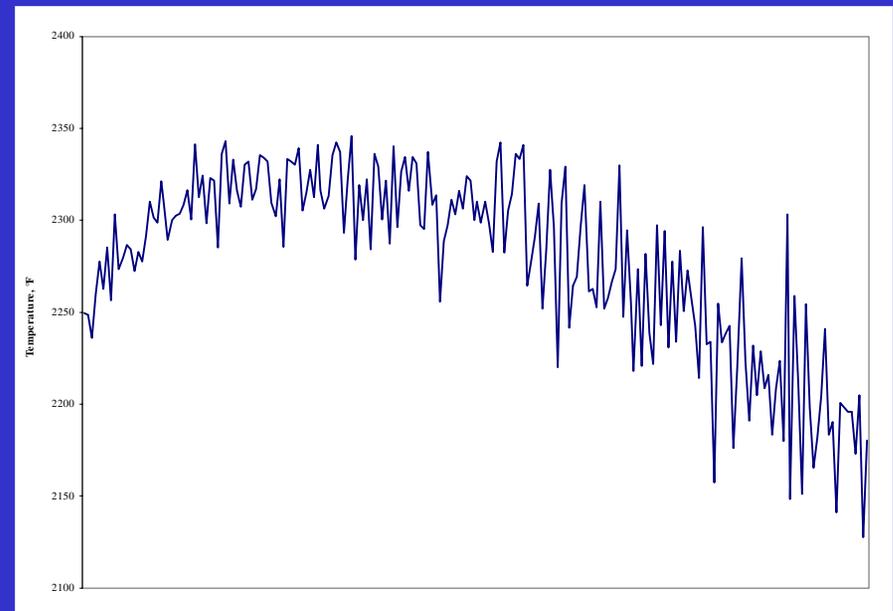
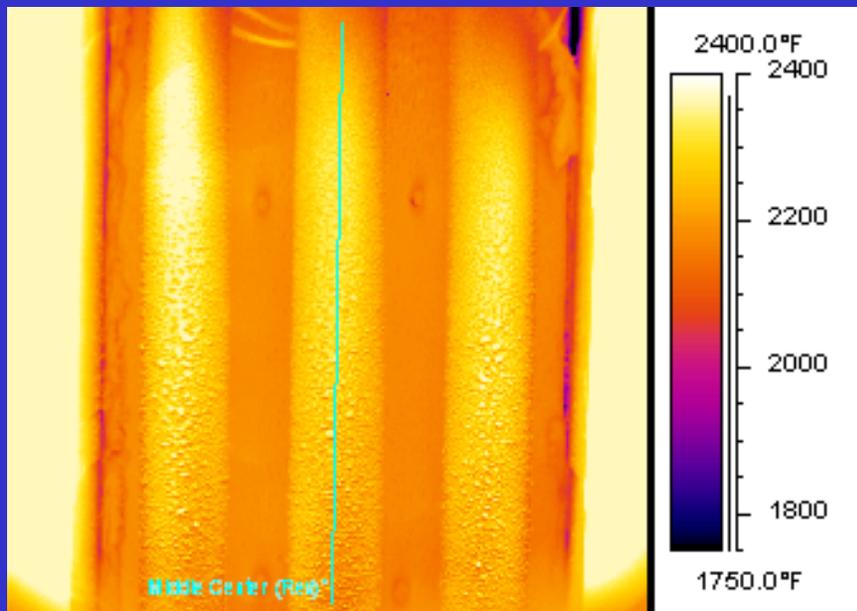
4PM Image 03 Test 7 After Coal-Fire – August 30, 2001

Middle Tube – Centerline Temperature

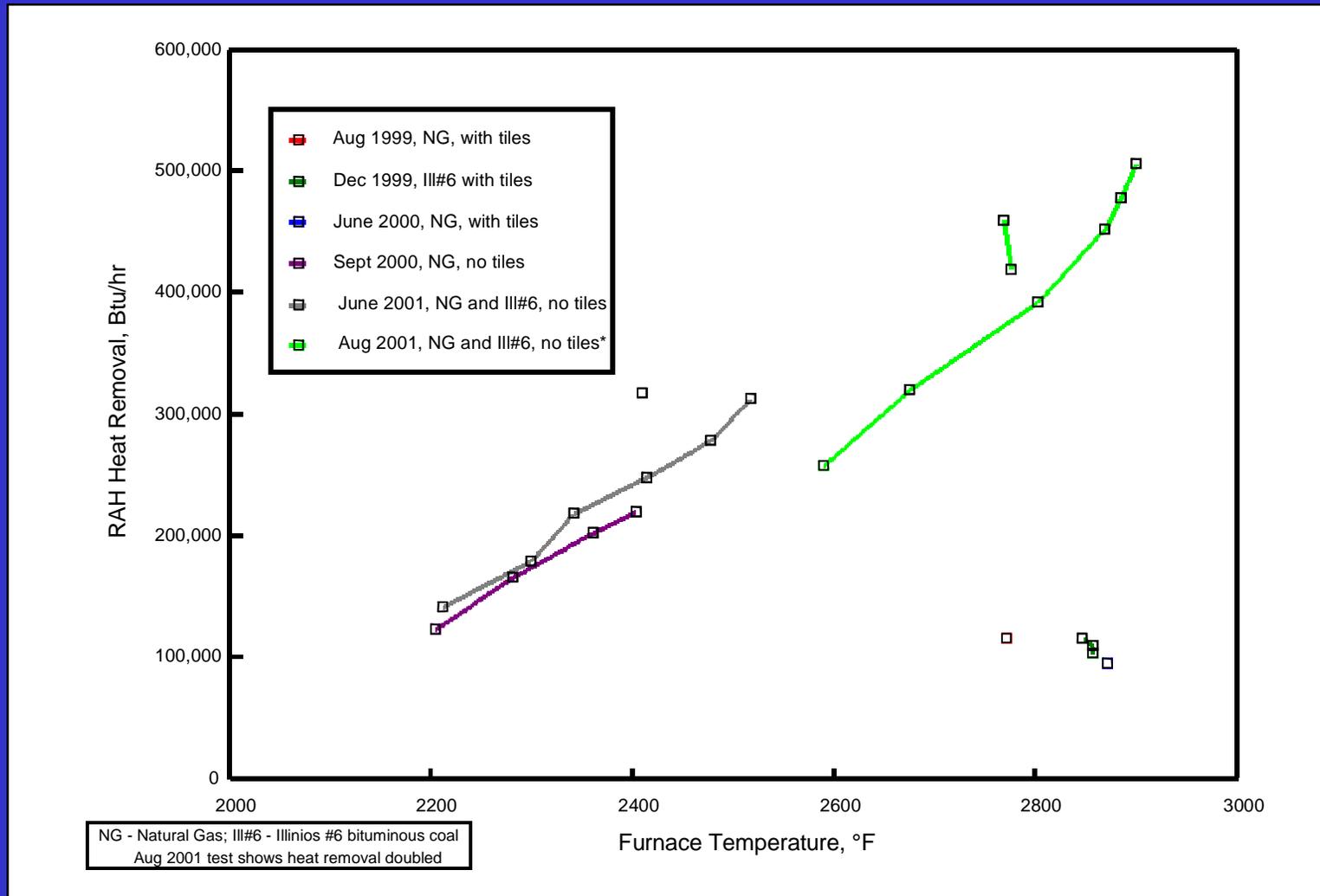


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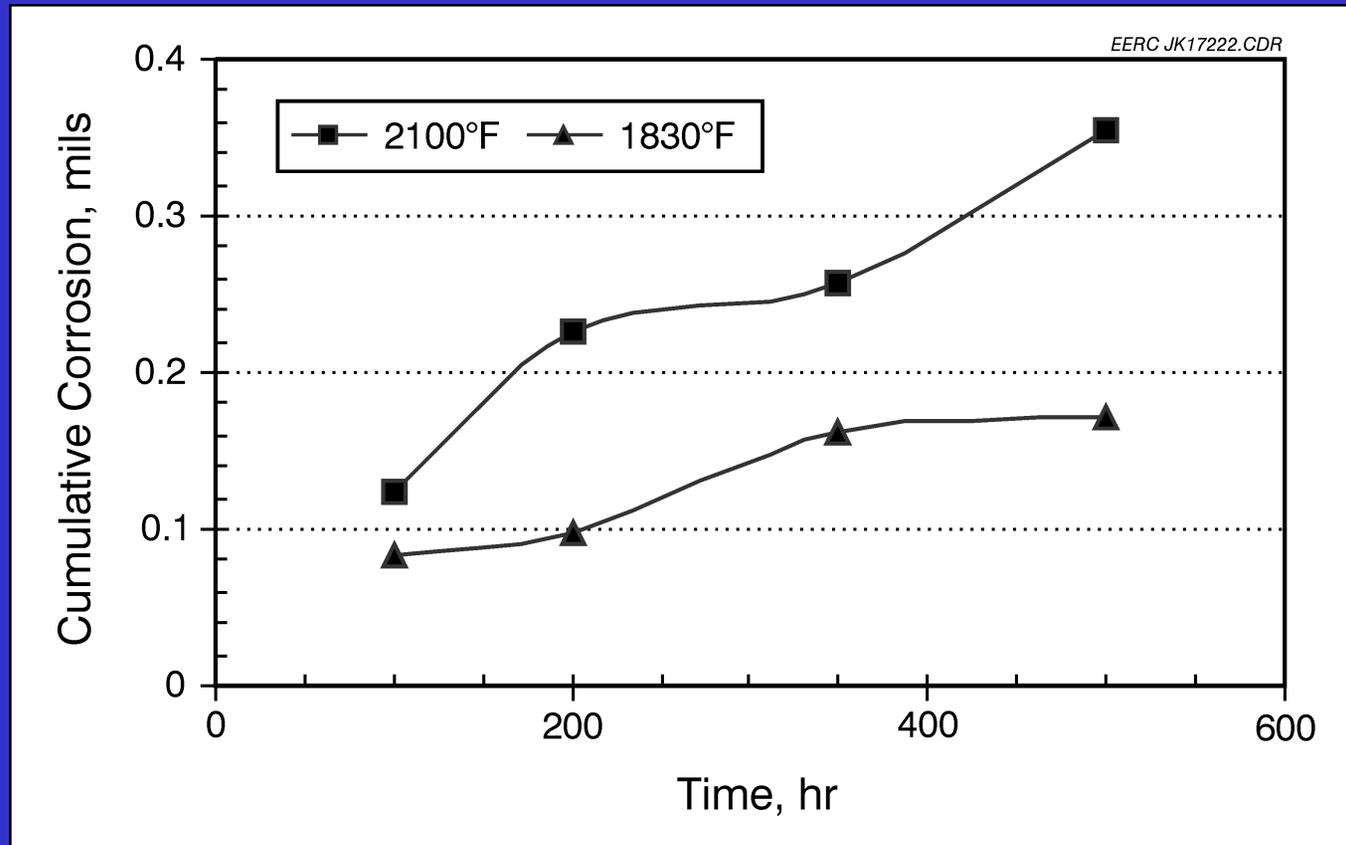
Middle Tube – Centerline Temperature



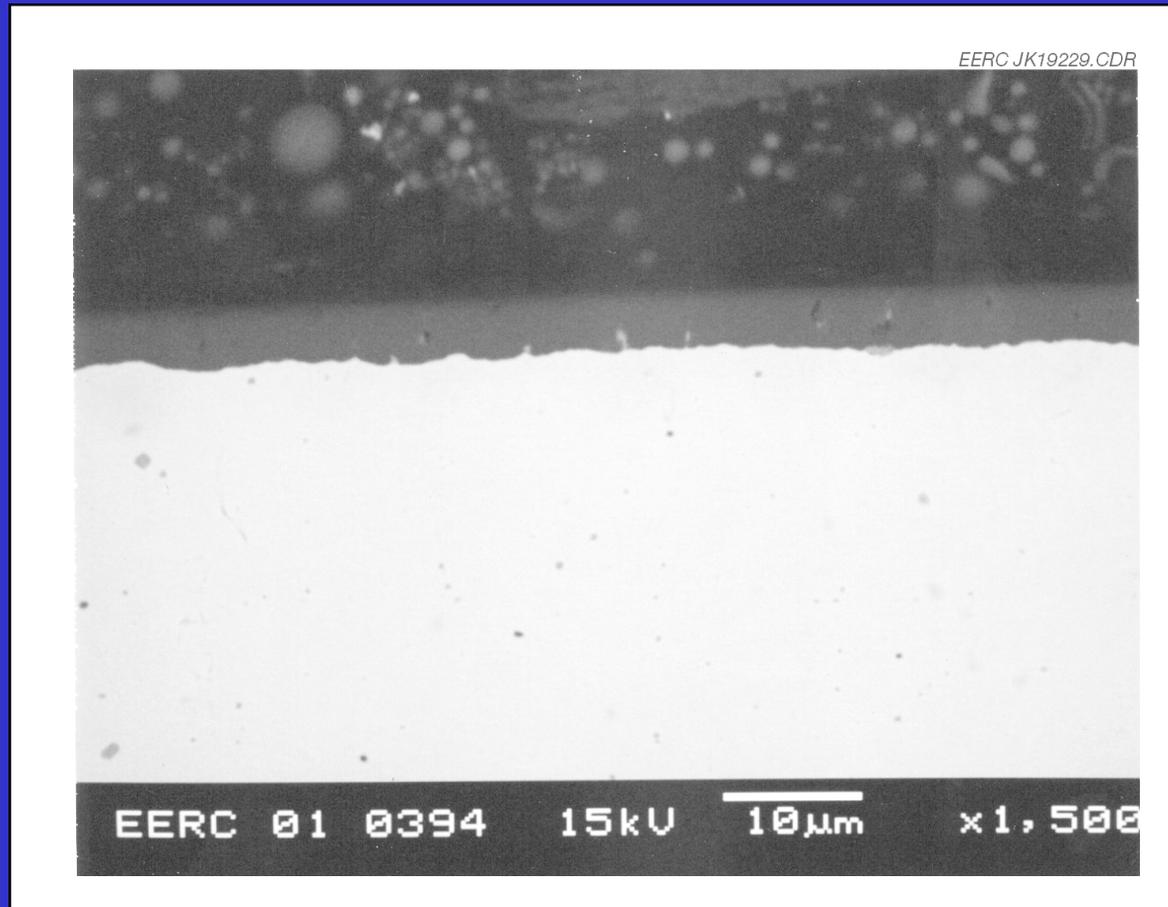
Heat Removal and Air Flow Rates September 2000 and June 2001 SFS Tests



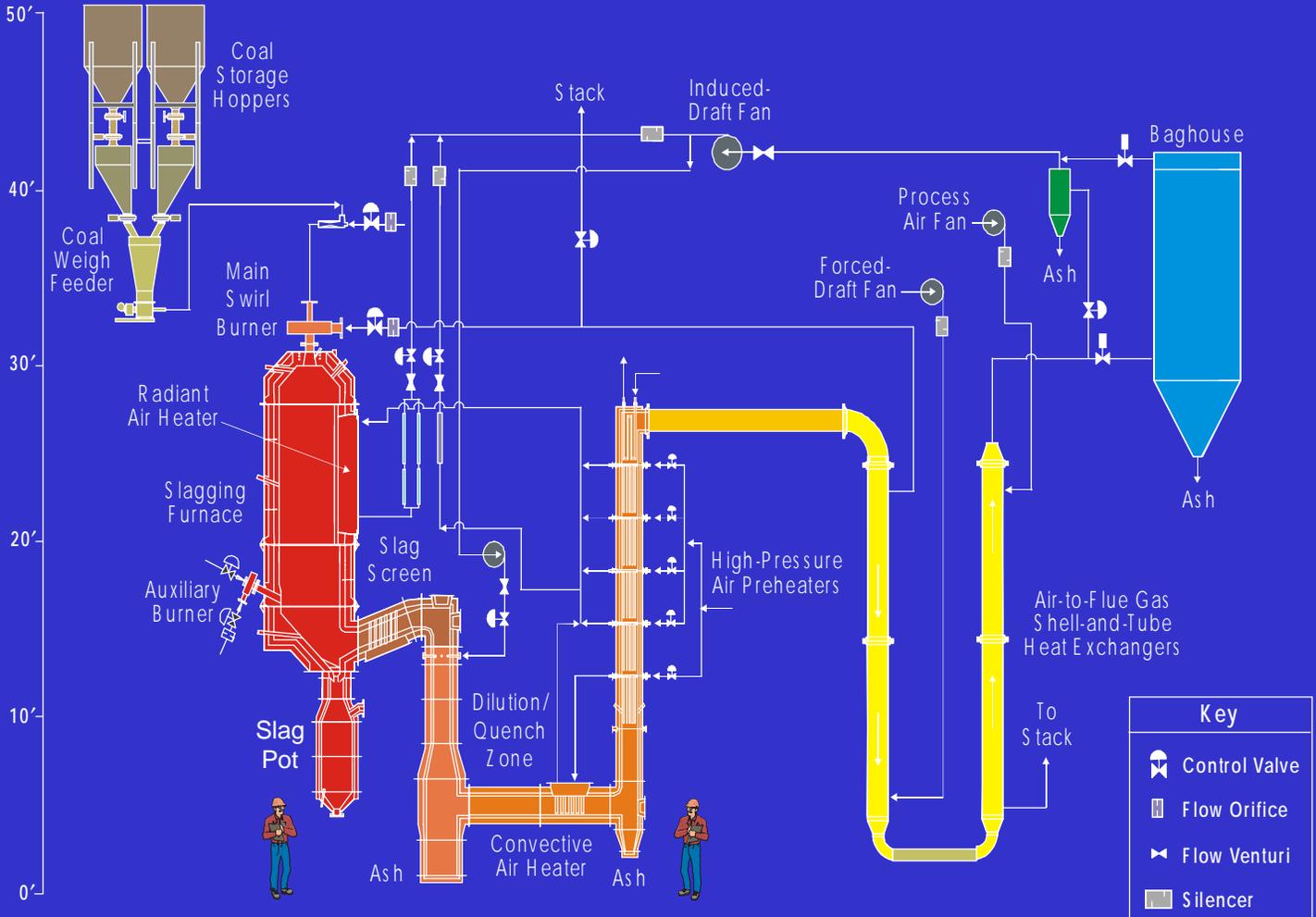
Corrosion of MA754 Under Coal Combustion Conditions



Protective Alumina Layer on MA956



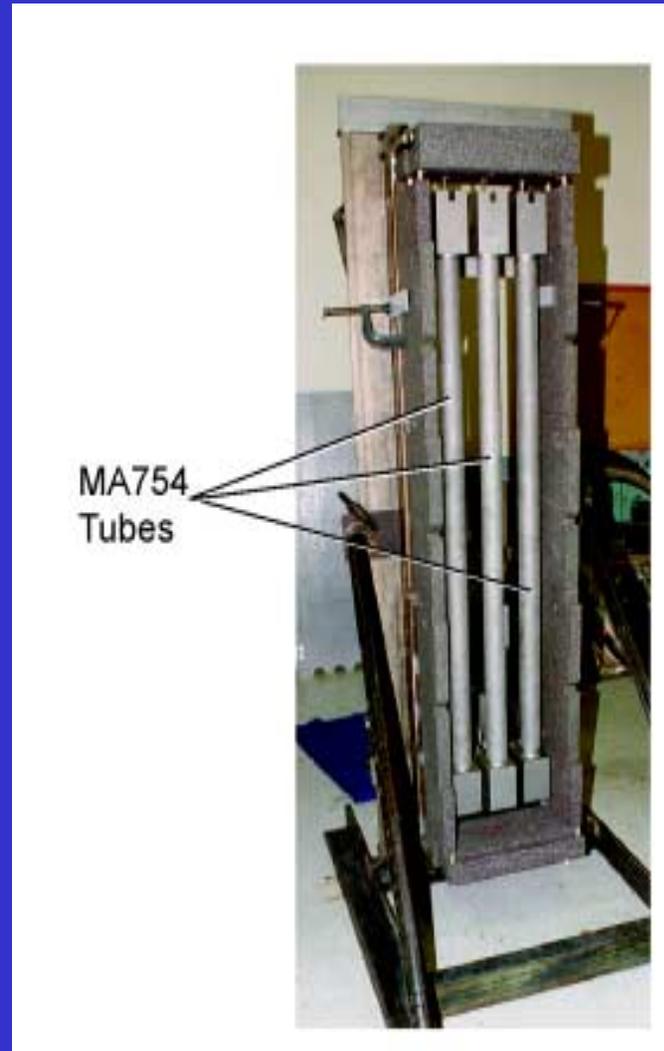
Combustion 2000 Slagging Furnace

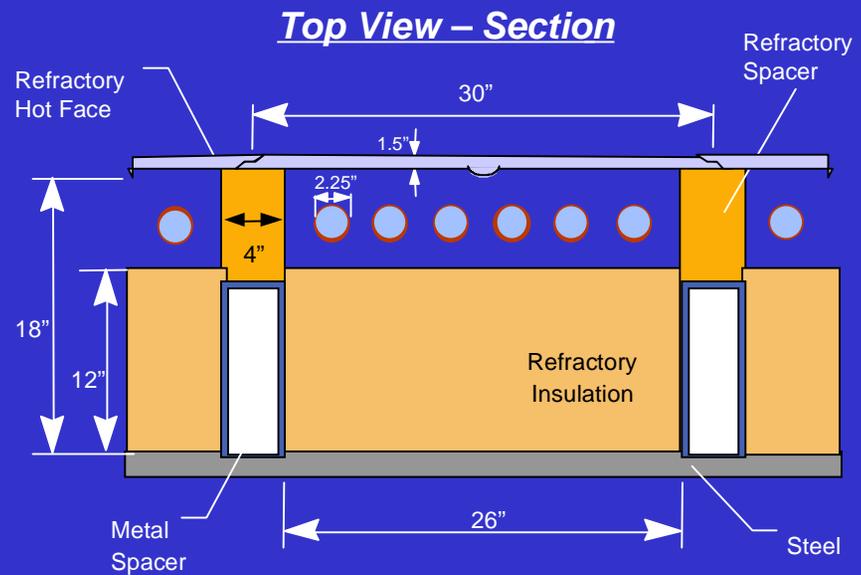
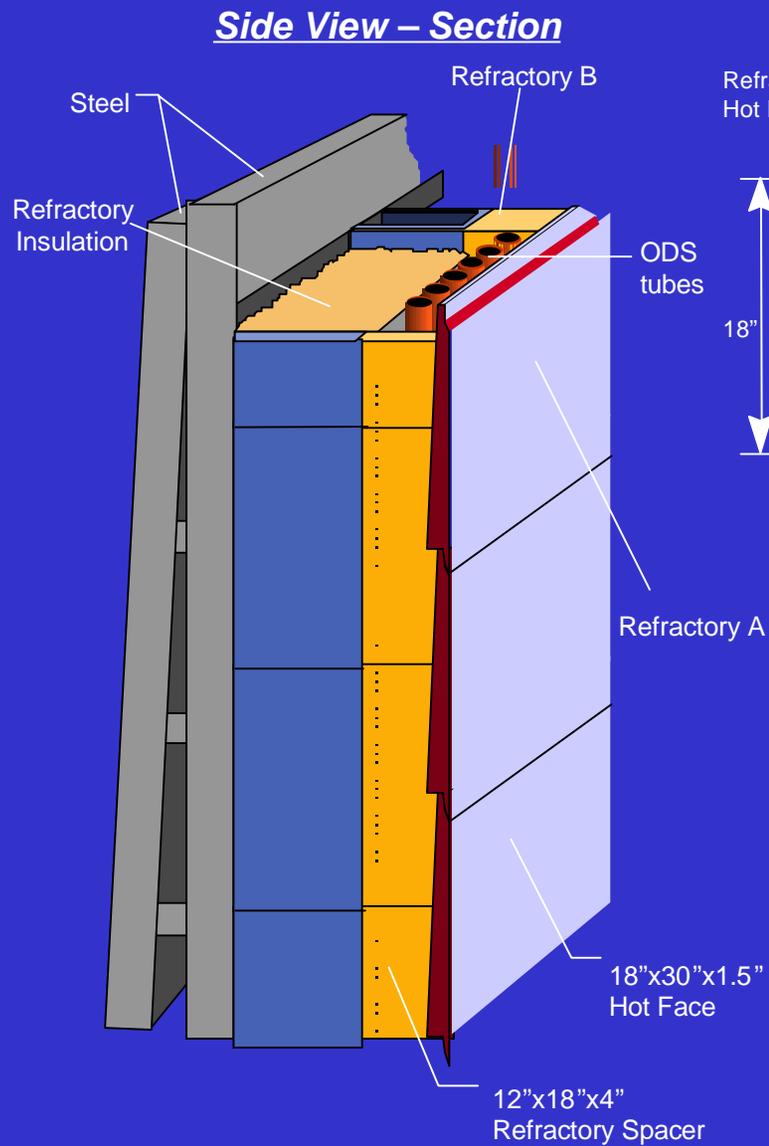


Key	
	Control Valve
	Flow Orifice
	Flow Venturi
	Silencer

EERC GW16849.CDR

Open View of RAH Test Panel





Hot Sections of Radiant Air Heater

Summary of Operating Experience

RAH Operation

- Heat transfer meets design criteria with Monofrax tiles.
- Standard process air 1750°F and 150 psig.
- 2000°F process air reached for short time at 100 psi.
- Slag layer less than 1 mm thick on panels.
- Thermal shock is biggest problem for ceramic panels.
- Corrosion of panels is secondary issue.
 - Additives may substantially reduce corrosion.
 - Prevent dripping to prevent channeling of slag.

Goals of HiPPS

- < 47% efficiency
- 1/10 emissions of particulates, SO_x, and NO_x
- 10% reduction in cost of electricity
- Efficiency to 55% with Illinois Basin coal–75% gas
- 2% less efficiency with high-moisture lignite

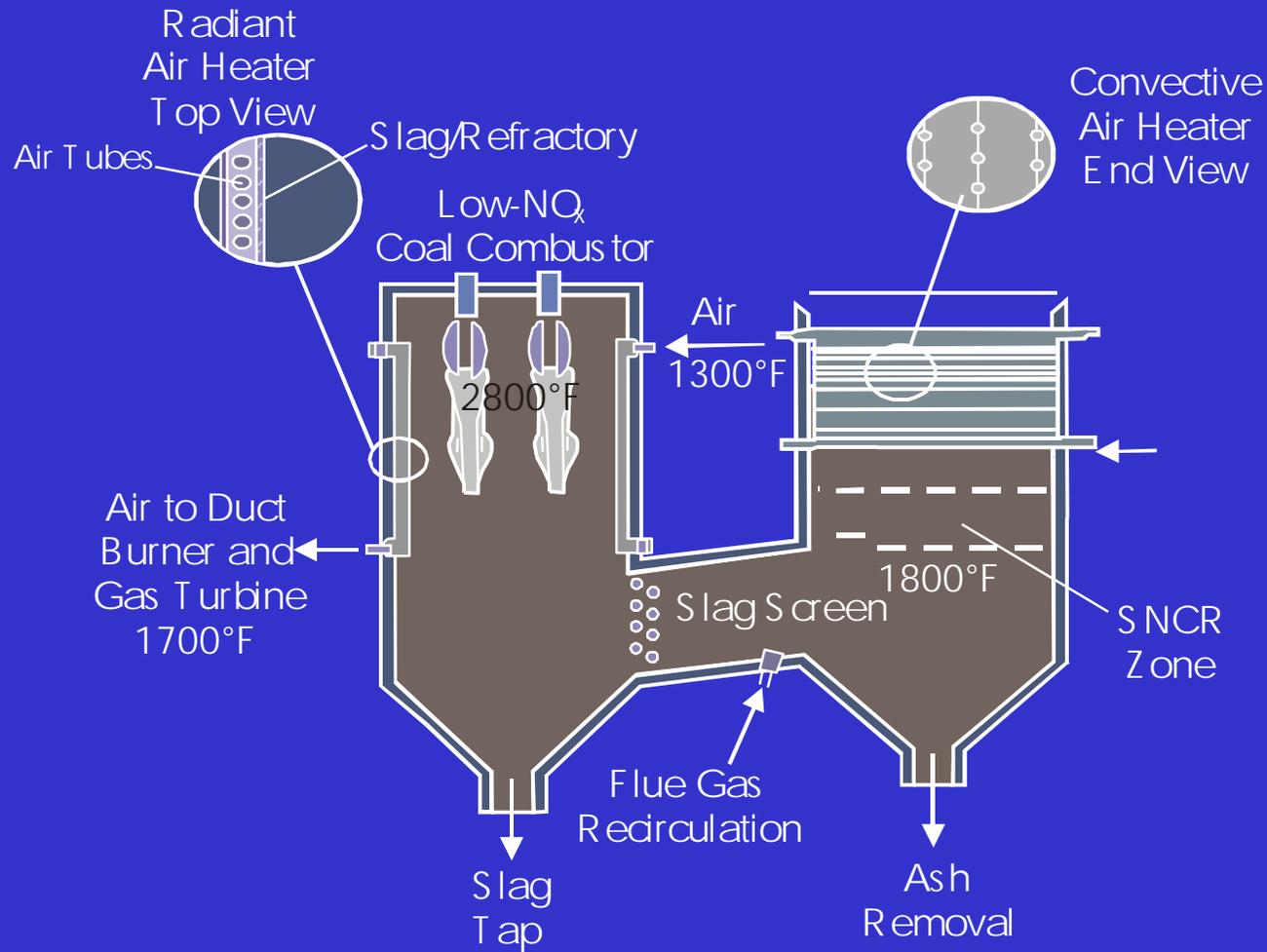
Pilot-Scale System

- Slagging furnace
- Slag screen
- Dilution-quench zone
- Process air preheater
- Convective air heater
- Radiant air heater
- Tube and shell heat exchangers

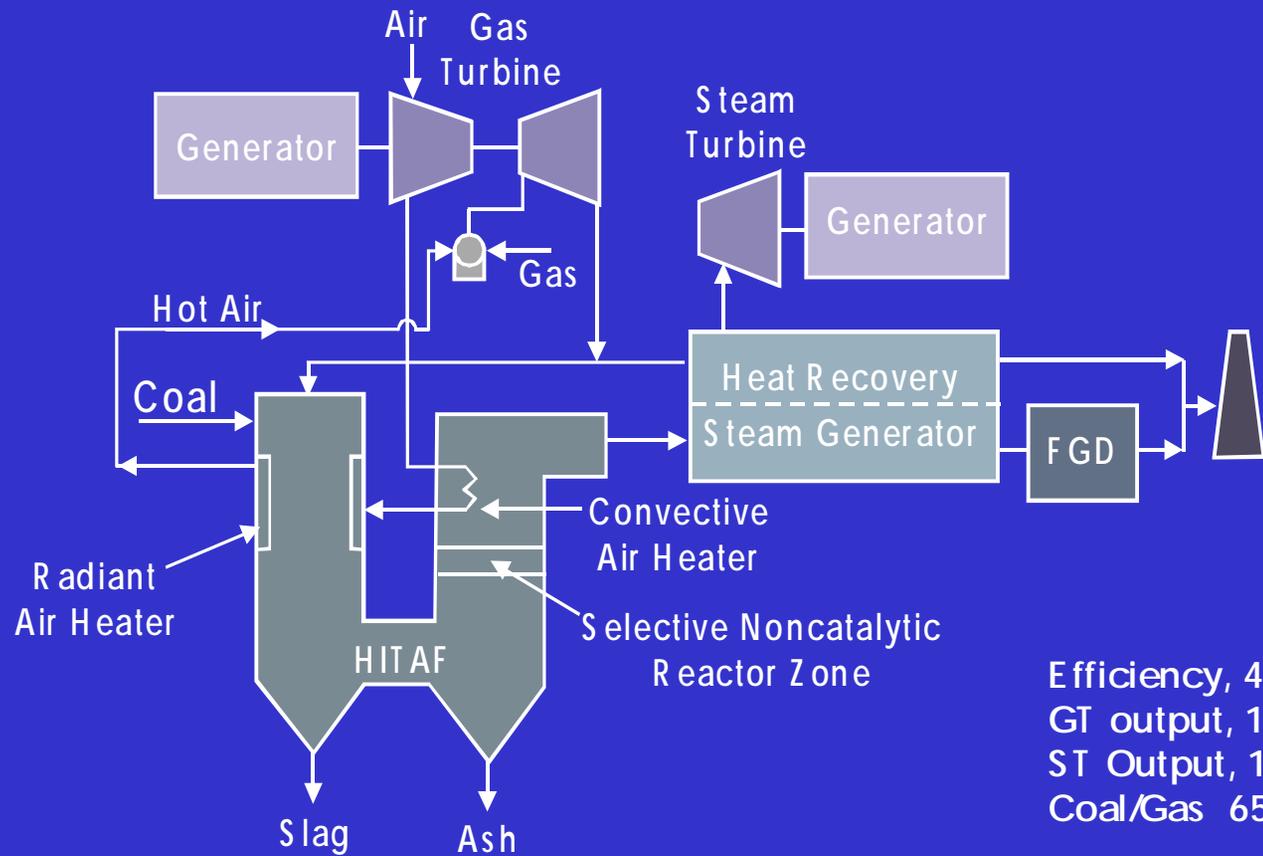
Slagging Furnace

- Maximum temperatures 2700°F–2900°F
- 2.5 MMBtu/air
- Residence time ~ 3.5 sec (Illinois Basin)
2.6 sec (Powder River Basin)
- Down-fired
- Data acquisition system

Conceptual Design of HITAF

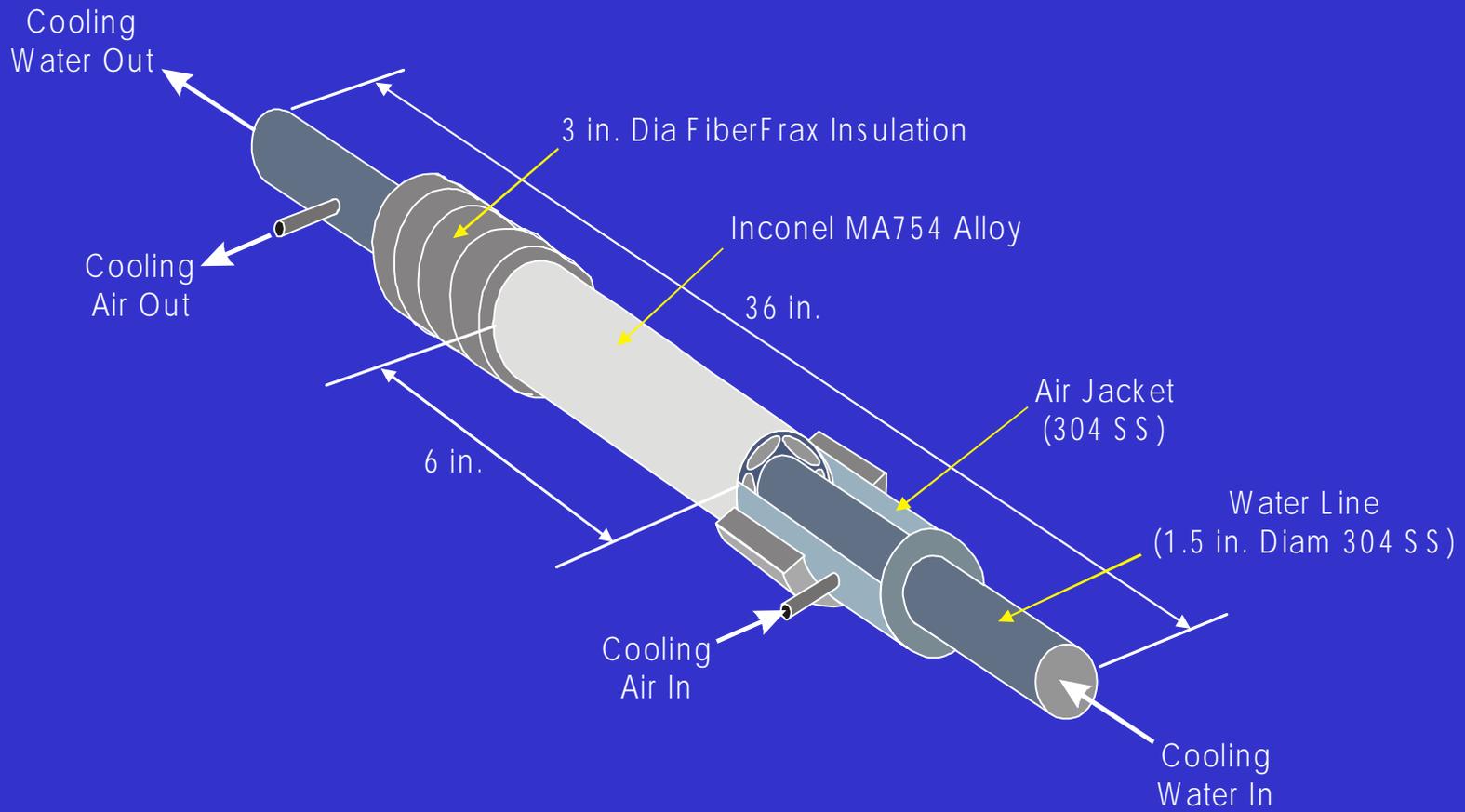


HiPPS Schematic

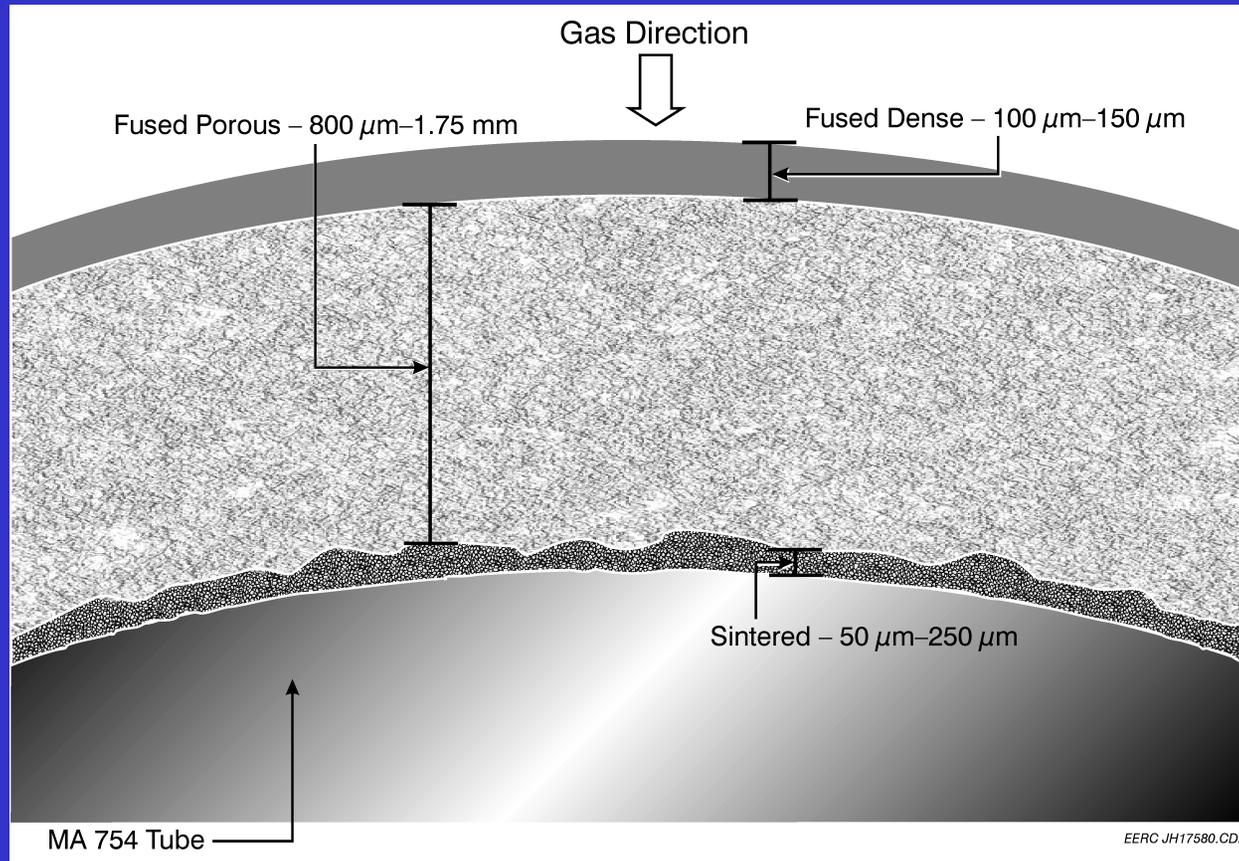


(Robson, et al., 1994)

Alloy Cooling Schematic



MA 754 Direct Exposure



- Surface cooled to 2000°F
- $1.5\ \text{mm}$ thick detached slag layer developed on surface
- No nickel or chrome in the detached slag layer
- $20\ \mu\text{m}$ thick attached slag layer
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- Surface recession average $2.2\ \text{mil}/110\ \text{hours}$ or $180\ \text{mil}/\text{year}$

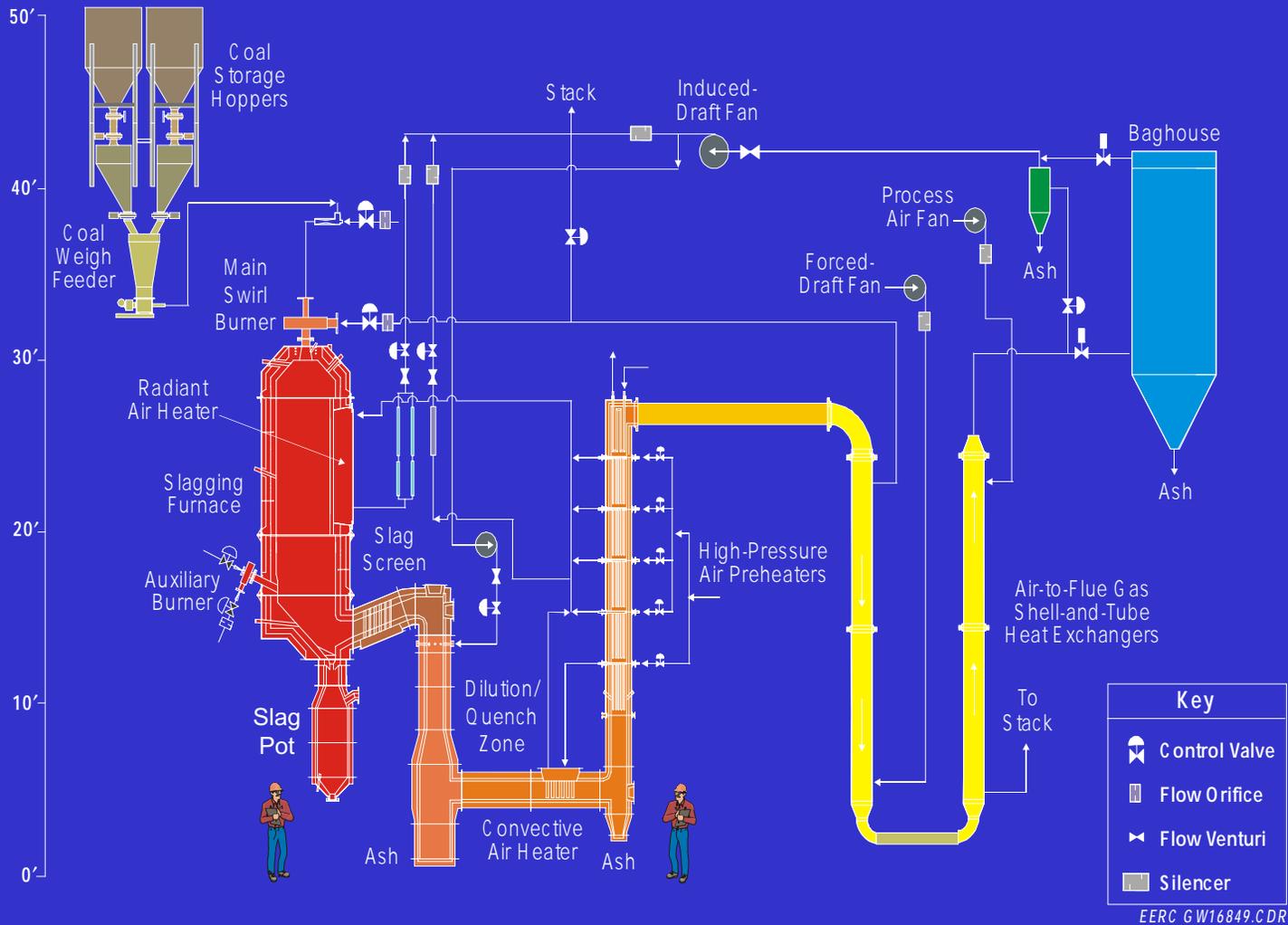
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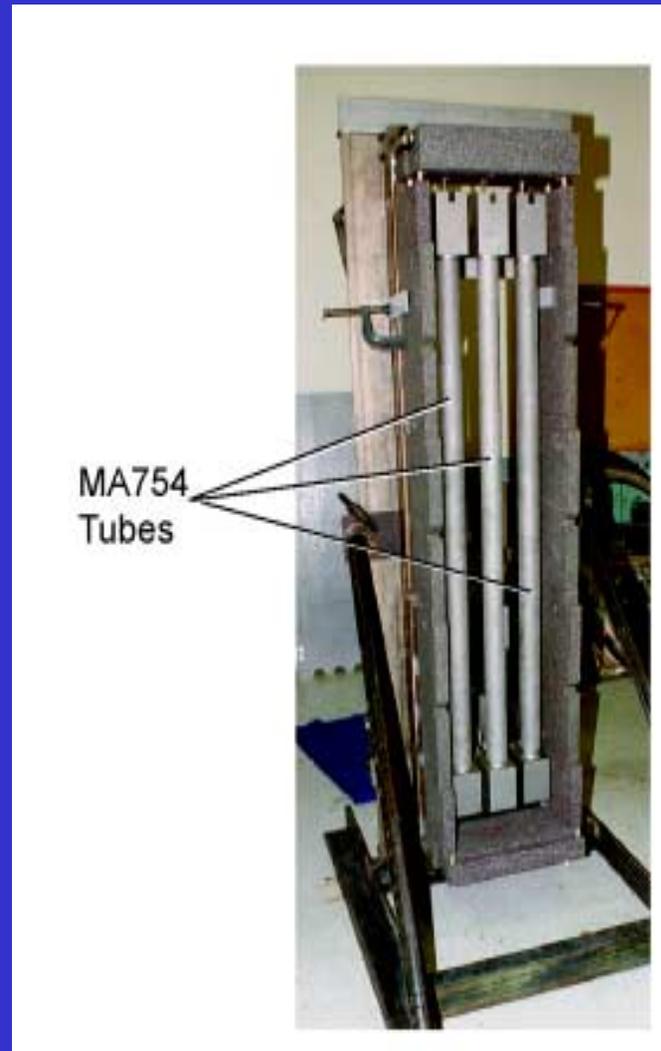
Conclusions

- Bare tube HiPPS using MA 956 has very low corrosion rates
- Heat transfer rates ~5 times heat transfer rates for the heat exchanger in the box (does not drop off with time as ash layer build)
- Cost of radiant heat exchange surface reduced by factor of 10
- Bare tube HiPPS has advantage over other HiPPS and conventional coal-based systems

Combustion 2000 Slagging Furnace



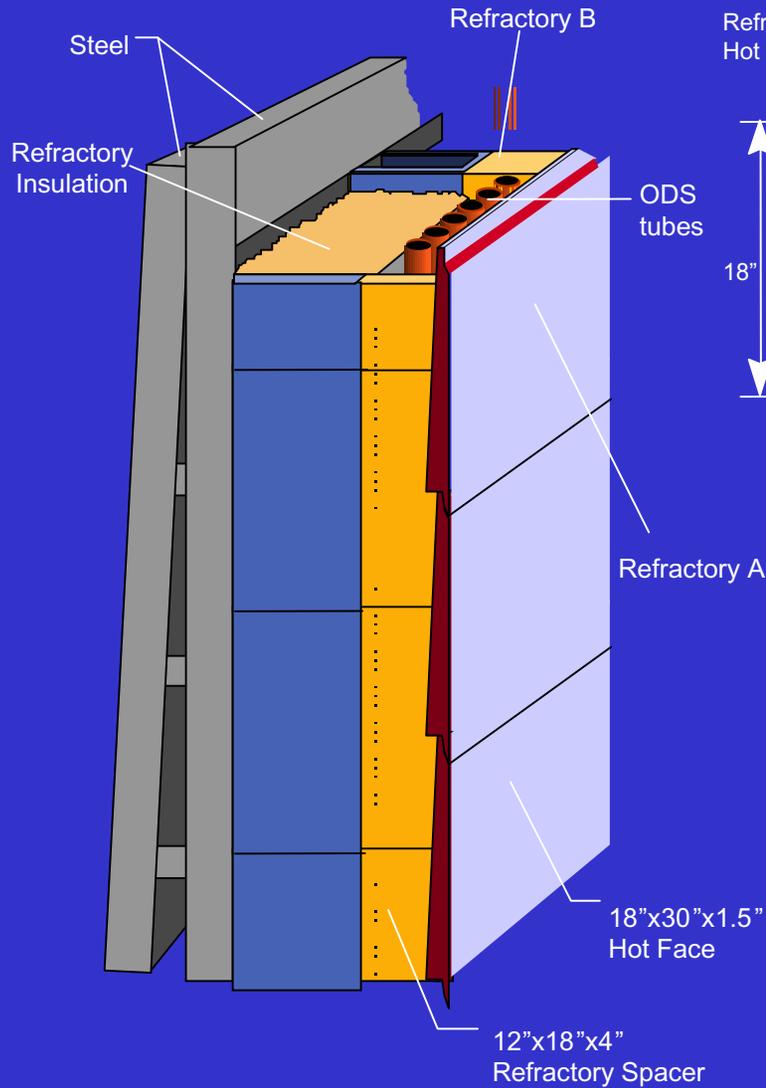
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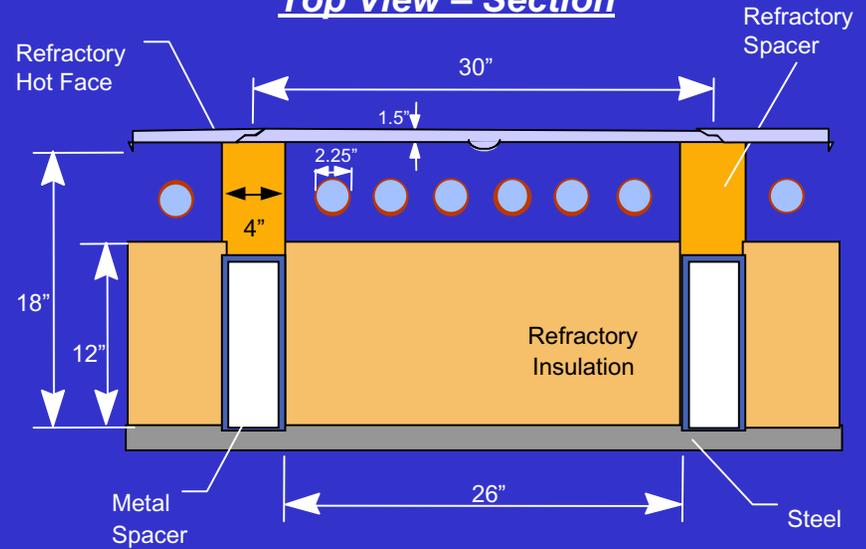
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Side View – Section



Top View – Section



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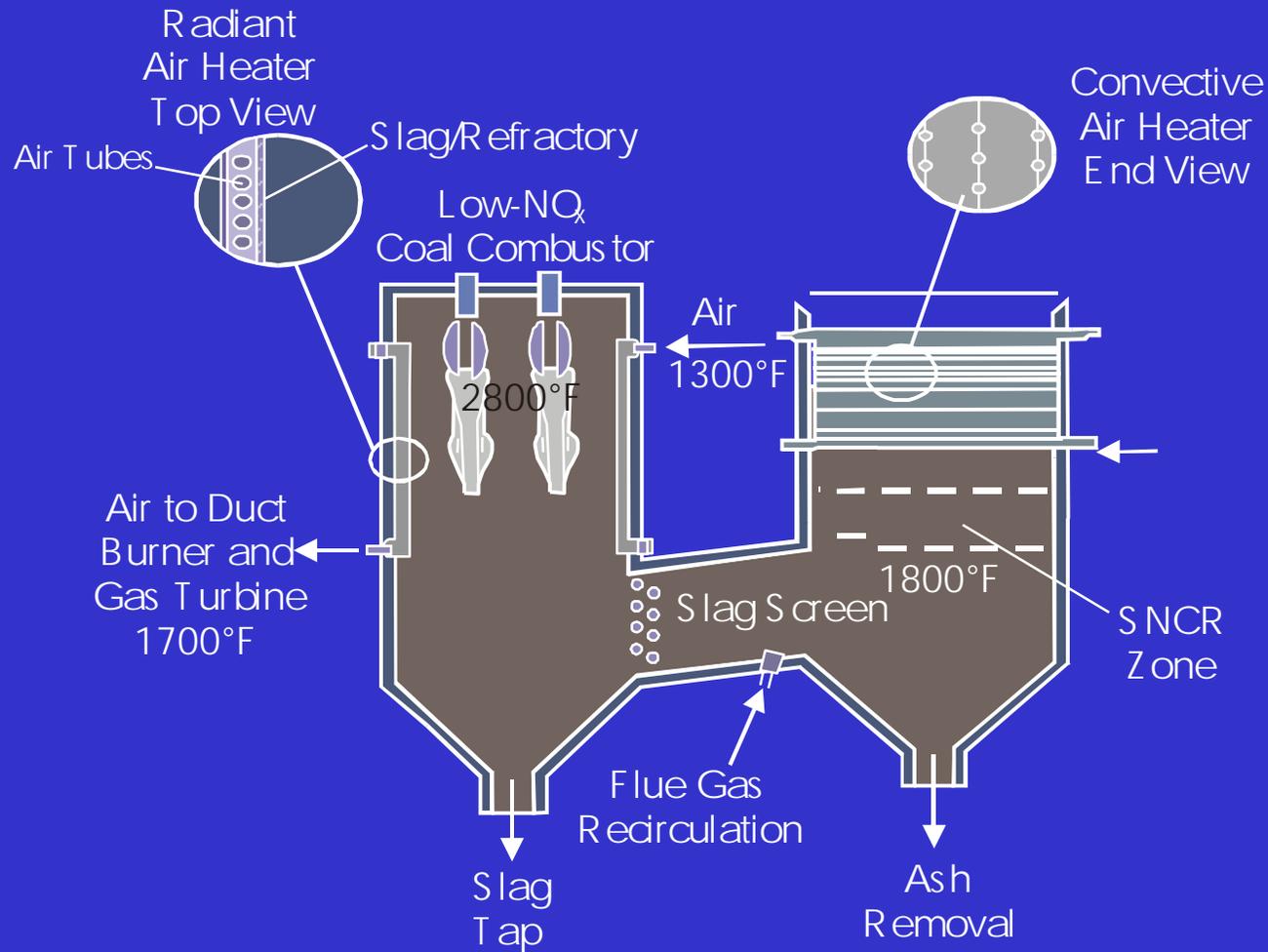
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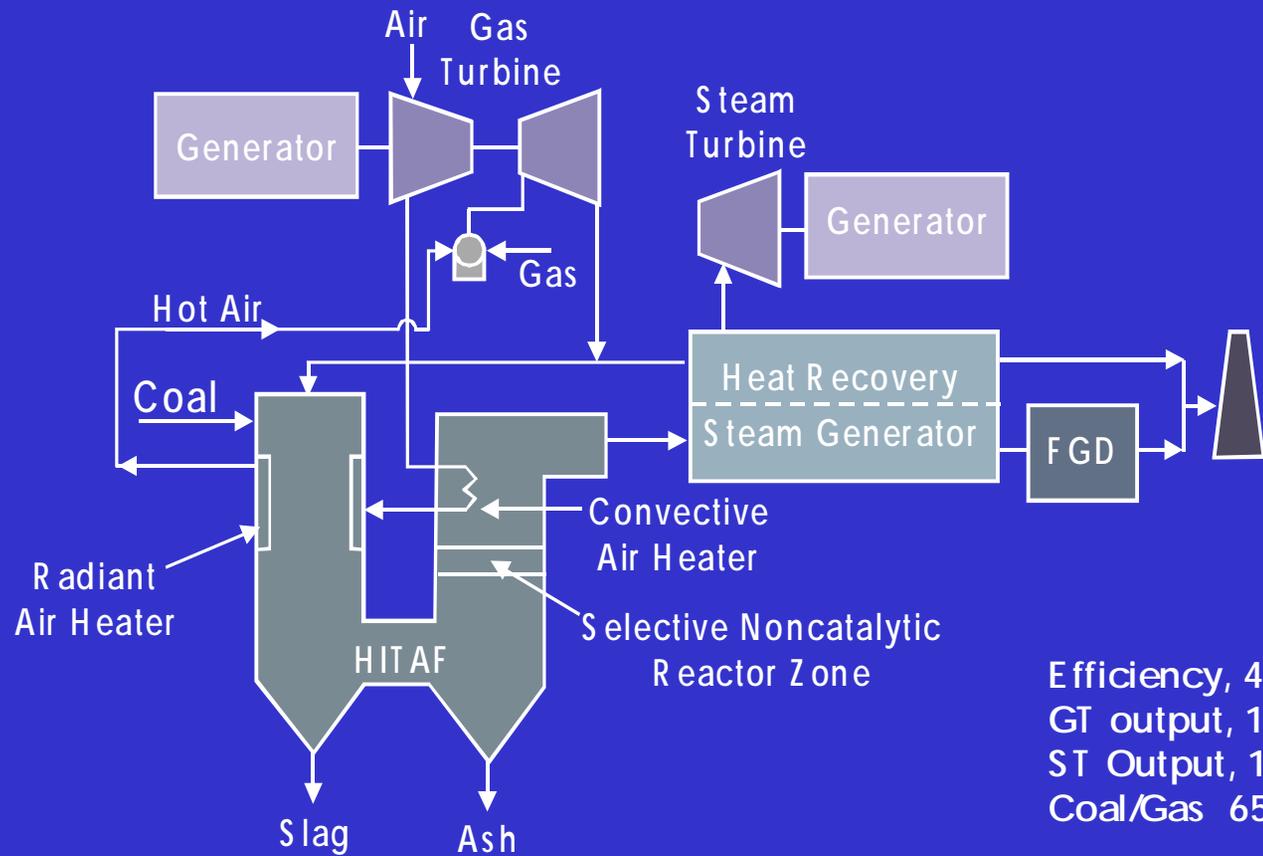
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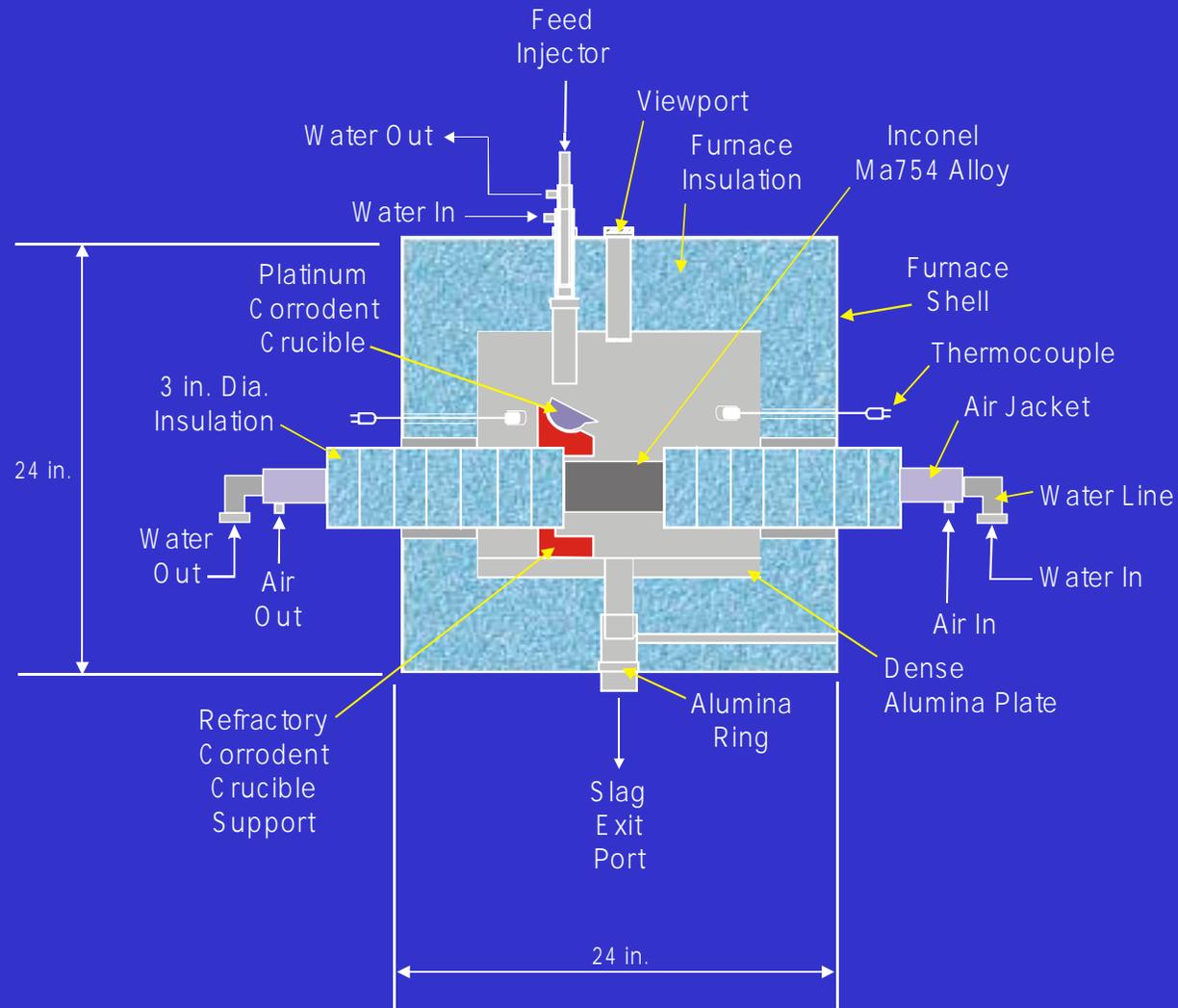


HiPPS Schematic

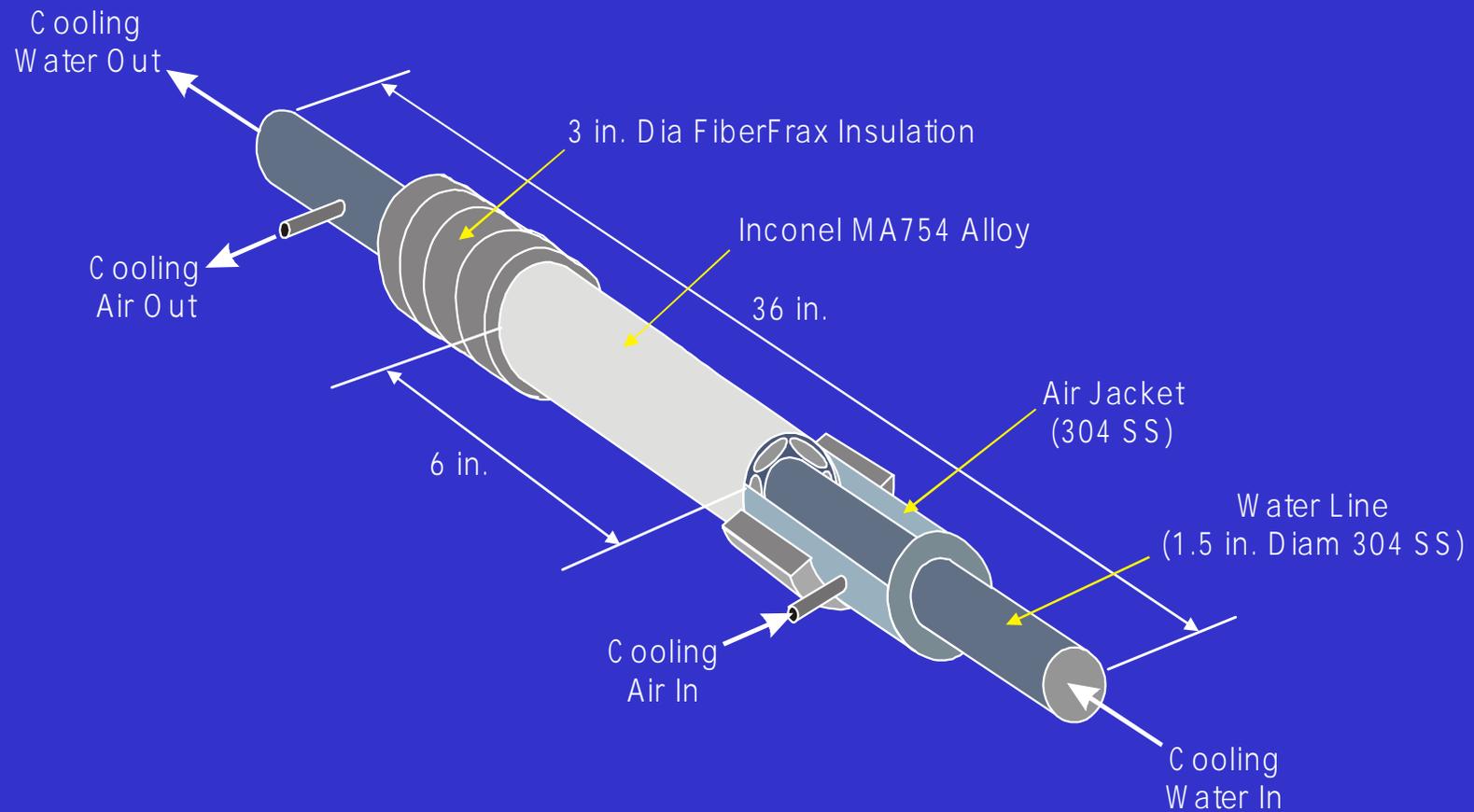


(Robson, et al., 1994)

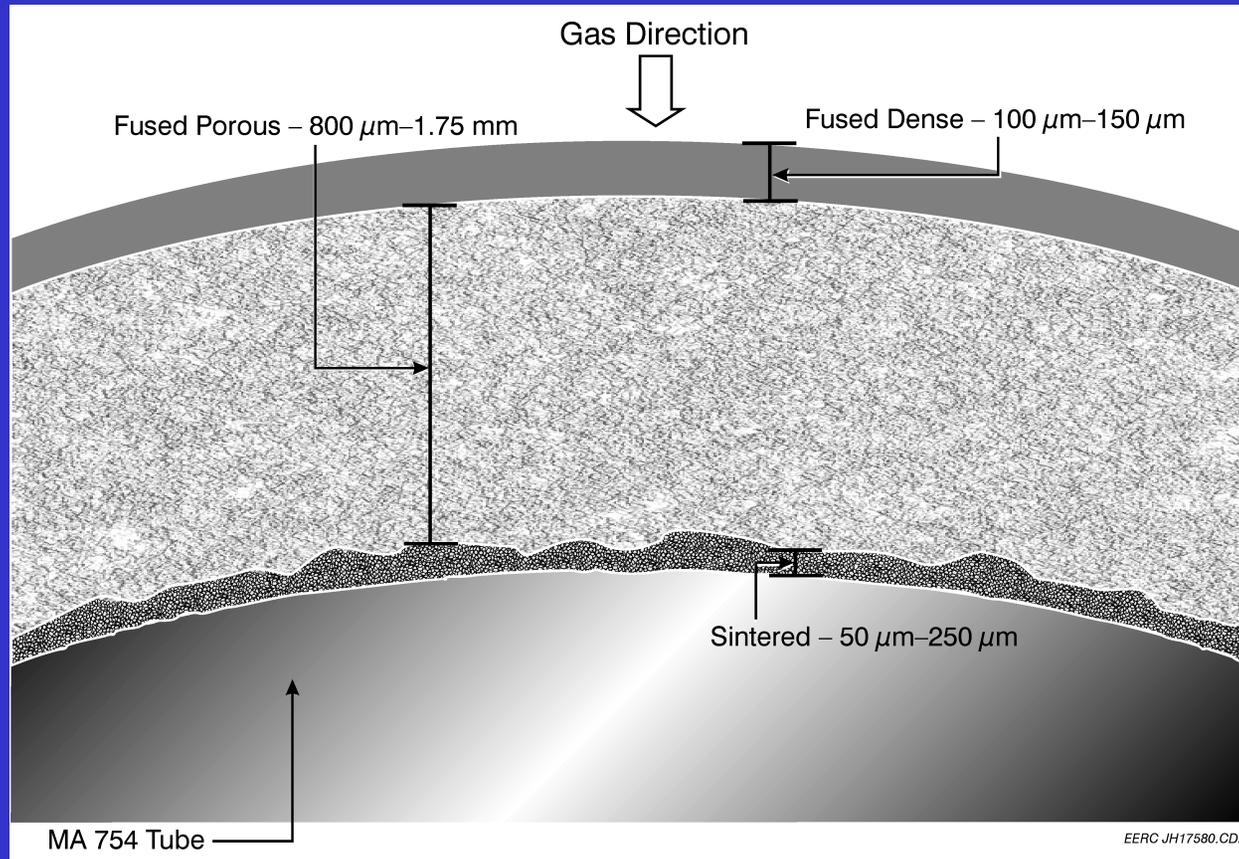
DSAFA Modified For Alloy Testing



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RAH Exchanger Tubes After August 2001 Test



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